Asthenosphere flow modulated by megathrust earthquake cycles

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Abstract

Subduction megathrusts develop the largest earthquakes, often close to large population centers. Understanding the dynamics of deformation at subduction zones is therefore important to better assess seismic hazards. Here, I develop consistent earthquake cycle simulations that incorporate localized and distributed deformation based on laboratory-derived constitutive laws by combining boundary and volume elements to represent the mechanical coupling between megathrust slip and solid-state flow in the oceanic asthenosphere and in the mantle wedge. The model is simplified, in two dimensions, but may represent a reference to interpret seismic and geodetic data. Megathrust earthquakes and slow-slip events modulate the strain-rate in the upper mantle, leading to large variations of effective viscosity in space and time and a complex pattern of surface deformation. While fault slip and flow in the mantle wedge generate surface displacements in the same, i.e., seaward, direction, the viscoelastic relaxation in the oceanic asthenosphere generates transient surface deformation in the opposite, i.e., landward, direction above the rupture area of the mainshock. Aseismic deformation above the seismogenic zone may be challenging to record, but it may reveal important constraints about the rheology of the subducting plate.

Introduction

The subduction of oceanic slabs beneath continents generates some of the largest earthquakes due to a wide, low-angle section cross-cutting the continental crust, where the frictional resistance is unstable (*Blanpied et al.*, 1995; *Dieterich*, 1979; *Nakatani*, 2001). The largest historical earthquakes, the 1960 Mw 9.5 Valdivia, Chile (*Moreno et al.*, 2011), 1964 Mw 9.2 Alaska (*Plafker*, 1965), 2004 Mw 9.2 Sumatra (*Ishii et al.*, 2005; *Vigny et al.*, 2005), and the 2011 Mw 9.1 Tohoku, Japan (*Fujiwara et al.*, 2011) earthquakes all developed at subduction zones around the Rim of Fire and many remaining seismic gaps deserve close attention, notably the Nankai trough in Japan (*Hyodo and Hori*, 2013), the Mentawai

islands in Sumatra (*Philibosian et al.*, 2017; *Rubin et al.*, 2017; *Sieh et al.*, 2008), the Guerrero section in Mexico (*Astiz et al.*, 1987; *Singh et al.*, 1981), the Cascadia in North America (*Goldfinger et al.*, 2003; *Heaton and Hartzell*, 1987), the Arakan in Myanmar (*Cummins*, 2007), the Makran in Iran (*Heidarzadeh and Kijko*, 2011; *Heidarzadeh et al.*, 2008; *Jackson and McKenzie*, 1984) and others elsewhere (*McCann et al.*, 1979; *Thatcher*, 1989; *Van Dissen and Berryman*, 1996).

Understanding the mechanics of earthquake production at subduction zones is key to better prepare for and mitigate seismic hazards. The magnitude of earthquake is in part controlled by the rheology of the surrounding rocks, as megathrust earthquakes preferentially initiate and propagate in cold, strong rocks. A wide range of fault slip styles have now been identified down-dip megathrusts, including creep, slow-slip events, very-low frequency earthquakes, tsunami earthquakes, typical megathrust earthquakes, and giant ruptures (*Araki et al.*, 2017; *Baba et al.*, 2018; *Ide*, 2012; *Kato and Nakagawa*, 2014; *Nakamura*, 2017; *Nakano et al.*, 2018; *Obara et al.*, 2004; *Plourde et al.*, 2015; *Radiguet et al.*, 2012; *Rogers and Dragert*, 2003; *Suenaga et al.*, 2016; *Toh et al.*, 2018; *Wallace and Beavan*, 2006). The style of rupture is dictated by the evolution of the frictional resistance during slip (*Collettini et al.*, 2011; *Leeman et al.*, 2016; *Mele Veedu and Barbot*, 2016; *Scuderi et al.*, 2017), the largest earthquakes probably involving strong weakening (*Noda and Lapusta*, 2013; *Sone and Shimamoto*, 2009; *Toro et al.*, 2004), but the rheology of country rocks may also play an important role (*Brantut et al.*, 2016; *Fagereng and Sibson*, 2010; *Goswami and Barbot*, 2018, in press; *Noda and Shimamoto*, 2010).

Subduction is thought to be permitted by a low viscosity asthenosphere that allows the rigid tectonic plates to float on top relatively underformed (*Burke*, 2011). However, the mechanical properties of the oceanic asthenosphere remain controversial, including the distribution of water, grain size, and the rheological characteristics of the lithosphere-asthenosphere boundary (*Mehouachi and Singh*, 2018). The rheological structure of the mantle wedge is even more uncertain, as the region exhibits a complex pattern of metamorphism, dehydration, temperature, and small-scale convection (*Wada and Wang*, 2009). Laboratory rock experiments constrain the rheological properties of olivine (*Karato and Jung*, 2003; *Mei and Kohlstedt*, 2000) and serpentinite (*Hilairet et al.*, 2007; *Reinen et al.*, 1991) well, but the in situ conditions remain elusive. As a result, there is no consensus on the effective viscosity at steady-state, the water content (and its spatial variations), and the pathways to arc volcanism (*Hu et al.*, 2014; *Lee and Wada*, 2017; *Ohzono et al.*, 2012; *Shibazaki et al.*, 2016) in the backarc.

Large earthquakes induce a significant stress change in the surrounding lithosphere (e.g., *Barbot et al.*, 2008; *Masuti et al.*, 2016; *Qiu et al.*, 2018; *Rollins et al.*, 2015; *Rousset et al.*, 2012, and references therein), leading to a transient acceleration of viscoelastic flow in the asthenosphere that is detectable in adequately designed geodetic networks (e.g., *Sathiakumar et al.*, 2017). The postseismic deformation provides important constraints on distributed deformation at short time scales that in principle can provide additional insight into the constitutive properties and in situ conditions in the upper mantle (*Bedford*

et al., 2016; *Broerse et al.*, 2015; *Govers et al.*, 2017; *Hu et al.*, 2014; *Klein et al.*, 2016; *Li et al.*, 2017; *Masuti et al.*, 2016; *Muto et al.*, 2016; *Pollitz et al.*, 2006; *Wang et al.*, 2012, and references therein).

