Laboratory friction and plastic flow laws predict transient deformation after subduction zone mega-quake

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The deformation transient that follows large subduction zone earthquakes is thought to be the response of a large-scale nonlinear system where slip on the megathrust and viscoelastic flow in the asthenospheric mantle are accelerated by the sudden coseismic stress change[1]. However, as numerical models of such complex systems are still in their infancy, bringing together theory and prediction is still a major challenge. Here, we consider the post-earthquake deformation of the 2011 Mw 9.2 Tohoku-Oki earthquake based on numerical simulations incorporating a non-linear viscoelastic model[2, 3] and stress-driven afterslip[4, 5] in a fully three-dimensional (3D) heterogeneous structure of the subduction zone, using state-of-the-art techniques in computational science[6, 7]. The combination of power-law viscoelastic flow and afterslip results in good agreement in horizontal component of the calculated 2.8 year displacements with observation data[8, 9, 10, 11]: Viscoelastic flow associated with transient spatial variation of effective viscosity is dominant in overall deformation pattern with opposing horizontal direction on the seafloor and the land, while afterslip accounts for eastward displacement on land and offshore outside the rupture area. This suggests that post-earthquake deformation of large subduction zones earthquakes can be reasonably well anticipated when incorporating the frictional and rheological properties of lithosphere rocks derived from laboratory experiments into comprehensive models and a plausible structural model. Such three-dimensional, multi-physics simulations provide an effective framework to gain more detailed insight into the physical properties of subduction zones.

Post-earthquake deformation can be interpreted as a process of relaxing the stress perturbation caused by the earthquake rupture. It generally consists of the deformation due to continued, mostly aseismic slip on the megathrust (afterslip)[12] and viscoelastic relaxation in the asthenosphere [1]. Afterslip relaxes the stress perturbation by localized deformation in the region of the fault plane that surrounds the earthquake rupture. Viscoelastic flow relaxes the coseismic stress change by distributed, plastic deformation in the surrounding mantle [13, 14]. The post-earthquake deformation of the 2011 Mw 9.2 Tohoku-Oki earthquake was captured by a wide array of land-based[15, 8] and seafloor[9, 10, 11] instruments. This widespread observation network captured a complex post-earthquake deformation field. Some near-trench seafloor stations moved seaward, in the opposite direction to the long-term subduction motion, while others moved landward (Fig. 1a). The post-earthquake vertical motion was also complex, with many seafloor stations moving in opposing directions than that on land. Several studies [9, 10, 16, 17, 18] claim that viscoelastic relaxation largely contributed to these patterns.

The 2011 Mw 9.2 Tohoku-Oki earthquake induced a large stress perturbation in the surrounding lithosphere that accelerated the flow in the oceanic asthenosphere and in the mantle wedge. It is natural to expect that viscoelastic relaxation during the post-earthquake period can be described by the constitutive properties of peridotite, a rock assemblage of mostly pyroxene and olivine, under high temperature and pressure conditions. Likewise, afterslip may be described by the frictional properties of the megathrust. Laboratory experiments suggest that the plastic deformation of mantle rocks is accommodated by a thermally activated flow that obeys a power-law relation between stress and strain-rate [2, 3]. The friction between the subducting slab and the upper plate is governed by a laboratory-derived kinematic friction law [4, 5] that predicts the velocity of afterslip based on the stress evolution. Incorporating the laboratory-derived constitutive properties for plastic flow and afterslip successfully explained the deformation that followed the 2012 Mw 8.6 Indian Ocean earthquake [14], for which the surrounding rheological structure is rather simple. In contrast, most studies of the Tohoku-Oki earthquake employed simplified rheological models with linear viscoelastic flow in the mantle and kinematic afterslip [10, 19, 17] or explored more realistic rock properties in two-dimensional models [16, 20]. Despite recent efforts, simulating the full three-dimensional response of the Japan subduction zone still represents a significant challenge, probably due to the combination of the geometrical complexity and the nonlinear governing equations. Finite element techniques afford some of the most flexibility to build realistic simulations, but the remaining difficulty lies in the computational cost of such calculations.

Here, we exploit a state-of-the-art finite-element method proposed in computational science [6, 7] to simulate the three-dimensional response of the lithosphere-asthenosphere system following the 2011 Mw 9.2 Tohoku-Oki earthquake with plastic flow in the mantle and afterslip on the megathrust. The approach also allows us to incorporate a realistic velocity structure for the Japanese margin, Earth's sphericity and laboratory-derived, nonlinear rock constitutive properties. We assume that the plastic flow of the upper mantle is accommodated by steady-state dislocation creep, with the following stress-strain-rate relationship [2]

$$\dot{\varepsilon} = K(C_{\mathrm{OH}})^r \sigma^n \exp\left(\frac{H}{RT}\right) \tag{1}$$

where $\dot{\varepsilon}$ is the norm of the strain-rate tensor, K is a pre-exponential factor, C_{OH} and r are the water concentration and its exponent, σ is the norm of deviatoric stress tensor, n is the stress exponent, $H = Q + p\,\Omega$ is the activation enthalpy, R is the universal gas constant, T is the temperature. The enthalpy incorporates the activation energy Q and the activation volume Ω and depends on the confining pressure p. As the model already exhibits significant complexity due to the coexistence of afterslip and viscoelastic flow with lateral variations of constitutive properties, and since its constitutive properties are still unclear, we ignore the transient creep that is thought to take place during the early stage of post-earthquake transients [21, 14]. We combine dislocation creep with diffusion creep, but the latter does not play a significant role in our short-term simulations (see Methods). The temperature profile is based on a two-dimensional model for the Tohoku region [22], which we expanded along strike with a mantle temperature of 1380°c (Fig. 1b), compatible with another study [14]. We converted the background shortening rate of 10^{-8} yr^{-1} to determine the background stress based on the rheological law[23]. We assume that the velocity of afterslip on the megathrust is governed by the rate- and state-dependent friction (see Methods for details), given by

$$V \quad = \quad V_* \exp\left(\frac{\tau - (\tau_{\mathrm{s}*} + \Delta\tau_{\mathrm{s}})}{A}\right) \;, \tag{2}$$

where τ is the shear traction, $\tau_{\mathrm{s}*}$ is the steady-state frictional resistance, $\Delta\tau_{\mathrm{s}}$ is a state variable [24]. A is a parameter that controls the fracture energy consumed during fault slip. For the initial condition of the simulation, we borrow the coseismic slip (Fig. 1a) and the fault constitutive properties (Fig. 1c and Extended Data Fig. 5b) from a simulation of giant earthquakes in the Tohoku region [25]. We divide the region into three plates: a continental plate that includes the North-American and Eurasian plates and two oceanic plates, the Pacific and the Philippine Sea plates. Each tectonic plate consists of an elastic layer near the surface (the crust and the lithospheric mantle) and a viscoelastic mantle layer below (Fig. 1c and Fig. 2). The elastic and viscoelastic layers in the three plates share the same elastic properties (Fig. 1c). Simulating the dynamics of this nonlinear system in three-dimensions with realistic elastic, frictional, and plastic properties require a large-scale computation environment of 10^4 computer cores and a state-of-the-art fast and scalable finite element solver[6, 7] (see Methods).

