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4 **Vehicle-Based Methane Detection, Attribution, and Quantification in the Upstream Oil and**
5 **Gas Sector: Method Overview and Controlled Release Validation**

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19 Quantification in the Upstream Oil and Gas Sector:
20 Method Overview and Controlled Release
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35 1. Abstract

36 Vehicle-based measurement systems occupy an important niche in the multi-scale methane
37 measurement landscape between component-level technologies (e.g. OGI) and aerial-based
38 methods. Performance evaluations are often limited to one dimension (e.g. quantification), while
39 methodological opacity limits interpretation and inter-comparisons between technologies. Here,
40 we develop a vehicle-based measurement system and processing framework incorporating a novel
41 weighted likelihood algorithm for automated source attribution. Using controlled release
42 experiments at two dedicated testing facilities, we characterize system performance across three
43 dimensions – detection, attribution, and quantification. The system achieved a 96.1 % true positive
44 detection rate with no false positives and a 90% detection limit as low as 0.024 kg/h with repeat
45 transects. Attribution accuracy was high at the source-group level, reaching 99.7 % in single-
46 source releases and 86 % in multi-source scenarios. Quantification was unbiased for low-to-
47 moderate complexity releases (2 source groups; slope=0.99, $R^2=0.81$) but overestimated under
48 highly complex conditions (5 source groups; slope=1.45, $R^2=0.91$). These results provide a
49 transparent performance benchmark, demonstrating that these systems are well-suited to survey
50 the large populations of low-to-moderate complexity sites (e.g. single wells and batteries), as a
51 screening layer in LDAR applications and to quantify the low-end of emission distributions in
52 inventories, reducing reliance on generic emission factors.

53 2. Introduction

54 Methane (CH₄), the primary component of natural gas, is a potent greenhouse gas with a 100-
55 year global warming potential 27-30 times that of CO₂ ¹. The oil and gas (O&G) sector accounts
56 for an estimated 44% of anthropogenic CH₄ emissions in Canada and 20% globally ^{2,3} and has
57 been identified as a key sector for CH₄ emission reduction ⁴. Jurisdictions including Canada, the
58 United States (US), and the European Union have implemented regulations targeting CH₄
59 emissions from this sector ⁵⁻⁸. These regulations mandate leak detection and repair (LDAR)
60 programs under which regular site-level emission screening is conducted to identify and repair
61 fugitive emission sources.

62 The growing interest in characterizing and reducing CH₄ emissions has driven the rapid
63 development of CH₄ measurement technologies for two primary applications: targeted monitoring
64 and mitigation (e.g. LDAR) and emission inventory development. Emerging regulatory programs
65 have accelerated this trend by providing pathways for the use of alternative CH₄ measurement
66 technologies beyond traditional optical gas imaging (OGI) surveys in LDAR programs ^{5,9}. These
67 technologies include remote sensing methods (satellite, aerial, and drone) and ground-based
68 approaches (vehicle-mounted, handheld, and stationary monitors). Fundamental trade-offs exist
69 among these technologies in terms of spatial and temporal coverage, attribution granularity, cost,
70 ease of deployment, detection sensitivity, and quantification accuracy. However, because of their
71 different advantages and capabilities, there is a growing consensus that multi-scale measurements
72 are essential for characterizing the overall CH₄ emission landscape ¹⁰⁻¹².

73 Vehicle-based measurement systems occupy an important niche in this multi-scale measurement
74 framework. Typically consisting of a vehicle equipped with a CH₄ analyzer, GPS, and
75 meteorological sensors, these systems offer spatial coverage and detection sensitivity that fall

76 between component-level OGI surveys and larger-scale aerial measurements ^{13–15}. Here, we focus
77 on fully mobile approaches that detect and quantify emissions during downwind transects, rather
78 than methods that rely on extended measurements at fixed downwind locations (e.g., OTM-33A).
79 Such vehicle-based systems have been used extensively to characterize CH₄ emissions from oil
80 and gas production sites ^{16–20}, urban environments and natural gas distribution networks ^{21–24},
81 biogas facilities ²⁵, and landfills ²⁶. In upstream O&G applications, emission rates are most
82 commonly estimated using atmospheric concentration measurements coupled with atmospheric
83 dispersion modelling in an inversion framework, although Lidar and tracer-based techniques have
84 also been used ²⁷.

85 To date, research on vehicle-based systems has largely focused on emission quantification, with
86 comparatively less attention given to detection sensitivity and source localization. Localization
87 approaches have varied widely across studies, including manual attribution ^{16,17,20}, automated
88 nearest-upwind-source algorithms whose reliability has not yet been evaluated ^{18,19}, triangulation
89 across multiple site visits under varying wind conditions ²¹, and optimization-based methods that,
90 despite evaluating potential source locations within a defined boundary, exhibited localization
91 errors of ~30–40 m within a 40–50 m domain ^{28,29}. Peer-reviewed controlled release evaluations
92 of both localization and detection performance for vehicle-based solutions remain scarce.
93 Ravikumar et al. ¹⁴ reported promising results for several systems, while Ilonze et al. ³⁰ observed
94 poor localization and were unable to establish a 90% probability of detection threshold for the
95 single vehicle-based system tested. Field-based estimates suggest detection limits below 0.5 kg/h
96 based on theoretical minimum detectable CH₄ enhancements and dispersion modeling ^{16,19}, while
97 controlled release experiments report limits ranging from 0.096 to > 10 kg/h ¹⁴. This variability is
98 difficult to interpret because it reflects differences in instrumentation, methodology, and operating

99 conditions, while many approaches rely on proprietary methods that are not fully disclosed. As a
100 result, reproducibility is limited and inter-study comparability is constrained, ultimately presenting
101 a barrier to the adoption of this technology in LDAR and inventory development applications.

102 In this study, we aim to improve the understanding of the role that vehicle-based measurement
103 systems can play within a multi-scale measurement framework through a detailed methods
104 description and comprehensive analysis of system performance. We develop a vehicle-based
105 measurement system and processing framework for automated CH₄ detection, source attribution,
106 and quantification in the upstream O&G sector. Using data collected from controlled-release
107 experiments at two dedicated testing facilities that simulate realistic single- and multi-source
108 upstream O&G emission scenarios, we present the first comprehensive and transparent
109 performance characterization of a vehicle-based measurement system across three dimensions—
110 detection, attribution, and quantification—and compare its capabilities with those of other
111 commonly used CH₄ measurement technologies. In doing so, we aim to establish a performance
112 benchmark that informs the broader scientific and regulatory communities about the capabilities,
113 limitations, and potential role of vehicle-based systems in LDAR programs and CH₄ inventory
114 development.

115 **3. Materials and Methods**

116 **3.1. Vehicle-based Measurement System**



117

118 **Figure 1.** Rooftop-mounted vehicle-based measurement system.

119 We collected measurements using a compact and portable vehicle-mounted system (Figure 1).
120 Mounted to any vehicle using standard roof racks, the system consists of a tunable diode laser
121 spectrometer (TDLAS; Axetris LGD Compact-A CH₄) with a precision (1σ) of ~ 0.2 ppm, a GPS
122 (GlobalSat), and a 2-D ultra-sonic anemometer (Gill WindUltra). Ambient air is drawn from above
123 the vehicle into an enclosure containing the TDLAS sensor by an air pump operating at a flow rate
124 of 0.6 LPM, where CH₄ concentrations are measured. Measurements of CH₄ concentration, wind
125 speed, wind direction, and vehicle location (latitude and longitude) are recorded at 2 Hz using a
126 micro controller (ESP32). An internal modem enables wireless data transmission and real-time

127 data viewing on any browser-enabled device. The system is powered by a 12 V lithium battery,
128 providing up to 8 hours of continuous operation, and has a total weight of <10 kg (22 pounds).
129 Inlet height depends on the height of the vehicle upon which it is mounted- in this study, it was
130 approximately 3 m. These measurements form the inputs to the processing framework described
131 below.

