1	Title					
2	Core Formation and Geophysical Properties of Mars					
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10	Keywords					
11	Mars, core formation, Fe-S alloys, Martian core, InSight					
12	Abstract					
13	The chemical and physical properties of the interiors of terrestrial planets are largely					
14	determined during their formation and differentiation. Modeling a planet's formation provides					
15	important insights into the properties of its core and mantle, and conversely, knowledge of those					
16	properties may constrain formational narratives. Here, we present a multi-stage model of Martian					
17	core formation in which we calculate core-mantle equilibration using parameterizations from					
18	high pressure-temperature metal-silicate partitioning experiments. We account for changing					
19	core-mantle boundary (CMB) conditions, composition-dependent partitioning, and partial					
20	equilibration of metal and silicate, and we evolve oxygen fugacity (fO_2) self-consistently. The					
21	model successfully reproduces published meteorite-based estimates of the bulk silicate Mars					

22 composition. This composition implies that the primordial material that formed Mars was

23 significantly more oxidized (0.7–1.4 log units below the iron–wüstite buffer) than that of the

Earth, and that core-mantle equilibration in Mars occurred at 45–91% of the evolving CMB

- 25 pressure. On average, at least 85% of accreted metal and at least 30% of the mantle were
- 26 equilibrated in each impact, a significantly higher degree of metal equilibration than previously

27 reported for the Earth. The modeled Martian core is rich in sulfur (16–20 wt%), with less than
28 one weight percent O and negligible Si.

29 We have used these core and mantle compositions to produce physical models of the presentday Martian interior and evaluate the sensitivity of core radius to crustal thickness, mantle 30 31 temperature, core composition, core temperature, and density of the core alloy. Trade-offs in 32 how these properties affect observable physical parameters like planetary mass, radius, moment 33 of inertia, and tidal Love number k_2 define a range of likely core radii: 1620–1820 km. Seismic 34 velocity profiles for several combinations of model parameters have been used to predict seismic 35 body-wave travel times and planetary normal mode frequencies. These results may be compared 36 to forthcoming Martian seismic data to further constrain core formation conditions and geophysical properties. 37

38 **1. Introduction**

In the absence of extensive seismic observations like those made available on Earth, our knowledge of the Martian interior relies largely on interpreting measurable geophysical properties, such as mass, radius, moment of inertia, and tidal responses, to constrain the depths, densities, and compositions of the rocky and metallic layers of the planet. While the ongoing InSight mission may directly measure the seismic properties of the interior (Panning et al., 2017), interpreting these data will require an understanding of the Martian composition.

The most detailed information about the chemistry of the Martian interior comes from
extrapolating the compositions of the Martian meteorites, particularly the Shergotty-NakhlaChassigny (SNC) group, back to their mantle source. Dreibus and Wänke (1985) developed a
canonical model for the silicate Mars (updated by Taylor, 2013) by measuring SNC elemental

49 abundances and proposing that their ratios reflect a mixture of volatile-rich and volatile-poor source material. In later studies, such as those of Lodders and Fegley (1997) and Sanloup (1999), 50 compositional models were constructed by matching the oxygen isotopic composition of the 51 52 SNCs to mixtures of known meteorite types. From these studies, Mars is interpreted to have a 53 mantle enriched in iron oxide (FeO) and a smaller core mass fraction relative to Earth, indicating 54 more oxidizing formational conditions (e.g., Rubie et al., 2011). The proximity of Mars to the 55 protoplanetary snow line during its formation may have resulted in accretion of a larger portion 56 of relatively oxidized, volatile-rich material. Mars is also thought to have a core enriched in sulfur, based on mass balance arguments (e.g., Anderson, 1972) and chalcophile element 57 depletions (Wänke and Dreibus, 1988). Addition of sulfur to iron significantly decreases its 58 59 melting temperature, so a high S content may have prevented crystallization of an inner core, 60 consistent with the lack of a modern geodynamo on Mars (Williams and Nimmo, 2004; Helffrich 61 2017).

62 One difficulty in evaluating the extant compositional models is determining whether they 63 accurately reflect the behavior of planetary materials during core formation. Single-stage core 64 formation models use metal-silicate partitioning data to determine a single pressuretemperature-oxygen fugacity $(P-T-fO_2)$ condition that can simultaneously reproduce the 65 Martian mantle abundances of several elements (e.g., Rai and van Westrenen, 2013; Righter and 66 67 Chabot, 2011: Steenstra and van Westrenen, 2018), but these models do not account for changing conditions during planetary growth. Rubie et al. (2015) calculated Martian core 68 formation in a multi-stage model with self-consistent fO_2 evolution, though their model did not 69 70 include S and only used the Martian FeO content (in addition to Earth's mantle composition) as a 71 constraint.

72 The core formation process on Mars has implications for the modern-day physical state of the planet's interior. Previous studies developed models of the Martian interior that match 73 74 geophysical parameters such as the bulk density and moment of inertia factor (MOI), and 75 geochemical properties inferred from the SNC meteorites. Sohl and Spohn (1997) developed one 76 model that matched the MOI and another that matched the Fe/Si ratio of Mars. These models 77 improved on earlier assessments by using equations of state to calculate the behavior of Martian 78 minerals at high pressure and temperature and constrained the core size to 1400–1700 km. 79 Bertka and Fei (1998) found a core size compatible with the range of Sohl and Spohn (1997) for 80 Fe–14wt%S (~1400 km). Later measurements of the MOI of Mars, its tidal Love number (k_2), 81 and tidal dissipation factor (O) seemed to only be matched by models with larger cores. For 82 example, Rivoldini et al. (2011) found that MOI and k_2 were best matched by cores 1730–1860 83 km in radius. Varying parameters such as the density of the core and the thermal structure of the 84 mantle can produce models that match these same constraints at a range of core sizes (Nimmo 85 and Faul, 2013), so it is important to evaluate the influence of these parameters. Khan et al. 86 (2018) inverted for the most likely ranges of several properties, including core composition, 87 core-mantle boundary (CMB) temperature, and lithospheric thickness, and they constructed 88 seismic velocity profiles based on these ranges. These results also suggest a large core (1730-89 1840 km), though their Bayesian method does not explicitly consider the influence of each 90 parameter on the determined core size. Larger cores necessarily have more moderate lowermost 91 mantle pressures, probably precluding a region of bridgmanite stability, though Bertka and Fei 92 (1997) determined that the existence of Martian bridgmanite is also highly temperature 93 dependent.