Our simulated deformation shows similar patterns to the observation data for the cumulative 2.8 year post-earthquake displacement in the horizontal direction (Fig. 3a) when we choose the following rock properties $K = 10^{0.56}\,\mathrm{MPa}^{-n}/\mathrm{s}$, C_{OH}=1,000 ppm H/Si, Q=430 kJ/mol, r=1.2, Ω=13.5 cm^3/mol and n=3 (see Methods). For simplicity, we assumed a similar average water content in the oceanic asthenosphere and in mantle wedge, even though water concentration may be large in the mantle wedge corner due to slab dehydration [26]. The values adopted for the activation energy and the activation volume fall well within the uncertainties constrained by laboratory experiments [3], e.g., $Q = 410 \pm 50\,\mathrm{kJ/mol}$ and $\Omega = 11 \pm 3\,\mathrm{cm^3/mol}$, despite the required extrapolation to different temperature and pressure conditions. This indicates that the physical and geological setting of the Japan subduction zone is understood well enough to make accurate predictions about how the lithosphere-asthenosphere system will deform in response to a large earthquake.

The temporal and spatial evolution of effective viscosity after the giant earthquake naturally results from the nonlinear constitutive relation (1) and plays an important role in the rapid and complex deformation that occurs during the post-earthquake period. In response to the large (above 1 MPa) stress perturbation in the upper mantle, the effective viscosity (see Methods) was largely reduced shortly after the earthquake in the depth of 80-180 km in the oceanic mantle and 100-200 km in the mantle wedge (Fig. 4). The flow of low-viscosity mantle material below the trench axis drives westward motion around the trench, explaining the continued displacement of the seafloor stations located above the coseismic rupture (MYGI, KAMS and KAMN, Fig. 3b). The accelerated flow in the mantle wedge contributes to the eastward displacement of GPS stations on land. Afterslip on the megathrust is essential to explaining the deformation on land, but also the spatial pattern of displacement of the seafloor stations, such as eastward displacement seen in the stations FUKU and MYGW (Fig. 3b). Both these stations are in locations where viscoelastic flow produces little horizontal displacement, making the post-earthquake response due to the afterslip dominant there (Fig. 4).

Despite the excellent fit at numerous stations in the far-field, there remain a few discrepancies with the near-field data, presumably because our model does not include some details of the coseismic rupture offshore. For example, the simulated horizontal displacement at the station FUKU is nearly half of the measured one, despite a good agreement in the azimuthal direction. A peak of the amplitude of afterslip in the green ellipse in Fig. 3b should be slightly closer to station FUKU to fit the data, perhaps indicating that the coseismic slip was overestimated in this region. Such afterslip distribution should also fit better the horizontal displacements in the southern part of the land area (the purple ellipse in Fig. 3a). In the vertical displacement, significant uplift is observed in the fore-arc (The purple circles in Fig. 4). In the trench-normal profile of the stations MYGI and MYGW, although viscoelastic flow in the simulation produces uplift in this region, subsidence due to the afterslip cancels it out (the green circles in Fig. 4). Furthermore, a significant portion of this uplift in viscoelastic flow is due to stress change associated with afterslip, which we inferred from simulations of viscoelastic flow that exclude afterslip (the green circles in Extended Data Fig. 8a). Without the interaction between afterslip and viscoelastic flow, the computed 2.8-year horizontal displacements are reduced by more than 10 % in some of the land stations, and the vertical ones change by more than 30 % in many stations in both the land and the seafloor (Extended Data Fig. 8b). As afterslip in the near field can be highly sensitive to the details of the coseismic rupture, these residuals may be caused by still unresolved slip patterns of the mainshock. Despite these shortcomings, our results highlight the nonlinear interactions among coseismic slip, afterslip and viscoelastic flow.

Remarkably, the spatial distribution of effective viscosity derived from laboratory data and coseismic stress change is similar to those inferred from optimization of simplified linear viscoelastic models. The effective viscosity shortly after the earthquake is around 2×10^{17} Pa s at the minimum both in mantle wedge and oceanic mantle. This is equivalent to the viscosity in a linear transient creep model that fits observed post-earthquake deformation during the early stage [10], which was attributed to the presence of fluid or partial melt in lithosphere-asthenosphere boundary (LAB) [10]. Our result suggests that such a low-viscosity layer is the transient response of nonlinear plastic flow to the large stress perturbation, rather than a permanent structure. The linear viscoelastic models with low viscosity layers have only limited applicability in the context of a nonlinear viscoelastic model with both spatially and temporally varying effective viscosity (Extended Data Fig. 7). A recent experiment implied that a LAB is not explained by the presence of water[27], which supports our interpretation.

Our study demonstrates that a rheological model of the plate boundary based on independent geological and geophysical data can make realistic, first-order predictions of the transient response of the lithosphere following giant earthquakes. Complex post-earthquake deformation of a large subduction zone earthquake can be well explained by taking into account the laboratory-derived friction and plastic flow laws in a three-dimensional structural model. The discrepancy between the simulation and the data should be reduced, in principle, by refined models of the coseismic rupture and the in situ conditions such as initial stress, temperature and confining pressure, properties that are usually constrained for long time scales [28, 29]. The approach is generally applicable to other ocean-continent subduction zones, implying that our understanding of rocks friction and plastic properties may be detailed enough to predict the slow deformation of the lithosphere during the interseismic period. The remaining challenge is to understand Earth's deformation at high strain-rates.

