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**Rayleigh wave H/V amplitude ratio measurement
using multicomponent ambient noise cross-correlations,
and its relationship to V_p/V_s**

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Abstract

The promise of passive seismology has increasingly been realized in recent years. Given the expense in installing and maintaining these seismic networks, it is important to extract as much information from the measurements as possible. In this context, the ellipticity or H/V amplitude ratio of Rayleigh waves can prove to be a valuable observable in ambient noise seismology due to its potential for constraining V_P structure, an advantage over group and phase-velocity dispersion, which are primarily sensitive to V_S . However, the suitability of the Rayleigh H/V ratio in noise-based studies depends on the accurate interpretation of measurements made on multi-component ambient-noise cross-correlations. We present a synthetic study that critically examines such measurements – commonly interpreted in terms of the Rayleigh H/V ratio – for realistic scenarios of spatially distributed and non-uniform noise sources. Using the Rayleigh-wave Green’s function in a laterally homogeneous medium, we rigorously model multi-component cross-correlation for arbitrary noise-source distributions and extract from them standard estimates of the H/V ratio. Variation of these measurements with V_P is studied empirically by brute-force simulation. We find that the measurements depart significantly from the theoretical Rayleigh wave H/V for the medium in

question, when noise sources are strongly directional or anisotropic. However, the sensitivity to V_P structure is comparable to that of the classic Rayleigh wave H/V. We also propose a new measurement for cross-correlations that has slightly greater sensitivity to V_P . Finally, uncertainty analysis on synthetic tests suggests that the ellipticity measurements can robustly resolve the V_p structure in the presence of noise (up to 10%). The primary utility of this method in scenarios when the noise level in the measured cross-correlations is significant ($\gtrsim 20\%$), is in being able to discern between different classes of models.

Keywords: *Ambient noise; Cross-correlations; H/V ratio; Rayleigh waves;*

1 Introduction

Ambient noise cross-correlation is a popular technique used to study shallow Earth structure using observations of the ambient seismic field on Earth, commonly known as ‘ambient noise’. The widespread use of this technique over the last 15 years has been largely based on the theoretical principle that the cross-correlation of a diffuse and equipartitioned noise wavefield recorded at two receivers, is proportional to the causal and anticausal far-field Green’s function between them (Shapiro and Campillo, 2004; Snieder, 2004; Weaver and Lobkis, 2004). Heavy pre-processing of raw noise records and averaging of cross-correlations over sufficiently long times is adopted in practice (Bensen et al., 2007), to recover ‘empirical Green’s functions’. Even so, most applications recover only the surface-wave Green’s function because the global noise field is dominated by ocean microseisms (Ardhuin et al., 2011, 2015) which originate near the Earth’s surface and strongly excite seismic surface waves. Since the traditional surface-wave measurements of phase and group velocity dispersion are dominantly sensitive to shear-wave velocity (V_S), ambient noise has primarily been used to study Earth’s V_S structure.

By contrast, recovery of P-wave velocities (V_P) from ambient noise is more challenging. Body waves, including P-waves, are hard to detect in ambient noise cross-correlations (due to weak excitation by shallow sources producing the noise wavefield) and the number of studies that have succeeded in doing so are limited (e.g. Roux et al., 2005a; Poli et al., 2012; Nakata et al., 2015, 2016; Liu et al., 2016; Saygin et al., 2017; Pedersen and Colombi, 2018; Wang et al., 2018). An alternative approach for studying V_P , that does not require P-wave observations, is to make use of the Rayleigh wave ellipticity or H/V ratio.

Rayleigh wave H/V ratio (ratio of horizontal to vertical component amplitudes) is an unconventional surface-wave observable that has a different sensitivity to Earth structure than the more widely used dispersion measurement. It has a shallower sensitivity to the three commonly used elastic parameters (V_P , V_S and density ρ ; Tanimoto and Rivera,

28 2008; Muir and Tsai, 2017) and has been used in inversions to constrain ρ and V_p (Lin
29 et al., 2012, 2014). Historically, the Rayleigh H/V ratio has seen limited use as a seis-
30 mological imaging tool, perhaps due to the difficulty in obtaining stable measurements
31 (Ferreira and Woodhouse, 2007; Tanimoto and Rivera, 2008). However, this has changed
32 in recent years, with many researchers exploring its potential for probing upper-crustal
33 structure, both in the context of classical earthquake seismology (Berbellini et al., 2016;
34 Lin et al., 2012; Ringler et al., 2019; Yano et al., 2009) and noise tomography (Lin et al.,
35 2014; Muir and Tsai, 2017). In the latter case, horizontal-to-vertical amplitude ratios
36 obtained from multi-component cross-correlations are interpreted as the Rayleigh-wave
37 H/V ratio, because the correlation signals are identified as containing Rayleigh waves
38 (their presence established by observations of elliptical particle motion) travelling be-
39 tween pairs of stations. By way of disambiguation, we note that such measurements
40 differ from the ‘H/V spectral ratio’ obtained from single-station noise records (Naka-
41 mura, 1989; Fäh et al., 2001) which may or may not be related to the Rayleigh wave
42 H/V ratio (Bonney-Claudet et al., 2006). In this paper, we are concerned only with
43 the Rayleigh-wave H/V ratio.

