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6 Seismic observation of tsunami at island broadband 7 stations

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12 Key Points:

- 13 • For quantification of seismic observation of tsunami, we evaluate scattering of
14 an incident tsunami for an axisymmetric structure.
- 15 • Ground deformation due to the tsunami loading is modeled using static Green's
16 functions.
- 17 • By fitting the modeled displacement to observed seismic data, the incident
18 tsunami is inferred from the seismic observation.

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Abstract

Previous studies have reported seismic observations of tsunami recorded at island broadband stations. Coastal loading by the tsunami can explain them. For further quantification, we model tsunami propagation assuming an axisymmetric structure: a conical island with a flat ocean floor. The total tsunami wavefield can be represented by superposition between an incident tsunami wave and the scattering. The ground deformation due to the total tsunami wavefield at the center is calculated using static Green's functions for elastic half-space with a first-order correction for bathymetry. By fitting the modeled displacement to observed seismic data, we can infer the incident tsunami wave, which can be interpreted as the virtual tsunami amplitude without the conical island. First, we apply this new method to three components of seismic data at a volcano island, Aogashima, for the 2015 Torishima-Oki tsunami earthquake. The estimated tsunami amplitude from the vertical component is consistent with the offshore array observation of absolute pressure gauges close to the island (1.5–20 mHz). The estimated incident azimuth from the three components is also consistent with ray theory. Second, we apply this method to seismic data at four island broadband stations in the Indian ocean for the 2010 Mentawai tsunami earthquake in Indonesia. Despite the limited observed frequency range from 0.5–2.0 mHz, the amplitudes and incident azimuths are consistent with past studies. These observations can complement offshore tsunami observations. Moreover, this method is applicable not only for a tsunami but also for background ocean infragravity wave activity.

1 Introduction

Crustal deformation beneath the ocean due to a massive shallow earthquake generates tsunami (e.g. [Satake, 2015](#)). Physically, these are also known as ocean infragravity waves or ocean external gravity waves. Although tsunami amplitudes are usually small in the deep ocean, they increase drastically as tsunami approaches the coast. Such large amplitudes cause severe damage in coastal areas. Understanding tsunami propagation is important for effectively evaluating the risk. Tsunami observations are also crucial for characterizing the source processes of an earthquake (e.g. [Satake, Fujii, Harada, & Namegaya, 2013](#)). Observations by offshore ocean bottom pressure gauges (e.g. Deep-ocean Assessment and Reporting of Tsunamis (DART) ([Bernard & Meinig, 2011](#))) are typically used for source inversion because of simple wave propagation in the pelagic environment.

Loading on the seafloor by tsunami causes ground deformation of the ground, and vice versa, which is detectable by land-based broadband seismic stations. For example, when the 2010 Maule earthquake hit Chile, a high-density tiltmeter network in Japan recorded ground tilt motions with a typical period of approximately one hour over a broad inland area facing the Pacific coast ([Kimura, Tanaka, & Saito, 2013](#)). Simple 2-D modeling for the deformation induced by the Chilean tsunami explained the observed tilt motions in the Japanese island arc ([Kimura et al., 2013](#)). During the 2004 Sumatra–Andaman earthquake, tilt motions from 0.3–0.6 mHz were recorded by a broadband seismometer at Showa station at the mouth of a bay in Antarctica ([Nawa et al., 2007](#)), and tilt motions with typical periods of approximately 1000 s were recorded by broadband seismometers at stations on islands in the Indian ocean ([Yuan, Kind, & Pedersen, 2005](#)). Although the order of observed amplitudes can be explained by tilt motions caused by tsunami loading, the mechanism is not yet fully understood.

Figure 1 shows an example of broadband seismic records at a volcano island, Aogashima, associated with tsunami when the 2015 Torishima earthquake (see section 5 for details). The observed larger amplitudes in horizontal components suggest the effect of tilt motions is dominant. All the seismic records lack the higher-frequency content.

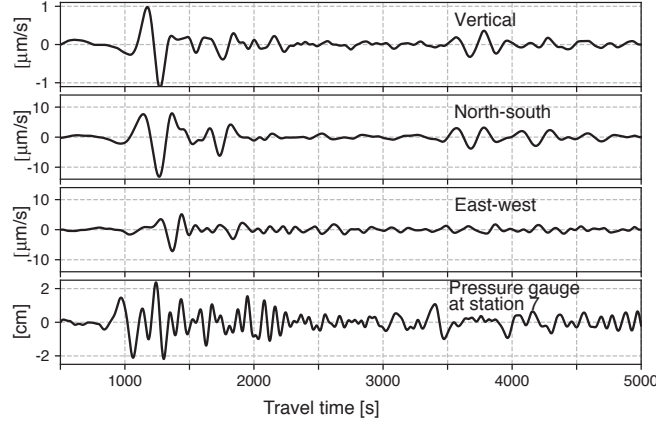


Figure 1. The upper three records show 3 components of the ground velocity recorded by a broadband seismometer at Aogashima (N.AOGF). The lowest record shows tsunami height at an offshore pressure gauge (station 7 shown in Figure 2). All the records are bandpass-filtered from 2 to 20 mHz.

70 To quantify ground motions at islands, we model the sloping effects in a semi-
 71 analytic manner for an axisymmetric conical island with a flat ocean floor (Fujima &
 72 Goto, 1994; Kânoğlu & Synolakis, 1998; Smith & Sprinks, 1975). Although the model
 73 is simple, it can express the complex wave propagation close to the shoreline. This
 74 simple model can explain the spatial pattern of coastal tsunami amplification around
 75 islands.

76 In section 2, we present a theory of tsunami propagation when an arbitrary
 77 tsunami wavefield enters a conical island. In section 3, we then estimate the ground
 78 deformation at the center of the island due to tsunami loading, which can be related to
 79 the incident tsunami wavefield. In section 4, using the axisymmetric assumption, we
 80 propose a new technique for estimating virtual tsunami amplitude without a conical
 81 island, which could be a proxy for offshore tsunami amplitude. In section 5, this
 82 method is applied to two examples: the 2015 Torishima earthquake in Japan and the
 83 2010 Mentawai tsunami earthquake in Indonesia.

84 **2 Theory of tsunami propagation for a conical island with a flat ocean** 85 **floor**

86 In this study, we consider scattering of tsunami around an axisymmetric conical
 87 island. For simplicity, we assume that the tsunami can be approximated as a linear
 88 long-wave because dispersion effects should be less important than topographic effects
 89 in this case. Following (Gill, 1982), we consider shallow-water equations derived us-
 90 ing the hydrostatic approximation. The displacement amplitude of the sea surface
 91 disturbance $\eta(r, \theta; t)$ satisfies the following governing equation in time domain:

$$92 \quad \frac{\partial^2 \eta(r, \theta; t)}{\partial t^2} = g_0 \nabla_h [D(r) \nabla_h \eta(r, \theta; \omega)], \quad (1)$$

93 where r is the radius, θ is the azimuth (Figure 3), g_0 is the gravity constant, ∇_h
 94 represents the spatial gradient in 2-D, and $D(r)$ is an axisymmetric water depth given

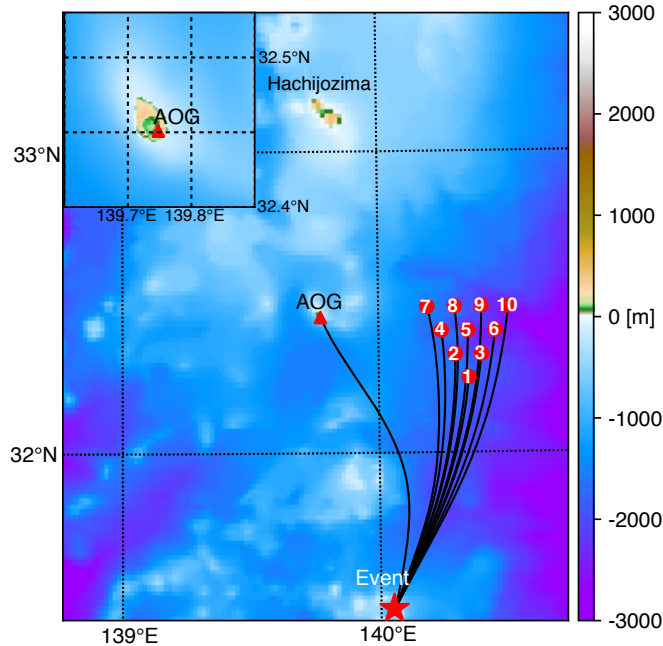


Figure 2. Station distribution of an array of 10 offshore pressure gauges (circles). The inset shows an enlarged map of Aogashima (AOG). The star symbol shows the hypocenter of the earthquake near Torishima on May 2, 2015. At approximately 33.1°N, Hachijojima north to Aogashima is also shown. The station numbers are shown in red circles.

95 by

$$96 \quad D(r) = \begin{cases} 0 & \text{if } r < r_0, \\ m(r - r_0) & \text{if } r_0 \leq r < r_1, \\ D_0 & \text{if } r_1 \leq r, \end{cases} \quad (2)$$

97 where r_1 is the radius of the root of the island, r_0 is the radius of the island, D_0 is
98 the sea surface height of the flat ocean from the sea bottom, and m is the slope given
99 by $D_0/(r_1 - r_0)$. The frequency-domain representation $\eta(r, \theta; \omega)$ satisfies the following
100 equation:

$$101 \quad -\omega^2 \eta(r, \theta; \omega) = g_0 D(r) \nabla_h^2 \eta(r, \theta; \omega) + g_0 \nabla_h D(r) \cdot \nabla_h \eta(r, \theta; \omega), \quad (3)$$

102 where ω is the angular frequency.

103 We note that, for negative frequency, $\eta(r, \theta, -\omega)$ is defined as the complex conju-
104 gate by $\eta^*(r, \theta; \omega)$ because the time domain representation should be a real function.
105 A Fourier component at a negative frequency $-\omega$ is, thus, defined by the complex
106 conjugate of that at a positive frequency ω . Here, we use the Fourier convention:

$$107 \quad F(\omega) = \int_{-\infty}^{\infty} f(t) e^{-i\omega t} dt, \quad (4)$$

108 where f is an arbitrary function as a function of time, t , and F is its Fourier component.