Methods

0.1 Rheology model for upper mantle

We used the dislocation creep model based on the laboratory-derived power-law relation and the linear Maxwell element in series:

$$\dot{\varepsilon} = K(C_{\mathrm{OH}})^r \sigma^n \exp\left(\frac{Q + p\Omega}{RT}\right) + \frac{1}{2\eta_{\mathrm{l}}}\sigma, \tag{3}$$

where η_{l} is a constant value for viscosity in the linear Maxwell element. This simplifies the treatment of diffusion creep, based on the idea that viscosity in diffusion creep is 10^{1-2} times larger than effective viscosity in dislocation creep shortly after earthquakes of Mw 8.2 and 8.6[14], and the influence of diffusion creep is not expected to be very large in the 2.8 years deformation after the 2011 Mw 9.2 Tohoku-Oki earthquake. We use $\eta_{\mathrm{l}} = 1 \times 10^{19}\,\mathrm{Pa\,s}$ for the whole of the region, which is nearly the average value of the viscosity structure estimated for steady state 2D model around the Japan Trench[23]. In tensor notation,

$$\dot{\varepsilon}_{ij} = K(C_{\mathrm{OH}})^r |\sigma'_{ij}|^{n-1} \exp\left(\frac{Q + p\Omega}{RT}\right) \sigma'_{ij} + \frac{1}{2\eta_{\mathrm{l}}}\sigma'_{ij}, \tag{4}$$

where the apostrophe denotes deviatoric tensor, and $|\cdot|$ is the norm of tensor (square root of the second invariant of the tensor). We defined effective viscosity to be $\eta_{\mathrm{eff}} = \sigma/2\dot{\varepsilon}$, thus

$$\eta_{\mathrm{eff}} = \frac{\eta_{\mathrm{p}}\eta_{\mathrm{l}}}{\eta_{\mathrm{p}} + \eta_{\mathrm{l}}} \tag{5}$$

where

$$\eta_{\mathrm{p}} = \frac{1}{2K(C_{\mathrm{OH}})^r} |\sigma'_{ij}|^{-n+1} \exp\left(-\frac{Q + p\Omega}{RT}\right). \tag{6}$$

Our temperature pattern (Fig. 1b) in the elastic slab is significantly different from the reference thermal model[22] in that it keeps a low temperature even in the depth deeper than 200 km. However, it affects little the simulation results because high pressure is dominant and does not arrow much viscoelastic flow in this depth. In the simulation, we use the values proposed from laboratory experiments[3] for