44 With the maturing of the field of ambient-noise seismology, it is important to rig-
45 orously analyse the estimation of Rayleigh H/V ratios from seismic-noise data. The
46 theoretical conditions for Green’s-function retrieval from noise correlations are often not
47 satisfied in reality due to non-stationary and heterogeneously distributed noise sources
48 (Stehly et al., 2006; Arduin et al., 2011, 2015; Ermert et al., 2017). Consequently,
49 a significant number of studies have warned of inaccurate empirical Green’s functions
50 that suffer from artefacts, as well as traveltime and amplitude errors (Fichtner, 2014;
51 Froment et al., 2010; Halliday and Curtis, 2008; Kimman and Trampert, 2010; Tsai,
52 2009, 2011; Yao and van der Hilst, 2009). It is therefore to be expected that Rayleigh
53 wave H/V ratios, which depend on relative amplitudes between components, are also
54 similarly affected. The work of Xu and Mikesell (2017) explicitly confirms biases in the
55 noise-correlation-derived Rayleigh-wave Green’s tensor arising from heterogeneous noise
56 sources.

57 In this study we do not invoke Green’s function interpretations for noise-correlation
58 signals; instead we model these signals rigorously for arbitrary spatial distributions of
59 noise sources (Section 2). To our knowledge, no previous study that models cross-
60 correlations in this manner has analysed the Rayleigh H/V measurement in detail.
61 Through a series of synthetic tests, we quantify the dependence of this measurement on
62 the anisotropy of noise-source distribution, as well as on model V_p , to assess its utility in
63 practice (Sections 3 and 4). Measurement uncertainties, estimated by adding Gaussian

64 noise to synthetic cross-correlation waveforms, shed light on the resolving power with
65 respect to V_P .

66 2 Methodology

67 2.1 Modelling theory

68 In this section, we describe how the multi-component CCs are synthesized and used to
69 obtain measurements of H/V ratio. In the frequency domain, ensemble-averaged CCs
70 under the assumption of spatially uncorrelated noise sources (Tromp et al., 2010; Sager
71 et al., 2018; Fichtner and Tsai, 2019) take the general form:

$$\mathcal{C}_{pq}(\mathbf{x}_\alpha, \mathbf{x}_\beta) = \int_{\oplus} d\xi G_{pi}^*(\mathbf{x}_\alpha, \xi) G_{qj}(\mathbf{x}_\beta, \xi) S_{ij}(\xi) \quad (1)$$

72 where $\mathbf{x}_\alpha, \mathbf{x}_\beta$ are the receiver locations; G_{mn} are elements of the Green's tensor satis-
73 fying $\mathcal{L}G_{mn}(\mathbf{x}, \xi) = \delta_{mn}\delta(\mathbf{x} - \xi)$ for a wave operator \mathcal{L} (subscripts m and n correspond to
74 the component of motion at the receiver location \mathbf{x} and the direction of the point force
75 at the source location ξ , respectively); S_{ij} is the power spectral density (PSD) matrix
76 of the noise sources, and the integral is over the Earth volume \oplus . In this study we
77 simplify eq. (1) with a few assumptions. First, noise sources are assumed to be present
78 only on the Earth's surface (e.g. Tromp et al., 2010), so the volume integral reduces to
79 a surface integral over its upper boundary Ω , and we can restrict our modelling to just
80 the surface-wave part of Green's function. Next, we consider noise sources acting in the
81 vertical (z) direction only, so the PSD matrix reduces to a single term, i.e. $S_{ij} = S\delta_{ij}\delta_{i3}$.
82 This ensures that we focus exclusively on Rayleigh waves, ignoring Love wave contribu-
83 tions in G . We further assume that the PSD is spatially uniform (Hanasoge, 2013, 2014;
84 Datta et al., 2019) so that the spatial and frequency dependence of S may be separated,
85 i.e. we write $S(\xi, \omega) = P(\omega)\sigma(\xi)$. These three simplifications lead to the expression:

$$\mathcal{C}_{pq}(\mathbf{x}_\alpha, \mathbf{x}_\beta; \omega) = P(\omega) \int_{\Omega} d\xi G_{pz}^*(\mathbf{x}_\alpha, \xi, \omega) G_{qz}(\mathbf{x}_\beta, \xi, \omega) \sigma(\mathbf{x}) \quad (2)$$