109 At high frequency, tsunami velocity $\sqrt{g_0 D(r)}$ near the coast decreases towards
110 zero. The coastal low-velocity region traps tsunami energy, which enhances tsunami
111 run-up height (e.g. Liu, Cho, Briggs, Lu, & Synolakis, 1995; Satake, 2015). Zero
112 velocity at the coast makes the governing equation singular. By using the axisymmetric

113 approximation, however, an analytic evaluation of the singularity becomes possible
 114 (Fujima & Goto, 1994).

115 Because the governing equation is axisymmetric, tsunami wavefield $\eta(r, \theta; \omega)$ can
 116 be expanded by a Fourier series with respect to the azimuth, in general, as:

$$117 \quad \eta(r, \theta; \omega) = \frac{1}{2} \phi_0(r; \omega) \\
 118 \quad + \sum_{n=1}^{\infty} [\phi_n(r; \omega) \cos(n\theta) + \phi_{-n}(r; \omega) \sin(n\theta)], \quad (5) \\
 119$$

120 where $\phi_n(r; \omega)$ is the radial function of azimuthal order n . We assume that an arbitrary
 121 incident tsunami wave $\eta^{in}(r, \theta; \omega)$ enters the island and is scattered in the sloping
 122 bottom (region II in Figure 3); thus, the total wavefield $\eta(r, \theta; \omega)$ in the flat ocean
 123 (region I in Figure 3) can be represented by superposition between the incident wave
 124 and the scattered wave (Fujima & Goto, 1994; Kânoğlu & Synolakis, 1998; Smith &
 125 Sprinks, 1975). In the following subsections, we evaluate $\phi_n(r; \omega)$ by considering the
 126 scattering for an arbitrary incident wave field using a semi-analytic method (Fujima
 127 & Goto, 1994; Kânoğlu & Synolakis, 1998).

128 2.1 Incident tsunami wavefield

129 First, let us consider an arbitrary incident arbitrary wavefield $\eta^{in}(r, \theta; \omega)$ in a flat
 130 ocean without the conical island virtually. The incident wavefield in a flat ocean η^{in}
 131 can be expanded by a Fourier series with respect to the azimuth and Bessel functions
 132 of the first kind with respect to the radial direction as follows:

$$133 \quad \eta^{in}(r, \theta; \omega) = \frac{1}{2} \zeta_0^{in}(\omega) J_0(k_0 r) \\
 134 \quad + \sum_{n=1}^{\infty} [\zeta_n^{in}(\omega) \cos(n\theta) + \zeta_{-n}^{in}(\omega) \sin(n\theta)] J_n(k_0 r), \quad (6) \\
 135$$

136 where J_n is the n th order Bessel function of the first kind, k_0 is the wavenumber given
 137 by $\omega/\sqrt{g_0 D_0}$, and $\zeta_n^{in}(\omega)$ is the coefficient.

138 2.2 Wave scattering by a conical island in a flat ocean (I)

139 The incident wave $\eta^{in}(r, \theta; \omega)$ enters the conical island area and the scattered
 140 wave amplitude is represented by $\eta^{sc}(r, \theta; \omega)$. The total tsunami amplitude η can be
 141 written as

$$142 \quad \eta(r, \theta; \omega) = \eta^{in}(r, \theta; \omega) + \eta^{sc}(r, \theta; \omega). \quad (7)$$

143 Let us consider the scattered wavefield $\eta^{sc}(r, \theta; \omega)$ for the flat ocean floor (I)
 144 (see Figure 3). The scattered wavefield $\eta^{sc}(r, \theta; \omega)$ can be represented by an outgoing
 145 wave in the flat ocean according to the causality of the scattered wave. For a positive
 146 angular frequency ω , the scattered wavefield can be written as

$$147 \quad \eta^{sc}(r, \theta; \omega) = \frac{1}{2} B_0(\omega) \zeta_0^{in}(\omega) H_0^{(2)}(k_0 r) \\
 148 \quad + \sum_{n=1}^{\infty} [B_n(\omega) \zeta_n^{in}(\omega) \cos(n\theta) + B_{-n}(\omega) \zeta_{-n}^{in}(\omega) \sin(n\theta)] H_n^{(2)}(k_0 r), \quad (8) \\
 149$$

150 where $H_n^{(2)}(\omega)$ is the n th order Hankel function of the second kind, which represents
 151 outgoing waves, and B_n shows the relative amplitudes of the scattered wave.

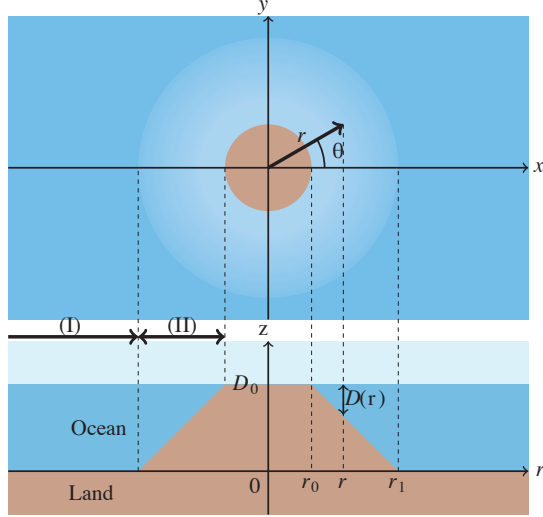


Figure 3. Schematic figure of the conical island. The upper panel shows the plan view of the island, and the lower panel shows the cross-section. The radius on the surface is r_0 and that of the base is r_1 .

152 In summary, $\phi_n(r; \omega)$ (equation (5)) in this region (I) is given by

$$153 \quad \phi_n(r; \omega) = \left(B_n(\omega) H_n^{(2)}(k_0(\omega)r) + J_n(k_0(\omega)r) \right) \zeta_n^{in}(\omega). \quad (9)$$

154 We note that the Bessel functions represent the incident waves and the Hankel functions represent the outgoing scattered waves.
155

156 2.3 Tsunami wavefield above the sloping bottom in region (II)

157 For the numerical calculation of $\phi_n(r; \omega)$ within region (II) ($r_0 \leq r \leq r_1$), we
158 define the amplitude A_n and the normalized radial function R_n as:

$$159 \quad \phi_n(r; \omega) = A_n(\omega) R_n(r; \omega) \zeta_n^{in}(\omega), \quad (10)$$

160 where R_n is normalized so that $R_n(r_0; \omega) = 1$ and A_n is the amplitude factor of ϕ_n at
161 $r = r_0$. Equation (5) in region (II) can be rewritten as follows:

$$162 \quad \eta(r, \theta; \omega) = \frac{1}{2} A_0(\omega) \zeta_0^{in}(\omega) R_0(r; \omega) \\ 163 \quad + \sum_{n=1}^{\infty} [A_n(\omega) \zeta_n^{in}(\omega) \cos(n\theta) + A_{-n}(\omega) \zeta_{-n}^{in}(\omega) \sin(n\theta)] R_n(r; \omega). \quad (11)$$

165 Inserting $\eta(r, \theta; \omega)$ into the governing equation (equation (3)) leads to the following
166 equation of R_n :

$$167 \quad \frac{d^2 R_n(r; \omega)}{dr^2} + \left(\frac{1}{r} + \frac{1}{D(r)} \frac{dD(r)}{dr} \right) \frac{dR_n(r; \omega)}{dr} + \left(\frac{\omega^2}{g_0 D(r)} - \frac{n^2}{r^2} \right) R_n(r; \omega) = 0. \quad (12)$$

168 Following [Fujima and Goto \(1994\)](#), we define the following dimensionless param-
 169 eters, ξ and β , to characterize this system. $\xi(r)$ is the radial phase defined as

$$170 \quad \xi(r) \equiv \int_{r_0}^r k(r') dr' = 2\omega \sqrt{\frac{(r-r_0)}{g_0}} \quad \text{if } r_0 \leq r \leq r_1, \quad (13)$$

171 where $k(r)$ is the local wave number given by

$$172 \quad k(r) \equiv \frac{\omega}{\sqrt{g_0 D(r)}}. \quad (14)$$

173 β is the azimuthal number along a circle with a radius of $2r_0$ defined by

$$174 \quad \beta \equiv \left. \frac{2\pi r}{\lambda(r)} \right|_{r=2r_0}, \quad (15)$$

175 where $\lambda(r)$ is wavelength defined by $2\pi/k(r)$. The reason for choosing this radius is
 176 discussed in section 6.

177 The change of variables from r and h to ξ and β leads to the following equation:

$$178 \quad \frac{d^2 R_n(\xi; \omega)}{d\xi^2} + \left(\frac{2\xi}{\xi^2 + \beta^2} + \frac{1}{\xi} \right) \frac{dR_n(\xi; \omega)}{d\xi} + \left(1 - \left(\frac{2\xi}{\xi^2 + \beta^2} \right)^2 n^2 \right) R_n(\xi; \omega) = 0. \quad (16)$$

179 Only in two extreme cases of the radius of the island ($r_0 = 0$ and $r_0 = \infty$) ([Fujima
 180 & Goto, 1994](#)) can we obtain the analytical solutions of $R(\xi)$, which are crucial for
 181 understanding the behavior of $R(\xi)$. Two independent solutions exist according to the
 182 governing equation; the only one satisfies the physical requirement, which is a finite
 183 amplitude of η at the shoreline. First, let us consider the analytical solution for an
 184 infinite radius of the island, which also represents a flat sloping bottom. Because β
 185 becomes infinite, $R_n(\xi)$ is given by

$$186 \quad R_n(\xi) \sim J_0(\xi). \quad (17)$$

187 Next, let us consider the analytical solution for the zero island radius case $r_0 = 0$.
 188 Because β becomes 0, $R_n(\xi)$ can be given by

$$189 \quad R(\xi) \sim \frac{J_{\sqrt{1+4n^2}}(\xi)}{\xi}. \quad (18)$$

190 Here, we choose a solution that has a finite amplitude at $\xi = 0$. At $\xi = 0$, only $R_0(\xi)$
 191 has a non-zero value, whereas $R_n(0) = 0$ for $n \neq 0$. In general, $R_n(\xi)$ has a significant
 192 value at $\xi = 0$ when $n \leq \beta$ ([Fujima & Goto, 1994](#)). Since the evaluation of the ground
 193 deformations requires only R_n for $n = 0, \pm 1$, as discussed in the following sections, all
 194 the $R_n(\xi)$ have significant values at around $\xi = 0$