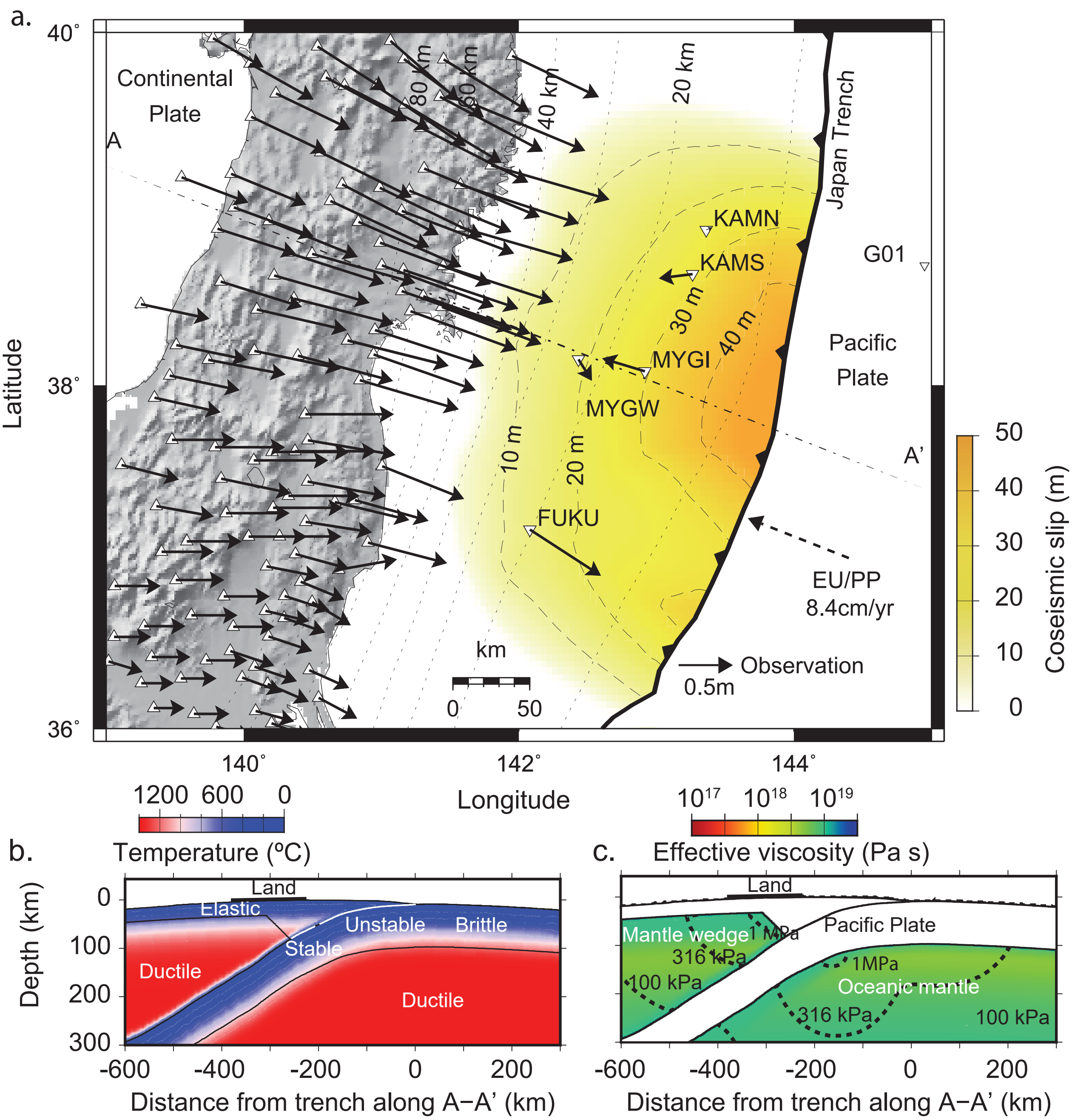

Figure 1: Post-earthquake deformation 2.8 years after the 2011 Tohoku-Oki Earthquake and surrounding material properties. a, Measured displacement in the land stations[15, 8] (triangles) and the seafloor stations[9, 11] (inverse triangles). We removed some land stations for visibility. Coseismic displacement is not available in the station G01. Dashed-dotted and dotted lines are the location of the cutting plane (A-A' profile) and the depth of the plate boundary, respectively. b, Assumed temperature structure and frictional properties in the A-A' profile. In the "unstable" region, where coseismic slip is input in our simulation, friction parameters are set as -0.2 MPa$\leq A - B \leq$-0.1 MPa and 0.2 m$\leq L \leq$0.3 m. In the "stable" region, where afterslip occurs in our simulation, $A - B$=0.1 MPa and L=13 m (also see Extended Data Fig. 5b). The temperature values in the layers of elastic materials are not used in the simulation. c, The assumed viscoelastic structure and the stress change along the A-A' profile. The mantle wedge and oceanic mantle are viscoelastic with μ_{v}=65 GPa. The remaining volume is elastic with μ_{e}=45 GPa. Poisson's ratio is ν=0.25 and density is ρ=3300 kg m^{-3} everywhere. The color indicates the effective viscosity before the earthquake and the computed stress distribution. Contribution from dislocation creep is dominant in the area with the light yellow, while viscosity in the linear term is dominant (see Methods) elsewhere. The dashed contour line indicates summation of background stress and coseismic stress (norm of deviatoric stress tensor).

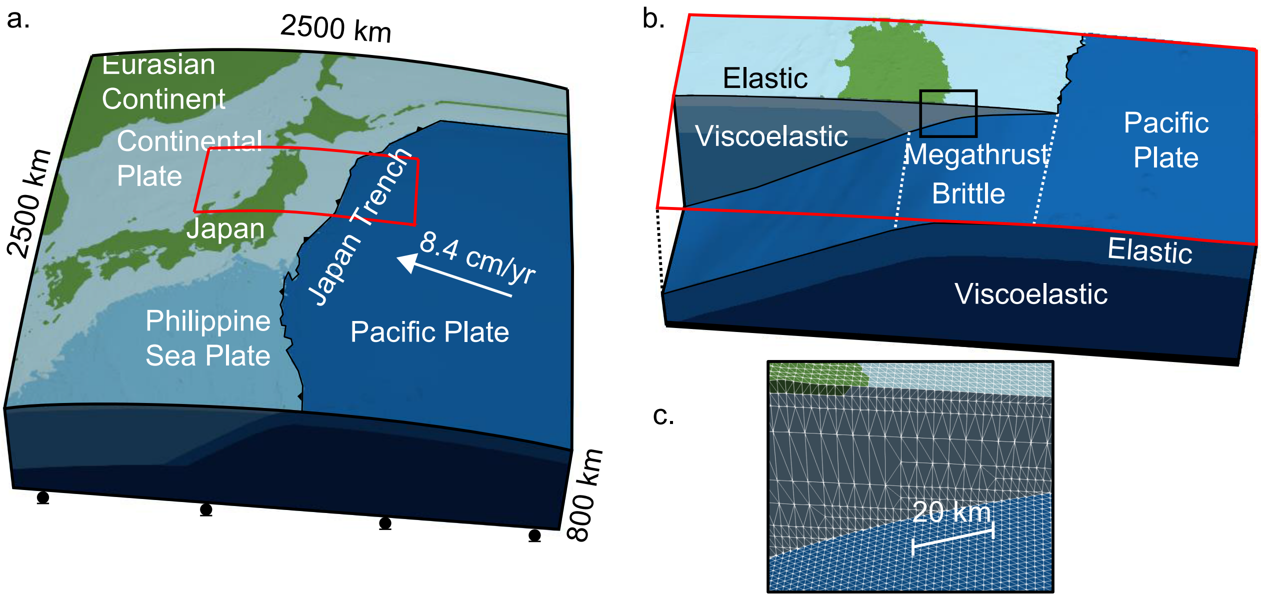

Figure 2: The finite-element model used in our study. a, Overview, b, close-up view for the region of the red rectangular in **a** with the location of the megathrust and c, close-up view for the region of the yellow rectangular in **b** with finite-element mesh patterns. The elements with the same color are in the same structural component (we have six of them, elastic and viscoelastic layer in three plates). The green color is used to distinguish the elements that are located above the sea level. The green elements have the same material properties as those in the continental plate.

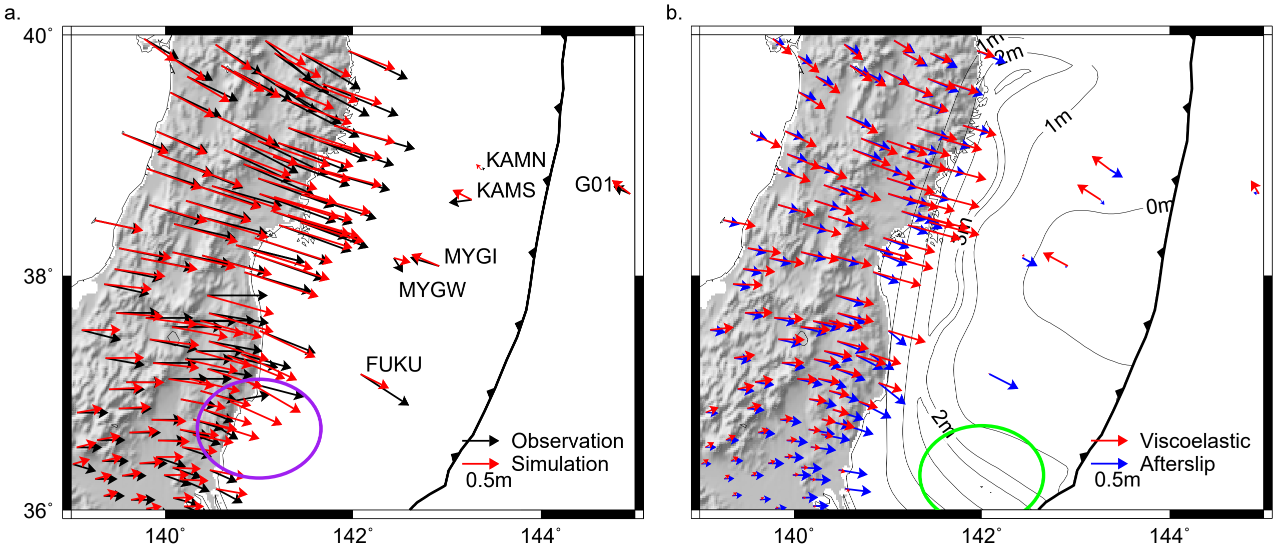

Figure 3: Post-earthquake deformation of the 2011 Tohoku-Oki earthquake. a, The horizontal component of 2.8-year post-earthquake displacements. In the station G01, displacement in the period 1.5 years and 2.8 years after the earthquake is plotted because of the limitation of data availability. In addition, the contribution from the plate convergence rate (shown in Fig. 1a), which is not included in our simulation scheme, is added to the simulation result in the station. b, The horizontal components of 2.8-year post-earthquake displacements in the simulation broken down into the contribution from afterslip and viscoelastic flow. The viscoelastic component includes the contribution from both coseismic slip and afterslip. The contour lines indicate accumulated afterslip for 2.8 years. A peak of the amplitude of afterslip in the green ellipse should be slightly closer to the station FUKU to fit better the horizontal displacements in FUKU and the purple ellipse.