While there has been much progress in our understanding of rock mechanics from laboratory experiments (*Brantut et al.*, 2011; *Ferri et al.*, 2010; *Han et al.*, 2007; *Hirth and Guillot*, 2013; *Hirth and Kohlstedt*, 2003; *Morrow et al.*, 2000, and references therein), producing consistent models of deformation that treat brittle and ductile behaviors consistently with realistic material properties still constitutes a challenge. This technical limitation hinders our understanding of the mechanics of the lithosphere-asthenosphere system across subduction zones. The deformation that accompanied and followed the 2011 Mw 9.2 Tohoku earthquake was captured across a wide frequency band by a large seismogeodetic network (*Hooper et al.*, 2013; *Nishimura et al.*, 2011; *Simons et al.*, 2011; *Wright et al.*, 2012; *Yagi and Fukahata*, 2011), including offshore (*Iinuma et al.*, 2016, 2012; *Tomita et al.*, 2017). The post-seismic deformation that followed the Tohoku earthquake seemed to contradict intuition. Seafloor geodesy data showed convincingly that the rupture area moved towards the ocean, as opposed to the expected landward direction for thrust-compatible motion. *Sun et al.* (2014) showed that this deformation was the hallmark of a low-viscosity oceanic asthenosphere responding to the coseismic stress perturbation. Recently, *Suito* (2017) and *Noda et al.* (2018) developed sophisticated models to decrypt the contributions of the asthenosphere and fault slip in surface observations following the Tohoku earthquake. These observations and modeling efforts demonstrate that more integrated models are needed to better understand and predict the deformation of the lithosphere.

Admittedly, subduction zones present some of the most challenging modeling settings in tectonophysics, including lateral variations of constitutive properties (*Hirahara*, 2002; *Muto*, 2011; *Muto et al.*, 2013, 2016; *Wang*, 2007) and important contributions from brittle and ductile deformation (*Freed et al.*, 2017). The goal of this paper is to produce a simple reference model of a typical ocean-continent subduction zone to discuss the predictions of deformation throughout the seismic cycle based on reasonable assumptions about frictional and viscoelastic properties. This is accomplished using the integral method, combining boundary- and volume-elements to resolve all phases of the seismic cycle under rate-and-state friction - with the notable exception of the radiation of seismic waves - and the mechanical coupling between brittle and ductile deformation. The approach was introduced by *Lambert and Barbot* (2016) to model the seismic cycle in the lithosphere-asthenosphere system on long transform faults under the anti-plane strain approximation. It was extended to incorporating shear heating and heat diffusion by *Goswami and Barbot* (2018, in press). Here, I develop the method further to model the seismic cycle on long thrust faults in conditions of in-plane strain. The method used here should not be confused with finite-element modeling (e.g., *Aagaard et al.*, 2013; *Malservisi et al.*, 2001; *Shibazaki et al.*, 2007), where the governing equations are projected on basis functions and where the numerical solution is obtained by solving a large algebraic system. With the integral method, the solution is analytic, based on

solving the governing equations exactly for a volume element, resulting in a more accurate and more numerically efficient solution. The numerical approximation lies in the spatial discretization of the fault and the surrounding volume. The displacement and stress kernels for a volume element can be used to directly image the anelastic deformation in Earth's interior (*Moore et al.*, 2017; *Qiu et al.*, 2018; *Tsang et al.*, 2016) and to simulate forward models of deformation (*Goswami and Barbot*, 2018, in press; *Lambert and Barbot*, 2016). The displacement and stress kernels for distributed deformation introduced by *Barbot et al.* (2017) are limited to a rectilinear geometry. To overcome this limitation, *Barbot* (2018) provided expressions for the displacement and stress kernels of triangle and tetrahedral elements, which is better suited for curvilinear meshing of topologically complex structures, such as subduction zones.

In the next section, I introduce the physical assumptions for modeling the seismic cycle and the viscoelastic flow in the upper mantle. Then, I describe the modeled dynamics of earthquakes and slow-slip events on the megathrust and how they modulate the effective viscosity in the upper mantle. I then describe the kinematics of surface deformation and the contributions of fault slip and viscoelastic flow throughout multiple earthquake cycles. The model reveals that viscoelastic flow in the oceanic asthenosphere creates transient landward displacements at the surface immediately above large earthquake ruptures. The large stress perturbation occasioned by earthquake ruptures induces a transient low-viscosity flow in the postseismic period followed by re-hardening.

Subduction dynamics with the integral method

The dynamics of the lithosphere during the seismic cycle is typically modeled with finite elements, a technique that allows realistic variations in elastic and viscoelastic properties and nonlinear constitutive laws. This approach has brought much insight into the rheology of plate boundaries at subduction zones (e.g., *Hu et al.*, 2014, 2016; *Klein et al.*, 2016; *Kyriakopoulos and Newman*, 2016; *Masterlark*, 2003; *Wang*, 2007), transform boundaries (e.g., *Allison and Dunham*, 2017; *Freed and Bürgmann*, 2004; *Masterlark and Wang*, 2002; *Takeuchi and Fialko*, 2013), and collision zones (*Castaldo et al.*, 2017; *Cattin and Avouac*, 2000; *Liu et al.*, 2016; *Wang and Fialko*, 2018). While finite-element modeling has proven versatile for forward and inverse modeling, notably using the adjoint method (*Agata et al.*, 2017; *Crawford et al.*, 2016), resolving the details of fault dynamics with this technique requires out-of-the-ordinary numerical resources and methods (*Agata et al.*, 2014; *Ichimura et al.*, 2016; *Uphoff et al.*, 2017). Viscoelastic simulations have also exploited the correspondence principle, whereby heterogeneous effective elastic properties are mapped into the viscoelastic properties by virtue of the Fourier or Laplace transforms (*Chanard et al.*, 2018; *Fukahata and Matsu'ura*, 2006; *Pollitz*, 1992, 1997; *Smith and Sandwell*, 2004). While elegant, this approach is limited to linear viscoelastic properties and often to vertical stratification of material properties, and ignores the coupling to brittle deformation, except for the work of *Kato* (2002). Meanwhile, fault