132 **3.2. Processing Framework**

133 Our framework for processing vehicle-based CH₄ measurements operates on time series of
134 atmospheric CH₄ concentration, wind speed, wind direction, and vehicle location (latitude and
135 longitude) along the vehicle path, along with measurement height and the locations and heights of
136 potential sources. It consists of four sequential steps: data preprocessing, CH₄ peak detection,
137 source attribution, and quantification, each described in detail below.

138 **3.2.1. Preprocessing**

139 First, the raw measurement time series are cleaned, formatted, and prepared for subsequent
140 analysis. This includes synchronizing measurements across instruments with different sampling
141 frequencies onto a common timeline, interpolating missing values, and correcting raw measured
142 wind speed and direction for vehicle motion. The CH₄ time series is shifted backward in time to
143 account for sensor response time and transit time in tubing between the inlet and the gas analyzer.

144 Hourly observations of cloud cover, cloud ceiling height, and 10 m wind speed from the nearest
145 airport are used to estimate discrete atmospheric stability classes³¹. In this approach, stability class
146 is determined from wind speed and estimates of a net radiation index. This index depends on cloud
147 cover, ceiling height, and insolation, which is estimated from solar altitude (a function of date,
148 time, and location).

149 **3.2.2. Peak detection**

150 We analyze the CH₄ time series to identify elevated CH₄ values (“peaks”). First, we calculate a
151 dynamic CH₄ baseline as an estimate of atmospheric background CH₄ concentrations using an
152 iterative mean suppression method inspired by Liland³² assuming that there are only CH₄ sources
153 and no sinks, such that the lowest measured concentrations reflect background levels. We prepare
154 the CH₄ signal by trimming leading and trailing NA values, thresholding the data to reduce the
155 influence of large amplitude CH₄ peaks, mirroring the signal at both ends to avoid edge effects,
156 and smoothing the resulting series. We then subsample the CH₄ data by taking the minimum value
157 within fixed intervals to simplify the shape of the smoothed signal and increase speed.

158 We estimate the baseline iteratively on the prepared CH₄ time series by moving a window of
159 exponentially decreasing sizes along the signal, calculating the mean value in each window and
160 replacing values that exceed the mean with the mean. Each window is applied first to the right
161 (time increasing direction) and then to the left to prevent directional bias.

162 We subtract the CH₄ baseline time series from the measured CH₄ time series to produce a time
163 series of excess CH₄ (eCH₄), which is then used for peak detection. Peaks in the eCH₄ time series
164 are identified using a spike detection algorithm described by Daniels et al.³³, which iterates
165 through each observation and evaluates conditions that define the start, end, and validity of CH₄
166 peaks. The algorithm requires three input parameters which can be adjusted depending on the
167 application and the sensitivity of the gas analyzer. Input parameter selection is discussed in more
168 detail in Section S1 of the supplementary information (SI), and values used in this analysis are
169 presented in Table S1. To minimize directional bias, we apply the algorithm in both the forward
170 (time-increasing) and backward (time-decreasing) directions. We merge peaks detected during

171 both passes and assign sequential ID numbers from left to right. An example of the baseline
 172 calculation and spike detection algorithm outputs is shown in Figure S1.

173 3.2.3. Source attribution

174 Once the peaks in the eCH₄ time series have been identified, we attribute each peak to a known
 175 potential source location using a weighted likelihood algorithm that considers measured wind
 176 characteristics and the relative locations of the peak and source. We define the peak location as the
 177 latitude and longitude coordinates at which the maximum eCH₄ value of a peak was recorded. We
 178 define a metric called the total attribution weight (w_t) that characterizes the probability of a source
 179 to be the origin of the plume. For a given CH₄ peak, w_t (Eq. 1) is calculated as the product of a
 180 distance weight w_d and azimuth weight w_a for each source within a search radius d_{max} of the peak
 181 location.

$$182 \quad w_t = w_d \times w_a \quad (1)$$

183 The distance weight depends on the distance from the source to the location of the measured
 184 peak. The x-axis is defined by the mean measured wind direction over a two-minute period. w_d
 185 decreases exponentially from 1 at an upwind distance (x) of 0 m to a minimum weight value w_{min}
 186 at a maximum distance d_{max} according to Eq. 2:

$$187 \quad w_d = e^{\log\left(\frac{w_{min}}{d_{max}}\right)(x^2+y^2)^{0.5}} \quad x \geq 0 \quad (2)$$

188 where y is the crosswind distance.

189 To consider the uncertainty of peak location, we also define an exponentially decreasing weight
 190 for negative upwind distances (i.e. downwind distances) to a much smaller downwind distance
 191 d_{back} , (Eq. 3).

$$192 \quad w_d = e^{\log\left(\frac{w_{min}}{d_{max}}\right)\left(\left(x\frac{d_{max}}{d_{back}}\right)^2+y^2\right)^{0.5}} \quad x < 0 \quad (3)$$

193 The azimuth weight (Eq. 4) depends on the azimuth of the source with the wind direction relative
194 to the peak location and is represented by a scaled Gaussian function that covers a triangular area.

$$195 \quad w_a = \frac{-y^2}{e^{2((x+d_{back})\sin(\sigma))^2}} \quad x > -d_{back} \quad (4)$$

196 where σ , the standard deviation of the Gaussian function, is taken to be the standard deviation
197 of the measured wind direction over a two-minute period. Figure S2 shows the distance, azimuth
198 and total weights as a function of upwind and crosswind distance. Intuitively, the highest weights
199 are assigned to sources that are directly upwind and close to the peak location.

200 **3.2.4. Source Grouping**

201 This vehicle-based method relies on downwind transect-based measurements of emitting
202 sources. When individual equipment is co-located on a site, attribution of measured emissions at
203 the source (equipment) level introduces additional uncertainty. In this framework, we group
204 adjacent equipment into source groups. Depending on the use case, grouping can be done manually
205 through visual inspection of source locations or automatically using hierarchical cluster analysis.
206 The appropriate grouping radius depends on measurement distance: for on-pad measurements like
207 those performed in this study, we group sources within a 10 m radius, while for more distant off-
208 pad measurements, grouping distances of 45 m or more may be appropriate. Attribution weights
209 are calculated for each individual source and each eCH₄ peak is attributed to the group containing
210 the source with the highest individual attribution weight.

211 **3.2.5. Quantification**

212 An emission rate is estimated for each attributed CH₄ peak through comparison of measured
213 eCH₄ values to those modelled with a Gaussian Plume Dispersion Model. This model is frequently
214 employed to describe time-averaged atmospheric dispersion of non-reactive pollutants and

215 assumes the dispersion of these pollutants follows a normal distribution in the vertical (z) and
 216 crosswind (y) directions. It assumes steady-state, uniform wind conditions and treats the source as
 217 a continuous point emitter. The equation can be obtained as the stationary solution to the
 218 atmospheric diffusion equation³⁴. For CH₄, total reflection of the plume off the ground is assumed,
 219 resulting in the following equation (Eq. 5) for modelled eCH₄ concentration at a point (x,y,z),
 220 where x is the along-wind distance from the source, y is the crosswind distance, and z is the height
 221 above ground, for an emitting source at height h:

$$222 \quad eCH_{4,model}(x, y, z) = \frac{Q}{2\pi\sigma_y(x)\sigma_z(x)u} e^{\frac{-y^2}{2\sigma_y^2}} \left[e^{\frac{-(z-h)^2}{2\sigma_z^2(x)}} + e^{\frac{-(z+h)^2}{2\sigma_z^2(x)}} \right] \quad (5)$$

223 where Q is the emission rate of the source at point (0,0,h), u is the mean horizontal wind speed,
 224 and $\sigma_y(x)$ and $\sigma_z(x)$ are the horizontal and vertical dispersion coefficients, respectively, which
 225 depend on atmospheric stability and the downwind distance from the source. We calculate these
 226 dispersion coefficients according to parameterizations for rural environments³⁵. For each
 227 attributed CH₄ peak, we determine wind direction using the geographic coordinates of the source
 228 and the peak, assuming the peak maximum occurs on the plume centerline directly downwind of
 229 the source. This is consistent with prior studies which have demonstrated that this assumption
 230 produces more accurate emission rate estimates than using measured wind directly^{17,25,28,36},
 231 however it is a conservative assumption that could result in underestimation of emission rates if
 232 the true plume centerline was not transected. Following the same studies, modeled eCH₄
 233 concentrations are calculated with Eq. 5 for each point in the measured CH₄ peak using a reference
 234 emission rate (Q_{ref}) of 1 g/s. The modeled and measured eCH₄ values are integrated (or summed)
 235 over the crosswind distance y, and the emission rate is estimated using Eq. 6.

$$236 \quad Q_{est} = \frac{\sum eCH_{4,meas}}{\sum eCH_{4,model}} \times Q_{ref} \quad (6)$$

237 When quantifying emissions for a source group, we calculate individual emission rates for each
238 source using its specific location and height and report the mean rate across the group. For sources
239 sampled across multiple transects, we use the mean emission rate across transects, which has been
240 shown to converge toward the true release rate, while the median tends to result in more
241 pronounced underestimation^{25,36}. If multiple source-groups on a site are tagged as emitting during
242 a measurement event, the group-level rates are summed to obtain the site-level emission rate.