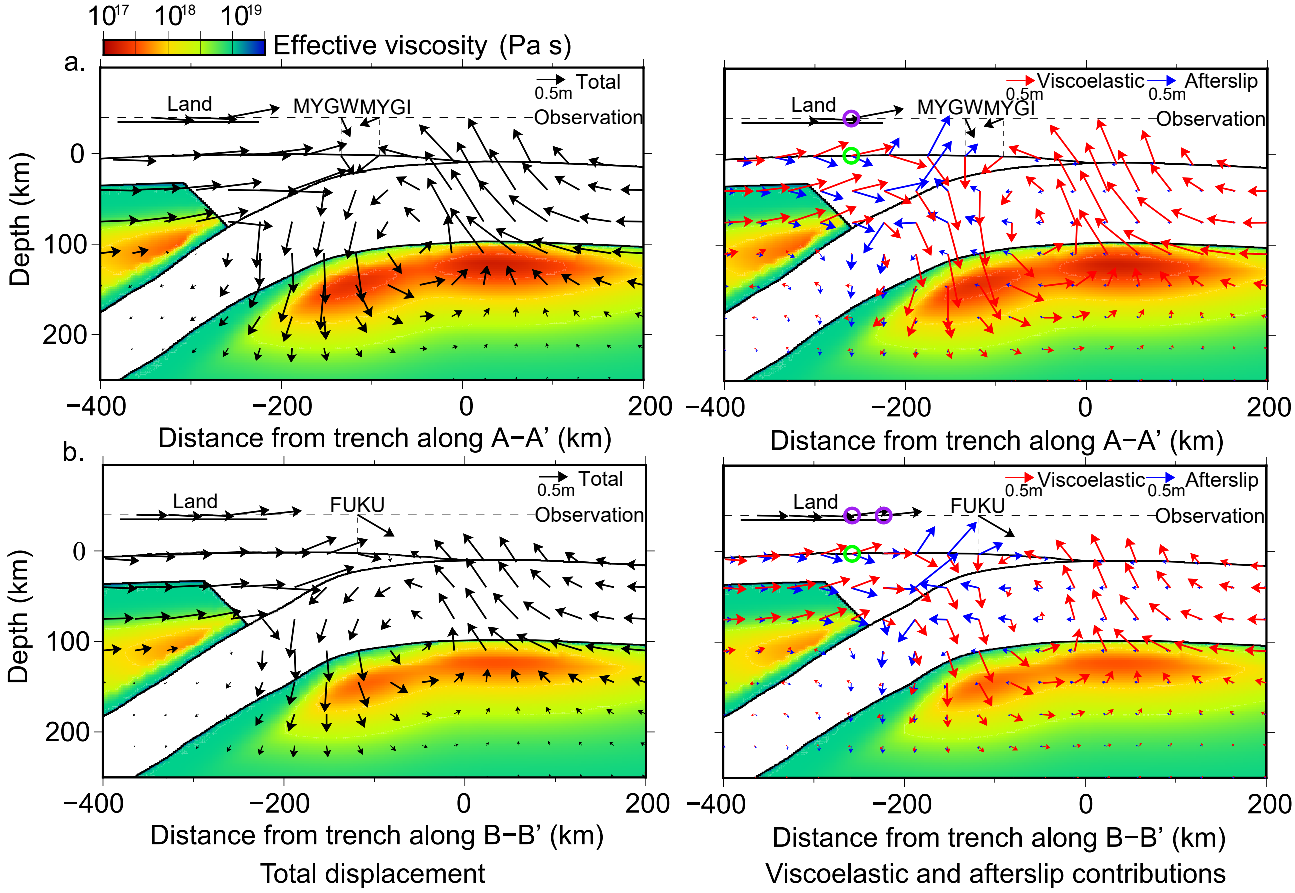

Figure 4: Simulation results on the cutting planes that are parallel to plate convergence direction, going through seafloor stations (a: the A-A' profile with MYGW and MYGI, b: the B-B' profile, which is parallel to A-A' and runs by the station FUKU). The figures on the left are for the total displacement after 2.8 years. The panels on the right show the contribution from afterslip and viscoelastic flow after 2.8 years. The color indicates the distribution of effective viscosity due to coseismic stress change. The black arrows on the horizontal dashed line are the observed displacements. In the location of purple circles, observation data shows uplift, while in the green circles, computed uplift viscoelastic displacement is canceled out by subsidence due to afterslip.

K, r and n, while Q and Ω were chosen within the error bar obtained in the same experiments, so that the computed displacement values are more consistent with the data. We set the C_{OH} value as an average in the upper mantle. Further study on more detailed variation of measured displacement should require considering heterogeneous distribution of water content[14, 30].