86 The evaluation of eq. (2) is still a three-step process in general, based on the invocation
87 of source-receiver reciprocity at one of the receiver locations (Tromp et al., 2010; Sager
88 et al., 2018). However in the specific case of working with a single receiver pair, as in
89 this synthetic study, it is most efficient to invoke reciprocity at both receiver locations
90 (Hanasoge, 2014; Xu et al., 2019), thereby rewriting eq. (2) as

$$\mathcal{C}_{pq}(\mathbf{x}_\alpha, \mathbf{x}_\beta, \omega) = \int_{\Omega} d\xi G_{zp}^*(\xi, \mathbf{x}_\alpha, \omega) G_{zq}(\xi, \mathbf{x}_\beta, \omega) P(\omega) \sigma(\mathbf{x}) \quad (3)$$

Hence \mathcal{C}_{pq} is computed as follows. First, we obtain the z-component of impulse response in the entire horizontal domain for sources placed at the receiver locations and acting in the p and q directions. Next, we spatially integrate the product of the two responses (after complex conjugating one of them), weighted by the source mask σ .

This formulation is completely general with regard to the type of Earth model considered and the manner in which the Green's functions are obtained (e.g. analytically or numerically). In our implementation, we work with 1-D, vertically stratified media for which surface-wave terms of the elastodynamic Green's tensor are semi-analytically computable in 2-D as well as 3-D.

2.2 Computation of the Green's function

In our forward modelling scheme, we only need the Rayleigh-wave terms of Green's function in 3-D (point sources). For laterally homogeneous media, these are (Aki and Richards, 2002, Sec 7.4):

$$G = \sum_n \frac{1}{8cUI_1} \begin{bmatrix} r_1(h)r_1(z)\frac{x^2}{r^2} & r_1(h)r_1(z)\frac{xy}{r^2} & -ir_2(h)r_1(z)\frac{x}{r} \\ r_1(h)r_1(z)\frac{xy}{r^2} & r_1(h)r_1(z)\frac{y^2}{r^2} & -ir_2(h)r_1(z)\frac{y}{r} \\ ir_1(h)r_2(z)\frac{x}{r} & ir_1(h)r_2(z)\frac{y}{r} & r_2(h)r_2(z) \end{bmatrix} \times H_0^{(1)}(k_n r) \quad (4)$$

where all symbols follow the Aki and Richards (2002) notation and $r = \sqrt{x^2 + y^2}$. The expression in eq. (4) differs from the one in Aki and Richards (2002) in its use of Cartesian rather than cylindrical coordinates (we work with a Cartesian grid ξ), and in its abandonment of the far-field approximation — the Hankel function of the first kind, $H_0^{(1)}$, is used instead of its asymptotic form, because the implementation of eq. (3) necessitates computation of Green's function at distances comparable to or shorter than the wavelength (see Sec 3.1).

To compute eq. (4), we solve the Rayleigh-wave eigenvalue problem by the method of Gombert and Masters (1988), as in Datta et al. (2017); Datta (2018). This gives c , U and the displacement eigenfunctions r_1, r_2 , which are numerically integrated to obtain I_1 . Finally, we restrict our analysis to the fundamental mode ($n = 0$), and because we only need to evaluate G for sources and receivers on the surface, we use $h = z = 0$ in eq. (4).

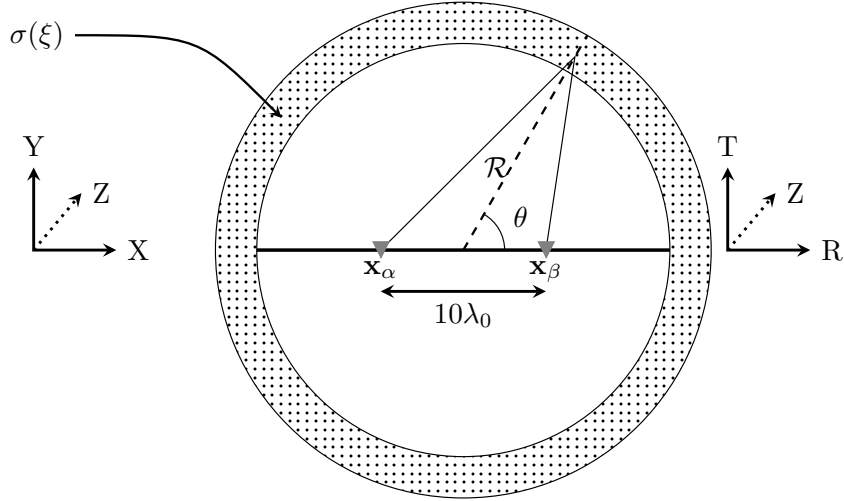


Figure 1: Schematic showing arrangement of sources (dots) and receivers (inverted triangles) in the modelling domain Ω . The coordinate axes R, T and Z, represent the radial, transverse and vertical directions respectively, for the receiver pair.