243 **3.3. Controlled Release Experiments**

244 Data from two controlled release experiments were used to evaluate the detection, attribution,
245 and quantification performance of the vehicle-based CH₄ measurement system and processing
246 framework. The measurements were conducted by Eotrac Incorporated (Eotrac) and provided for
247 detailed analysis.

248 **3.3.1. Measurement Protocol**

249 Eotrac’s standard work practice is five driven loops or “transects” around the periphery of the
250 site, hereafter referred to as a “measurement event”, at driving speeds between 5 to 10 km/h. In
251 both controlled release experiments, Eotrac was informed of potential source locations; however,
252 specific release locations and flow rates were kept blind during testing. Data was therefore
253 collected in a way that is representative of upstream O&G field deployments, in which potential
254 source locations on site are known, but the precise locations and rates are not.

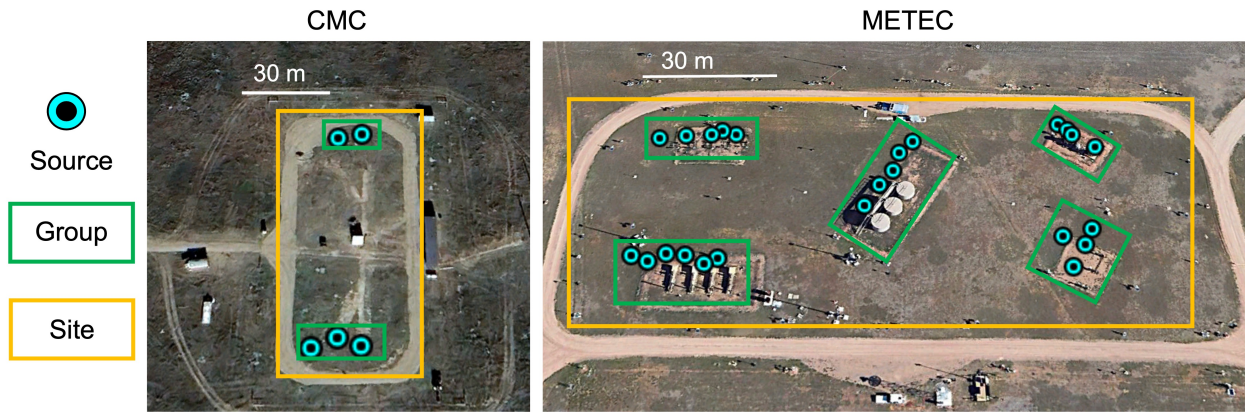
255 **3.3.2. Carbon Management Canada**

256 Controlled release testing was conducted at the Carbon Management Canada (CMC) test facility
257 at their Newel County field research station near Brooks, Alberta over five days from March 24 to
258 28, 2025. With five possible source locations divided into two source groups (Fig. 2, left), the site

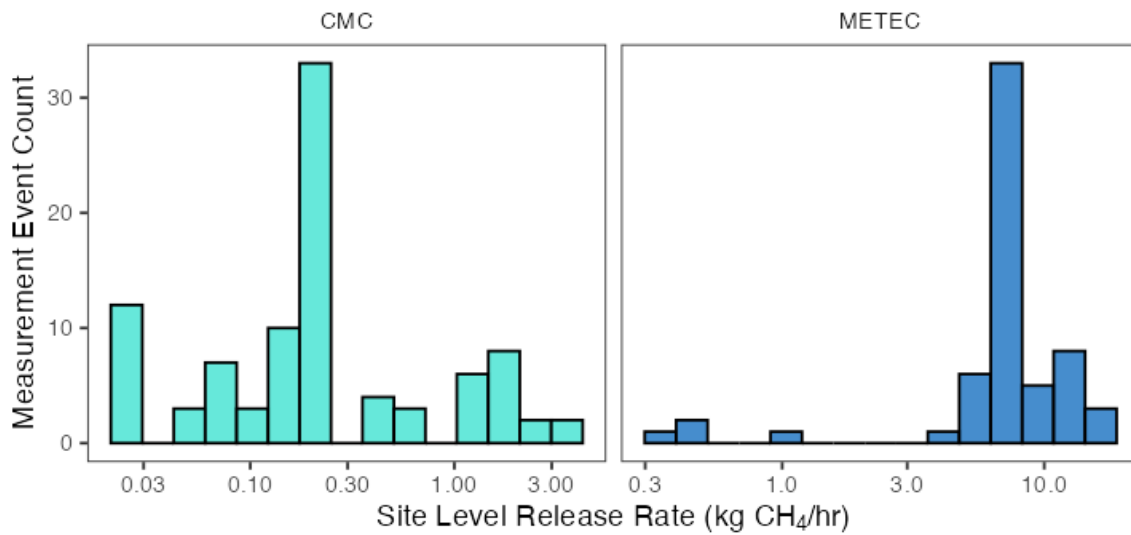
259 configuration during these tests simulated real-world emission sources such as tanks, separator
260 buildings, and well-pad equipment representative of a production site of low to moderate
261 complexity. Release heights ranged from 0 to 5 m, and release rates ranged from 0.025 to 3.564 kg
262 CH₄/h, with 74% of releases concentrated below 0.25 kg/h as shown in Figure 3 (left). In total, 97
263 measurement events were performed across five days, with events dominated by single-source
264 releases (88%), followed by multi-source releases (8%), and no-source releases (4%).

265 **3.3.3. Methane Emissions Technology Evaluation Center**

266 Controlled release testing was conducted at the Methane Emissions Technology Evaluation
267 Center (METEC) in Fort Collins, Colorado over three days from April 28 to 30, 2025. Releases
268 followed the ADED 2.0 blind controlled testing protocol ³⁷, which aims to simulate realistic multi-
269 source emission scenarios representative of normal baseline operational emissions, periodic
270 maintenance, and equipment failures. The portion of the site used for this experiment contained 24
271 potential source locations divided into five source groups (Fig. 2, right), including tanks,
272 separators, and well pads, ranging in height from 1 to 5 m. Total site-level release rates ranged
273 from 0.343 to 16.443 kg CH₄/h, with a cluster around 7 kg/h (Fig. 3, right). In total, 62
274 measurement events were performed, two of which were no-release, with the rest performed during
275 multi-source releases with a mean of 4.5 emitting source groups per measurement event. With the
276 large number of source groups and multi-source emission scenarios, this is representative of a
277 highly complex O&G production site.



278
 279 **Figure 2.** Map of the CMC (left) and METEC (right) controlled release facilities used in these
 280 experiments, showing individual source locations (blue circles), source groups (green outline), and
 281 full site (orange outline).



282
 283 **Figure 3.** Distribution of site-level release rates across measurement events for the CMC (left) and
 284 METEC (right) controlled release experiments.

285 3.4. Analysis Methods

286 While measurements during the controlled-release experiments were conducted in a blinded
 287 fashion, the analysis presented here was performed after release rates and locations were unblinded

288 and provided by Eotrac, to facilitate evaluation of method performance. The processing framework
289 used here differs slightly from that used by Eotrac, which may contribute to differences between
290 our results and those reported in their controlled release white paper³⁸. Data from both experiments
291 were included in all analyses, except for the probability of detection (POD) analysis, which only
292 used data collected during single-source release scenarios. The performance characterization
293 presented here is specific to the hardware, processing framework, and measurement protocol
294 applied in this study.