195 This ordinary differential equation can be solved using the numerical Livermore
 196 Solver for Ordinary Differential Equations (LSODE) ([Radhakrishnan & Hindmarsh,
 197 1993](#)). Although R_n is integrated from $\xi = 0$ outward with respect to ξ , the governing
 198 equation at $\xi = 0$ is a singularity. For this reason, $R_n(\xi)$ is integrated from $\xi = \Delta\xi$
 199 numerically. $R_n(\Delta\xi)$ can be evaluated analytically by the asymptote ([Fujima & Goto,
 200 1994](#)). $R_n(\Delta\xi)$ can be represented by Taylor expansion up to the second order when
 201 $\Delta\xi \ll 1$ and $\beta \neq 0$ ([Fujima & Goto, 1994](#)):

$$202 \quad R_n(\Delta\xi) \approx \left(1 - \frac{1}{4} \Delta\xi^2 \right). \quad (19)$$

203 Accordingly, the first order initial boundary conditions of R_n at $\xi = \Delta\xi$ are given by

$$204 \quad R_n(\Delta\xi) = 1, \quad (20)$$

$$205 \quad \left. \frac{dR_n(\xi)}{d\xi} \right|_{\xi=\Delta\xi} = -\frac{1}{2}\Delta\xi. \quad (21)$$

207 2.4 Boundary condition between (I) and (II)

208 We evaluate the boundary condition between (I) and (II) at $r = r_1$ for this
 209 equation. Continuity of the amplitude for each azimuthal order, n , and the first
 210 derivative at the boundary between regions (I) and (II) leads to the following boundary
 211 condition:

$$212 \quad A_n(\omega)R_n(\xi_1) = J_n(k_0r_1) + B_n(\omega)H_n^{(2)}(k_0r_1), \quad (22)$$

$$213 \quad A_n(\omega) \left(\frac{dR_n(\xi)}{d\xi} \frac{d\xi}{dr} \right) \Big|_{\xi=\xi_1} = \frac{dJ_n(k_0r)}{dr} \Big|_{r=r_1} + B_n(\omega) \frac{dH_n^{(2)}(k_0r)}{dr} \Big|_{r=r_1}, \quad (23)$$

214 where $\xi_1 \equiv \xi(r_1)$. We can estimate A_n and B_n by solving this equation.
 215

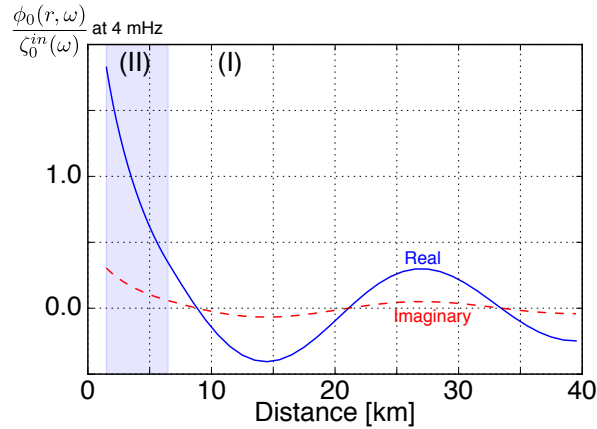


Figure 4. $\phi_0(r; \omega)/\zeta_0(\omega)$ at 4 mHz for Aogashima, the parameters of which are given in Table 1. The blue line shows the real part and the red dashed line shows the imaginary part.

216 Figure 4 shows the induced tsunami wavefield with azimuthal order 0 for the unit
 217 amplitude of the incident wave ($\phi_0(r; \omega)/\zeta_0^{in}(\omega)$) at 4 mHz. The parameters are those
 218 for Aogashima given in Table 1. At approximately $r = r_0$, $\phi_0(r; \omega)/\zeta_0^{in}(r; \omega)$ is larger
 219 than 1, which indicates amplification due to confinement along the coast. We discuss
 220 this in detail in section 6.

221 3 Ground deformation by tsunami loading

222 To estimate ground motions due to tsunami, we assume that they can be rep-
 223 resented by static deformation caused by tsunami loading (e.g. Sorrells & Goforth,
 224 1973) because the phase velocity of seismic waves (on the order of 4 km/s) is much
 225 faster than that of a tsunami (on the order of 0.01 km/s) in coastal areas. Loading on
 226 the seafloor by the modeled tsunami wavefield is convolved with static Green's func-
 227 tions in a semi-infinite medium with the following correction for bathymetric effects.
 228 Because the radius of the island, r_0 , is much smaller than r_1 in most cases, we evaluate
 229 the deformation, $\mathbf{u}(\omega)$, at the center of the island for simplicity. Note that the tilt mo-

Table 1. Parameters (radius of the island r_0 , slope m , and ocean depth D_0) used in this study based on ETOPO1 (Amante & Eakins, 2009). These parameters were estimated by the non-linear least-squares technique using MINPACK (Moré et al., 1984) with trial and error. f_β is a reference frequency used as $\beta = 1$ in equation (15).

station	radius r_0 [km]	slope m	ocean depth D_0 [km]	f_β [mHz]
AOG	1.5	0.20	1.0	2.9
RER	29	0.070	4.2	0.39
AIS	4.9	0.18	2.0	1.5
DGAR	12	0.017	4.2	0.29
CRZF	10	0.034	3.0	0.45

tion at the center is also calculated because the horizontal component of a broadband seismometer is sensitive to tilt motion in this frequency range (Aki & Richards, 1980).

To evaluate the bathymetric correction for the Green’s functions in a semi-infinite medium, the displacement $\mathbf{u}(x, y, z)$ and stress $\boldsymbol{\sigma}(x, y, z)$ in a Cartesian coordinate system (x, y, z) is expanded by the powers of slope, m , up to the first order (Segall, 2010; Williams & Wadge, 2000):

$$u_i(x, y, z; \omega) = u_i^{(0)}(x, y, z; \omega) + u_i^{(1)}(x, y, z; \omega)m + \mathcal{O}(m^2), \quad i = x, y, z \quad (24)$$

$$\sigma_{ij}(x, y; \omega) = \sigma_{ij}^{(0)}(x, y, z; \omega) + \sigma_{ij}^{(1)}(x, y, z; \omega)m + \mathcal{O}(m^2), \quad i, j = x, y, z, \quad (25)$$

where \mathcal{O} indicates "order of", u_i is the displacement, σ_{ij} is the stress, $^{(0)}$ shows the 0th order term, and $^{(1)}$ shows the first order terms. Based on the estimation of the first order terms described in appendix A, the first order terms with respect to the slope, m , becomes comparable to the second order terms. Therefore, we neglect the first order terms below.

The displacement and tilt on the surface ($z = D_0$) and at the center ($x = y = 0$) are corrected for elevation from $z = 0$ as follows:

$$u_\alpha(0, 0, D_0) = u_\alpha^{(0)}(0, 0, 0) - D_0 \left. \frac{\partial u_z^{(0)}}{\partial \alpha} \right|_{z=0}, \quad \alpha = x, y, \quad (26)$$

$$u_z(0, 0, D_0) = u_z^{(0)}(0, 0, 0), \quad (27)$$

$$\left. \frac{\partial u_z}{\partial \alpha} \right|_{x=y=0, z=D_0} = \left. \frac{\partial u_z^{(0)}}{\partial \alpha} \right|_{x=y=z=0}, \quad \alpha = x, y. \quad (28)$$

The first-order corrections of horizontal displacement according to the location change are related to the corresponding 0th-order tilt motions. The correction of vertical displacement and tilt motion according to the location change is negligible in the first order because the surface pressure causes a vertical strain $\partial u_z^{(0)}/\partial z = 0$ at the free surface in a half space (Farrell, 1972).

Static Green’s functions $g_r^z(r)$, $g_\theta^z(r)$, and $g_z^z(r)$ at a surface point $\mathbf{r} = (r, \theta, 0)$ for a vertical force at the origin in a semi-infinite medium are given by (Jaeger, Cook,

& Zimmerman, 2007; Segall, 2010)

$$g_r^z(r) = \frac{1}{4\pi} \frac{1}{\lambda + \mu} \frac{1}{r}, \quad (29)$$

$$g_\theta^z(r) = 0, \quad (30)$$

$$g_z^z(r) = \frac{1}{4\pi\mu} \frac{\lambda + 2\mu}{\lambda + \mu} \frac{1}{r}, \quad (31)$$

where r is the radius in a cylindrical coordinate system (Figure 3), μ , and λ are Lamé's constant of the ground, the superscript on the Green's tensors refers to the direction of the point force, and the subscript refers to the direction of displacement. By convolving forcing by the total tsunami wavefield and the static Green's functions with bathymetric corrections, we can estimate the displacement and tilt at the center.

4 Virtual tsunami amplitude and direction without a conical island

Based on the total tsunami wavefield (section 2) and the Green's functions (section 3), we can relate the ground particle velocity at the center to the incident tsunami using a transfer function. The axisymmetric assumption of the island simplifies the transfer function concerning the azimuthal dependence. By deconvolving the transfer function from observed seismic data in the vertical component, we can infer the incident tsunami amplitude, η^v , at the center assuming that the island is virtually removed. By deconvolving the transfer function from observed seismic data in the horizontal component, we can estimate the spatial gradient of η^v , which shows the propagation direction together with a single plane wave assumption.