117 2.3 H/V ratio measurement

118 Rayleigh waves are polarized in the radial-vertical (R-Z) plane and their H/V ratio refers
119 to the ratio η of the radial to vertical displacement amplitudes (e.g. Maupin, 2017). In a
120 laterally homogeneous medium, η is easily obtained from the displacement eigenfunctions
121 evaluated at the surface. By definition,

$$\eta(\omega) = \frac{r_1(z=0, \omega)}{r_2(z=0, \omega)}. \quad (5)$$

Equivalently, one may write

$$\eta = \frac{|G_{RZ}|}{|G_{ZZ}|} = \frac{|G_{RR}|}{|G_{ZR}|}. \quad (6)$$

122 The equivalence between eqs.(6) and (5) is seen from eq. (4), when the x, y axes are
123 oriented along the radial and transverse directions respectively (e.g. Fig. 1). Since the
124 second index in the Green's tensor G_{ij} refers to the source orientation, eq. (6) asserts
125 that η is a medium property, independent of whether the source (point-force) is vertical
126 or radial.

127 In the case of CCs, most studies define the Rayleigh H/V ratio analogously to eq.
128 (6) using the corresponding elements of the cross-correlation tensor: $\mathcal{C}_{RR}, \mathcal{C}_{ZZ}, \mathcal{C}_{ZR}, \mathcal{C}_{RZ}$
129 (Lin et al., 2014; Muir and Tsai, 2017). If equivalence between cross-correlations and
130 Green's function holds, the two CC measurements, Γ^R and Γ^Z , correspond to virtual
131 sources oriented radially and vertically, respectively:

$$\begin{aligned}\Gamma^R &= \frac{f(\mathcal{C}_{RR})}{f(\mathcal{C}_{ZR})} \sim \eta \\ \Gamma^Z &= \frac{f(\mathcal{C}_{RZ})}{f(\mathcal{C}_{ZZ})} \sim \eta.\end{aligned}\tag{7}$$

132 Here, f represents the operations applied to the CCs to obtain robust measurements.
 133 In this study, we 1) Determine the envelope of the cross-correlation signal, 2) Pick its
 134 maximum value on the causal and anti-causal branches, 3) Average the two values thus
 135 obtained.

136 We note that the interpretation of Γ^R or Γ^Z as the Rayleigh wave H/V ratio (right
 137 side of eq. (7)) is supported in this study by the fact that the CCs are constructed
 138 from Rayleigh waves alone. The superscript of these ratios in eq. (7) represents the
 139 virtual source direction. On the other hand, since cross-correlations and Green's func-
 140 tions are not equivalent (e.g. Roux et al., 2005b), especially when source illumination is
 141 anisotropic, we define a third measurement Γ , which does not afford an interpretation
 142 in terms of a virtual source. The term Γ makes use of \mathcal{C}_{RR} and \mathcal{C}_{ZZ} , and based on the
 143 forward model eq. (2), we estimate that it should be related to η^2 :

$$\Gamma = \frac{f(\mathcal{C}_{RR})}{f(\mathcal{C}_{ZZ})} \sim \eta^2.\tag{8}$$

144 3 Simulations

145 We perform a suite of simulations designed to empirically assess the sensitivity of H/V
 146 measurements to V_p structure, as well as gross geometrical features of the noise-source
 147 distribution σ . These are the two quantities which we vary in our forward modelling,
 148 while other parameters are held fixed. As explained in the previous section, our mod-
 149 elling scheme entails a 1-D, depth-dependent Earth model $M(z)$ in which the Green's
 150 functions are computed, and a 2-D horizontal domain $\Omega(x, y)$ on which the sources are
 151 distributed (the Earth model is implicitly uniform throughout Ω). Here we first describe
 152 the fixed parameters, pertaining to Ω , and then the model variations, which involve both
 153 M and Ω .