295 **3.4.1. Detection Classifications**

296 We evaluated overall detection performance at the measurement event level using all available
297 controlled release data. A positive detection occurs if an eCH₄ peak is attributed to any equipment
298 on site during a measurement event. We classified all measurement events (n=161) into four
299 detection categories: true positive (TP), false positive (FP), true negative (TN), and false negative
300 (FN) detections.

301 For a measurement event with a non-zero release rate, detection outcomes were classified as
302 either TP, when emissions are present and a detection is reported, or FN, when emissions are
303 present but no detection is reported. The fractions of each outcome were calculated using Eq. 7
304 and 8:

$$305 \quad TP \text{ fraction} = \frac{N_{TP}}{N_{TP} + N_{FN}} \quad (7)$$

$$306 \quad FN \text{ fraction} = \frac{N_{FN}}{N_{TP} + N_{FN}} \quad (8)$$

307 For a measurement event with a release rate of zero, outcomes were classified as either FP, when
308 a detection is reported despite no emissions being present, or TN, when no detection is reported,
309 calculated using Eq. 9 and 10:

310
$$FP\ fraction = \frac{N_{FP}}{N_{FP} + N_{TN}} \quad (9)$$

311
$$TN\ fraction = \frac{N_{TN}}{N_{FP} + N_{TN}} \quad (10)$$

312 These metrics represent the average detection performance across the range of conditions tested
313 during the controlled release experiments, including release rates, source and site configurations,
314 and meteorological conditions.

315 **3.4.2. Evaluating Probability of Detection (POD)**

316 We used individual transect-level data from single-source releases (n=428) to investigate factors
317 impacting POD. Detection outcomes for each transect were classified by a binary detection
318 variable (yes/no). Through a binary logistic regression, we explored factors influencing detection
319 probability, including emission rate, source-sensor distance and height offset, and meteorological
320 conditions. Emission rate was the dominant predictor, increasing the odds of detection by several
321 orders of magnitude and substantially exceeding the effects of other predictors. Detection
322 probability decreased with increasing distance and height offset, reflecting plume dilution and
323 reduced plume intersection, and increased under more stable atmospheric conditions. However,
324 limited coverage of these variables in the dataset limits our ability to fully evaluate their effects.
325 Given the strong influence of emission rate, subsequent analysis focuses on the relationship
326 between POD and emission rate, representing average detection performance across the sampling
327 geometries and meteorological conditions encountered during the controlled release experiments.

328 We modeled the relationship between probability of detection (POD) and emission rate using an
329 exponential function (Eq. 11), which ensures a POD of zero at an emission rate (x) of zero, and
330 can represent the skewed nature of the response variable.

331
$$POD = 1 - e^{-a*x^b} \quad (11)$$

355 was one true source and five potential source locations, divided into two source groups (Fig. 2,
356 left). We assessed attribution accuracy as the percentage of CH₄ peaks correctly attributed at the
357 source level, group level, and facility level (entire site). For METEC multi-source releases, up to
358 five source groups were emitting simultaneously, and we assessed attribution accuracy as the
359 percentage of emitting and non-emitting source groups correctly and incorrectly identified as
360 emitting across all measurement events.

361 **3.4.4. Quantification**

362 We evaluated the quantification performance of the measurement system and processing
363 framework by comparing estimated site-level emission rates to the true release rates. We excluded
364 select CH₄ peaks from the analysis when they fell outside the “operational envelope” of the
365 method, including peaks detected during stationary periods or very low driving speeds (<3 km/h),
366 and peaks for which the ratio of horizontal source distance to the relative source-inlet vertical
367 offset was less than 8:1. This reflects the physical limitations of measuring emissions from a tall
368 source, and the need for adequate distance for the plume to disperse downward toward the inlet.
369 Additionally, a source group had to be tagged on at least two transects to be included in
370 quantification, increasing confidence in both attribution and emission rate estimates. After
371 applying these criteria, we retained 72 of 89 CMC measurement events with detected emissions,
372 while all METEC events were included, although the same restrictions were applied to individual
373 peaks. We plotted true versus estimated site-level emission rates for each measurement event and
374 performed a linear regression through the origin. Systematic bias in the method was evaluated via
375 the slope of the best-fit line, where a slope near 1 indicates minimal bias, while R² captures the
376 overall strength of the relationship between true and estimated rates. The fraction of emission

377 estimates within a factor of 2 (-50 to +100% error) and a factor of 3 (-67 to +200% error) of the
378 true release rate was also calculated.

379 As an example of regulatory LDAR applications in Canada, we defined emission rate bins by
380 order of magnitude (0-1, 1-10, 10-100 kg/h) to reflect the different repair timelines prescribed for
381 leaks of different magnitudes under Canada's amended oil and gas CH₄ regulations ⁷. We evaluated
382 the ability of this method to correctly triage site-level emission rates by the proportion of emission
383 rates correctly classified by magnitude bin.

384 **3.4.5. Site-level Emission Rate Uncertainty**

385 For each measurement event, we estimated site-level emission rate uncertainty using a
386 bootstrapping approach. For each iteration (n=1000), we resampled emission rate estimates with
387 replacement within each source group and calculated the mean emission rate across resampled
388 estimates. We summed source group means to produce a site-level total emission rate. This process
389 was repeated 1000 times per measurement event to generate empirical distributions of site-level
390 total emission rates, from which bootstrapped-derived 95% confidence intervals (2.5th and 97.5th
391 percentiles) were calculated. Only source groups with two or more emission rate estimates were
392 included. Relative uncertainty for each measurement event was calculated using Eq. 13:

$$393 \quad \text{Relative Uncertainty} = \frac{(CI_{97.5} - CI_{2.5})/2}{\bar{Q}_{site}} \times 100 \quad (13)$$

394 Mean relative uncertainty was then calculated across all measurement events.

395 **4. Results and Discussion**

396 **4.1. Detection Rate and Probability of Detection**

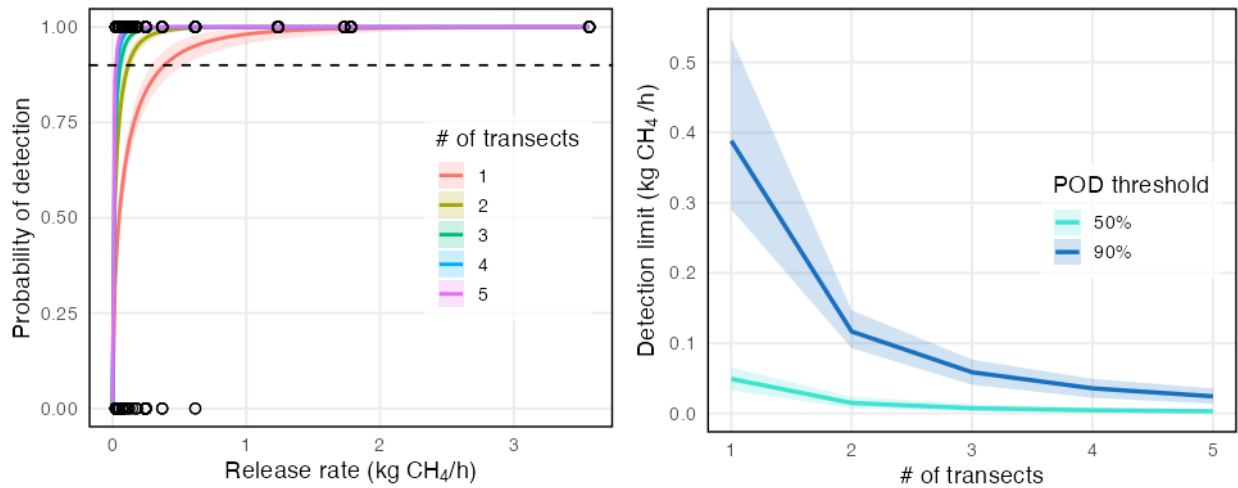
397 Based on the combined results from the two controlled release experiments, the vehicle-based
398 measurement system had a true positive detection rate of 96.1% across all measurement events
399 (Figure 4). Out of the six events in which emissions were present but not detected (false negative),
400 all six were at release rates < 1 kg/h, with 4/6 at the lowest emission rate tested (0.024 kg/h), and
401 the remaining two from incomplete measurement events in which the measurement event only
402 partially overlapped with the release timing, and consequently fewer than five transects were
403 performed. The system exhibited a false positive rate of 0%, meaning emissions were only detected
404 when they were truly present.