94 Here we present a new model of Martian core formation, which improves upon previous studies by implementing multi-stage differentiation with comparisons to a large suite of major, 95 96 minor, and trace elements in Mars. The core and mantle compositions predicted by this core 97 formation model were used to construct mineralogical, density, and seismic velocity profiles for 98 the Martian interior. We explicitly considered how planetary structure is influenced by core 99 composition as well as geophysical parameters such as crustal thickness and thermal structure. 100 Additionally, we introduced more realistic calculations of liquid Fe-S alloy densities at high 101 pressures and temperatures, improving our understanding of the core's physical properties. 102 Seismic properties were assessed across the model suite, allowing predictions of both the body 103 wave travel times and normal mode oscillation frequencies for the different models. The new 104 self-consistent models of core formation, internal structure, and seismic properties presented here 105 help tie together the history of early Mars with its modern state and produce geophysical 106 predictions that can be compared to seismic results obtained by the InSight mission.

107 **2.** Methods

We have constructed a model of multi-stage core formation to investigate Martian formational properties and a model of planetary physical structure to investigate geophysical properties of modern Mars. Further details on each of these, as well as a description of our seismological calculations, can be found in the supplementary materials.

112 2.1 Core formation

113 Chondritic primordial material was equilibrated at a fixed fO_2 to form planetesimals, then 114 these planetesimals were sequentially added to the proto-Mars, and experimentally-determined 115 metal–silicate partitioning data (Supplementary Table S1) were used to model the chemistry of

core formation. The composition of the primordial material was based on CI chondrites (after
Dreibus and Wänke, 1985; Taylor, 2013), enhanced in refectory elements (Mg, Al, Si, Ca, V, Cr,
Fe, Co, Ni, W, Ti) by a factor of 1.9 (Taylor, 2013) to create relative depletions in moderately
volatile elements (Na, P, S, K, Mn). Mars was constructed from 1,000 Ceres-sized (0.001 M_{Mars})
planetesimals.

121 In each accretionary step, one planetesimal (the impactor) was equilibrated with the 122 proto-Mars (the target). Equilibration took place between the entire impactor mantle, a portion of 123 the impactor core, and a portion of the target mantle; the core of the proto-Mars was assumed to 124 be undisturbed by impacts. In each step, metal-silicate equilibration took place at a constant 125 fraction of the growing CMB pressure and at the liquidus temperature. Pressure at the CMB was 126 increased linearly from 1 GPa to 20 GPa (Rivoldini, 2011). Mg, Al, Ca, Na, K, and P were 127 assumed to be perfectly lithophile. In each step, major elements Si, Fe, O, and Ni were 128 partitioned first, allowing fO_2 to evolve self-consistently following the methodology of Rubie et 129 al. (2011) as updated in Fischer et al. (2017), then trace elements and S were partitioned. Finally, 130 the unequilibrated portion of the impactor core and the metallic portion of the equilibrated 131 material were added to the proto-Martian core, and the unequilibrated portion of the target 132 mantle and the silicate portion of the equilibrated material were combined to form the proto-133 Martian mantle. This procedure was repeated for each impacting planetesimal.

Adjustable parameters in the model include: the equilibration fraction (the portion that participates in the metal–silicate reaction) of the impactor core (denoted k) and target mantle; depth of equilibration, expressed as a fraction of the evolving CMB pressure (denoted P_{equil}/P_{CMB}); and the initial oxidation state of accreted material. To evaluate the sensitivity of the resulting core and mantle compositions to these formational parameters and to constrain them,

the equilibration fractions of the impactor core and target mantle were each varied in the range 0.1–1.0, the depth of equilibration was varied in the range 0.01–1.0, and the initial fO_2 of the accreted material was varied from IW–3 to IW. Uncertainties were evaluated using a Monte Carlo analysis.

143 2.2 Physical structure

144 Using the core and mantle compositions calculated in the core formation model, radial 145 profiles of density and seismic wave speeds were constructed. The Martian temperature profile 146 (the "aerotherm") was calculated based on an adiabat from the median CMB conditions of 147 Rivoldini et al. (2011) (~20 GPa and ~2000 K). These conditions correspond to a mantle 148 potential temperature of 1600 K, consistent with previous estimates (e.g., Nimmo and Faul, 149 2013; Zheng et al., 2015). The lithospheric thermal boundary layer was approximated as a layer 150 of linearly increasing temperature which intersects the adiabat at ~ 200 km, the estimated base of 151 the thermal boundary (e.g., Khan et al., 2018).