154 3.1 Fixed parameters

155 Rayleigh wave H/V ratio is a frequency-dependent quantity but for the sake of simplicity,
 156 we present results in this paper for a single frequency, $f_0 = 0.1$ Hz. This value (10 s
 157 period) is chosen because it lies in between the primary and secondary microseism peaks

158 at ~ 7 and 15 s. (Peterson, 1993; Ardhuin et al., 2015). This choice of frequency
 159 dictates nearly all other choices relating to the simulation geometry. We model the PSD
 160 of the noise sources, $P(\omega)$, with a narrow-band Gaussian centered at $f_0 = 0.1$ Hz (see
 161 Fig. 3f). The corresponding wavelength, λ_0 , is used to fix the uniform grid spacing
 162 $\Delta h \leq \lambda_0/4$ and separation between receivers, $|\mathbf{x}_\alpha - \mathbf{x}_\beta| \geq 10\lambda_0$, well above the typical
 163 requirement of three wavelengths (Bensen et al., 2007; Luo et al., 2015). The size of the
 164 domain Ω is chosen to be at least twice the receiver separation in both directions, i.e.,
 165 $[x_{min}, x_{max}, y_{min}, y_{max}] = 20\lambda_0 \times [-1, 1, -1, 1]$.

166 We have $\lambda_0 \approx 35$ km for Earth model M_0 (section 3.2), which leads to the values
 167 $\Delta h = 8$ km, $\mathbf{x}_\alpha = (-164 \text{ km}, 0)$, $\mathbf{x}_\beta = (164 \text{ km}, 0)$ and $\Omega = \{-600 \text{ km} < x <$
 168 $600 \text{ km}, -600 \text{ km} < y < 600 \text{ km}\}$. Note that the receivers are kept off-grid, since
 169 they are turned into sources in our implementation eq. (3). Finally, we use a temporal
 170 sampling interval of 1 s and generate a time series of length 400 s.

171 3.2 Models used

172 The 1-D Earth model we work with is PREM (Dziewonski and Anderson, 1981) without
 173 the ocean layer; we call this model M_0 . Simulations are performed for 20 variants of this
 174 model, which differ only in their V_p values — a relative perturbation in the range -9%
 175 to $+10\%$ is applied uniformly at all depths to the model V_p .

176 Each Earth model M is used in conjunction with a particular model for the source
 177 distribution σ over the domain Ω . We use different classes of σ . *Uniform distribution*
 178 where the sources have uniform strength everywhere in the domain; *Ring distribution*
 179 where sources are present at some distance (\mathcal{R}) from the center of domain within a strip
 180 of width $d\mathcal{R}$ (Fig. 1), and *Arc distribution* where sources are confined to an arc, with
 181 given \mathcal{R} and $d\mathcal{R}$, oriented at some angle to the receiver pair. We use $\mathcal{R} = 250$ km and
 182 $d\mathcal{R} = 40$ km for ring and arc distributions. Three arc distributions are implemented to
 183 cover the range of possible scenarios of source directionality with respect to the receiver
 184 pair: *parallel* ($\theta = -15^\circ$ to 15°), *oblique* ($\theta = 30^\circ$ to 60°), and *orthogonal* ($\theta = 75^\circ$ to
 185 105°). The arcs have uniform source strength in the aforementioned ranges for θ , but
 186 are cosine tapered to zero over an additional 5° at both ends.

187 The five source-distribution models utilized for the simulations are shown in Fig. 2.

188 4 Analysis and results

189 We start by examining the CC obtained for each of the noise-source distributions in
 190 Earth model M_0 (Fig. 3). The effect of anisotropic source distributions is readily
 191 observed on the amplitude (in positive and negative branches, A^+ , A^-) as well as arrival