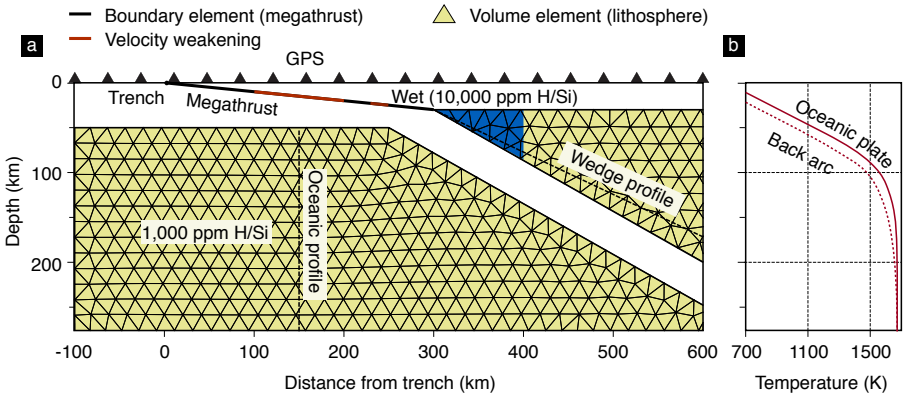

Figure 1: Schematic of a two-dimensional subduction zone model in plane strain with the integral method. a) Geometry of the subduction zone model, mesh elements, and physical properties. Fault slip is represented with boundary elements (segments); plastic strain within the lithosphere is represented with volume elements (yellow triangles). Earthquakes and slow-slip events occurs in velocity-weakening fault patches (red line). The mantle wedge corner (blue region) is wetter than the surrounding mantle, with $C_{\mathrm{OH}} = 10,000\,\mathrm{ppm}$ H/Si. The region close to the subducting slab interface is elastic and not meshed. The dashed lines indicate the location of the strain-rate and effective viscosity profiles in Figures 3 and 2. The displacement history is evaluated at the surface, simulating the measurements of geodetic stations (GPS, black triangles). b) Vertical temperature profiles assumed in the oceanic plate and the backarc region. The physical properties in the upper mantle are vertically stratified, except for different temperatures and water contents in the oceanic asthenosphere and in the mantle wedge.

dynamics is efficiently simulated with the boundary-integral method (*Ando*, 2016; *Lapusta and Liu*, 2009; *Liu and Rice*, 2005; *Tse and Rice*, 1986), which is most efficient because only the fault surface is sampled numerically, the rest of the domain being accounted for analytically. It is natural to augment the boundary-integral method with volume elements to represent distributed deformation (*Barbot*, 2018; *Barbot et al.*, 2017; *Goswami and Barbot*, 2018, in press; *Lambert and Barbot*, 2016). This alternative approach, the integral method, shares the advantages of the boundary-integral method but incorporates multiphysics, distributed deformation.

The subduction model consists in a trench-perpendicular cross-section of the half-space that includes the megathrust and the surrounding viscoelastic upper mantle (Figure 1). The fault is assumed planar, extends from the trench to 300 km towards the volcanic arc, from 0 to 30 km depth, and is discretized with $N = 200$ finite-width patches (*Okada*, 1992). The oceanic asthenosphere is represented by an unstructured simplex mesh (*Persson and Strang*, 2004) of triangular elements (*Barbot*, 2018) confined in a polygon that mimics the shape of the subducting slab. The mantle wedge is represented by another set of triangular elements confined in a triangle region delimited by the continental

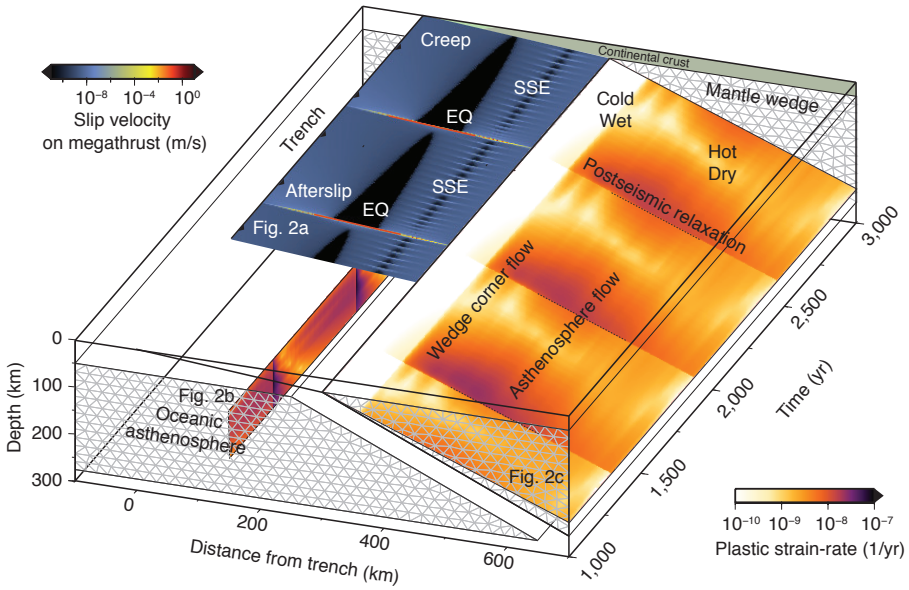

Figure 2: Evolution of the dynamics of fault slip and viscous strain in space and time in a two-dimensional, plane-strain subduction zone model. Earthquakes (EQ) and slow-slip events (SSE) occur on a long megathrust (low-angle fault with colors indexed by the instantaneous slip velocity) cross-cutting the continental crust. Viscoelastic flow (colored by strain rate) in the upper mantle, modeled with triangular elements (grey mesh), is modulated by the seismic cycle, with shorted postseismic transients in the oceanic asthenosphere and long periods of strain acceleration in the mantle wedge.

crust (the upper boundary is close to the brittle-ductile transition), the downgoing slab and an arbitrary lower limit of 300 km below which little viscoelastic deformation is expected. All triangles have sides of ~ 20 km, resulting in 907 triangular elements overall. The models with a finer mesh show similar results, indicating numerical convergence.