152 The Martian core was assumed to be a homogenous liquid alloy in the Fe–S system, with 153 the S fraction specified by the core formation model. Density-pressure relationships for the core 154 were calculated by reference to published equations of state for Fe–S alloys. The core S content 155 is a function of the formational parameters discussed above, so it was necessary to interpolate 156 between equations of state for several alloys to calculate densities over a range of compositions. 157 We used four equations of state: γ -Fe (Komabayashi and Fei, 2010), Fe₃S (Seagle et al., 2006), 158 FeS (Urakawa et al., 2007), and FeS₂ (Thompson et al., 2016). These equations of state all 159 describe solids, so it was necessary to correct for the difference in density between these and 160 liquid alloys. While it would have been more straightforward to use liquid equations of state, 161 there are not enough data to adequately constrain liquid Fe–S alloy densities over a range of

162	compositions (Section 4.4). Each constructed density and velocity profile of Mars corresponds to					
163	a specific set of physical (crust thickness, mantle temperature, core temperature, volume change					
164	(ΔV) of melting of Fe–S alloys) and formational (initial fO_2 , volatile loss, equilibration depth,					
165	degree of equilibration) parameters. To test the sensitivity of core radius and density/velocity					
166	structure to these parameters, crust thickness was varied in the range 25-85 km, mantle potential					
167	temperature was varied in the range 1500-1800 K, the temperature contrast across the CMB was					
168	taken to be 0–600 K, and ΔV of melting was taken to be 2–5%. Each combination of parameters					
169	implies a value for the MOI and k_2 , which can be compared to the values measured by Mars-					
170	orbiting satellites (Konopliv et al., 2011, 2016) (Section 4.4).					
171	3. Martian core formation					
172	The composition of the Martian mantle, as inferred from SNC meteorites, can be used to					
173	constrain the conditions of core formation. The core formation conditions implied by the mantle					
174	composition can then be used to place constraints on the composition of the core.					
175	3.1 Mantle composition and implications for the formation of Mars					
176	An example of a Martian mantle composition produced by this model is shown in Figure					
177	1. Of the previous studies on Martian mantle composition, we primarily compare our results to					
178	those of Taylor (2013) due to that study's reporting of uncertainties, which other studies lack					
179	(e.g. Dreibus and Wänke, 1985; Lodders and Fegley, 1996; Sanloup, 1999). The composition					
180	predicted by this study best matches those of Taylor (2013) (Figure 1) and Dreibus and Wänke					
181	(1985) due to use of the same bulk composition (Section 2.1). We obtain good agreement with					
182	Lodders and Fegley (1996) and Sanloup (1999) when we instead use their bulk compositions.					
183	Within uncertainty, calculated mantle abundances of most major, minor, and trace elements are					

184 consistent with those of Taylor (2013), except for Cr and K (Figure 1). The anomalously low 185 concentration of Cr might arise because we are extrapolating beyond the fO₂ conditions of the 186 metal-silicate partitioning experiments. Taylor (2013) obtained the mantle K abundance from 187 gamma ray spectroscopy measurements of the surface K/Th ratio; this difference in methodology 188 likely accounts for the discrepancy in K. To constrain conditions of the formation and 189 differentiation of Mars, first the fO₂ at which the primordial material equilibrated was adjusted to 190 match the reported FeO content of the Martian mantle. The mantle FeO content implies that 191 Mars was built of material with an initial oxidation of state of IW-1.4 to IW-0.7, which 192 corresponds to a core mass fraction for Mars of 0.18-0.27 (Figure 2a). This higher fO_2 and 193 relatively smaller core than Earth (e.g., Rubie et al., 2011, 2015; Fischer et al., 2017) reflects the 194 accretion by Mars of relatively oxidized primordial material, which likely originated further from 195 the Sun.

196 Constraints on the degree of equilibration were obtained by comparing the calculated 197 mantle compositions with literature values, as shown in Figure 3a. Possible values of k are found 198 to be 0.84–1.0 for whole-mantle equilibration, based on matching the mantle abundances of 199 TiO₂, S, and Co; other elements are consistent with this range but do not provide such tight 200 constraints. This degree of metal equilibration is significantly higher than that found for Earth by 201 examining the variation of mantle trace elements and the Hf–W isotopic system, which imply 202 that k for Earth is 0.2-0.55 (e.g., Fischer and Nimmo, 2018; Fischer et al., 2017). A lower k for 203 Earth is consistent with the accretion of giant differentiated impactors, whose large cores would 204 not have efficiently emulsified. Mars' high k is consistent with the accretion of smaller 205 impactors, possibly including undifferentiated ones that would exhibit $k \sim 1$. Varying the 206 equilibration fraction of the target silicate does not significantly change the mantle composition

207	for values above ~ 0.3 , consistent with its limited effect on composition above a certain threshold
208	for the Earth (Fischer et al., 2017). Reducing the degree of silicate equilibration requires a
209	corresponding increase in k ; since k is already near unity (its maximum value) for the case of
210	whole-mantle equilibration, it is more likely that silicate equilibration was similarly high.
211	An analogous procedure was used to constrain the depth of metal-silicate equilibration
212	(Figure 3b). Simultaneously matching the Martian mantle abundances of Ni, Co, and S requires
213	that P_{equil}/P_{CMB} fall in the range 0.40–0.91 (for $k = 0.9$ and whole-mantle equilibration); again,
214	other elements are consistent with this range, but do not further constrain it. This pressure range
215	implies that, on average, equilibration took place in a deep magma ocean but not as deep as the
216	core-mantle boundary. It overlaps with the relative depth of equilibration found for the Earth
217	using similar models (Fischer et al., 2017; Rubie et al., 2011, 2015), which may suggest a similar
218	relative depth of melting on the two planets. Applying this range to the modern Martian CMB
219	implies an average equilibration pressure of ~13 GPa, similar to the results of single-stage
220	partitioning studies (e.g., Rai and van Westrenen, 2013; Righter and Chabot, 2011). Single-stage
221	models necessarily partition elements at a fixed fO_2 and do not incorporate changes in pressure
222	and temperature as a planet grows, so the model presented here represents a more realistic
223	approach.