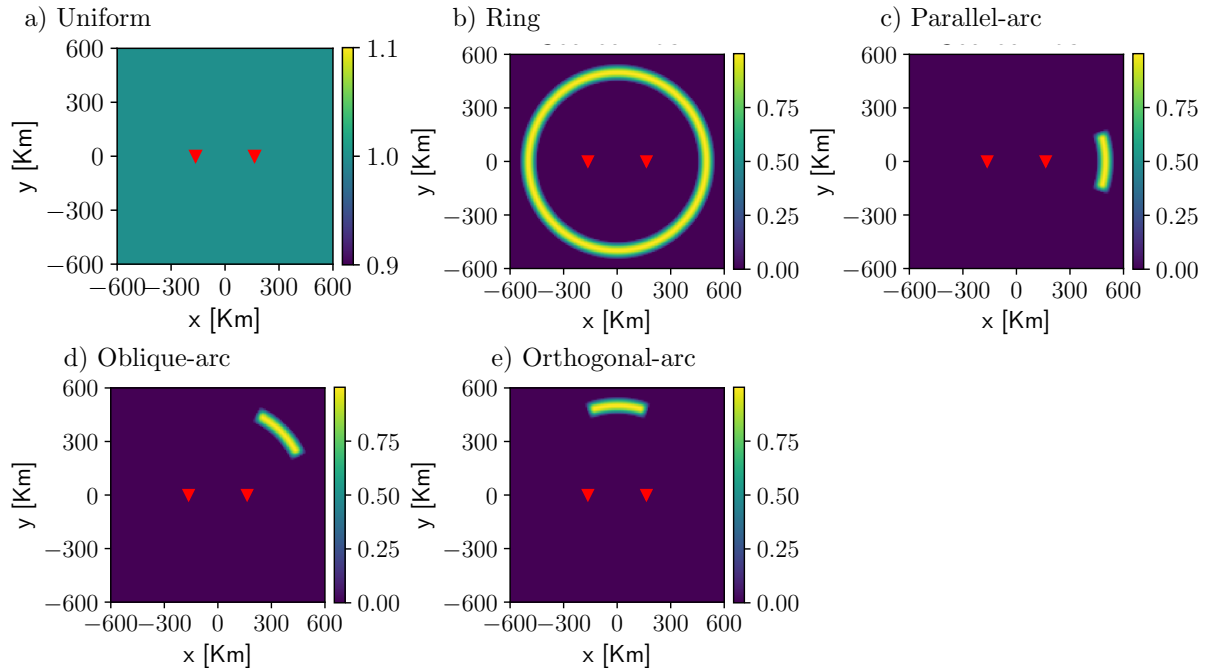


Figure 2: Different noise source distributions as defined in the text and identified here by the individual plot titles. The red triangles mark the receiver locations.

192 time (T_{CC}) of signals in the CC. Uniform and ring distributions show $A^+ = A^-$ and
 193 nearly the same arrival times as for Rayleigh waves (T_R) with one of the receivers acting
 194 as a virtual source. In contrast, the arc-type distributions have $A^+ \neq A^-$ and $T_{CC} = T_R$
 195 holds only for the parallel-arc configuration. These observations are well understood in
 196 terms of stationary and non-stationary phase sources (e.g. Xu and Mikesell, 2017).

197 Next, we look at various H/V measurements obtained for all our Earth models with
 198 varying V_P . Fig. 4 shows that the H/V ratio measurements for the uniform and ring
 199 distributions have an excellent match with the theoretical Rayleigh wave H/V ratio, i.e.
 200 we find $\Gamma^R = \Gamma^Z \approx \eta$ and $\Gamma \approx \eta^2$. On the question of sensitivity to V_p , this implies that
 201 Γ offers better resolution than Γ^R or Γ^Z — the ‘dynamic range’ of η , i.e. the difference
 202 between its maximum and minimum values over the range of Earth models used, is
 203 $\eta_{DR} \approx 0.085$ whereas for η^2 it is slightly higher, $\eta^2_{DR} \approx 0.104$ (also apparent from the
 204 slopes of the graphs in Fig. 4).

205 Moving on to the anisotropic (arc-type) noise source distributions, the condition
 206 $\Gamma^R = \Gamma^Z$ continues to hold in all cases, but the equivalence relations between the CC-
 207 derived H/V and the theoretical Rayleigh wave H/V, break down for the oblique-arc
 208 and orthogonal-arc distributions. The discrepancies are particularly large in the latter
 209 case, and are consistent over the range of Earth models used. A quantitative summary
 210 is provided in Table 1.