The dynamics of fault slip is controlled by rate-and-state friction where the frictional resistance follows (*Dieterich*, 1979; *Ruina*, 1983)

$$\tau = \left[\mu_0 + a \ln \frac{V}{V_0} + b \ln \frac{\theta V_0}{L}\right] \bar{\sigma} \ , \tag{1}$$

with the aging law

$$\dot{\theta} = 1 - \frac{V\theta}{L} \ , \tag{2}$$

where a is a non-dimensional parameter that controls the fracture energy and the velocity dependence of friction, b is another non-dimensional parameter that controls the degree of weakening and the dependence on the state variable, V_0 is a reference slip velocity, and L is a characteristic weakening distance that

controls the critical nucleation size (*Rubin and Ampuero*, 2005; *Ruina*, 1983)

$$h^* = \frac{GL}{(b-a)\bar{\sigma}} \ . \tag{3}$$

Fault regions with $b - a < 0$ are stable, but fault regions of characteristic size R may generate spontaneous slip instabilities if $R > h^*$ (e.g., *Lapusta and Barbot*, 2012). For example, *Liu and Rice* (2005) showed that slow-slip events emerge spontaneously for $R/h^* \sim 1$ and *Mele Veedu and Barbot* (2016) established that period-doubling sequences of slow and fast ruptures occur for specific values of R/h^* close to unity. The fault is loaded with a background rate of $V_l = 10^{-9}$ m/s. I define the seismogenic zone on the megathrust by the region of the fault extending from 10 to 20 km that intersects the continental upper- and mid-crust. Because of the low dip angle of the megathrust, the resulting seismogenic zone is about 100 km wide, large enough to generate elasto-dynamic ruptures. While other models can explain long-term and short-term slow-slip events (e.g., *Goswami and Barbot*, 2018, in press; *Matsuzawa et al.*, 2010), I follow *Liu and Rice* (2005) and model long-term slow-slip events as stable-weakening regions ($R/h^* \sim 1$) extending from 23 to 25 km depth (see Table 1).

In the upper mantle, the rheology of solid-state flow is dominated by the strength of olivine, the weakest and most abundant mineral. I assume that the viscoelastic flow is accommodated by a combination of diffusion creep and dislocation creep at steady-state, where the norm of the strain-rate follows

$$\begin{aligned} \dot{\epsilon} = A_1 \left(C_{\mathrm{OH}}\right)^{r_1} \exp\left(-\frac{Q_1 + p\,\Omega_1}{RT}\right) \sigma^n \\ + A_2 \left(C_{\mathrm{OH}}\right)^{r_2} d^{-m} \exp\left(-\frac{Q_2 + p\,\Omega_2}{RT}\right) \sigma \ , \end{aligned} \tag{4}$$

where $\dot{\epsilon}$ is the norm of the plastic strain-rate, C_{OH} is the water content, p is the overburden, T is the temperature, R is the universal gas constant, and σ is the norm of the deviatoric stress. Dislocation creep is characterized by the activation energy Q_1 and activation volume Ω_1, the water sensitivity exponent r_1, the prefactor A_1, and the stress exponent $n = 3.5$. Diffusion creep is associated with the activation energy Q_2 and activation volume Ω_2, the water sensitivity exponent r_2, the grain size $d = 1$ mm, the grain size sensitivity exponent m, and the prefactor A_2. In the oceanic plate, the temperature follows the cooling half-space model with a plate age of 2×10^{15} s, i.e., ~ 60 Myr and a basal mantle temperature of 1673 K. I use the constitutive properties of wet olivine with with 1,000 ppm H/Si reported by *Hirth and Kohlstedt* (2003) and summarized in Table 1. Viscoelastic flow is driven by a background horizontal strain rate of $\dot{\epsilon}^0_{22} = 10^{-15}$ /s.

In the mantle wedge, I assume that deformation is accommodated by diffusion creep and dislocation creep following (4) with the same constitutive parameters as in the oceanic mantle. However, I assume a large water content $C_{\mathrm{OH}} = 10,000$ ppm H/Si in the mantle wedge corner up to 400 km away from the trench, associated with the dehydration of peridotite and arc volcanism, and

a damped water content of $C_{\mathrm{OH}} = 1,000$ ppm H/Si elsewhere (Figure 1). I also build a thermal profile assuming a slightly older plate age of ~ 70 Myr. This is obviously a simplification, but it reflects how the remaining uncertainties on the mantle wedge rheology still limit our understanding of this important region. For example, *Muto* (2011) and *Klein et al.* (2016) assume a lower viscosity at steady-state in the mantle wedge than in the oceanic mantle, but *Muto et al.* (2013) and *Muto et al.* (2016) consider the opposite. I also ignore the low-viscosity region below the volcanic arc (*Hu et al.*, 2014; *Muto et al.*, 2016) as it mainly affects the vertical displacement in the near field.