224

3.2 Light elements in the Martian core

The core formation conditions implied by the Martian mantle composition indicate that S is the dominant light element in the core, consistent with previous studies (e.g., Lodders and Fegley, 1996; Sanloup et al., 1999; Steenstra and van Westrenen, 2018; Taylor, 2013; Wänke and Driebus, 1985). Sulfur is siderophile at the $P-T-fO_2$ conditions of Martian core formation, with D_S values as high as 600, comparable to D_{Ni} (Fischer et al., 2015). The majority of Martian

230 S must be in the core, but the mantle abundance also appears to be greater than that of the Earth 231 (e.g., Wang and Becker, 2017), implying that bulk Mars is relatively sulfur-rich. The range of 232 core mass fractions implied by the mantle FeO content, 0.18–0.25 (Section 3.1), is consistent 233 with a range of volatile element depletion factors of $0.28-0.68 \times CI$ (Figure 2b). Taylor (2013) 234 argued for a refractory element enrichment of 1.9× CI (equivalent to a volatile element depletion 235 of $0.6 \times$ CI) based on a survey of lithophile volatile element abundances in Mars. Enriching Mars 236 in refractory elements by this factor leads to a core S content of 18 wt%, with the uncertainty of 237 the Monte Carlo analysis expanding this to a preferred range of 16–20 wt% (95% confidence 238 interval; Supplementary Table S2). This corresponds to a bulk Mars with 4.2 wt% S, within the 239 bulk abundance estimates of Steenstra and van Westrenen (2018). If Mars instead is assumed to 240 have bulk S equivalent to an H chondrite, it would have a core S content of 12 wt%. Bulk S 241 content equivalent to a pristine EH chondrite results in a core S content of 21 wt%; this may be 242 taken as the upper limit for core S in a chondritic Mars since EH is the most S-rich of all 243 chondrite groups (Lodders and Fegley, 1998).

244 The Martian core contains little O (<1 wt%; Supplementary Table S2) despite the more 245 oxidizing core formation conditions compared to the Earth. This is largely due to the less 246 extreme conditions of metal-silicate equilibration on Mars, since O partitions more strongly into iron alloys at higher T (e.g., Fischer et al., 2015). Previous studies which predicted O at the few-247 248 percent level in the Martian core (e.g., Steenstra and van Westrenen, 2018) calculated 249 partitioning at modern lowermost mantle conditions (inconsistent with our findings; Figure 3b). 250 The other light element considered here, Si, only enters the Martian core at trace levels 251 (Supplementary Table S2). Like O, it is less siderophile at lower temperatures, but it is also less siderophile at higher fO_2 (e.g., Fischer et al., 2015), further reducing its core abundance. 252

253 C or H partitioning into the core were not modeled despite suggestions that these may be 254 present in greater-than-trace abundances (e.g., Chi et al., 2014; Zharkov and Gudkova, 2005). 255 There are few constraints on the planetary or mantle abundances of these highly volatile 256 elements, and thus it is difficult to determine their total budgets. Qualitatively, Mars is too small 257 and S-rich to dissolve substantial H in its core, with Clesi et al. (2018) estimating 60 ppm. The 258 solubility of C is also much reduced in S-rich core alloys (Tsuno et al., 2018). For a nominal 259 bulk C content of 1000 ppm, Tsuno et al. (2018) found that a Martian core at IW-1.0 with 16 260 wt% S would have ~0.5 wt% C; this may be taken as an upper bound for the more S-rich core 261 composition presented here. Better constraining the abundances and partitioning of these highly 262 volatile elements is a target for future studies.

263

4. Geophysical properties of Mars

The core and mantle compositions predicted by the core formation model were used to construct phase assemblages (Supplementary Figure S1) and produce density and velocity profiles (Figures 4 and 5) of the Martian interior. In addition to composition, these profiles depend on physical properties of the Martian interior. By comparing to the mass, radius, MOI, and k_2 , constraints can be placed on some of Mars' geophysical properties. The resulting solution space allows for predictions of core radii and seismic properties.

270 4.1 The lithospheric boundary layer

The rigid lithosphere at a planet's surface does not participate in mantle convection, so its heat flow is conductive, with temperatures increasing approximately linearly with depth. On Earth, this rapidly increasing temperature leads to high seismic velocities in the conductive lid and a corresponding low-velocity zone (LVZ) in the uppermost adiabatic mantle. Mars is a

275	stagnant lid planet and is inferred to have a laterally variable lithosphere up to 300 km thick (e.g.,
276	Grott et al., 2013). This produces a thick thermal boundary layer on a small planet, so the low-
277	velocity effect which confined to a small portion of the Earth's mantle will extend over a
278	sizeable portion of the Martian mantle. As seen in Figure 5, this may be a property of first-order
279	importance for Martian seismology (Section 4.6). Since the magnitude of the decrease is
280	dependent on the thermal structure of the lithosphere, mantle potential temperatures may be
281	inferred by measuring the LVZ's seismological effects (Zheng et al., 2015).
282	The magnitude of this effect, however, cannot be well-constrained with our current
283	knowledge of Martian temperature and structure. The calculations shown here use an upper
284	mantle thermal boundary layer thickness of 200 km (Khan et al., 2018) and a range of mantle
285	potential temperatures around 1600 K (Nimmo and Faul, 2013). Lithospheric thickness directly
286	influences the size of the LVZ, but also reduces its magnitude, since a deeper thermal boundary
287	would be shallower and closer in slope to the mantle adiabat. Changing the mantle potential
288	temperature at a constant lithospheric thickness likewise requires changing the slope of the
289	lithospheric temperature profile (Supplementary Figure S2). Increasing potential temperature by
290	100 K for a 200 km lithospheric boundary increases the magnitude of the LVZ by 0.2 km/s for
291	compressional waves and 0.1 km/s for shear waves. These effects may be complicated by lateral
292	variations in lithospheric thickness due to features such as the hemispherical dichotomy and the
293	Tharsis volcanic province.
294	4.2 Lowermost mantle conditions