405 The detection sensitivity improves substantially with the number of measurement transects, as
406 shown by POD curves as a function of the emission rate for 1-5 transects (Figure 5, left). For a
407 single measurement transect, we estimated a 90% POD and 95% CI of 0.388 (0.291, 0.535) kg/h.
408 This drops by a factor of three to 0.117 (0.093, 0.147) kg/h for two transects, continuing to drop
409 with additional transects, reaching 0.024 (0.014, 0.036) kg/h for five transects, with marginal gains
410 per additional transect beyond three (Figure 5, right).

No Emission	False Positive 0 (0%)	True Negative 6 (100%)
Emission Present	True Positive 149 (96.1%)	False Negative 6 (3.9%)
	Detected	Not Detected

411

412 **Figure 4.** Confusion matrix of detection performance at the measurement-event level across both
 413 controlled release experiments.



414

415 **Figure 5.** (Left) Probability of Detection curves as a function of release rate for 1-5 measurement
 416 transects. (Right) Detection limit (kg CH₄/h) as a function of the number of measurement transects
 417 at 50% (light blue) and 90% (dark blue) probability of detection thresholds, with shaded regions
 418 representing 95 % confidence interval.

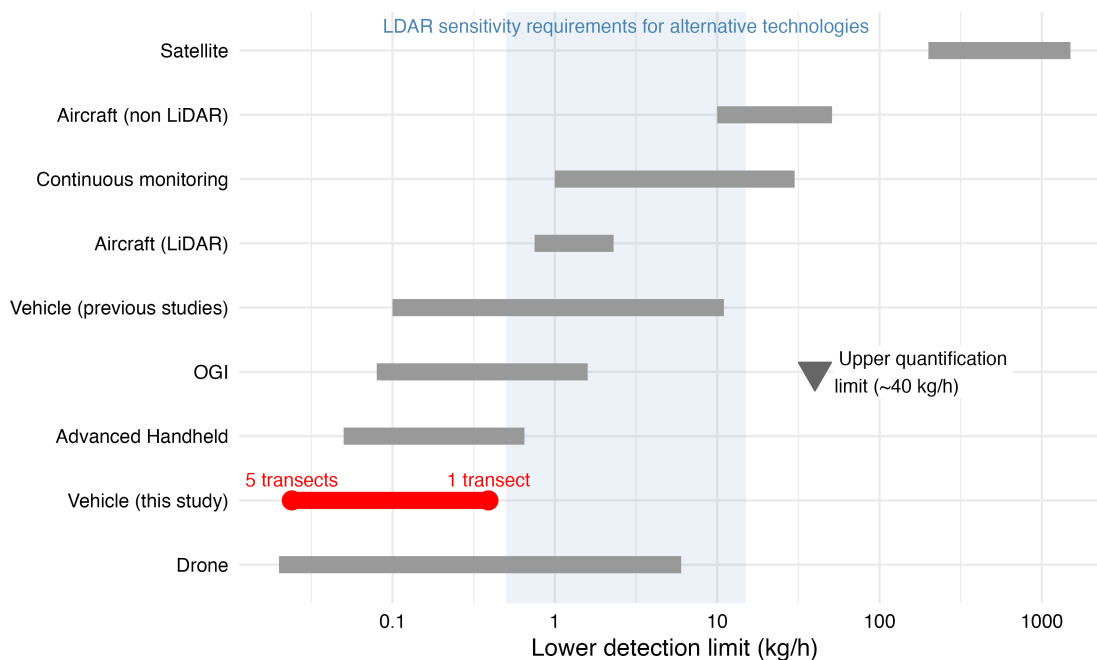
419 The detection sensitivities reported here represent average performance across the conditions
 420 encountered during the controlled release experiments for the measurement system tested. As the

421 CH₄ sensor used in this system has a relatively low measurement precision of ~0.2 ppm (1 σ),
422 detection sensitivity is expected to increase for more sensitive CH₄ sensors with which smaller
423 perturbations in the CH₄ time series could be detected. Furthermore, as discussed in Section 2.3,
424 detection performance is expected to vary with additional parameters identified in our binary
425 logistic regression, including source-to-sensor distance and height offset, and atmospheric
426 stability. While the release conditions are representative of typical on-site measurements of an
427 O&G site, further investigation is needed to characterize the impact of these parameters on
428 detection performance across a wider range of measurement conditions.

429 A key finding of this work is that detection sensitivity can be tuned by adjusting the number of
430 measurement transects, rather than depending solely on refinements to the measurement system
431 itself, e.g. increasing sensor precision. This illustrates a trade-off between sensor quality and
432 measurement effort that can be leveraged to meet target detection thresholds. High detection
433 sensitivities are achievable with a low-cost, lower-precision sensor than the research-grade
434 analyzers (e.g., cavity ring-down or off-axis integrated cavity output spectroscopy instruments)
435 typically employed in vehicle-based measurement studies, provided sufficient transects are
436 performed. Based on the POD analysis, we recommend a minimum of three transects per
437 measurement event, with up to five where detection of very low-emission sources is a priority.

438 Compared to other CH₄ detection technologies, including OGI and advanced handheld detection
439 methods, this vehicle-based approach achieves comparable or superior detection performance with
440 a lower detection limit well below the detection requirements for alternative technologies outlined
441 in LDAR regulations^{5,7,9}. Figure 6 illustrates the range of lower detection limits (90% POD
442 detection thresholds when available) of CH₄ detection technologies from recent controlled release
443 literature^{13–15,30,39–45}. Specific detection limit ranges and references for each technology are listed

444 in Table S2. Ilonze et al.³⁰ reported 90% POD limits ranging from 0.06 to 1.32 kg/h for handheld
 445 OGI and from 0.04 to 1.15 kg/h for advanced handheld solutions, while Zimmerle et al.¹⁵ reported
 446 90% POD for OGI of 0.12 and 1.59 kg/h for surveyors with high and low experience, respectively.
 447 In contrast to OGI, the vehicle-based method is not expected to exhibit dependence on operator
 448 skill, provided simple driving instructions can be followed. There are, however, other potential
 449 limitations to applying this method, including site layouts that do not permit complete driven loops
 450 around the site. While detection performance was high across the range of emission heights tested
 451 here, previous studies have highlighted that truck-based detection performance may degrade for
 452 tall sources (e.g. tanks) compared to other equipment types⁴⁶.



453
 454 **Figure 6.** Comparison of CH₄ lower detection limit ranges across measurement technologies for
 455 other technologies (grey bars) and the vehicle-based method tested in this study (red bar).
 456 Detection limits represent 90% POD thresholds unless otherwise noted (Table S2). Ranges are
 457 derived from published literature. The shaded blue region represents the range of detection
 458 sensitivity requirements for use of alternative technology in LDAR programs; more sensitive

459 detection limits can result in reduced screening frequency requirements. The upper quantification
460 limit for quantitative OGI (QOGI) technology is also shown (grey triangle).

461 **4.2. Attribution Performance in Single- and Multi-Source Releases**

462 In single-source release experiments, attribution accuracy was 100% at the site level, 99.7% at
463 the group level, and 49% at the source level. These results indicate very strong performance in
464 identifying the emitting source group, while highlighting challenges in pinpointing the precise
465 within-group source. This limitation is expected for downwind mobile measurements, where
466 uncertainty in the peak location combined with wind variability and plume turbulence make it
467 difficult to resolve exact leak locations, and is consistent with findings from Ilonze et al. ³⁰, who
468 reported lower localization performance at the source (equipment) level for mobile solutions
469 (vehicle and drone) relative to handheld technologies. For this reason, we opt to attribute peaks at
470 the group level rather than the source level.