0.2 Coseismic slip and fault friction setting

To compute post-earthquake deformation, we take over an M9-class earthquake scenario calculated in an earthquake cycle simulation in the Tohoku region carried out by Nakata *et al.*[25]. This simulation supposes that space-time variations in slip velocity are assumed to be a slip with a frictional interface. We assume that equilibrium equation in shear stress on the fault plane, which is described as,

$$\frac{d\tau_i}{dt} = F_i(\mathbf{V} - \mathbf{V}_{\mathrm{pl}}, \dot{\boldsymbol{\varepsilon}}^{\mathrm{inelastic}}) - \gamma\frac{dV_i}{dt} \tag{7}$$

where τ_i and V_i are shear stress and slip velocity on a FEM node i on the fault. V_i is in the direction opposite to the convergence rate (Fig. 1). $\mathbf{V}$ and $\mathbf{V}_{\mathrm{pl}}$ are vectors whose components are V_i and $V_{\mathrm{pl}i}$, the plate convergence rate. $V_{\mathrm{pl}} = 8.4\mathrm{cm/yr}$ is used for the whole region in this study. $\boldsymbol{\varepsilon}^{\mathrm{inelastic}}$ is inelastic strain in the targeted 3D body. The second term introduces the effect of the seismic radiation damping[31]. We use $\gamma = 0.3\mu/2c$, which is used in Nakata *et al.*[25] to reproduce a shorter duration during the 2011 Tohoku-Oki earthquake[32], where μ is the rigidity and c is the shear wave velocity. In many studies the simulations with elastic homogeneous half-space have been carried out, where $\dot{\boldsymbol{\varepsilon}}^{\mathrm{inelastic}} = 0$. This makes F_i a linear function of $\mathbf{V}$ and enable F_i to be discretized by the boundary integral equation method (BIEM). In this study, we evaluate F_i directly by using the finite element method (see Section 0.3), in which F_i can be a function of both $\mathbf{V}$ and $\dot{\boldsymbol{\varepsilon}}^{\mathrm{inelastic}}$, and arbitrary geometry and material heterogeneity can be considered. It should be noted that a BIEM approach that can incorporate inelastic strain in elastic homogeneous half-space was proposed recently[33]. The rate- and state-dependent friction law is used to model frictional behavior on the plate interface as

$$V_i = V_* \exp\left(\frac{\tau_i - (\tau_{\mathrm{s}*i} + \Delta\tau_{\mathrm{s}i})}{A_i}\right), \tag{8}$$

$$\frac{d\Delta\tau_{\mathrm{s}i}}{dt} = \frac{B_i}{L_i/V_*}\exp\left(-\frac{\Delta\tau_{\mathrm{s}i}}{B_i}\right) - \frac{B_i V_i}{L_i}. \tag{9}$$

(8) represents a fault constitutive law that determines V_i for a given τ_i and a value of $\tau_{\mathrm{s}i}(=\tau_{\mathrm{s}*i} + \Delta\tau_{\mathrm{s}i})$, where $\Delta\tau_{\mathrm{s}i}$ is a state variable which is analogous to the "strength as a threshold"[24] and $\tau_{\mathrm{s}*i}$ the steady state strength with $V_i = V_{\mathrm{pl}}$. (9) is an aging law[5]. The frictional parameter B controls strength recovery, while L controls slip weakening. Time integration is performed using an adaptive time step fifth-order Runge-Kutta algorithm[34]. In our simulation, initial value of τ_i and $\Delta\tau_{\mathrm{s}i}$ is extracted from a time step right after the earthquake in the simulation of Nakata *et al.*[25](Extended Data Fig. 5a). The values are multiplied by 0.7, because the coseismic slip computed in their simulation fits best the coseismic crustal deformation data when multiplied by 0.7 (mentioned in the next paragraph). The initial value of V_i is calculated with (8). Frictional parameters are also the same as in Nakata *et al.*[25], excluding that small patches for M7 earthquakes are removed (Extended data Fig. 5b).

Extended Data Fig. 6 shows the coseismic slip, the same as in Fig. 1, which we extracted from the cycle simulation results, and comparison between computed and observed coseismic displacement. Although this slip model is not inferred from observation data, it fits the horizontal component of coseismic crustal deformation data well when multiplied by 0.7. The stress distribution computed in response to this coseismic slip is used as the stress perturbation to compute power-law viscoelastic flow and afterslip evolution.

0.3 Finite-element modeling

In the finite-element modeling, we discretize the equations for viscoelastic deformation and fault friction using the mesh shown in Fig. 2. The mesh was constructed using an updated version of a meshing technique for quadratic tetrahedral elements based on a background structured grid[7]. In the method, at first a uniform background cell covering entire targeted domain was used, and it defined the resolution of the layer interfaces as ds. The geometries of the ground surface and interfaces were simplified slightly to maintain good element quality. At the same time, unnecessary elements were merged to generate larger elements elsewhere. This method enables automated and robust construction of high-resolution tetrahedral mesh directly from digital elevation model (DEM) data of crustal structure without creating a CAD (computer-aided design) model. The updated version of the meshing algorithm carries out an additional post process to minimize the simplification of the geometry in the ground surface and interfaces as much as possible. Input elevation data sets are based on 900 m resolution topography data (JTOPO30), the CAMP model[35] and a velocity data set for the Japanese Island[36]. With $ds = 2$ km and little simplification of the geometry, shear stress distribution on the fault, which is essential for computing stress-driven afterslip, is evaluated accurately in the target problem. The finite element mesh has 1,402,810,116 degree-of-freedom (DOF) and 346,885,129 tetrahedral elements. In viscoleastic material and elastic material, rigidity is μ_{v}=65 GPa and μ_{e}=45 GPa, respectively. Poisson's ratio is ν=0.25 and density is ρ=3300 kg m^{-3} everywhere. This setting follows Sun et al. (2014)[10].

To evaluate F_i in (7), we applied an algorithm based on a viscoelastic finite element formulation[37, 38], which we modified to consider nonlinear viscoelasticity. Slip velocity $\mathbf{V}$ is input to the finite-element model using the split node technique[39] to evaluate response displacement rate. We consider the effect of gravity using surface gravity approximation[40]. Since no inertia term is included in the equations, the problem is quasi-static, which ends up with solving an elliptic problem in every time step. It means we need to solve the system which has billions of DOF. We introduced a modified version[41] of a massively-parallel FEM solver for computing crustal deformation[7] based on "GAMERA"[6] (a physics-based seismic wave amplification simulator, enhanced by a multi-Grid method, Adaptive conjugate gradient method, Mixed precision arithmetic, Element-by-element method, and pRedictor by Adams-Bashforth method).

We run the calculation using 2048 computer nodes (16384 computer cores) of the K computer at RIKEN, Advanced Institute for Computational Science[42], each computer node of which has one CPU (Fujitsu SPARC64 VIIIfx 8 core 2.0 GHz) and 16 GB of memory, for 7.5 hours to obtain the post-earthquake deformation for 2.8 years shown in Fig 3.

0.4 Viscoelastic and afterslip contributions

Fig. 3b and the figures in the right in Fig. 4 present breakdown of computed displacement into contribution from viscoelastic flow and afterslip. This is calculated in the following manner:

1. Extract accumulated 2.8 year afterslip distribution that is computed based on the nonlinear interaction of the rate- and state-dependent friction law and the nonlinear rock constitutive properties in the original simulation.