There is some disagreement as to whether the Martian mantle contains bridgmanite, the major component of Earth's lower mantle. Some studies find that the P-T conditions of the lowermost Martian mantle lie within the bridgmanite stability field (e.g., Bertka and Fei, 1998),

298 some do not (e.g., Sohl and Spohn, 1997; Khan and Connolly, 2008; Khan et al., 2018), and 299 several are inconclusive (e.g., Bertka and Fei, 1997; Rivoldini et al., 2011). At a lower mantle 300 temperature of 2000 K, the parameterization of Fei et al (2004) suggests that bridgmanite 301 becomes stable at 22.9 GPa. This CMB pressure corresponds to a core radius of approximately 302 1500 km; such a core is smaller than any in Figure 4, but it could be produced by, for example, a 303 low S content, a shallow crust, and no CMB thermal boundary layer. Such a small core is 304 difficult to reconcile with geophysical constraints (see Section 4.4). The bridgmanite stability 305 field grows with temperature, so a hot lower mantle might support bridgmanite at slightly lower 306 pressures. At 2500 K, bridgmanite becomes stable at 22.2 GPa, corresponding to a 1570 km 307 core; such temperatures could only be produced by a CMB thermal boundary layer with a large 308 temperature contrast. This would tend to increase the core radius well beyond this size, meaning 309 that it seems unlikely that bridgmanite exists within modern Mars. A bridgmanite layer would 310 affect mantle convection, increase the temperature of the lower mantle, and reduce heat flow 311 from the core, impacting the both the areothem and the contrast across a CMB thermal boundary 312 layer (Bruer et al., 1998; Michel and Forni, 2011). Thus, if a bridgmanite layer does exist, its 313 thickness will strongly constrain mantle temperature (Bertka and Fei, 1997); the possibility of 314 such a layer in Mars' hotter past may have influenced the convective regime of the Martian 315 mantle towards single-plume upwelling (Sohl and Spohn, 1997).

316

4.3 The crust

317 The outer layers of a planet have an outsized influence on the planet's MOI due to their 318 large radial distance from the center of gravity. Konopliv et al. (2011) determined the Martian 319 MOI to be 0.3644 ± 0.0005 but found that altering crustal thickness by 25 km changes the MOI by 0.0017. Therefore, uncertainties in crustal structure dominate the inertia-based constraints on 320

321 models of the Martian interior. Some recent studies use an even tighter bound on MOI (Khan et 322 al, 2018). Determining the average crustal properties pertinent to a spherically-symmetric model 323 is complicated by the fact that the Martian crust contains a significant dichotomy between the 324 northern and southern hemispheres, various volcanic provinces, impact basins, and 325 heterogeneous regolith. Constraints from orbital gravity measurements and surface topography 326 imply that mean crustal thickness must lie within 57 ± 24 km (Wieczorek and Zuber, 2004), with 327 some studies preferring different portions of this range. We find that within a narrow range of 328 crust sizes (55 ± 10 km) the Martian MOI can be matched with a wide range of core sizes (1500-329 1850 km). Fortunately, InSight measurements are likely to strongly constrain crustal thickness 330 beneath the landing site (Panning et al., 2017), which will allow for tighter constraints on core 331 size.

332 4.4 Core radius

We have evaluated the effects of five parameters on the core radius of Mars: the thickness of the crust, temperatures of the mantle and core, sulfur content of the core, and densities of liquid Fe–S alloys. All core radii calculated here are consistent with the core mass fraction range determined in the core formation model (Section 3.1; Figure 2).

(1) Thickness of the crust. A thick layer of relatively light crustal material requires a
larger core to maintain consistency with the Martian radius and bulk density. Varying
the crustal thickness in the range 25–85 km (Wieczorek and Zuber, 2004)
corresponds to a change in core radius of 94 km, with thicker crusts corresponding to
larger cores. The planet's MOI is very sensitive to crustal parameters, so only a small
portion of this range of crust thicknesses is consistent with measurements (Section
4.3).

344	2) Temperature of the mantle. Martian internal temperature profiles depend on the
345	thermal history of the planet, its radiogenic heat production, and its convective
346	regime. These features are not well constrained, making temperatures difficult to
347	evaluate. Lowermost mantle temperatures of 1800-2100 K bracket the "hot" and
348	"cold" endmembers of Rivoldini et al. (2011). This range corresponds to mantle
349	potential temperatures of 1500-1800 K, consistent with published estimates (e.g.,
350	Nimmo and Faul, 2013). This temperature range corresponds to a change in core
351	radius of 122 km, with larger cores corresponding to hotter mantles.
352	3) CMB thermal boundary layer. Previous studies (e.g., Khan et al., 2018) have
353	generally not considered any significant temperature change across the CMB due to
354	the absence of a Martian geodynamo (Williams and Nimmo, 2004). It is possible that
355	the core is hotter than the overlying mantle, leading to a thin region of rapidly
356	increasing temperatures, analogous to Earth's lowermost mantle. We have
357	investigated models with uppermost core temperatures ranging from 0-600 K above
358	the lowermost mantle temperature, within the allowable range of CMB heat flow (see
359	supplementary materials for more details). This range corresponds to a change in core
360	radius of 103 km, with hotter cores being less dense and thus larger.
361	(4) Sulfur content of the core. Since S is much lighter than Fe, a core with a large S
362	component will have a reduced alloy density, and thus must be larger. Our
363	compositional results (Section 3.2) indicate that to maintain consistency with the
364	inferred mantle composition, the Martian core contains 16-20 wt% S; this range
365	corresponds to 65 km of variability in core size. A core S content of 12-21 wt%
366	encompasses the range of 2.0-5.4 wt% bulk Martian S, corresponding to the