I simulate the evolution of traction, slip-rate and the state variable of the aging law on the megathrust and the three independent components of the stress tensor in the upper mantle using the integral method (*Goswami and Barbot*, 2018, in press; *Lambert and Barbot*, 2016) over multiple earthquake cycles. I use the four/fifth-order accurate Runge Kutta method with adaptive time steps to model all stages of the seismic cycle within the radiation damping approximation. At each time step, I determine the slip acceleration using (1), the rate of the state variable using (2), and the strain-rate components $\dot{\epsilon}_{22}$, $\dot{\epsilon}_{23}$, and $\dot{\epsilon}_{33}$ following (4). To account for the full coupling of all the deformation processes, I convolve the rates of deformation with the traction and stress kernels and determine the resulting stress rates in the half-space. The rate of shear traction in the dip direction on the megathrust is obtained with

$$\dot{\tau} = K(V - V_{\mathrm{l}}) + \sum_{\beta} M_{\beta}(\dot{\epsilon}_{\beta} - \dot{\epsilon}^{0}_{\beta}) \ , \tag{5}$$

where K is the matrix of self interactions, the summation is over $\beta = 22, 23, 33$, and M_{22}, M_{23}, and M_{33} are the matrices of shear traction due to a unit strain in the volume elements for the components 22, 23, and 33, respectively. The rate of stress in the volume elements is given by

$$\dot{\sigma}_{\alpha} = J_{\alpha}(V - V_{\mathrm{l}}) + \sum_{\beta} L_{\alpha\beta} \left(\dot{\epsilon}_{\beta} - \dot{\epsilon}^{0}_{\beta}\right) \ , \tag{6}$$

where α takes the values 22, 23, and 33, J_{α} is the stress caused by fault slip, which will cause postseismic relaxation, and $L_{\alpha\beta}$ are the matrices for stress change in the component α to due strain in the volume elements for the component β (see Appendix A). The stress interactions matrices are calculated with analytic solutions (*Barbot*, 2018). The simulation includes the nucleation, propagation, and arrest of large seismogenic-zone earthquakes and long-term slow-slip events, and the postseismic relaxation of the stress perturbation by afterslip on the megathrust and viscoelastic flow in the upper mantle. I simulate the deformation for 3,000 years, including 6 earthquakes, and about 120 slow-slip events. On my mid-2012, dual-core processor laptop with 8 Gb of memory, the calculation of the Green's function takes two minutes. The simulation requires about 50,000 time steps, which take 45 minutes to compute.

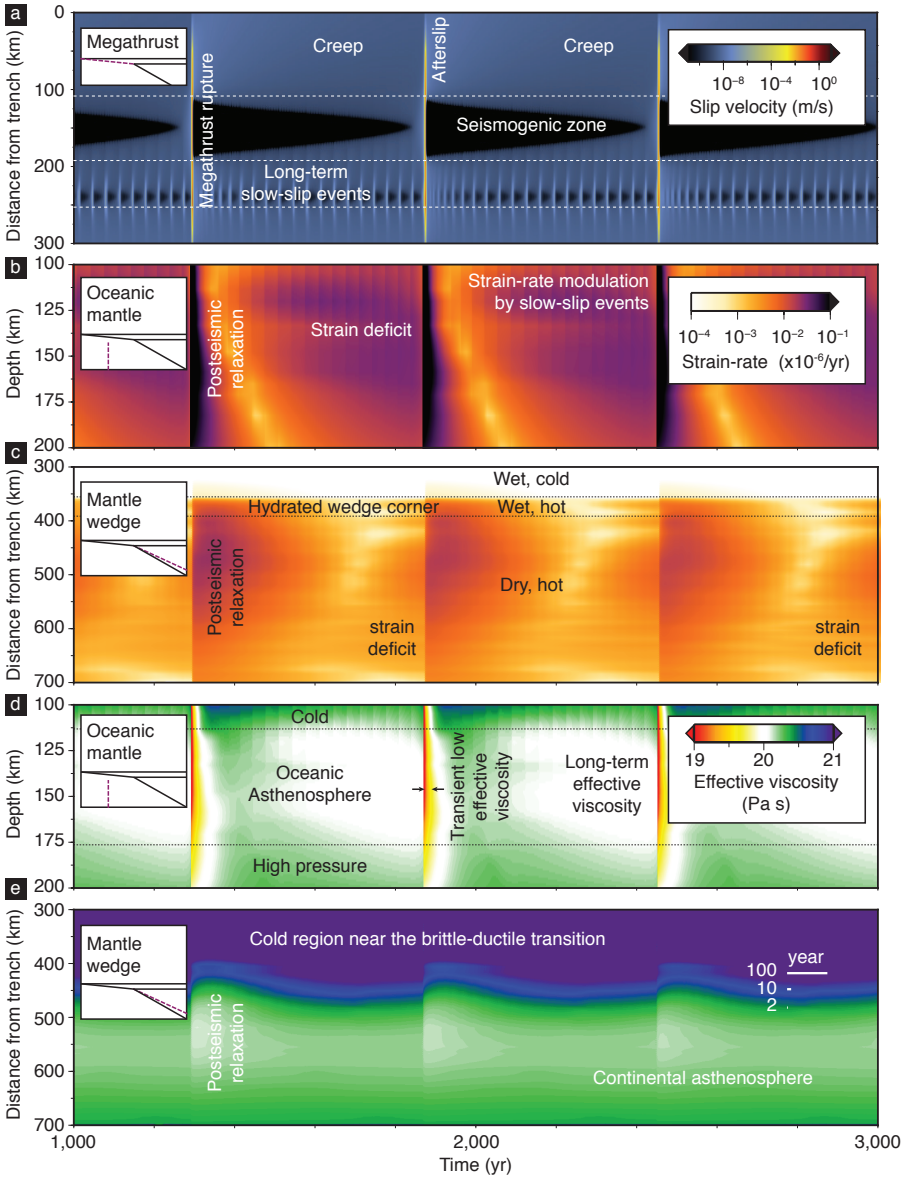

Figure 3: Time series of slip velocity on the megathrust, and strain-rate and effective viscosity in the upper mantle. a) Earthquake break all of the seismogenic zone every 500 yr and long-term slow-slip events emerge every 25 yr on average. b) The plastic flow in the oceanic asthenosphere and c) mantle wedge is modulated by the seismic cycle. d) In the oceanic asthenosphere, the nonlinear dependence to stress of dislocation creep leads to rapid postseismic transients with an effective viscosity reduced by at least an order of magnitude. e) Postseismic viscoelastic flow in the mantle wedge concentrates in a region between 450 and 600 km from the trench, and is little affected by the presence of water below the brittle-ductile transition.