4.1 Transfer function of the vertical component

The vertical ground velocity at the origin $v_z(\omega)$ due to the tsunami deformation can be represented by convolution between tsunami loading and the static Green's function as:

$$v_z(\omega) = -\rho g_0 \omega e^{i\pi/2} \int_{r_0}^{\infty} \int_0^{2\pi} \eta(r, \theta; \omega) g_z^z(r) r dr d\theta, \quad (32)$$

where $v_z(\omega)$ is the particle velocity in the z component given by $i\omega u_z(\omega)$. Let us evaluate the integration using equations (5), (9), and (10). Because the integrand is axisymmetric, the higher order contributions with respect to azimuthal order ($n \geq 1$) such as:

$$-\rho g_0 \omega e^{i\pi/2} \int_{r_0}^{\infty} \phi(r; \omega) g_z^z(r) r dr \int_0^{2\pi} \cos(n\theta) d\theta \quad (33)$$

are canceled out. Here, we define the virtual tsunami amplitude, $\eta^v(\omega)$, without the island as

$$\eta^v(\omega) \equiv \eta^{in}(r, \theta; \omega)|_{r=0}. \quad (34)$$

The virtual tsunami amplitude can be related to the particle velocity v_z using a transfer function $T_{\eta z}$:

$$v_z(\omega) = T_{\eta z}(\omega) \eta^v(\omega), \quad (35)$$

where $T_{\eta z}(\omega)$ is the transfer function of the tsunami to vertical ground velocity, defined as

$$T_{\eta z}(\omega) \equiv -e^{i\pi/2} \pi \omega \rho g_0 (I_1^z(\omega) + I_2^z(\omega)), \quad (36)$$

296 The integrals I_1^z and I_2^z are defined as

$$297 \quad I_1^z(\omega) \equiv \int_{r_1}^{\infty} \left(B_0(\omega) H_0^{(2)}(k_0 r) + J_0(k_0 r) \right) g_z^z(r) r dr, \quad (37)$$

$$298 \quad I_2^z(\omega) \equiv \int_{r_0}^{r_1} A_0(\omega) R_0(r) g_z^z(r) r dr, \quad (38)$$

299
300 respectively. Figure 5a shows an example of the vertical transfer function $T_{\eta z}(\omega)$ for
301 Aogashima. Below 5 mHz, the transfer function is flat. At 0 frequency, the amplitude
302 and phase of the transfer function can be explained by the theoretical solution for a
303 flat ocean (Ben-Menahem & Singh, 2000) as discussed in section 6. The amplitude
304 decreases with a frequency above 5 mHz because tsunami wavelength becomes smaller
305 than the island scale r_0 .

306 4.2 Transfer function of the horizontal component

307 Let us consider the transfer function of the horizontal component for tsunami
308 incidence in the same manner. The horizontal ground velocity at the origin $\mathbf{v}_h(\omega)$ due
309 to tsunami deformation can be represented by

$$310 \quad \mathbf{v}_h(\omega) \equiv \begin{pmatrix} v_x(\omega) \\ v_y(\omega) \end{pmatrix} = -\rho g_0 \omega e^{i\pi/2} \int_{r_0}^{\infty} \int_0^{2\pi} \eta(r, \theta; \omega) \left(g_r^z - D_0 \frac{\partial g_z^z}{\partial r} \right) \begin{pmatrix} -\cos \theta \\ -\sin \theta \end{pmatrix} r dr d\theta. \quad (39)$$

311 Because $\cos \theta$ and $\sin \theta$ have orthogonality with respect to the azimuthal integration,
312 only $n = \pm 1$ in terms of η contributes to the integration, as follows:

$$313 \quad \begin{pmatrix} v_x(\omega) \\ v_y(\omega) \end{pmatrix} = \frac{i}{2} T_{\eta h}(\omega) \begin{pmatrix} \zeta_1^{in} \\ \zeta_{-1}^{in} \end{pmatrix} = i \frac{T_{\eta h}(\omega)}{k_0} \nabla_h \eta^{in}(r, \theta; \omega) \Big|_{r=0}. \quad (40)$$

314 Here, $T_{\eta h}(\omega)$ is given by,

$$315 \quad T_{\eta h}(\omega) = 2\pi \omega \rho g_0 \left(I_1^h(\omega) + I_2^h(\omega) \right), \quad (41)$$

316 where integrals I_1^h and I_2^h are defined as

$$317 \quad I_1^h(\omega) \equiv \int_{r_1}^{\infty} \left(B_1(\omega) H_1^{(2)}(k_0 r) + J_1(k_0 r) \right) \left(g_r^z - D_0 \frac{\partial g_z^z}{\partial r} \right) r dr, \quad (42)$$

$$318 \quad I_2^h(\omega) \equiv \int_{r_0}^{r_1} A_1(\omega) R_1(r) \left(g_r^z - D_0 \frac{\partial g_z^z}{\partial r} \right) r dr. \quad (43)$$

319
320 The spatial gradient of the surface displacement $\nabla_h \eta|_{r=0}$ can be related to the flow
321 rate, \mathbf{Q} (Satake, 2015), at the origin defined as

$$322 \quad \mathbf{Q} = \int_{D_0 - D(r)}^{D_0} \mathbf{v}_h dz = \frac{i g_0}{\omega} \nabla_h \eta^{in} \Big|_{r=0} \quad (44)$$

323 $D(r)$ is water depth at r and D_0 is water depth of the flat ocean floor (Figure 3).

324 For simplicity, we assume that η can be represented by a single plane wave
325 incidence with the relative travel time, $\mathcal{T}(r, \theta)$, to the origin. The gradient can be
326 written as

$$327 \quad \nabla_h \eta^{in}(r, \theta; \omega) = -i \omega \eta^{in}(0, \theta; \omega) \nabla_h \mathcal{T}(r, \theta) = \eta^{in}(0, \theta; \omega) (-i k_0) \mathbf{e}_r, \quad (45)$$

328 where \mathbf{e}_r is the propagation direction of the tsunami. Then, we obtain the following
329 relationship:

$$330 \quad \mathbf{v}_h(\omega) = T_{\eta h}(\omega) \eta^v(\omega) \mathbf{e}_r. \quad (46)$$

331 $T_{\eta h}$ represents the transfer function from the tsunami incidence to horizontal ground
 332 velocity at the center. This result shows that the observed ground velocity is parallel
 333 to the tsunami propagation direction under the single plane-wave assumption. Figure
 334 5a shows an example of the horizontal transfer function $T_{\eta z}(\omega)$ for Aogashima. The
 335 transfer function has a broad peak at 5 mHz. At 0 frequency, the amplitude and phase
 336 of the transfer function can be explained by the theoretical solution for a flat ocean
 337 (Ben-Menahem & Singh, 2000) as discussed in section 6. The amplitude also decreases
 338 with a frequency above 5 mHz.

339 Below 1 mHz, tilt motion induced by tsunami is dominant in the horizontal compo-
 340 nent of seismic sensors (Kimura et al., 2013; Nawa et al., 2007). The horizontal
 341 acceleration contribution due to tilt motion ($\nabla_h u_z$, where u_z is the vertical displace-
 342 ment) is given by $g_0 \nabla_h u_z$ (e.g. Rodgers, 1968; Wielandt & Forbriger, 1999). Then, the
 343 tilt motion at the origin, $v(\omega)$, due to deformation by the tsunami can be represented
 344 by

$$345 \quad \mathbf{v}_h^{tilt}(\omega) = \frac{g_0 \nabla_h u_z}{i\omega} = \frac{-\rho g_0}{i\omega} \int_{r_0}^{\infty} \int_0^{2\pi} \eta(r, \theta; \omega) \frac{\partial g_r^z}{\partial r} \begin{pmatrix} -\cos \theta \\ -\sin \theta \end{pmatrix} r dr d\theta. \quad (47)$$

346 The higher order contributions ($n \neq \pm 1$) are again canceled out.

$$347 \quad \mathbf{v}_h^{tilt}(\omega) = \frac{i}{2} T_{\eta h}(\omega) \begin{pmatrix} \zeta_1^{in} \\ \zeta_{-1}^{in} \end{pmatrix} = i \frac{T_{\eta h}^{tilt}(\omega)}{k_0} \nabla_h \eta^{in}(r, \theta; \omega)|_{r=0}. \quad (48)$$

348 Here, the transfer function due to tilt, $T_{\eta h}^{tilt}(\omega)$, of the tsunami to horizontal ground
 349 velocity is given by,

$$350 \quad T_{\eta h}^{tilt}(\omega) = \frac{2\pi \rho g_0}{\omega} (I_1^t(\omega) + I_2^t(\omega)), \quad (49)$$

351 where integrals I_1^t and I_2^t are defined by

$$352 \quad I_1^t(\omega) \equiv \int_{r_1}^{\infty} \left(B_1(\omega) H_1^{(2)}(k_0 r) + J_1(k_0 r) \right) \frac{\partial g_h^r(r)}{\partial r} r dr, \quad (50)$$

$$353 \quad I_2^t(\omega) \equiv \int_{r_0}^{r_1} A_1(\omega) R_1(r) \frac{\partial g_z^z(r)}{\partial r} r dr. \quad (51)$$

354 Then, we also obtain the following relationship:

$$355 \quad \mathbf{v}_h^{tilt}(\omega) = T_{\eta h}^{tilt}(\omega) \eta^v(\omega) \mathbf{e}_r. \quad (52)$$

356 Figure 5b shows that the tilt effects of the horizontal transfer function are domi-
 357 nant, specifically at low frequencies. Below 1 mHz, the transfer function approaches the
 358 theoretical solution for a flat ocean (Ben-Menahem & Singh, 2000), which is propor-
 359 tional to ω^{-1} . With increasing frequency, the contribution of the tilt effect decreases.
 360 Although the amplitudes of horizontal components are an order of magnitude larger
 361 than those of vertical components, the estimated virtual tsunami amplitude from hori-
 362 zontal components is more ambiguous. This is because tilt motions, which are the
 363 spatial derivative of vertical motion, are more sensitive to small-scale bathymetric
 364 changes and crustal heterogeneity.
 365

366 5 Comparison with observations

367 During huge shallow earthquakes, the horizontal components of broadband seis-
 368 mometers located on an island often record tilt motion associated with tsunami (e.g.,
 369 the 2004 Sumatra earthquake (Yuan et al., 2005)), although the contribution of low-
 370 frequency seismic waves excited by the earthquake (Kimura et al., 2013; Yuan et al.,
 371 2005) disturbs the tsunami signal. The amplitudes of vertical components are too