367	difference between the most S-poor (H) and S-rich (EH) chondrites (Lodders and
368	Fegley, 1998). This range changes core radius by 141 km.
369	(5) Effect of melting on Fe–S alloy densities. Since the Martian core is thought to be
370	entirely molten (Konopliv et al., 2011), its geophysical parameters must be calculated
371	with reference to liquid Fe-S alloys. Unfortunately, there are few equation of state
372	studies in this liquid system, and the available ones do not generally extend to the
373	relevant <i>P</i> – <i>T</i> conditions. Some previous studies (e.g., Rivoldini et al., 2011; Khan et
374	al., 2018) have attempted to overcome this difficulty by extrapolating the extant
375	liquid data, but this may underestimate the true density (Figure 6). Several equation
376	of state studies have pointed out that the ΔV between solid and liquid Fe–S alloys
377	should be quite small at high pressures, on the order of 1.5% for the Earth's CMB
378	(Seagle et al., 2006) and only slightly greater for Martian CMB conditions. The
379	ambient ΔV is ~16% for FeS (Kaiura and Toguri, 1979), dropping to only ~4–5% at a
380	few GPa (Nishida et al., 2011). For this study, we have chosen to use the interpolation
381	of the solid densities and correct for a melting effect based on the eutectic melting
382	curve of Fe–S alloys (Campbell et al., 2008), leading to a 3.6% ΔV of melting at the
383	Martian CMB that decreases at greater depth. We have also investigated the effect of
384	imposing fixed ΔV values from 2–5%. This range corresponds to a change in core
385	radius of 56 km.

One of the geophysical constraints on the Martian interior comes from its deformation in response to tidal forcings from the Sun, Phobos, and Deimos. The tidal Love number k_2 has been determined from spacecraft and lander tracking data, most recently in Konopliv et al. (2016), which reported a value of 0.169 ± 0.006 . To evaluate the consistency between this value and our

390 profiles of the Martian interior, we used a simplified two-layer parameterization for calculating 391 k_2 (see supplementary materials for more details). The dissipation of tidal energy within Mars is 392 dependent on the rigidity of the core and mantle layers and their relative sizes. A liquid core 393 cannot sustain shear stress, so its rigidity is negligible; therefore, a very rigid mantle requires a 394 large core to match the planetary k_2 . This tradeoff indicates that, for example, a mean mantle 395 rigidity of $\mu = 80$ GPa requires a core 1840–1900 km in radius to match k_2 , while a softer mantle 396 with $\mu = 60$ GPa only requires a 1540–1640 km core (Supplementary Figure S3). If the Martian 397 mantle accurately reflects the volumetrically averaged shear modulus of ~73 GPa calculated 398 here, then the core should be 1740–1820 km in radius. It is possible to produce a core of at least 399 this size through several combinations of the parameters considered above, even accounting for 400 the constraint on crust size from MOI. The relationship between core radius and the geophysical 401 and geochemical parameters considered here is illustrated in Figures 7 and S4, and can be 402 parameterized by the following equation:

$$R_{core} = 564 + 1.49 \, d_{crust} + 10.1 \, C_{core}^{S} + 0.183 (C_{core}^{S})^{2} + 0.115 \, \Delta T_{TBL}$$

404 +0.000108
$$(\Delta T_{TBL})^2$$
 + 0.423 T_P + 14.8 ΔV_{core} + 0.337 $(\Delta V_{core})^2$ (1)

405 where R_{core} is the radius of the core (km), d_{crust} is the thickness of the crust (km), C_{core}^{S} is the S 406 content of the core (wt%), ΔT_{TBL} is the temperature contrast across the core–mantle thermal 407 boundary layer (K), T_{P} is the mantle potential temperature (K), and ΔV_{core} is the volume change 408 of melting associated with the core alloy (%; e.g., for a 2% volume change of melting, $\Delta V_{core} =$ 409 2). This equation reproduces the results of our geophysical model with a root mean squared 410 misfit of 9 km for core radii of 1450–2000 km and the parameter ranges listed above and should 411 not be applied to more extreme cases. Future seismological constraints on crust thickness and

412 core radius can be inserted into this equation to help constrain geophysical properties of the413 Martian interior.

414 It is also possible that the Martian mantle is less rigid than the melt-free anhydrous 415 idealization depicted here and by other studies. Shear moduli are significantly reduced by both 416 the presence of H and partial melts in mantle minerals. The 300 ppm water suggested to reside in 417 the Martian mantle (Taylor, 2013) would not significantly reduce the mean shear modulus, but 418 Martian water abundances are extremely uncertain. Partial melting is another possibility; fluids 419 cannot support shear stress, so partial melts would decrease the mean shear modulus by the same 420 amount as their volume fraction. Selecting a crust size of 55 km, a potential temperature of 1600 421 K, a core S content of 18 wt%, no TBL, and ΔV of melting of 3% returns a core 1620 km in 422 radius. To match k_2 , this core would require a mean mantle rigidity of 55 GPa, a 15% reduction 423 from our nominal value. This amounts to a basal magma ocean 500 km deep. Such a feature is 424 unlikely, but volumetrically significant melting may also occur beneath the Martian lithosphere 425 (Duncan et al., 2018). Ultimately, some combination of mantle-softening and core-expanding 426 parameters must be responsible for the observed Martian k_2 .

427 4.5 Density and velocity profiles of the Martian interior

We consider the effects of the same five geochemical and geophysical parameters (crust thickness, core and mantle *T*, core S content, Fe–S ΔV of melting) on the density and velocity structure of the Martian interior (Figure 4). Unlike some previously-modeled velocity profiles (e.g., Khan and Connolly, 2008; Zharkov and Gudkova, 2009), we predict a low-velocity zone in the upper mantle due to the steep lithospheric temperature gradient (Section 4.1). Our results share many properties in common with previous LVZ models, such as the large contrast between adiabatic and lithospheric temperatures (Nimmo and Faul, 2013) and a gradual olivine–

435	wadsleyite phase transition due to the high FeO content. This study predicts a V_S in the
436	lowermost mantle that is smaller than V_P at the top of the core, whereas the otherwise similar
437	LVZ model of Zheng et al. (2015) does not (Figure 5). The lower V_P of Zheng et al. (2015) is
438	likely due to their use of FeS data for the thermophysical properties of the core alloy; FeS has a
439	reduced density and bulk modulus compared to our more moderate composition.