Dynamics of anelastic deformation at subduction zones

I describe the dynamics of fault slip and viscoelastic flow in the two-dimensional subduction zone model during the seismic cycle. With the combination of parameters discussed in the previous section, I obtain typical megathrust earthquakes that rupture all the seismogenic zone every $\sim 500\,\mathrm{yr}$. The long-term slow-slip events emerge every $\sim 25\,\mathrm{yr}$, but their recurrence times are modulated by the earthquake cycle (Figures 2 and 3). Following each large rupture, afterslip propagates up-dip towards the trench and down-dip into the slow-slip region. The slow-slip events are accelerated for about 150 yr, after which they resume their natural recurrence pattern (Figure 3a). The accretionary prism undergoes creep, but this is a simplifying modeling assumption, as in reality this region undergoes a complex faulting style (*Araki et al.*, 2017; *Hetland and Simons*, 2010; *Hubbard et al.*, 2015; *Nakano et al.*, 2018; *Suenaga et al.*, 2016).

Each large earthquake induces a stress perturbation in the surrounding rocks that triggers a transient flow acceleration in the upper mantle. In the oceanic asthenosphere (dashed vertical profile in Figure 1), the postseismic relaxation takes 20 to 200 years, depending on the amplitude of the stress perturbation and the local effective viscosity (Figure 3b). After this, the flow continues at rates lower than steady state to preserve the long-term strain-rate. The accumulation of slow-slip events gradually accelerates viscoelastic flow in the oceanic asthenosphere, suggesting a possible mechanical coupling between the two mechanisms. During the postseismic transient the effective viscosity reduces from its background, steady-state value, by at least one order of magnitude, with a short excursion below $\eta_{\mathrm{eff}} = 10^{19}\,\mathrm{Pa\,s}$. This is compatible with several studies that require transient creep to explain the sudden drop of effective viscosity immediately after the earthquake (e.g., *Hu et al.*, 2016; *Klein et al.*, 2016; *Sun et al.*, 2014). It is possible that nonlinear flow laws, not transient creep, are responsible for this effect. *Masuti et al.* (2016) found that a combination of both transient creep and nonlinear flow laws are required to explain the geodetic data following the 2012 Mw 8.6 Indian Ocean earthquake and *Qiu et al.* (2018) found that linear transient creep was the simplest way to explain the last decade of geodetic data along the Sumatran subduction zone (not excluding nonlinear transient creep). A more thorough comparison of the candidate rheological models is required to address the constitutive properties of the subducting slab.

The flow in the mantle wedge (dashed profile in Figure 1) is also modulated by the seismic cycle. With the rheological parameters chosen, the acceleration of viscoelastic flow is less pronounced than in the oceanic asthenosphere (Figure 3c,d). The strain rates are maximum between 450 and 600 km from the trench. The presence of a large water content in the mantle wedge corner does not lead to rapid flow there, presumably due to the dominant effect of low temperatures. It is possible that ductile or semi-brittle shear zones below the brittle-ductile transition afford faster relaxation transients (*Goswami and Barbot*, 2018, in press; *Takeuchi and Fialko*, 2013). More insight into the spatial

distribution of serpentinized rocks and into the pathways of water and partial melt is needed to better constrain the rock rheology near the mantle wedge corner.

As recent studies demonstrate (*Hu et al.*, 2016; *Noda et al.*, 2018; *Suito*, 2017; *Sun et al.*, 2014), the surface deformation caused by the interaction of fault slip and mantle flow continues to surprise. In Figure 4, I describe the evolution of the trench-perpendicular surface displacement deficit, i.e, the difference between the displacement and the long-term average, throughout the seismic cycle. In a post-processing step, I establish the contributions of fault slip, flow in the oceanic lithosphere, and flow in the mantle wedge to the surface displacements in space and time. Above the megathrust, the displacement is dominated by fault slip, but its effect is reduced over time by the combined effect of slow-slip events and relocking. All of earthquakes, slow-slip events, afterslip, and creep create seaward displacement. Postseismic relaxation in the oceanic asthenosphere is the only mechanism that creates significant landward displacements above the megathrust. These accumulate within a few years following large earthquakes and largely recede late in the seismic cycle. The flow in the oceanic asthenosphere also creates landward displacements in the outer rise and on land (i.e., more than 300 km from the trench). With the modeling assumptions presented in the previous section, the viscoelastic flow in the mantle wedge creates a lower-amplitude postseismic relaxation than flow in the oceanic lithosphere, but it still contributes significantly to the surface displacements on land. There, all sources of deformation produce displacements in the same direction. The amplitude of these different contributions would be largely affected by, among others, the size of the earthquakes, the age of the subducting plates, and the rheology of the mantle wedge. While the patterns of the model are not expected to change significantly within modest variations from the modeling assumptions, some adjustments may be needed to fit particular tectonic contexts and reduce local geophysical data.

Conclusions

I describe how the integral method can be used to simulate the seismic cycle at subduction zones to couple fault slip and viscoelastic strain. The approach is computationally efficient, and may resolve all the phases of the seismic cycle including off-fault deformation, but excluding the radiation of seismic waves. The model integrates laboratory-derived constitutive laws for friction and plastic flow. While more data are needed to constrain the rheology of the mantle wedge in particular, the model may constitute a reference point to understand the dynamics of subduction zones, i.e., predict quasi-static deformation, prepare seismo-geodetic networks, and test the merit of alternate models.