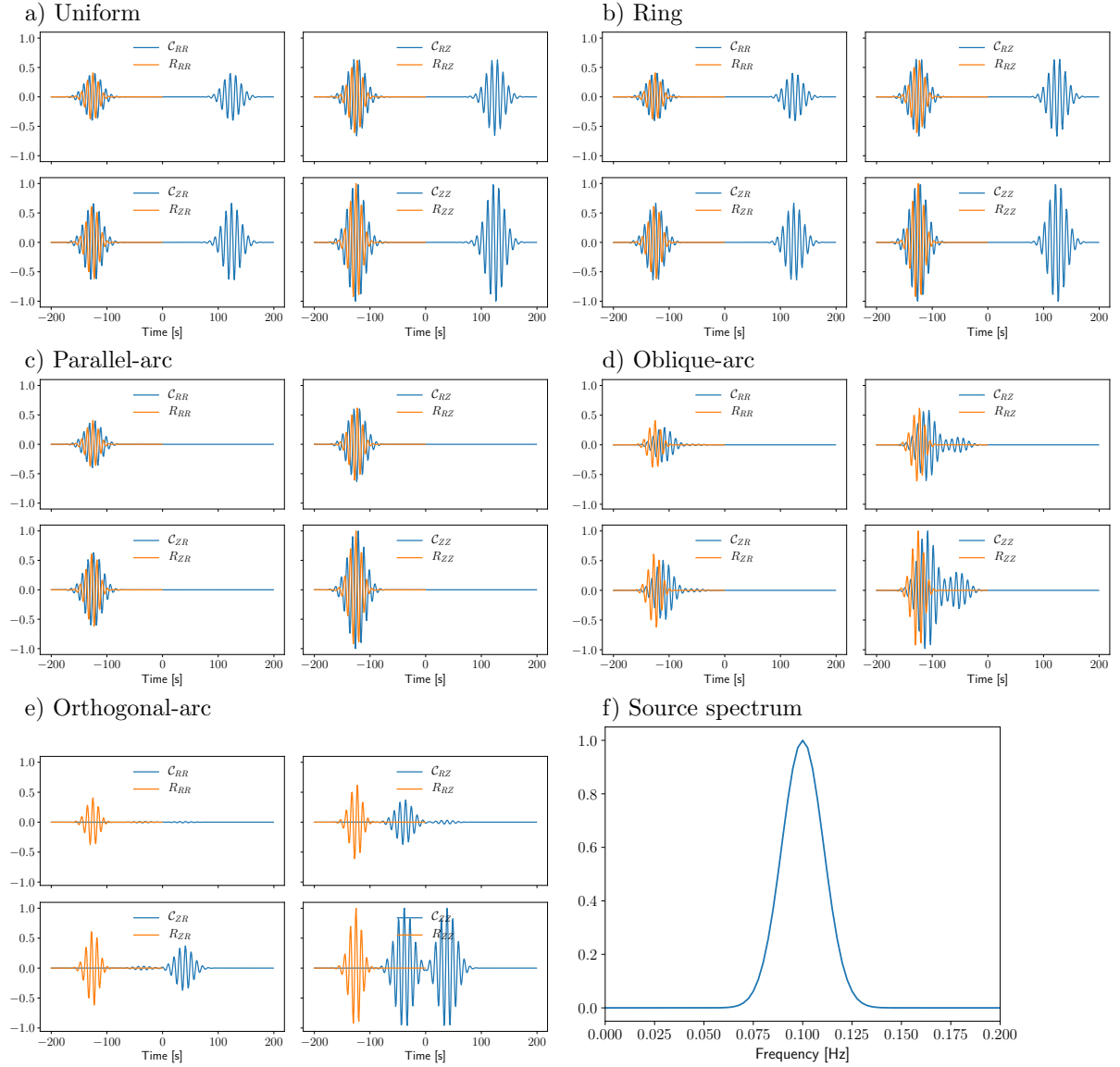


Figure 3: Panels (a)-(e) show the synthetic CCs generated for the corresponding source distributions in Fig. 2. Each panel contains four plots for the four components (clockwise from top left) C_{RR} , C_{RZ} , C_{ZZ} and C_{ZR} . The corresponding Rayleigh wave from receiver α to receiver β has also been presented for comparison. The amplitudes are normalized with respect to the maximum within a panel. (f) $P(\omega)$ for the noise sources, centred at 0.1 Hz.