440

4.6 Seismic properties

441 Mode center frequencies for the suite of models have been calculated (Figure 8a and S5). Overall, as expected, radial, core-sensitive, and Stonely modes are affected by adjusting the five 442 443 parameters described above. Stonely modes are confined to the CMB and are very challenging to 444 observe even on Earth. Modes with center frequencies below 5 mHz are unlikely to be detectable 445 on Mars (Panning et al., 2017), but radial modes (on the left of Figure 8a) above this period may 446 display changes in frequency of several percent. While not affected by the physical properties of 447 the core itself, we note that models with different crustal thicknesses and mantle potential 448 temperatures will result in different frequencies for the fundamental modes, which are a target 449 for observation (Bissig et al., 2018). Thus, any observations of normal modes on Mars will aid in 450 discrimination between these different models of Martian formation.

451 Body wave travel times (Figure 8b) show that a range of phases that are reflected at the 452 CMB or travel through the core are sensitive to the parameters explored here. As all the models 453 investigated have an LVZ in the upper mantle (Section 4.1), shadow zones are evident in the 454 travel time curves, most prominently in the direct S phase. Models with larger cores show earlier 455 arriving core-reflected phases (for example ScS), whilst signals like PKP are delayed as V_P in the 456 core is lower than that of the mantle. SKS, which travels through the mantle as a shear wave and 457 through the liquid core as a compressional wave, has delay times that vary little though the

458 model suite as V_s in the mantle is very close to V_P in the core. If it can be observed, SKKS, which 459 transits the core twice, would be a better indicator of core size; SKKS's amplitude may be 460 insufficient to observe in InSight data however. Because V_P just below the CMB is higher than 461 V_S just above the CMB in our models, we predict the presence of minor arc SKKS at a wide 462 range of distances (Helffrich, 2017).

463 The InSight site is roughly 20° from Cerberus Fossae (Taylor et al., 2013). At such a 464 distance, one of the clearest core signals we hope to observe will be ScS. Figure 9 shows 465 predicted travel times for this phase at this epicentral distance for the full suite of core models. 466 Nearly all the parameters behave in the same way: shorter ScS travel times correspond to larger 467 core radii. Thus, even though all properties may not be discernable from such an observation, a 468 travel time should permit us to roughly estimate core radius in this framework. Mantle potential 469 temperature has effects on the radius-ScS time relationship which are not co-linear with the 470 other parameters because a hotter potential temperature both decreases mantle velocities and 471 changes core radius. Both crustal thickness and mantle potential temperature may be obtainable 472 from other seismological observables (e.g., receiver function analysis for the former, and 473 estimates of the sub-lithospheric LVZ for the latter), making this kind of analysis more valuable 474 as the possible parameter space is narrowed down further.

475

5. Conclusions

A multi-stage core formation model has successfully reproduced meteorite-based
compositions of the bulk silicate Mars and has been used to determine conditions of core
formation and the composition of the Martian core. The high FeO content of the Martian mantle
relative to that of Earth is due to formation from primordial material initially equilibrated at
approximately IW–1.25. On average, >85% of incoming metal was equilibrated with >30% of

481	the Martian mantle upon impact, and equilibration took place at a depth of 45–91% of the
482	evolving CMB pressure. The light element composition of the Martian core is dominated by S
483	(16–20 wt%), with <1 wt% O and negligible Si.

484 We have considered the possible ranges of various geophysical parameters (mantle and 485 core temperatures, crustal thickness, and density of the Fe–S core alloy) and evaluated the effects 486 of varying these parameters on the structure of the Martian interior. The core alloy densities 487 calculated here are somewhat higher than those of previous studies due to different 488 interpretations of the Fe-S equation of state data. Conservative parameter combinations imply 489 that the core could be as small as 1620 km, though this size is not consistent with geophysical 490 constraints on tidal Love number k_2 unless the Martian mantle is significantly softened by the 491 presence of melt or water. Larger values of the crustal thickness, mantle temperature, core 492 temperature, or S content imply larger cores (Equation 1). If the Martian mantle is not subject to 493 any softening effects, the core can be as large as 1820 km while maintaining consistency with 494 geophysical observations. We have calculated seismic phase arrival times and planetary normal 495 modes for a variety of parameter combinations to facilitate comparison with InSight's upcoming 496 seismological measurements. Whatever the results of these observations, the actual core radius 497 implies a particular combination of geophysical and geochemical parameters, meaning that 498 constraints on core radius will help elucidate the thermal, physical, and compositional state of the 499 Martian interior.

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equilibration, $P_{equil}/P_{CMB} = 0.66$, and initial fO_2 of IW-1.2.





542 Fig. 2. a. The tradeoff between the initial fO_2 of Mars' primordial material and the partitioning of

543 Fe between mantle and core. The green shaded region indicates the range of calculated FeO

544 contents that are consistent with Taylor (2013), which constrain the initial fO_2 to be IW-0.7 to

545 IW–1.4. The corresponding core mass fraction is 0.17–0.26 (grey curve and grey horizontal

shaded bar). **b.** The tradeoff between bulk S content and S content of the core (purple). For the

same range of core mass fractions as in **a** (grey curve and grey horizontal shaded bar), the total S

548 content of bulk Mars is constrained to be $0.20-0.68 \times CI$. The purple shaded region represents

the range of core S contents from the core formation model. Dashed lines represent 95%

550 confidence intervals at $P_{equil}/P_{CMB} = 0.66$ and k = 0.9.