The postseismic relaxation in the oceanic asthenosphere that follows large earthquakes is characterized by a transient flow with a low effective viscosity explained by the nonlinear stress dependence of dislocation creep. Flow in the oceanic asthenosphere creates landward surface displacements above the

coseismic rupture and seaward displacements away from it. Offshore geodetic data are admittedly challenging to obtain, despite recent progress (*Maksymowicz et al.*, 2017; *Tomita et al.*, 2017; *Wallace et al.*, 2016; *Yokota et al.*, 2016), but these measurements may be most effective to constrain the rheology of the subducting slab and fault processes near the trench. The rheological properties of the mantle wedge are less well constrained, but viscoelastic flow in the backarc contributes significantly to postseismic deformation, producing displacement compatible with all other deformation mechanisms above the land.

While the modeling technique introduced here is still in its infancy, it represent a potentially efficient approach to model deformation in tectonically complex settings. Further applications of the integral method to three-dimensional problems may bring new insight into the mechanics of subduction zones.

Appendix A Finite element deformation in plane strain

The deformation in a half-space induced by uniform plastic flow of a volume element can be obtained analytically with the surface integral (*Barbot*, 2018)

$$u_i(\mathbf{x}) = 2\mu\,\epsilon_{jk}\int_{\partial\Omega} G_{ji}(\mathbf{x},\mathbf{y})\,n_k(\mathbf{y})\ \mathrm{dA}\ , \tag{7}$$

where $u_i(\mathbf{x})$ is the displacement field, μ is the shear modulus (not friction), ϵ_{ij} is the transformation strain (assumed deviatoric), $G_{ij}(\mathbf{x},\mathbf{y})$ is the Green's function for the displacement component j at coordinate $\mathbf{x}$ due to a force component i at coordinates $\mathbf{y}$, and $\partial\Omega$ is the surface of the volume element with normal vector n_i. I consider the deformation under the two-dimensional in-plane strain approximation caused by plastic flow within a triangular element (Figure 1). The deformation simplifies to

$$\begin{aligned}
u_2(x_2,x_3) = \int_{\partial\Omega} & G_{22}(x_2,x_3,y_2,y_3)\,(m_{22}n_2+\epsilon_{23}n_3) \\
& + G_{32}(x_2,x_3,y_2,y_3)\,(m_{32}n_2+m_{33}n_3)\ \mathrm{d}y_2\,\mathrm{d}y_3 \\
u_3(x_2,x_3) = \int_{\partial\Omega} & G_{23}(x_2,x_3,y_2,y_3)\,(m_{22}n_2+\epsilon_{23}n_3) \\
& + G_{33}(x_2,x_3,y_2,y_3)\,(m_{23}n_2+m_{33}n_3)\ \mathrm{d}y_2\,\mathrm{d}y_3\ ,
\end{aligned} \tag{8}$$

where, in general, $m_{ij} = \lambda\,\delta_{ij}\epsilon_{kk} + 2G\,\epsilon_{ij}$ is the moment density. Then, the stress field induced by plastic flow of a triangular element can be obtained by differentiation.

Figure 5 shows the three stress components σ_{22}, σ_{23}, and σ_{33} induced by plastic flow within a triangular element of the mesh used in Figure 1 for each of the strain components ϵ_{22}, ϵ_{23}, and ϵ_{33}. These stress interactions are calculated analytically (*Barbot*, 2018) for all the strain components of all volume elements and evaluated at the center of all triangular elements and fault patches, forming

the full matrices M_β and $L_{\alpha\beta}$, with $\alpha, \beta = 22, 23, 33$, in equations (5) and (6). As the geometry remains static, these matrices are computed only once, and the remaining calculation only involves matrix-vector products, making the integral method numerically efficient.

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Table 1: Summary of the physical parameters representing fault slip and upper mantle strain constrained from laboratory experiments (*Hirth and Kohlstedt*, 2003; *Nakatani*, 2001). Friction properties are for a granitic rock. Diffusion and dislocation creep properties are for wet olivine.

Region	Parameter	Symbol	Value	Remark
Megathrust				
	Shear modulus	G	30 GPa	
	Effective confining pressure	$\bar{\sigma}$	100 MPa	
	Static friction coefficient	μ_0	0.6	
	Steady-state parameter	a	1×10^{-3}	
		$b - a$	-4×10^{-3}	velocity-strengthening
	Evolution effect parameter		2×10^{-3}	seismogenic zone
			1×10^{-3}	slow-slip region
	Characteristic weakening distance	L	5 cm	slow-slip region
			50 cm	elsewhere
	Loading rate	V_l	10^{-9} m/s	
	Reference slip velocity	V_0	10^{-6} m/s	
	Shear wave speed	V_s	3×10^3 m/s	
Upper mantle				
	Driving strain rate	$\dot{\epsilon}^0_{12}$	10^{-15} s^{-1}	all other components 0.
	Basal mantle temperature	1673	K	
Dislocation creep				
	Pre-factor[a]	A_1	90	
	Power-law stress exponent	n	3.5	
	Activation energy	Q_1	480 kJ/mol	
	Activation volume	Ω_1	11×10^{-6} m^3/mol	
	Water fugacity exponent	r_1	1.2	
Diffusion creep				
	Pre-factor[b]	A_2	10^6	
	Grain size	d	10 mm	
	Grain size exponent	m	3	
	Activation energy	Q_2	335 kJ/mol	
	Activation volume	Ω_2	4×10^{-6} m^3/mol	
	Water fugacity exponent	r_2	1.0	

[a]The pre-factor for dislocation creep is in units of MPa^{-n} s^{-1} (ppm H/Si)$^{-r_1}$.
[b]The pre-factor for diffusion creep is in units of MPa^{-1} s^{-1} μm^m (ppm H/Si)$^{-r_2}$.