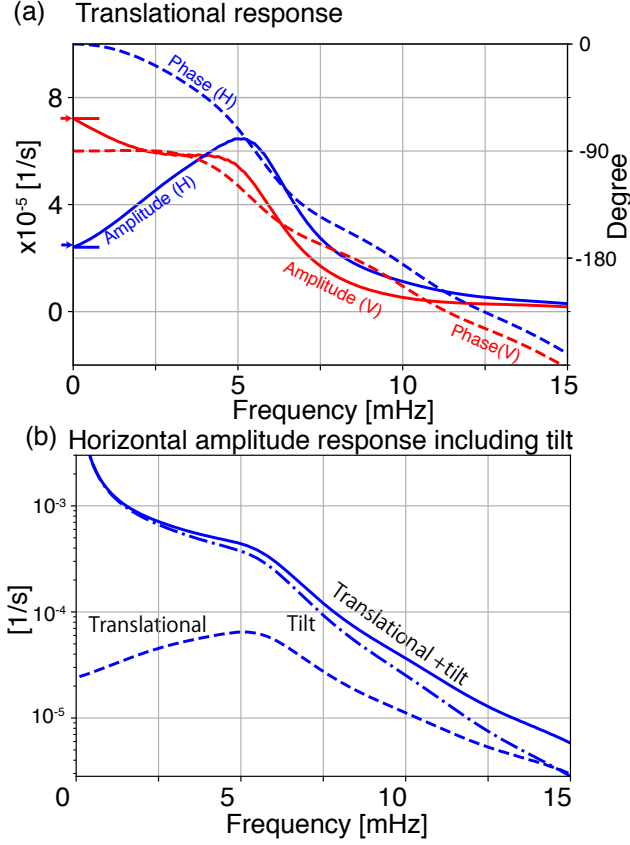


Figure 5. (a) Transfer function of translational motions against frequency. The dashed lines show the phases and the solid lines show the amplitudes, where (V) in the figure represents the vertical component and (H) shows the horizontal component. The red and blue lines show the vertical and horizontal transfer functions, respectively. Red and blue arrows at 0 mHz show the theoretical amplitudes for a flat ocean (Ben-Menahem & Singh, 2000) in vertical and horizontal components respectively. The phase shift can be explained by the arrival delay (approximately 70 s). (b) Amplitude of the transfer function of the horizontal component against frequency according to the contribution of translational motion, tilt motion, and both. The contribution of tilt motion is dominant below 5 mHz. We note that phases of the transfer function due to tilt are analytically the same as those of horizontal transfer function at all frequencies.

372 small to detect because the vertical response is much smaller than the tilt response,
373 as shown in Figure 5.

374 In order to suppress the noise, we apply this method to tsunami earthquakes,
375 which cause a much larger tsunami than expected from the seismic moment. We
376 determine the virtual tsunami amplitude and direction for two tsunami earthquakes:
377 (1) the 2015 volcanic tsunami earthquake near Torishima, Japan, and (2) the 2010
378 Mentawai tsunami earthquake in Indonesia. These results are verified by ray theory
379 and other geophysical observations.

380 5.1 Torishima 2015 Earthquake in Japan

381 A compensated-linear-vector-dipole (CLVD) type earthquake occurred on May
382 2, 2015, near Torishima island, Izu–Bonin arc, Japan (Figure 2), generating an abnor-
383 mally large tsunami (*e.g.* 0.5 m at Hachijozima 180 km north of the epicenter) for
384 the moment magnitude of M_w 5.7, determined by the U.S. Geological Survey. The
385 tsunami was caused by large deformation in a shallow part of a submarine volcanic
386 body (Fukao et al., 2018). A triangular array of ocean bottom pressure (OBP) gauges
387 recorded an off-shore tsunami (Sandambata et al., 2017). They were deployed 100 km
388 northeast of the epicenter with a station separation of approximately 10 km (Figure
389 2). All tsunami waveforms with amplitudes of approximately 2 cm are similar to each
390 other (Figure 6). A tsunami earthquake with a surface wave magnitude of M_s 5.6 in
391 the same area occurred on June 13, 1984 (Kanamori, Ekström, Dziewonski, Barker,
392 & Sipkin, 1993; Satake & Kanamori, 1991); their focal mechanisms suggest magma
393 injection with the submarine volcano (Fukao et al., 2018; Kanamori et al., 1993).

394 At Aogashima island, close to the array, a broadband seismometer (STS2) of
395 F-net (Okada et al., 2004) was deployed by the National Research Institute for Earth
396 Science and Disaster Prevention (NIED). Because seismic waves from tsunami earth-
397 quakes were relatively small at a low-frequency of 1.5–20 mHz, the broadband seis-
398 mometer recorded clear ground motions associated with the tsunami (Figure 1). We
399 can compare the estimated virtual tsunami amplitudes from the seismic observations
400 with near deep ocean bottom pressure gauge.

401 Using the vertical component of the broadband seismometer, we infer the virtual
402 tsunami amplitude. The modeled parameters of the conical island are given in Table
403 (1). Using the transfer function, $T_{\eta z}(\omega)$, shown by Figure 5a, we estimate the virtual
404 tsunami amplitude $\bar{\eta}^v(\omega)$ by deconvolution:

$$405 \quad \bar{\eta}^v(\omega) = \frac{T_{\eta z}^*(\omega)}{T_{\eta z}^*(\omega)T_{\eta z}(\omega) + w} v_z(\omega), \quad (53)$$

406 where w is the water level, which is 5×10^{-3} of the squared amplitude of $T_{\eta z}$ at 5
407 mHz. The $\bar{\eta}^v$ is converted in time domain. Figure 6 shows the comparison of $\bar{\eta}^v(t)$
408 with observed tsunami amplitudes by the pressure gauges against the relative travel
409 time. The estimated amplitude of approximately 2.5 cm and the relative travel times
410 are consistent with the offshore observations. The ray theoretical arrival times should
411 coincide with the peak time, but the figure shows slight delays in the peak time,
412 which are attributed to dispersion due to the finite wavelength. This result verifies the
413 feasibility of this method.

414 Next, let us consider the propagation direction from the observed horizontal
415 components shown in Figure 5b. Using the transfer function, $T_{\eta h}$, for horizontal
416 components, the tsunami amplitude with a propagation direction of $(\bar{\eta}_x^v, \bar{\eta}_y^v)$ can be
417 defined as,

$$418 \quad \begin{pmatrix} \bar{\eta}_x^v(\omega) \\ \bar{\eta}_y^v(\omega) \end{pmatrix} \equiv \frac{T_{\eta h}^*}{T_{\eta h}^*(\omega)T_{\eta h}(\omega) + w} \begin{pmatrix} v_x(\omega) \\ v_y(\omega) \end{pmatrix}, \quad (54)$$

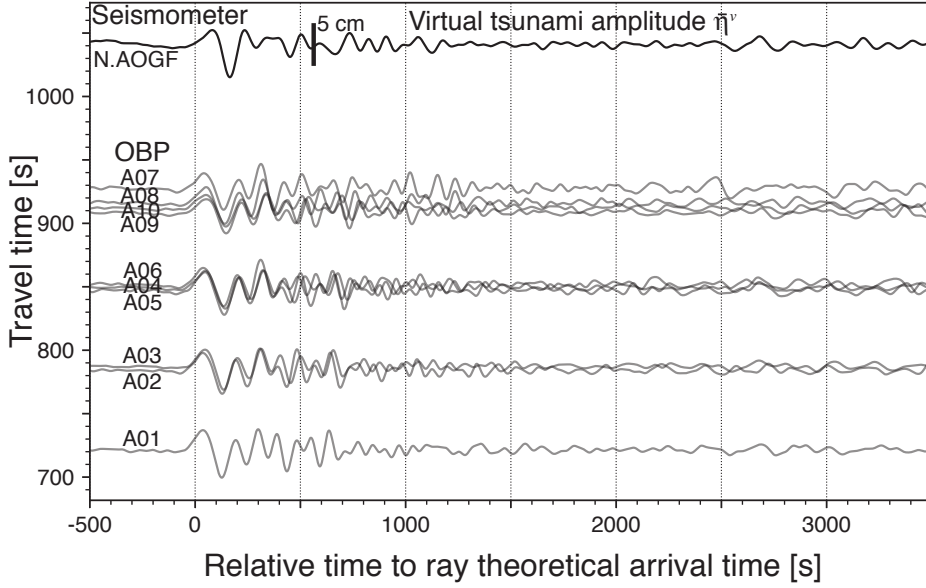


Figure 6. Estimated virtual tsunami amplitude with array observations by absolute pressure gauges. The vertical axis shows travel time predicted by ray theory and the horizontal axis shows relative time to the ray theoretical arrival time. Here, travel times are calculated by fast marching (Rawlinson, 2005; Rawlinson & Sambridge, 2005) using the long wave approximation. The uppermost record shows the virtual tsunami amplitude estimated from the vertical ground velocity at Aogashima (N.AOGF). The lower record shows 10 records of ocean bottom pressure gauges. These records are bandpass filtered from 1.5 to 20 mHz (4th order Butterworth, zero phase). The amplitude scales are the same throughout all records. The maximum amplitudes are approximately 2 cm.

419 where w is the water level, which is 1×10^{-3} the squared amplitude of $T_{\eta h}$ at 5 mHz.
 420 With the single plane wave assumption, $(\bar{\eta}_x^v, \bar{\eta}_y^v)$ can be interpreted as $\bar{\eta}^{in} e_r$ (equation
 421 (46)). Figure 7a shows the comparison among $\bar{\eta}_x^v$, $\bar{\eta}_y^v$, and $\bar{\eta}^v$. The waveforms at
 422 approximately 1000 s are consistent with each other.

423 The particle motions of the horizontal components (Figure 7b) shows a linear
 424 polarization, which is consistent with the ray path shown in Figure 2. The consistency
 425 suggests that the assumptions related to the approximations of the conical island and
 426 the single plane wave are appropriate. Although the horizontal amplitude is slightly
 427 larger than the vertical amplitude, the discrepancy can be attributed to the slightly
 428 off-center station to the southwest. Phases of the later arrival at approximately 3000 s
 429 in Figure 7 are different in different components because they are composed of multiple
 430 scattering waves.