552 Fig. 3. a. Variation in the mantle concentrations of TiO₂ (blue), Co (red), and S (yellow) as a 553 function of the degree of impactor core equilibration, k. Dashed lines are 95% confidence 554 intervals. The colored regions illustrate where the calculated compositions are consistent with the 555 previously published values of Taylor (2013) for TiO₂ and Co, and Wang and Becker (2017) for 556 S. The grey shaded bar indicates the range of k in which all three elements can be matched. 557 These values of k suggest that most metal was emulsified and equilibrated before merging with 558 the Martian core. Calculation was performed for whole mantle equilibration, $P_{equil}/P_{CMB} = 0.66$, 559 and initial fO_2 of IW-1.2. **b.** Variations in the mantle concentrations of Ni (green), Co (red), and 560 S (yellow) as a function of core-mantle equilibration pressure (expressed as a fraction of the 561 evolving CMB pressure). The colored regions illustrate where the calculated compositions are 562 consistent with the previously published values of Taylor (2013) for Ni and Co and Wang, and Becker (2017) for S. These values of equilibration pressure suggest that equilibration occurred in 563 564 a deep magma ocean, but not at the core–mantle boundary. Calculation was performed for k =0.9, whole mantle equilibration, and initial fO_2 of IW-1.2. 565



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Fig. 4. Martian density profiles calculated by varying a single parameter at a time: core S content (a), temperature contrast between the lowermost mantle and uppermost core (assuming a thin thermal boundary layer at the CMB) (b), mantle potential temperature (c), crustal thickness (d), and ΔV of melting of Fe–S alloys (e). The shaded region in (a) corresponds to our preferred S range of 16–20 wt% from the core formation model at initial $fO_2 = IW-1.2$, $P_{equil}/P_{CMB} = 0.66$

572 and k = 0.9 (Section 3.2).





575 profiles between this and several previous studies (dashed line: Sohl and Spohn, 1997 "Model

576 A"; dotted line: Zheng et al., 2015 "LVZ Model"; dot-dashed line: Zharkov and Gudkova, 2009

577 "M14_3 Model"). The profile for this study corresponds to a core sulfur content of 18 wt%,

578 crustal thickness of 50 km, thermal boundary layer temperature contrast of 300 K, and mantle

579 potential temperature of 1600 K. The low-velocity zone in the upper mantle is a consequence of

580 the steep lithospheric temperature profile within the stagnant lid on Mars (Section 4.1).



582

583 Fig. 6. Densities of solid (Chen et al., 2008; Kombavashi et al., 2010; Seagle et al., 2006; 584 Thompson et al., 2016; Urakawa et al., 2004) and liquid (Anderson and Ahrens, 1994; Balog et 585 al., 2003; Morard et al., 2018; Nishida et al., 2011) alloys in the Fe-S system calculated from 586 equations of state at 20 GPa and 2000 K. The solid line is a linear fit to the solid data, and the dashed lines are offset from this line according to fixed ΔV of melting up to the 1 bar ΔV of FeS 587 (Kaiura and Toguri, 1979). The grey box indicates the range of S contents within uncertainty of 588 589 the core formation model and the range of ΔV between that of Fe and FeS at these conditions. All 590 liquid equations of state have been extrapolated beyond the pressure conditions of the original 591 measurements, save for the Fe-10S study (Balog et al., 2003) which was based on sink/float 592 experiments with large (~20%) error bars. Using this data point to derive the properties of the 593 Fe–S alloy (Khan et al., 2018; Rivoldini et al., 2011) results in an implied ΔV greater than that of 594 FeS at 1 bar, which is physically unlikely. Red squares represent some previous models of the Martian core alloy (a: Rivoldini et al., 2011; b: Khan et al., 2018; c: Sohl and Spohn, 1997; d: 595 596 Zharkov and Gudkova, 2005; e: Kavner et al., 2001; f: Bertka and Fei, 1998; g: Sanloup, 1999; 597 h: Lodders and Fegley, 1997; i: Khan and Connolly, 2008). Studies a-f are plotted at the same 598 P-T conditions as the equation of state points, while studies **g**-**i** have fixed (P-T independent) 599 core densities.



600

601 **Fig 7.** Tradeoffs between parameters that influence core size as parameterized by Equation 1. 602 Each panel represents a fixed combination of ΔV of melting (constant throughout each column) 603 and mantle potential temperature (constant throughout each row) and shows the combinations of 604 core S content and CMB thermal boundary layer temperature contrast that can produce cores of a

605 certain size. Each contour connects cores of the same radius. All plots correspond to a 55 km

606 crust. For this crust size, the approximate MOI constraints on core size (1550–1700 km) are

607 indicated by dashed lines. Supplementary Figure S4 shows alternate versions of this figure

608 corresponding to different crustal thicknesses.



609 Fig. 8. Seismological observables corresponding to four models with different core S contents. a.

610 Normal mode center frequencies. The radial modes sit on the vertical axis (l=0). InSight's

- broadband seismometer is expected to be unable to detect those modes under 5 mHz. **b.** Body
- 612 wave travel time predictions for a 5 km deep marsquake. Seismic phases P, PP, PcP, Pdiff, S, SS,
- 613 $\,$ ScS, S_{diff}, PcS, ScP, SP, PKP, SKS, and SKKS are shown.
- 614



Fig. 9. Relationship between core radius and predicted ScS arrival time. Travel times are

618 predicted for an epicentral distance of 20° and a marsquake depth of 5 km. The impact of each

619 of the five parameters on core radius is discussed in Section 4.4. In each case the larger symbol

- 620 corresponds to the lowest value of the parameter that is being varied.

631 Appendix A. Supplementary materials

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