2. Compute elastic response displacement $\mathbf{u}_{\mathrm{afterslip}}$ due to the extracted afterslip. $\mathbf{u}_{\mathrm{afterslip}}$ corresponds to the blue arrows in Fig. 3 and 4.

3. $\mathbf{u}_{\mathrm{viscoelastic}} = \mathbf{u}_{\mathrm{original}} - \mathbf{u}_{\mathrm{afterslip}}$, where $\mathbf{u}_{\mathrm{viscosity}}$ and $\mathbf{u}_{\mathrm{original}}$ correspond to the red and black arrows in Fig. 3 and 4, respectively.

We also present a result post-earthquake deformation simulation with "no interaction" between viscoelastic flow and afterslip (Extended Data Fig 8). In this simulation, we computed viscoelastic flow without the friction law (the red arrows in Extended Data Fig 8a), while computing afterslip without the nonlinear rock constitutive properties, only with pure elasticity. We finally summed up these to compute total deformation without their interaction (the red arrows in Extended Data Fig 8b).

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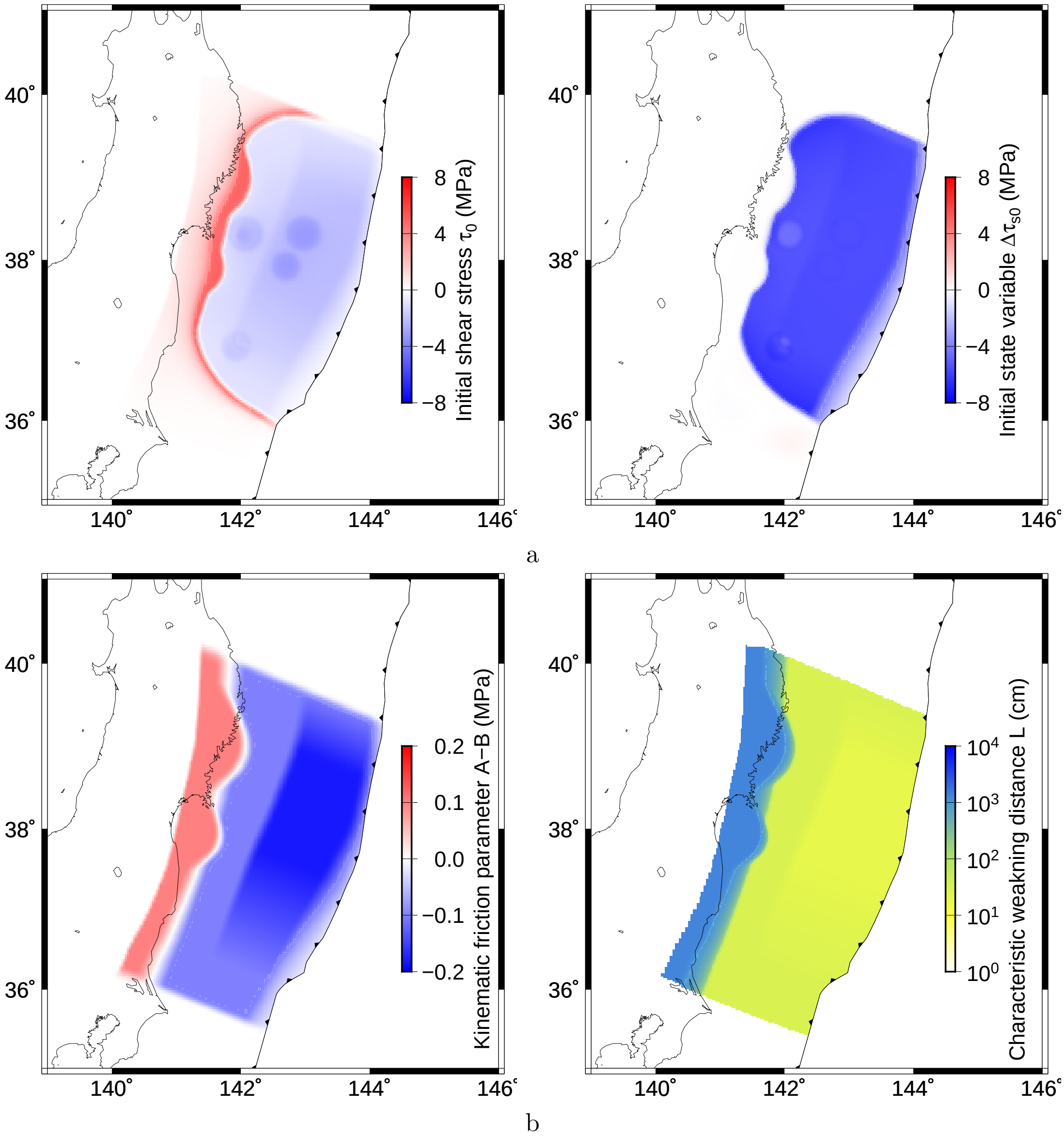

Figure 5: (Extended Data) The variables and parameters taken over from Nakata et al.[25]. a, Shear stress and state variable. Initial value of slip velocity V_i is calculated using these values with (8). b, Frictional parameters.