471 For the multi-source controlled release experiments conducted at METEC, attribution
472 performance was assessed at the group level by determining whether emitting and non-emitting
473 groups were correctly identified. Across all measurement events, 86% (n=238) of the 277 emitting
474 groups were correctly tagged as emitting, and 15% (n=2) of the 13 non-emitting groups were
475 incorrectly tagged as emitting. While attribution performance decreases slightly under complex
476 multi-source release scenarios relative to single-source releases, the results demonstrate a strong
477 performance in identifying emitting groups and a low false positive rate.

478 Overall, these results indicate that the measurement system is well-suited for identifying
479 emission locations at the sub-facility scale, even in complex emission scenarios. This level of
480 attribution granularity is sufficient for inventory applications, in which emission rates are typically
481 reported at the facility scale. Furthermore, given the rapid site-level screening time (< 10 minutes),

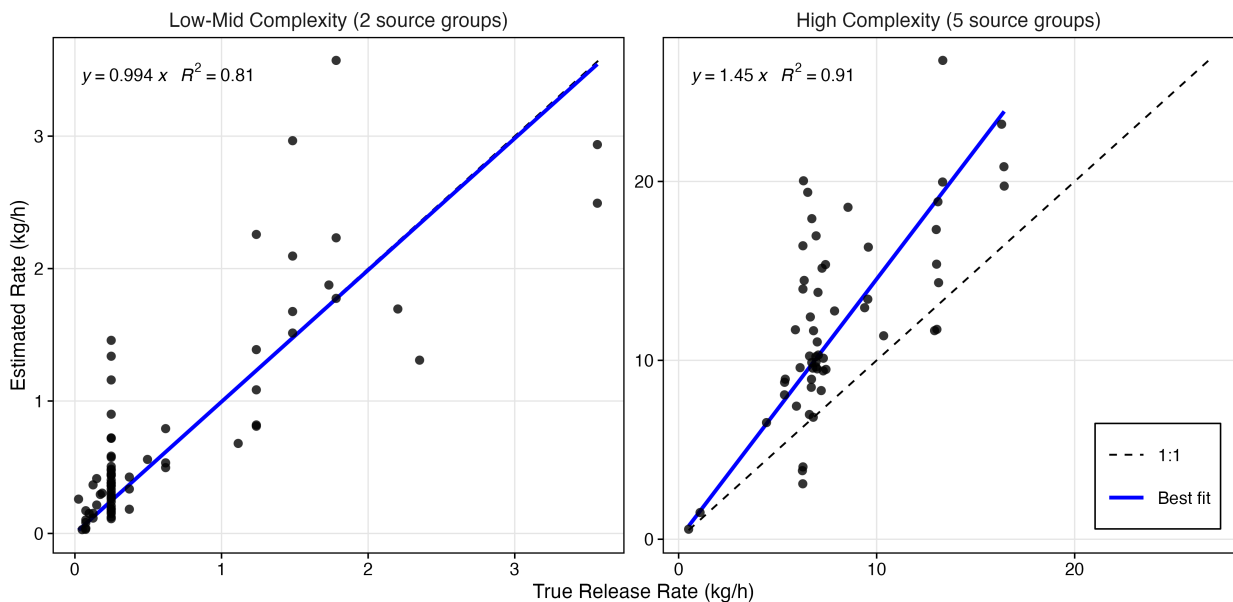
482 this approach could be a valuable complement to more intensive LDAR survey techniques,
483 enabling rapid triage and prioritization of component-level follow-up inspections.

484 **4.3. Site-level Quantification Performance**

485 Quantification performance varied significantly with release complexity. For low-to-moderate
486 complexity release scenarios (1-2 emitting source groups), quantification performance was
487 unbiased with a regression slope of 0.992 and $R^2=0.81$ (Fig. 7, left). For high-complexity release
488 scenarios (mean 4.5 simultaneous emitting source groups), estimated site-level emission rates were
489 systematically higher than true release rates, with a regression slope of 1.45 and $R^2=0.91$ (Fig. 7,
490 right). This overestimation of 45% is consistent with challenges in attributing emissions in an
491 environment with multiple co-located source groups emitting simultaneously. In these scenarios,
492 plume overlap between adjacent sources can increase the likelihood that emissions from one source
493 are partially attributed to a neighbouring source, inflating total site-level emissions. The high R^2
494 value suggests that the method reliably captures relative differences in site-level emission rates
495 despite these challenges with overestimation.

496 Overall, we find that 78% of emission estimates are within a factor of 2 error (-50 % to +100%)
497 and 95% are within a factor of 3 error (-67% to +200%). Quantification error tends to be larger for
498 small release magnitudes (see Figure S3), particularly below 1 kg/h. Across all individual
499 measurement events, quantification error ranges from -50.4% to 347.5% (2.5th to 97.5th percentile),
500 however when emission rates below 1 kg/h are excluded, this range narrows to -39.7% to 170.2%.
501 Figure S4 shows uncertainty for each site-level emission estimate represented by error bars,
502 derived via bootstrapping of individual emission estimates. Mean relative uncertainty across all
503 measurement events was 40%, comparable to uncertainties reported for other CH₄ monitoring
504 solutions^{27,43}.

505 These results are within a reasonable range of other vehicle-based quantification approaches,
506 which have reported factor-of-two performance ranging from roughly 18–92% depending on the
507 study and technology^{14,27–29}. More broadly, the factor-of-two performance of 78% demonstrated
508 here exceeds that of several other commonly used CH₄ quantification technologies. Factor-of-two
509 performance ranging from 25-46% has been reported for QOGI^{27,47} between 36-40 % for drone-
510 based methods, between 50-78% for continuous monitors, and 33% for hi-flow samplers²⁷. Our
511 individual error range (95% CI) for rates above 1 kg/h (-39.7% to 170.2%) is comparable to that
512 of Bridger Gas Mapping LiDAR (-58.5% to 129.4%, calculated from Bell et al.⁴⁸ SI), generally
513 considered among the most accurate quantification technologies available but requiring greater
514 logistical effort and cost.



515
516 **Figure 7.** Estimated vs true site-level emission rates during the CMC experiments (left),
517 representative of a low-to-moderate complexity site, and the METEC experiments (right),
518 representative of a high complexity site. Linear regression line through the origin is shown in blue,
519 and the 1:1 line is represented by the dashed line.

520 To our knowledge, this is the first study evaluating the quantification performance of this type
521 of vehicle-based measurement system in release scenarios of varying complexity, as previous
522 studies using this approach have focused exclusively on single-source release scenarios^{25,28,29,36}.
523 Our results highlight that complex multi-source scenarios introduce quantification challenges that
524 are not present with a single source, but that the method reliably captures relative differences in
525 site-level emission magnitudes as reflected in the high R^2 of 0.91. Future work should focus on
526 refining methods for robust separation of overlapping plumes, to avoid double-counting emissions
527 from co-located sources.

528 4.4. LDAR and Inventory Applications

529 We now examine how the system performance evaluated above translates to the two primary
530 applications motivating this work: LDAR programs and emission inventory development.
531 Categorization accuracy into Canada's regulatory LDAR repair threshold bins was high in the low-
532 mid complexity release scenario at 94% (51/54) correct classification in the 0-1 kg/h bin and 83%
533 (15/18) in the 1-10 kg/h bin (Table 1). In high complexity scenarios, classification accuracy was
534 100% in the 0-1 kg/h (1/1) and 10-100 kg/h (12/12) bins but dropped to 49% (22/45) for the 1-
535 10 kg/h bin, largely due to the overestimation bias observed at complex release sites. With a mean
536 true release rate of 6.7 kg/h in this bin, the systematic 45% overestimation shifted many estimates
537 across the 10 kg/h threshold into the next regulatory bin. Notably, all misclassifications were off
538 by only one bin, and most (26/29) were assigned to the higher bin rather than the lower, suggesting
539 a conservative bias from a regulatory perspective.

540

541 **Table 1.** Summary of quantification and categorization performance of the vehicle-based
542 measurement system.