431 To quantitatively estimate the propagation direction, we assume that the virtual
 432 tsunami amplitude is given by $\bar{\eta}^v$ from the vertical component. Then, equation (46)
 433 leads to

$$434 \begin{pmatrix} \bar{\eta}_x^v(\omega) \\ \bar{\eta}_y^v(\omega) \end{pmatrix} = \bar{\eta}^v \begin{pmatrix} \sin \varphi \\ \cos \varphi \end{pmatrix}, \quad (55)$$

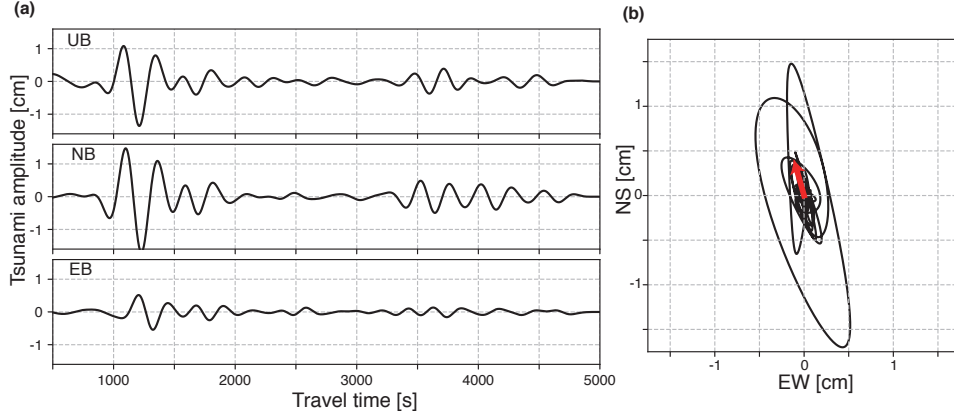


Figure 7. (a) The three components of the estimated tsunami waveform. The first is 2–5 mHz with a 6th order Butterworth filter. (b) Particle motions of the horizontal components from 2 to 5 mHz. The red arrow shows the estimated propagation direction with root mean squared amplitudes from 0 to 500 s.

435 where φ is the propagation azimuth, which, in this case, can be estimated by

$$436 \quad \varphi = \frac{\pi}{2} - \arctan 2 \left(\int_{t_0}^{t_1} \bar{\eta}_y^v(t) \bar{\eta}^v(t) dt, \int_{t_0}^{t_1} \bar{\eta}_x^v(t) \bar{\eta}^v(t) dt \right), \quad (56)$$

437 where $\arctan 2$ is 2-argument arc-tangent, t_0 is 0 s, and t_1 is 5000 s. The red arrow
 438 in Figure 7 shows the propagation direction φ , whose length shows the root mean
 439 squared amplitude from 0 to 5000 s. Because the integration in the above equation,
 440 which represents covariance between the vertical and horizontal components, suppress
 441 incoherent parts, which originate from the higher noise level and scattered wavefield,
 442 the estimation is expected to be robust. Figure 8 shows the comparison between the
 443 estimated azimuth and the ray azimuth at the station. This figure shows that they
 444 are consistent within 10 degrees. We also note that the above method enables us
 445 to estimate the propagation direction without introducing a 180° uncertainty (e.g.
 446 Takagi, Nishida, Maeda, & Obara, 2018).

447 5.2 Mentawai 2010 in Indonesia

448 The 2010 Mentawai earthquake (Mw 7.8) caused a destructive tsunami in the
 449 Mentawai Islands, west of Sumatra in Indonesia (Satake, Nishimura, et al., 2013). The
 450 tsunami amplitude reached 9.3 m on the west coasts of North and South Pagai Island.
 451 Seismological data analyses show that the earthquake was a tsunami earthquake (e.g.
 452 Lay et al., 2011). For the analysis, we use four broadband stations located on islands
 453 DGAR, RER, CRZF, and AIS shown in Figure 9. For the estimation of tsunami
 454 amplitude, we use the water level (see equations (53) and (54)), which is 5% of the
 455 maximum squared amplitude in a frequency range from 0.7 to 2 mHz.

456 Because most island radii (Table 1) are larger than that of Aogashim, as shown in
 457 Figure 10, their transfer functions are not sensitive to tsunami above 1 mHz, as shown
 458 in Figure 11. Hence, we focus on a signal with a typical frequency of 1 mHz. The
 459 estimated virtual tsunami amplitudes were 0.4 cm at DGAR, 1.3 cm at AIS, 0.9 cm at
 460 CRZF, and 0.6 cm at RER. Arrival times of the estimated waveforms are consistent
 461 with the ray theoretical values. The arrival time at DGAR is advanced because the
 462 simple symmetric model is too simple to model a large island with a larger root size
 463 r_1 of approximately 260 km (see Table 1). Although DART station 5601 recorded a

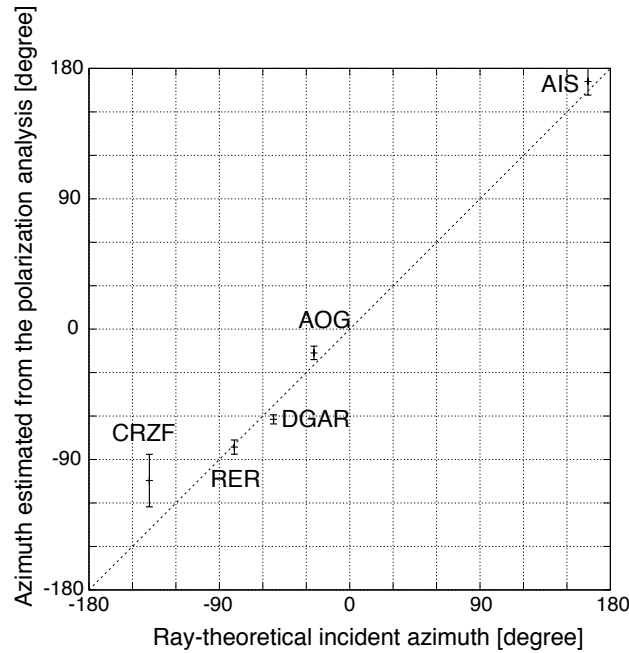


Figure 8. Propagation azimuths at stations. The horizontal axis shows the propagation azimuths estimated by this method utilizing broadband seismic data, whereas the vertical axis shows azimuths based on ray theory. To estimate the error of the propagation azimuth, we made 10^5 bootstrap samples and we estimated the error bars of 1σ by the use of moving block bootstrap resampling (Vogel & Shallcross, 1996). We made 10^5 bootstrap samples with a block length of 50 s at Aogashima and that of 100 s at the other stations respectively.

464 maximum tsunami amplitude of 1 cm (Satake, Nishimura, et al., 2013), it is located
 465 1,600 km south to the epicenter. Because there are no offshore stations close to the four
 466 seismic broadband stations, we compare the virtual tsunami heights $\bar{\eta}^v$ with numerical
 467 results by NOAA Center for Tsunami Research, which are maximum tsunami heights
 468 at an offshore points close to the stations based on the NOAA forecast method using
 469 MOST model with the tsunami source inferred from DART data (Gica, Spillane, Titov,
 470 Chamberlin, & Newman, 2008). The calculated maximum wave heights of about 5 mm
 471 for RER, about 14 mm for AIS, about 14 mm, and about 8 mm for CRZF are consistent
 472 with our estimations.

473 The map in Figure 9 shows the estimated propagation directions using three compo-
 474 nents of broadband seismometers, as shown in the previous subsection. Although
 475 the estimated azimuths are slightly different from the ray paths on this large scale,
 476 the difference can be attributed to strong refraction close to the islands. Indeed,
 477 the relationship between the propagation azimuths estimated from the seismic stations can
 478 be explained by the azimuths predicted by ray theory, as shown in Figure 8. These are
 479 consistent with ray paths within 10 degrees except for CRZF. The deviation could be
 480 explained by scattering due to the neighboring island (Figure 10), which may break
 481 the single plane wave approximation.

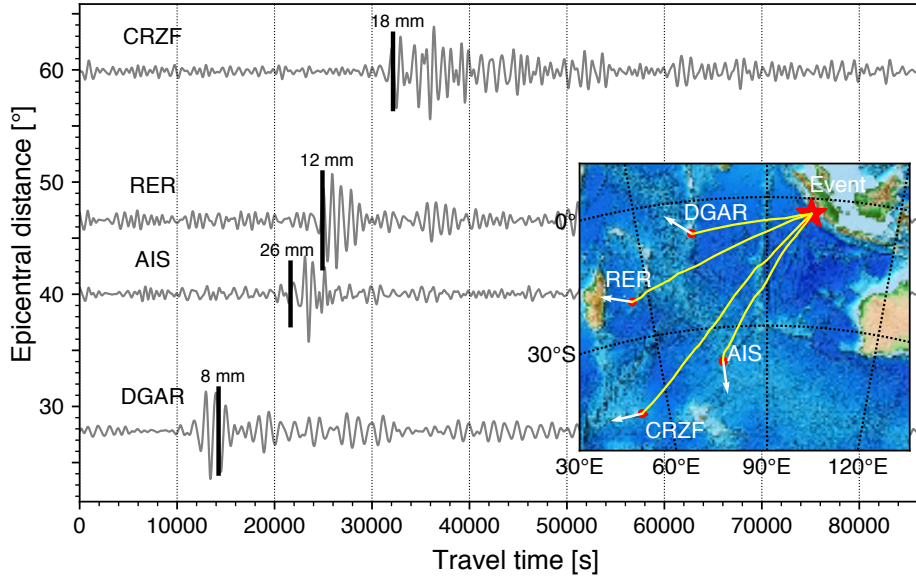


Figure 9. Virtual tsunami amplitudes at four stations for the 2010 Mentawai earthquake (Oct 25, 2010). 0.7–2 mHz (order 6). The map in the inset shows the station locations and the earthquake location. The bold black bars show the corresponding ray theoretical arrival times with amplitude scales.

6 Characteristics of the transfer function according to the slope and radius

Tsunami trapping in the coastal slope of a conical island is crucial for characterizing the transfer functions. This section describes the amplification characteristics due to trapping in coastal areas, where the trapping condition (Longuet-Higgins, 1967) is given by,

$$\frac{\partial}{\partial r} \left(\frac{D(r)}{r^2} \right) \geq 0. \quad (57)$$

For the case of a conical island, the condition can be simplified as

$$r \leq 2r_0. \quad (58)$$

This relationship indicates that a larger conical island will trap more inshore areas.

β defined in equation (15) is crucial for characterizing the trapping effect. β can be interpreted as the ratio of the circumference, $4\pi r_0$ at $r = 2r_0$, to the wavelength, λ . In other words, β shows the azimuthal number of the trapped mode. Here, we define the cut-off frequency f_β as $\beta = 1$. Above this frequency, the tsunami is trapped in inshore areas. f_β is also a good proxy for ground deformation at the center because the deformation becomes significant when the radius of the island becomes larger than the wavelength. Consequently, the ground deformation becomes small with increasing frequency above the frequency. The f_β value, therefore, characterizes the cut-off frequency of the transfer functions. Table 1 shows f_β for the islands, which correspond to the cut-off frequency shown in Figure 11.