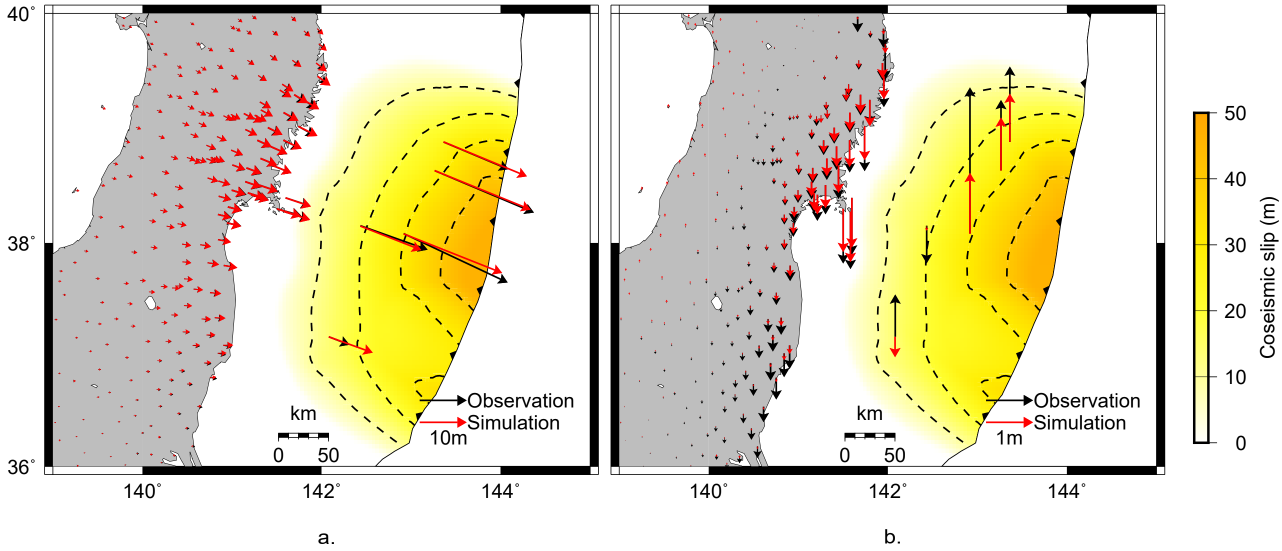

Figure 6: (Extended Data) Input coseismic slip based on Nakata *et al.*[25] and comparison between computed and observed coseismic displacement, including both the land[15, 43] and seafloor stations[44].

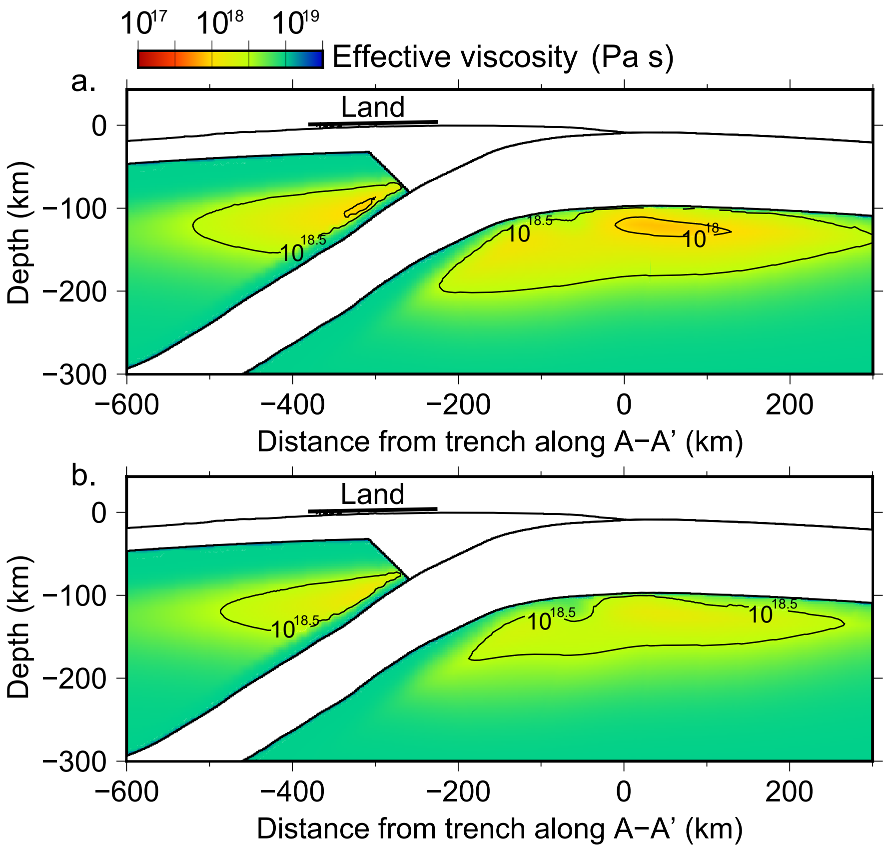

Figure 7: (Extended Data) Distributions of effective viscosity at a, 1 year and b, 2.8 years after the earthquake. The distribution of viscosity varies with time.

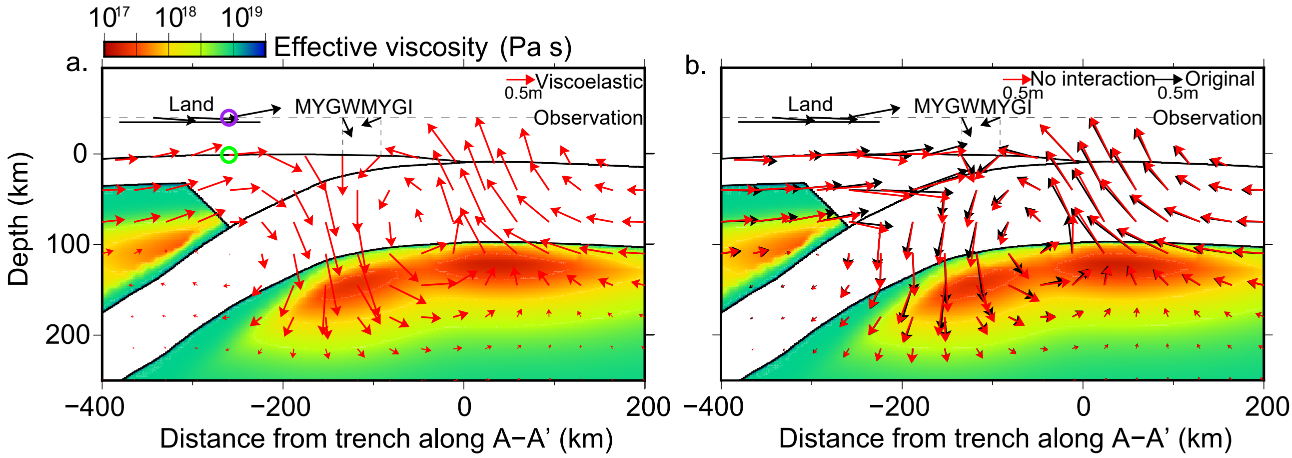

Figure 8: (Extended Data) a, Power-law viscoelastic flow in 2.8 years without considering afterslip in the cutting plane of the station MYGI and MYGW. In the green circle, uplift is significantly smaller than in the case with afterslip, shown in Fig. 4a. b, Comparison between the total 2.8-year displacement in the original simulation (black, the same as "total" in Fig. 4) and the result without interaction between afterslip and viscoelastic flow (red). As a result, the computed horizontal displacements are reduced by more than 10 % in some of the land stations, and the vertical ones change by more than 30 % in many stations in both of the land and the seafloor.

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