Site Type	Magnitude bin (kg/h)	Num. meas. events	Mean release rate (kg/h)	MAE (kg/h)	MAPE	% correctly categorized
Low-Mid Complexity (CMC)	0-1	54	0.24	0.19	100%	94%
	1-10	18	1.78	0.58	34%	83%
High Complexity (METEC)	0-1	1	0.51	0.04	8%	100%
	1-10	45	6.71	4.60	69%	49%
	10-100	12	13.70	4.34	31%	100%

543 Results are divided by site complexity and emission rate magnitude bin. MAE= mean absolute
544 error; MAPE= mean absolute percentage error. “% correctly categorized” reflects the proportion
545 of total emission rate estimates that fell within the correct magnitude bin.

546

547 Although quantification performance degrades at high-complexity sites, this limitation should
548 be considered in the context of LDAR requirements for the O&G site population. Under the
549 amended Canadian oil and gas CH₄ regulations⁷, survey requirements include comprehensive
550 inspections between once per year to once per quarter for active sites, in addition to an annual
551 third-party inspection and screening inspections multiple times per year at all sites. The regulation
552 estimates approximately 447800 sites in Canada will be affected, of which active and inactive
553 unplugged well sites together account for 412200 sites, or roughly 92% of the total site population.
554 These well sites, along with facilities such as single-well batteries and small compressor stations,
555 represent the types of low-to-moderate complexity sites where this method is expected to perform
556 with minimal quantification bias.

557 Recent studies in Canada have found that OGI-based surveys miss a significant portion of total
558 site-level emissions compared to aerial-based methods^{12,49}, highlighting critical gaps in LDAR
559 programs that rely primarily on OGI measurements and emphasizing the need for multi-scale
560 measurement approaches to capture the full emissions picture. In addition to demonstrating

561 comparable or greater detection sensitivity and superior quantification performance than OGI,
562 vehicle-based surveys offer several practical advantages that could address these gaps. At less than
563 10 minutes per site, vehicle-based surveys are significantly faster than OGI, where site-level
564 survey durations can range from 1-2 hours for satellite well pads to several days for large
565 facilities⁵⁰, enabling broad coverage of the large population of sites required under regulations.
566 The speed and scalability of vehicle-based surveys make them well-suited as a rapid-screening
567 layer, flagging sites and source groups for targeted OGI follow-up and directing those resources
568 where they are most needed. Operator-induced performance variability is also low compared to
569 OGI¹⁵, and unlike aerial surveys in which the quality of modeled wind speed data from third-party
570 databases is a major contributor to uncertainty, the vehicle-based method measures wind
571 continuously and locally near the point of emission, which is important in complex environments.
572 Limitations include challenges in pinpointing individual leaking components, as well as
573 constraints common to ground-based methods more broadly: site-access constraints, such as
574 obstructions to full transects around a site, and unfavourable plume geometries arising from tall
575 sources measured at close range. In certain cases, tall and highly complex sites may therefore be
576 better suited to aerial survey methods. Taken together, these advantages and constraints suggest
577 that vehicle-based surveys could serve as a valuable complement to, rather than replacement for,
578 component-level OGI surveys and aerial approaches.

579 Beyond LDAR applications, vehicle-based measurement methods could help to fill a persistent
580 gap in emission inventory development by increasing the number of low-level emitters that are
581 directly measured. Emissions from oil and gas are well-documented to follow a heavy-tailed
582 distribution, where a relatively small number of large emitters contribute disproportionately to
583 total emissions^{18,51-53}. However, low-level emitters remain an important and often under

584 considered component of the inventory picture. Conrad et al.⁵⁴ estimated that 24% of provincial
585 CH₄ emissions in Alberta originated from sources below the detection limit of the Bridger Gas
586 Mapping LiDAR, with their bottom-up inventory relying primarily on equipment counts, emission
587 factors, and OGI data rather than direct measurement. Similarly, Williams et al.⁵³ estimated that
588 30% of CH₄ emissions from O&G sites across the contiguous United States originate from sources
589 emitting less than 10 kg/h. Ravikumar et al.⁵⁵ demonstrated that a detection limit of 0.1 kg/h is
590 sufficient to maximize detected emissions from the O&G sector during periodic leak surveys, a
591 threshold well within the sensitivity demonstrated here. The performance demonstrated in this
592 study, particularly the 90% POD threshold as low as 0.024 kg/h and the near-unbiased
593 quantification performance at low-to-moderate complexity sites, suggests that the vehicle-based
594 method is well-suited to characterize the lower end of the emission distribution that aerial and
595 satellite methods are likely to miss, with considerably less time and effort than methods of
596 comparable detection sensitivity such as QOGI, thereby reducing reliance on generic emission
597 factors and limited component-level data.

598 Future work should focus on characterizing the influence of measurement distance and source
599 height on detection performance, validating quantification performance at higher emission
600 magnitudes, and developing reliable methods for the separation of overlapping plumes from
601 closely co-located sources in order to address overestimation at high complexity sites. Together,
602 these advances would further establish vehicle-based measurements as a high-performance and
603 practical complement to existing CH₄ monitoring approaches.

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838 **Supplementary Materials**

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840 **Vehicle-Based Methane Detection, Attribution, and Quantification in the Upstream**
841 **Oil and Gas Sector: Method Overview and Controlled Release Validation**

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853 **S1 Input Parameter Selection for Spike Detection Algorithm**

854 The spike detection algorithm described in Daniels et al. requires three input parameters:

- 855 1. **Going-up threshold (ppm):** a peak begins when the increase in consecutive concentration
856 values exceeds this threshold.
- 857 2. **Return threshold (%):** a peak ends when the concentration value returns to this predefined
858 percentage of the maximum peak value.
- 859 3. **Peak amplitude threshold (ppm):** a peak is retained if the maximum concentration value
860 of the peak exceeds this threshold.

861 The selection of input parameters depends on the use-case scenario. As described by Daniels et al.
862 (2024), the parameters were designed to balance each other out and therefore do not require precise
863 tuning. For example, the going-up-threshold should be set to a value much lower than the peak
864 amplitude threshold, to tag peaks that build more slowly. Any peak that fails to reach the peak
865 amplitude threshold will be filtered out. Table S1 outlines the input parameters chosen for the
866 Axetris gas analyzer. Figure S1 shows the result of the spike detection algorithm applied to the
867 CH₄ timeseries.

868 An advantage to this algorithm is that it can be applied directly to raw instrument signals without
869 requiring noise filtering, provided the peak amplitude threshold is set above the instrument noise
870 level. Noise filtering can alter the max eCH₄ location and peak amplitude, two parameters that
871 must be known as precisely as possible for our attribution and quantification steps.

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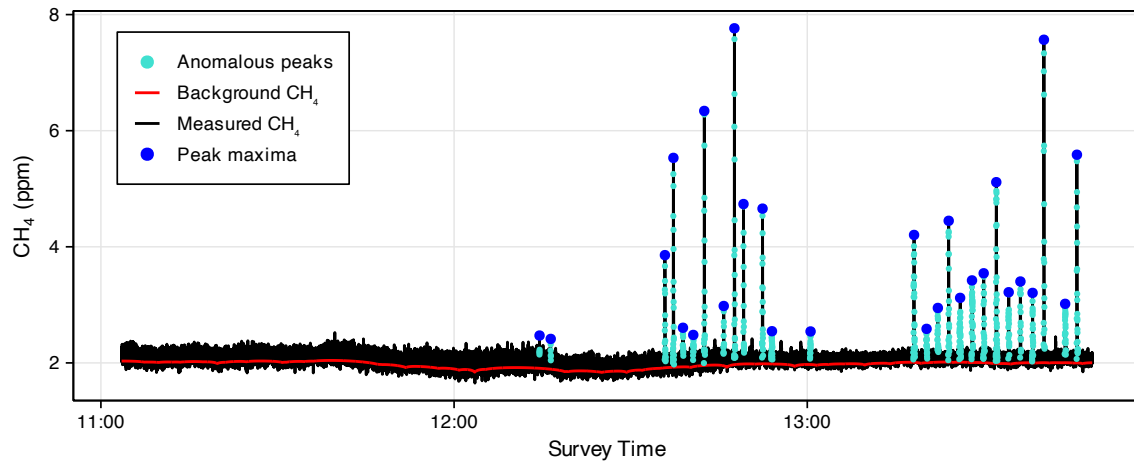
873 **Table S2.** Input parameters for spike detection algorithm.