With a smaller slope m , more tsunami energy is trapped in the inshore area due to the slow propagation speed. In this case, the transfer function exhibits a peak

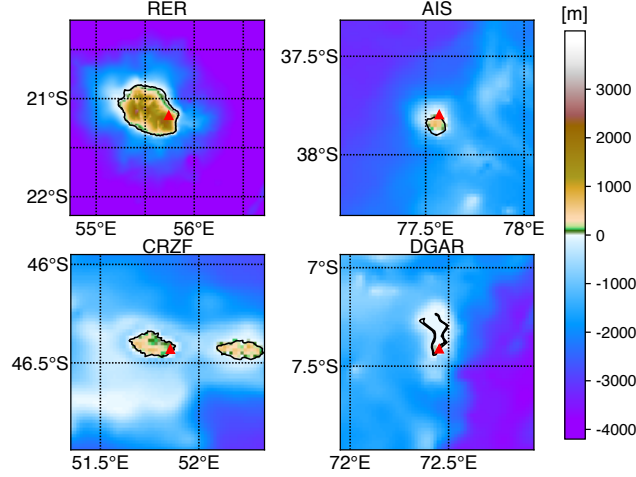


Figure 10. Enlarged maps of the islands. Stations are indicated by red triangles.

504 at approximately f_β . The translational transfer functions of DGAR and CRZF with
 505 smaller slope, m , show peaks at approximately f_β .

506 At much lower frequencies than f_β , we can neglect scattering by the island
 507 because the wavelength of the tsunami becomes much larger than the island scale.
 508 Moreover, the contribution of ground deformation in the inshore area becomes negli-
 509 gible. In this limit, the transfer functions are approximated by those of a semi-infinite
 510 medium loaded by pressure fluctuations on the surface given by [Ben-Menahem and](#)
 511 [Singh \(2000\)](#):

$$512 \quad \lim_{\omega \rightarrow 0} T_{\eta z}(\omega) = \frac{e^{-i\pi/2} \sqrt{g_0 D_0}}{2(\lambda + \mu)} \frac{\lambda + 2\mu}{\mu} \rho g_0, \quad (59)$$

$$513 \quad \lim_{\omega \rightarrow 0} T_{\eta h}(\omega) = \frac{\sqrt{g_0 D_0}}{2(\lambda + \mu)} \rho g_0, \quad (60)$$

$$514 \quad \lim_{\omega \rightarrow 0} T_{\eta h}^{tilt}(\omega) = \frac{\lambda + 2\mu}{2(\lambda + \mu)\mu} \rho \frac{g_0^2}{\omega}. \quad (61)$$

516 Figure 5a and Figure 11 show that the transfer functions approaching zero frequency
 517 also approach the above values. Figure 11 (d) also shows that $T_{\eta h}^{tilt}(\omega)$ actually ap-
 518 proaches equation (61) in the low frequency limit.

519 At frequencies higher than about $10f_\beta$, the wavelength of tsunami becomes much
 520 smaller than the island scale. Consequently, the scattering by small scale bathymetric
 521 changes breaks the basic assumption of this method. Thus, f_β could be a proxy for
 522 the characteristics when evaluating the transfer function.

523 7 Potential applications for ocean infragravity waves

524 Although tsunami in this frequency range is ocean infragravity waves excited
 525 by an earthquake, ocean infragravity waves are also excited by the other geophys-
 526 ical processes. For example, they are excited persistently along shorelines by incident
 527 ocean swell through nonlinear processes and travel across the ocean with a typical
 528 height on the order of 1 cm in pelagic regions ([Rawat et al., 2014](#); [Tonegawa et al.,](#)
 529 [2018](#)). The background ocean infragravity-wave activities are also key for understand-
 530 ing background seismic wavefields know as seismic hum because they are the primary

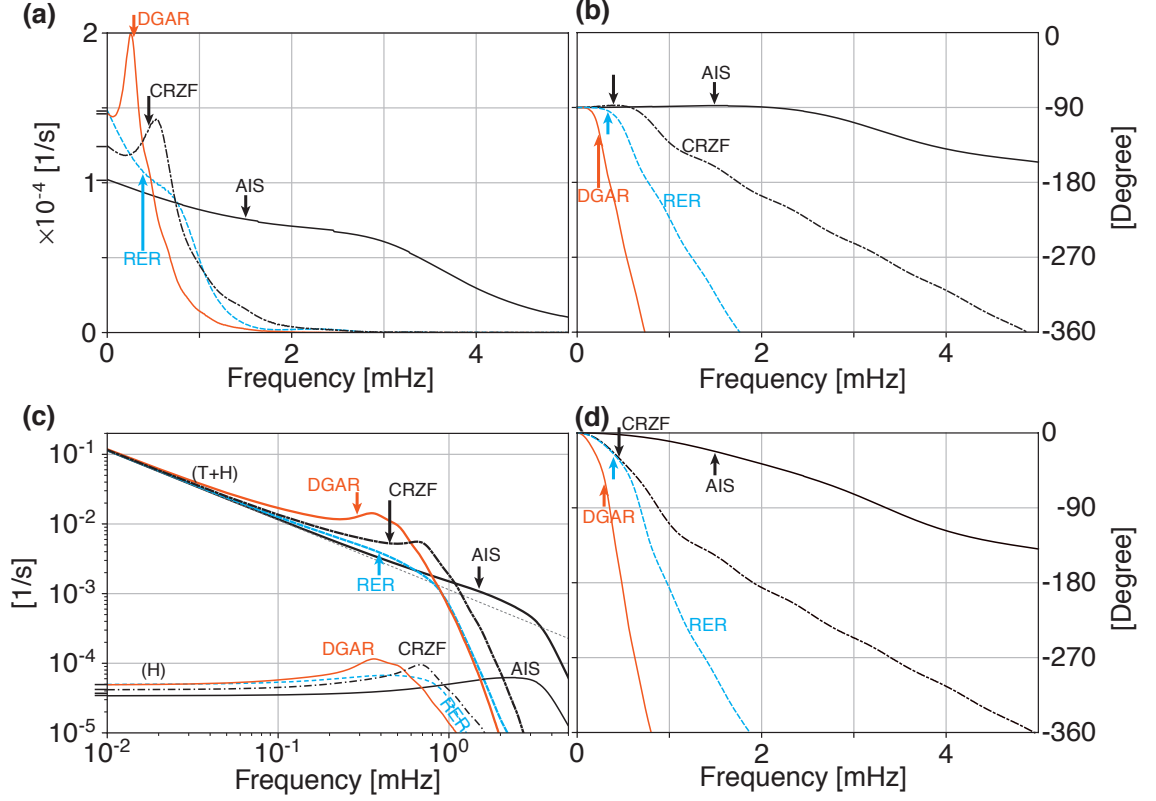


Figure 11. (a) Amplitudes of transfer functions for vertical components against frequency at the four broadband stations, composed of one IRIS IDA station, DGAR (Diego Garcia, Chagos islands), and three GEOSCOPE stations RER (La Réunion Island, France), CRZF (Port Alfred - Ile de la Possession - Crozet Islands, France), and AIS (Nouvel Amsterdam, TAAF, France). Station locations are shown in Figure 9. Black tick marks at 0 mHz show theoretical amplitudes for a flat ocean (equation (59)) in vertical components. The f_β values are shown by arrows. (b) Phases of the transfer functions for vertical components against frequency. (c) Amplitudes of transfer functions for horizontal components against frequency. Labels (H) shows the horizontal components due to translational motion, and (H+T) shows the horizontal component including the tilt effect. Black tick marks at 0 mHz show the theoretical amplitudes for a flat ocean (equation (60)) in horizontal components, and the straight dot-line in gray shows the theoretical amplitudes caused by the tilt motion for a flat ocean (equation (61)). (d) Phases of the transfer functions for horizontal components against frequency.

531 excitation source (Ardhuin, Gualtieri, & Stutzmann, 2015; Nishida, 2013, 2017; Rhie
 532 & Romanowicz, 2004). Observed equipartition of energy between Love and Rayleigh
 533 waves (Fukao, Nishida, & Kobayashi, 2010; Nishida, Kawakatsu, Fukao, & Obara,
 534 2008) suggests a topographic coupling between ocean infragravity waves and seismic
 535 surface waves. Seismic observations at island broadband stations could be used to
 536 understand the excitation mechanisms because modeling of ocean infragravity waves
 537 requires further researches (Ardhuin et al., 2015; Ardhuin, Rawat, & Aucan, 2014).

538 Our proposed technique for estimating virtual tsunami amplitude is applicable
 539 not only for tsunami but also for random wavefields of the background ocean infra-
 540 gravity waves. Seismic observations at islands could elucidate ocean infragravity wave
 541 activities. The wave action model WAVEWATCH III has recently been extended from
 542 the swell band to ocean infragravity waves (Ardhuin et al., 2014) and recovers the
 543 observed energy of wave height within 50%. Our method could be used to improve
 544 such models.

545 8 Conclusions

546 In this study, we consider that an arbitrary tsunami in a flat ocean floor enters
 547 a conical island. The scattering wavefield is evaluated using a semi-analytical
 548 method, which is an extension of the theory of Fujima and Goto (1994). Then, we
 549 calculate ground deformation due to tsunami loading at the center of the conical is-
 550 land using static Green's functions with a first-order correction for bathymetry. In
 551 this formulation, the ground motions can be represented by convolution between the
 552 transfer functions and the incident tsunami amplitudes at the station. The transfer
 553 functions are characterized by a cutoff frequency, f_β , and they approach those given
 554 by Ben-Menahem and Singh (2000) for a semi-infinite medium loaded by pressure on
 555 the surface without an island. By deconvolving the transfer functions from seismic
 556 data, we can infer the incident tsunami wavefield, which can be interpreted as the
 557 virtual tsunami amplitude without the island. Thus, we propose a new technique for
 558 estimating the virtual tsunami amplitude and propagation direction from seismic data
 559 using the assumption of a single plane wave.