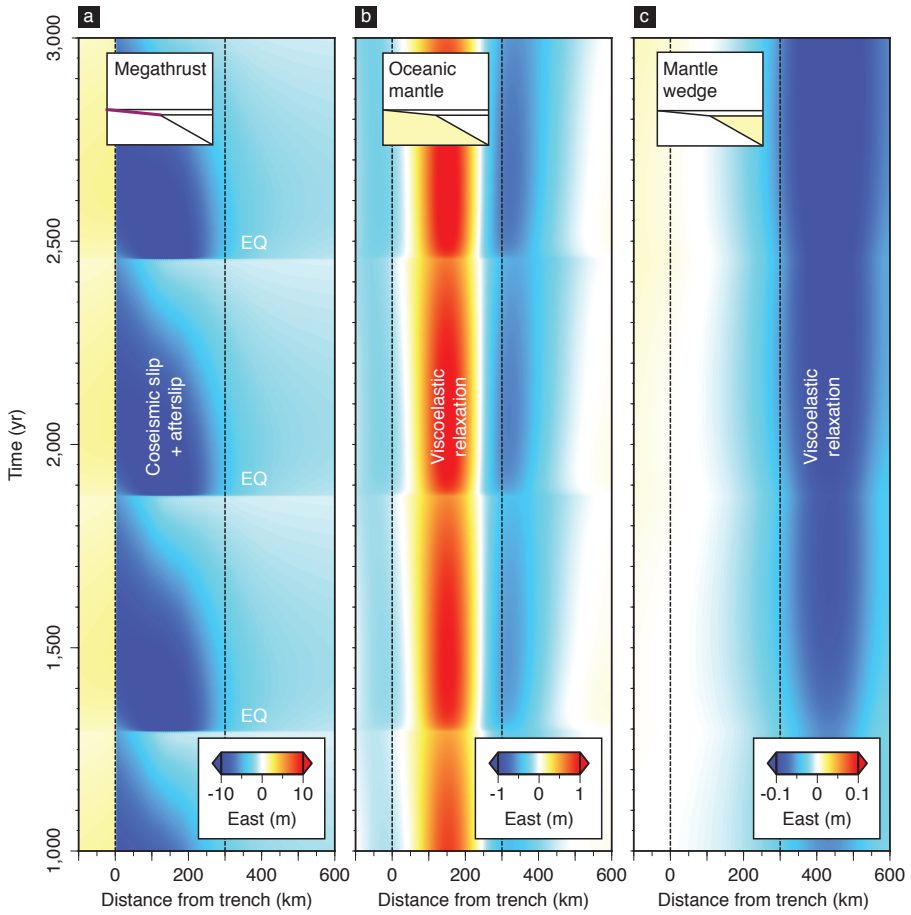

Figure 4: Contribution of (a) fault slip, (b) flow in the oceanic asthenosphere, and (c) flow in the mantle wedge to trench perpendicular surface displacements throughout the seismic cycle. (a) Fault slip produce seaward displacements above the megathrust and small landward displacement in the outer-rise. (b) Postseismic viscoelastic flow in the oceanic asthenosphere produces landward surface displacements above the coseismic rupture and mostly seaward displacements outside this region. (c) Postseismic relaxation in the mantle wedge is weaker under my modeling assumptions, and produces mostly seaward displacement above the land, 300 km and beyond from the trench. Due to the high viscosity in the mantle wedge, the postseismic relaxation following an earthquake still continues when a new one occurs.

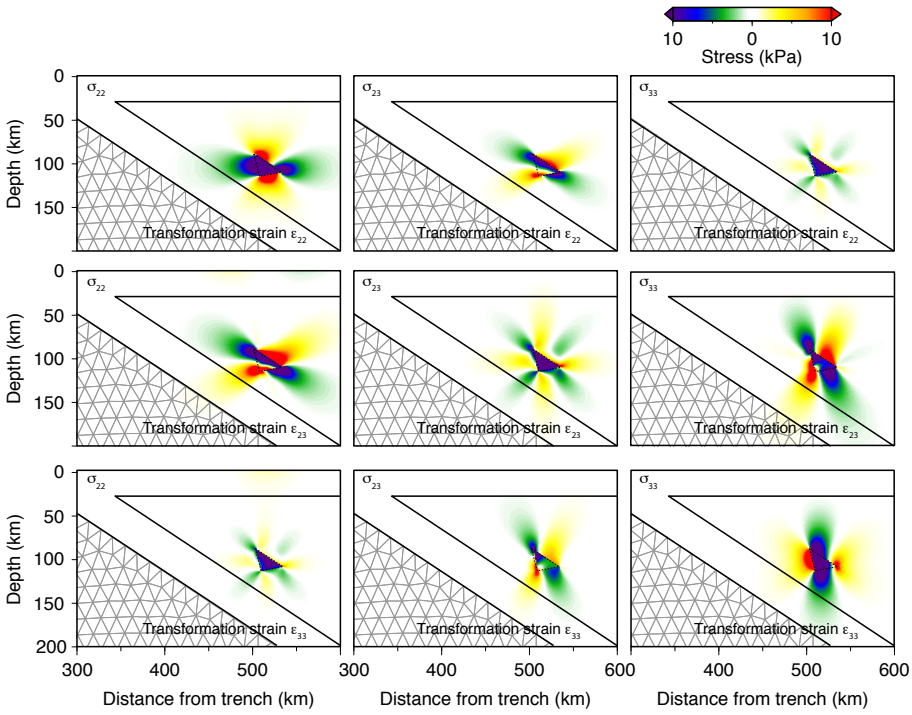

Figure 5: Stress fields induced by uniform plastic flow in a triangular volume element. From left to right, the columns show the stress component σ_{22}, σ_{23}, and σ_{33}. The rows, from top to bottom, are for the transformation strain component ϵ_{22}, ϵ_{23}, and ϵ_{33}. All transformation strain component have an amplitude of one microstrain. The rigidity is assumed $G = 30\,\mathrm{GPa}$.