Input Parameter	Value
Going-up Threshold	0.05 ppm
Amplitude Threshold	0.5 ppm
Return Threshold	50 %

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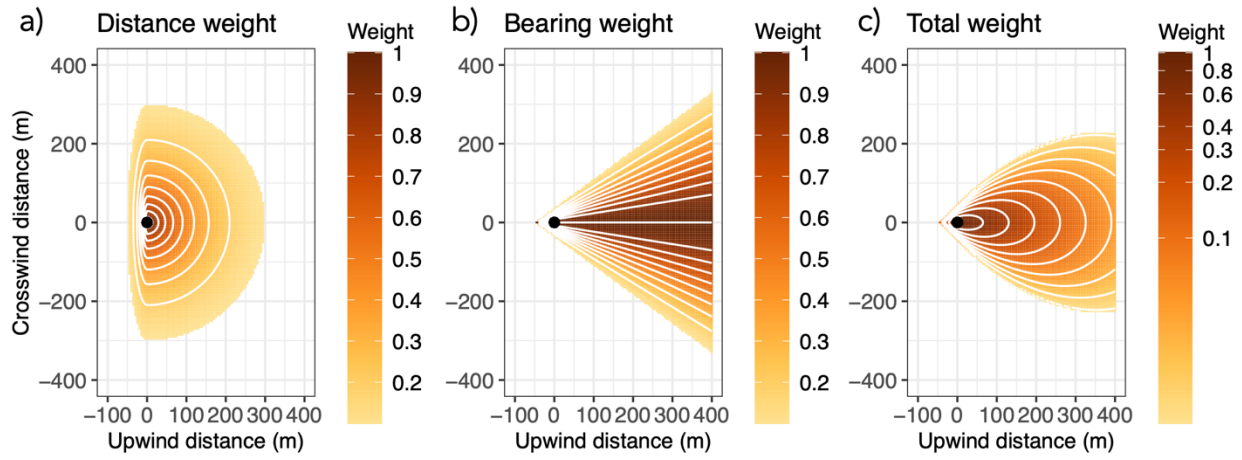
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876 **Figure S8.** Timeseries of measured CH₄ concentration (black), calculated CH₄ baseline (red), CH₄
877 peaks (turquoise), and peak maxima (blue).



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879 **Figure S9.** Attribution distance weight (a), azimuth weight (b) and total weight (c) as a function
880 of upwind and crosswind distance



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883 **Table S3.** Lower detection limit ranges and corresponding references for various CH₄ monitoring
 884 technologies. Detection limits correspond to 90% probability of detection thresholds unless
 885 otherwise noted.

Technology	Lower Detection Limit Range (kg/h)	References
OGI	0.06 to 1.593	Ilonze et al., 2026 Zimmerle et al., 2020
Advanced Handheld	0.04 to 0.65	Ilonze et al., 2026
Aircraft LiDAR	0.75 to 2.3	Bell et al., 2022 ¹ Conrad et al., 2023 ¹
Aircraft (non-LiDAR)	10 to 51	Conrad et al., 2023 ² El Abbadi et al., 2024 ³
Continuous Monitoring	1 to 30	Bell et al., 2023 Ilonze et al., 2024 McManemin et al., 2026
Drone	0.02 to 6	McManemin et al., 2026 Ravikumar et al., 2019 ⁴
Vehicle (previous studies)	0.1 to 11	Ravikumar et al., 2019 ⁴
Satellite	200 to 1500	Sherwin et al., 2023, 2024 ⁵
Vehicle (this study)	0.024 to 0.39	This study

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887 ¹ At reference windspeed of 3 m/s and typical altitude of 152 m (Bell et al.) and 175 m (Conrad et al.)

888 ² At reference windspeed of 3 m/s and typical altitude of 900 m for Kairos and 3000 m for AVIRIS-NG

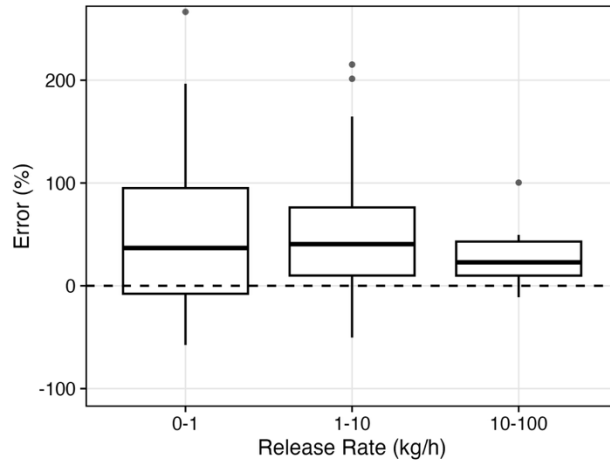
889 ³ 90 % detection limit not reported, aircraft consistently quantified emissions above 10 kg/h

890 ⁴ Reports rates where POD is 100%

891 ⁵ Approximate detection limits

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893 **Figure S10.** Percent quantification error by release magnitude bin.



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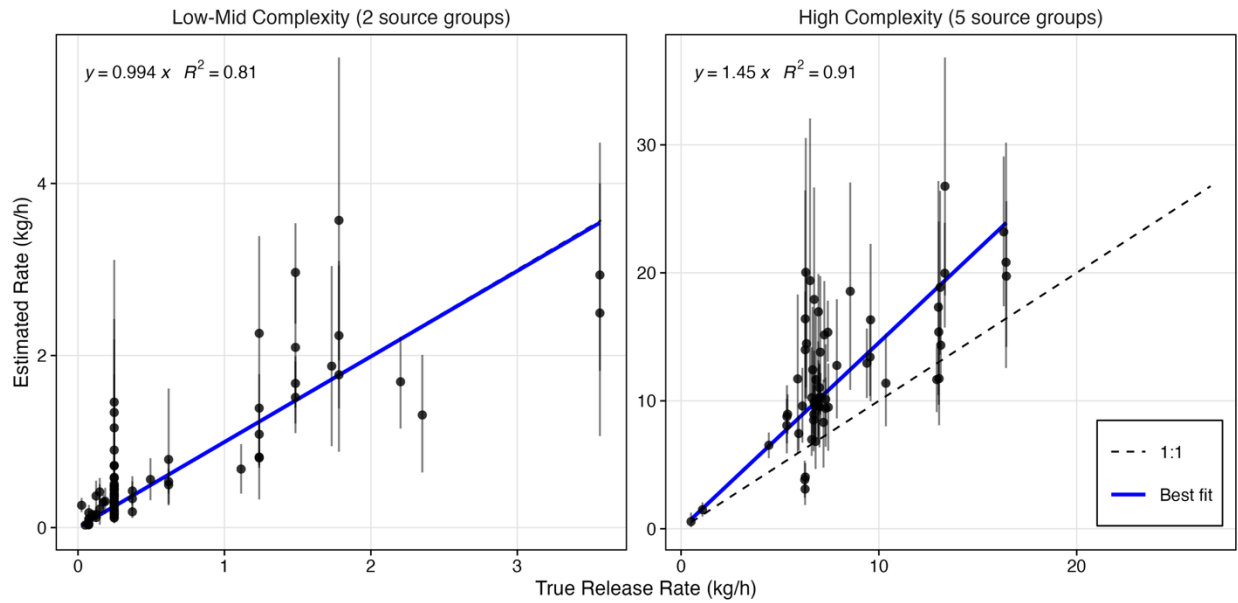
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899 **Figure S11.** Estimated vs true site-level emission rates during the CMC experiments (left),
900 representative of a low-to-moderate complexity site, and the METEC experiments (right),
901 representative of a high complexity site. Linear regression line through the origin is shown in blue,
902 and the 1:1 line is represented by the dashed line. Uncertainty for each site-level emission estimate
903 represented by error bars, derived via bootstrapping of individual emission estimates.



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906 **6. References**

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