560 First, we apply this technique to seismic records from Aogashima volcanic island
 561 when the Torishima Oki earthquake hit on May 2, 2015. The estimated tsunami
 562 amplitude is quantitatively consistent with an array observation of pressure gauges
 563 close to the island from 1.5 to 20 mHz. The incident angle estimated from the seismic
 564 data is also consistent with the ray-theoretical value. We also apply this method
 565 to seismic data at four broadband stations located on islands in the Indian ocean
 566 for the tsunami earthquake in Mentawai, Indonesia on October 25, 2010. Although
 567 the observed frequency range is limited from 0.5 to 2.0 mHz, the incident angles
 568 are consistent with ray theoretical values. This method can, therefore, complement
 569 offshore tsunami observations.

570 Because this technique is formulated for an arbitrary incident wavefield, it could
 571 be employed not only for tsunami but also for background ocean infragravity waves,
 572 which are excited along shorelines by incident ocean swell through nonlinear processes.
 573 Further research should develop this method in order to elucidate background ocean
 574 infragravity wave activities using broadband seismic stations located on islands.

A Correction of ground deformation for tilt

Following Segall (2010), we estimate the first order correction of displacements $u_i^{(1)}$ ($i = x, y, z$) for the bathymetry as induced displacement by the first order stress $\sigma_{ij}^{(1)}$ in a cylindrical coordinate (r, θ, z) , given by

$$\sigma_{zz}^{(1)} = 0, \quad (\text{A.1})$$

$$\sigma_{rz}^{(1)} = -\frac{dh}{dr}(\sigma_{zz}^{(0)} - \sigma_{rr}^{(0)}), \quad (\text{A.2})$$

$$\sigma_{\theta z}^{(1)} = -\frac{dh}{dr}\sigma_{r\theta}^{(0)} \quad (\text{A.3})$$

at $z = 0$. Here, the 0th-order terms in Cartesian coordinates satisfy

$$\frac{\partial \sigma_{ij}^{(0)}}{\partial x_j} = 0 \quad (\text{A.4})$$

with boundary conditions given by

$$\sigma_{zz}^{(0)} = -p(x, y), \sigma_{zx}^{(0)} = 0, \sigma_{zy}^{(0)} = 0. \quad (\text{A.5})$$

We note the following relationships:

$$\left. \frac{\partial \sigma_{rz}^{(0)}}{\partial z} \right|_{z=0} = \left. \frac{\partial \sigma_{\theta z}^{(0)}}{\partial z} \right|_{z=0} = \left. \frac{\partial \sigma_{zz}^{(0)}}{\partial z} \right|_{z=0} = 0, \quad (\text{A.6})$$

on the free surface of the island. This result is obtained by representing the stress in terms of the Newtonian potential functions (Love, 1929, section 1.1).

The first order displacement can be calculated by convolution between the Green's function in a semi-infinite medium and $\sigma_{ij}^{(1)}$ on the surface. The corresponding components ($\sigma_{rz}^{(1)}$ and $\sigma_{r\theta}^{(1)}$) can be calculated by convolution between $-p$ and static Green's functions of surface traction for normal traction in a semi-infinite space (Jaeger et al., 2007; Segall, 2010). The Green's functions $g_{xx}^{\sigma z}, g_{xy}^{\sigma z}, g_{yy}^{\sigma z}$ in a Cartesian coordinate system are given by

$$g_{xx}^{\sigma z} = \frac{1}{2\pi} \frac{\mu}{\lambda + \mu} \frac{-x^2 + y^2}{r^4} + \frac{1 + 2\nu}{2} \delta(r), \quad (\text{A.7})$$

$$g_{xy}^{\sigma z} = -\frac{1}{2\pi} \frac{\mu}{\lambda + \mu} \frac{2xy}{r^4}, \quad (\text{A.8})$$

$$g_{yy}^{\sigma z} = \frac{1}{2\pi} \frac{\mu}{\lambda + \mu} \frac{x^2 - y^2}{r^4} + \frac{1 + 2\nu}{2} \delta(r). \quad (\text{A.9})$$

Note that Jaeger et al. (2007) does not include two terms of $\delta(r)$ because they are defined outside the source regions. The two terms can be estimated as the limit of a disk load given by Farrell (1972) as r approaches 0, as shown in the next section. For the convolution between $g_{ij}^{\sigma z}$ and $\sigma_{ij}^{(0)}$, calculation in the wavenumber domain is convenient (Segall, 2010). $G_{ij}^{\sigma z}$, which is the Fourier component of $g_{ij}^{\sigma z}$ in the wavenumber domain, is given by

$$G_{xx}^{\sigma z} = \frac{1}{2} \frac{\mu}{\lambda + \mu} \frac{-k_x^2 + k_y^2}{k_x^2 + k_y^2} + \frac{1 + 2\nu}{2} \quad (\text{A.10})$$

$$G_{xy}^{\sigma z} = \frac{1}{2} \frac{\mu}{\lambda + \mu} \frac{-2k_x k_y}{k_x^2 + k_y^2} \quad (\text{A.11})$$

$$G_{yy}^{\sigma z} = \frac{1}{2} \frac{\mu}{\lambda + \mu} \frac{k_x^2 - k_y^2}{k_x^2 + k_y^2} + \frac{1 + 2\nu}{2} \quad (\text{A.12})$$

611 Figure A.1 shows a typical example of induced 0th-order stress $\sigma_{zz}^{(0)} - \sigma_{rr}^{(0)}$ and
 612 $\sigma_{r\theta}^{(0)}$, which is stress induced by the tsunami wavefield with an azimuthal order of 1
 613 ($\zeta_1^{in} = 1$) for Aogashima at 4 mHz. Because $\sigma_{zz}^{(0)} - \sigma_{rr}^{(0)}$ and $\sigma_{r\theta}^{(0)}$ are an order of
 614 magnitude smaller than $\sigma_{zz}^{(0)}$ at the surface, we can neglect the first order stress $\sigma_{ij}^{(1)}$.
 615 Consequently, the first order displacement $u^{(1)}$ is also negligible. Although the first
 616 order correction of normal traction $\sigma_{zz}^{(1)}$ is negligible, those of shear traction, $\sigma_{zx}^{(1)}$ and
 617 $\sigma_{zy}^{(1)}$, are significant.

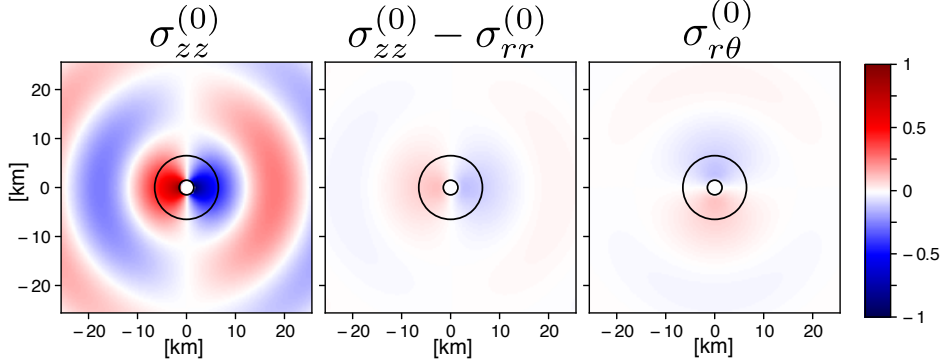


Figure A.1. Stress σ_{zz} is imposed on the surface. σ_{rr} is the induced principle stress on the surface, which is one order of magnitude smaller than the imposed stress. The inner circle shows the radius of the island at sea level, r_0 , and the outer circle shows the radius of the island on the seafloor r_1 .

618 B Stress components by surface loads on a half-space

619 Stress components by surface loads on a half-space are given Jaeger et al. (2007)
 620 as

$$621 \quad \sigma_{xx} = \frac{1}{2\pi} \left[\frac{3x^2z}{r^5} + \frac{(1-2\nu)(y^2+z^2)}{r^3(z+r)} - \frac{(1-2\nu)z}{r^3} - \frac{(1-2\nu)x^2}{r^2(z+r)^2} \right] \quad (\text{B.1})$$

$$622 \quad \sigma_{xy} = \frac{1}{2\pi} \left[\frac{3xyz}{r^5} - \frac{(1-2\nu)xy(z+2r)}{r^3(z+r)^2} \right] \quad (\text{B.2})$$

$$623 \quad \sigma_{yy} = \frac{1}{2\pi} \left[\frac{3y^2z}{r^5} + \frac{(1-2\nu)(x^2+z^2)}{r^3(z+r)} - \frac{(1-2\nu)z}{r^3} - \frac{(1-2\nu)y^2}{r^2(z+r)^2} \right]. \quad (\text{B.3})$$

625 Because the surface values are singular, we derive the simplified form on the surface
 626 below.

627 Let us consider that stress components by a disk load (Love, 1929; Lubarda,
 628 2013) are given by

$$629 \quad \sigma_{rr} = \frac{p}{2} \begin{cases} 1 + 2\nu, & r < R \\ -(1-2\nu)\frac{R^2}{r^2}, & r \geq R \end{cases} \quad (\text{B.4})$$

$$630 \quad \sigma_{\theta\theta} = \frac{p}{2} \begin{cases} 1 + 2\nu, & r < R \\ (1-2\nu)\frac{R^2}{r^2}, & r \geq R \end{cases} \quad (\text{B.5})$$

631

632 where R is the radius of the disk and p is the pressure applied uniformly over the disk
633 area. The limits of stress as R approaches 0 have the following forms:

$$634 \quad \sigma_{xx} = \frac{1}{2\pi} \frac{\mu}{\lambda + \mu} \frac{-x^2 + y^2}{r^4} + \frac{1 + 2\nu}{2} \delta(r) \quad (\text{B.6})$$

$$635 \quad \sigma_{xy} = -\frac{1}{2\pi} \frac{\mu}{\lambda + \mu} \frac{2xy}{r^4} \quad (\text{B.7})$$

$$636 \quad \sigma_{yy} = \frac{1}{2\pi} \frac{\mu}{\lambda + \mu} \frac{x^2 - y^2}{r^4} + \frac{1 + 2\nu}{2} \delta(r). \quad (\text{B.8})$$

637
638 These representations are also given by the limit of equation B.1 as z approaches 0.

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