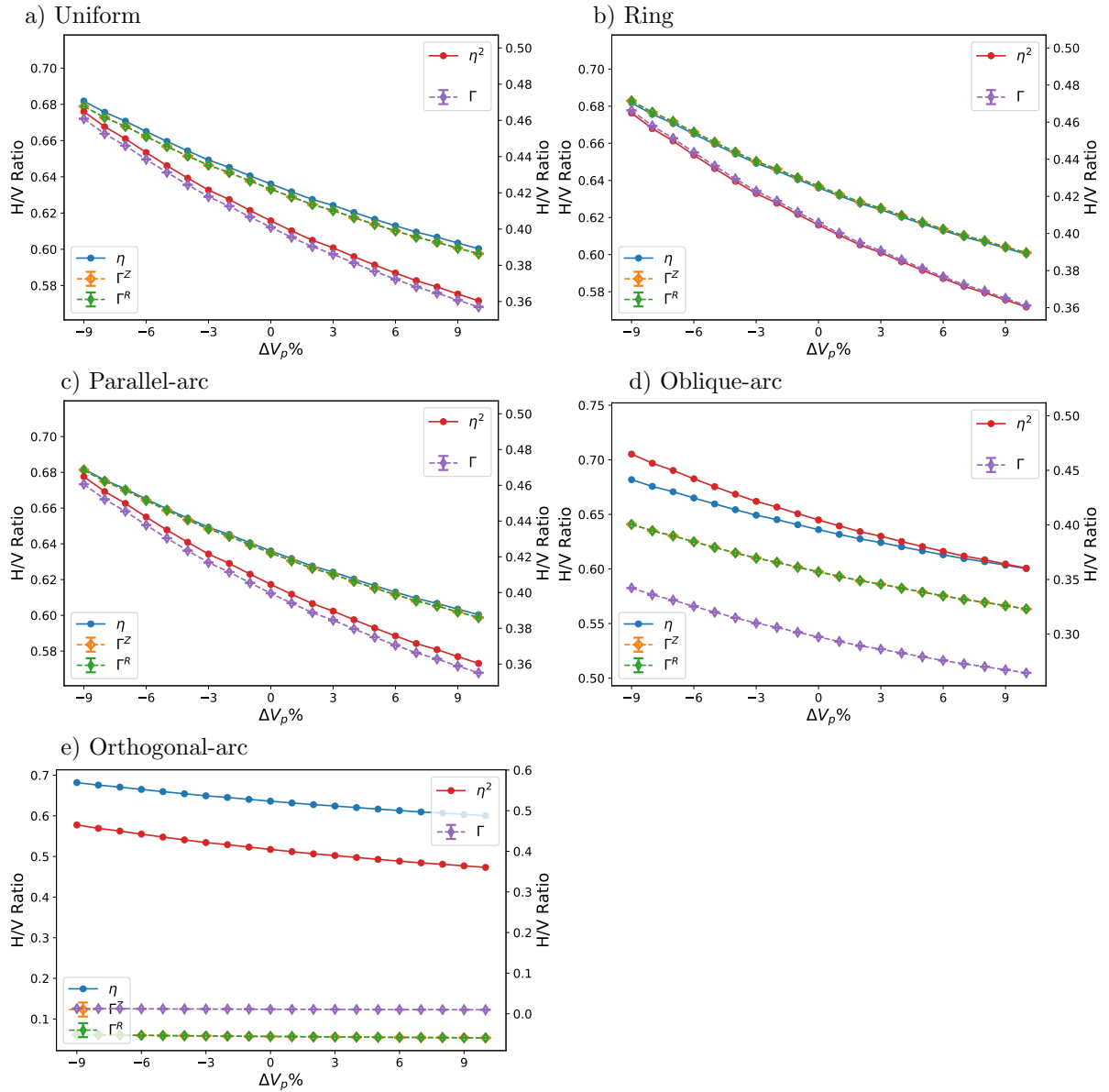


Figure 4: H/V ratio measurements obtained from CCs for different noise source distributions (as indicated in the plot titles a-e), and compared with the Rayleigh wave H/V for the medium, which is unrelated to noise source distribution. Note that we have used separate y-axes for different curves, shown on the left and right sides of each plot. The legend boxes attached to these two axes identify the curves associated.

4.1 Measurements with added synthetic noise

Since our aim in this study is to assess the sensitivity of H/V measurements to V_P , we compute uncertainty estimates for the measurements by adding noise to our CC waveforms. The magnitudes of uncertainties, compared with the dynamic range of the measurements (over the range of V_P values considered) sheds light on the usefulness of these measurements in practice. Synthetic waveforms with noise, $\tilde{S}(t)$ may be obtained by adding noise $N(t)$, of chosen strength, to the noise-free signal $S(t)$, as

$$\tilde{S}(t) = S(t) + \frac{\alpha k}{100} N(t), \quad (9)$$

where α is the desired signal to noise ratio and k is a scaling factor to bring the noise amplitudes to the signal level. N is computed in the frequency domain, using the power spectrum of the signal:

$$N(\omega) = P(\omega)\chi(\omega) \quad (10)$$

where $P(\omega) = S^*(\omega)S(\omega)$, $\chi(\omega) = [\mathcal{N}(0, 1) + j\mathcal{N}(0, 1)]/\sqrt{2}$ and $\mathcal{N}(\mu, s)$ represents a Gaussian random variable with mean, μ , and standard deviation, s .

H/V ratio calculations are performed for a given amount of noise (viz. 2%, 5% and 10%) and for each source distribution and Earth model, using all three H/V ratios eq. (7) and eq. (8). The results are shown in Fig. 5, with standard error estimated from 1000 realizations of added random noise.

As in the noise-free case, the mean trend of estimated H/V ratio in the presence of added noise closely follows the theoretical curves for homogeneous, ring and parallel-arc distributions. For the oblique-arc distribution there is a significant departure of mean trend from the theoretical curves containing a large error. For the orthogonal-arc distribution the H/V observation are completely erroneous. The uncertainty in estimated H/V ratios (Γ^R , Γ^Z , and Γ) in the presence of noise is presented in Table 1. This helps us evaluate the efficacy of measurements based on the thresholds given by η_{DR} for Γ^R and Γ^Z , and by η_{DR}^2 for Γ . We infer two things from the observed values. First, meaningful measurements can only be made for up to 15% random Gaussian noise. Beyond this noise level, the uncertainties in CC-derived H/V ratios exceed the η_{DR} or η_{DR}^2 thresholds. Second, noise has a lower impact on Γ in comparison to Γ^R and Γ^Z , due to its larger dynamic range.

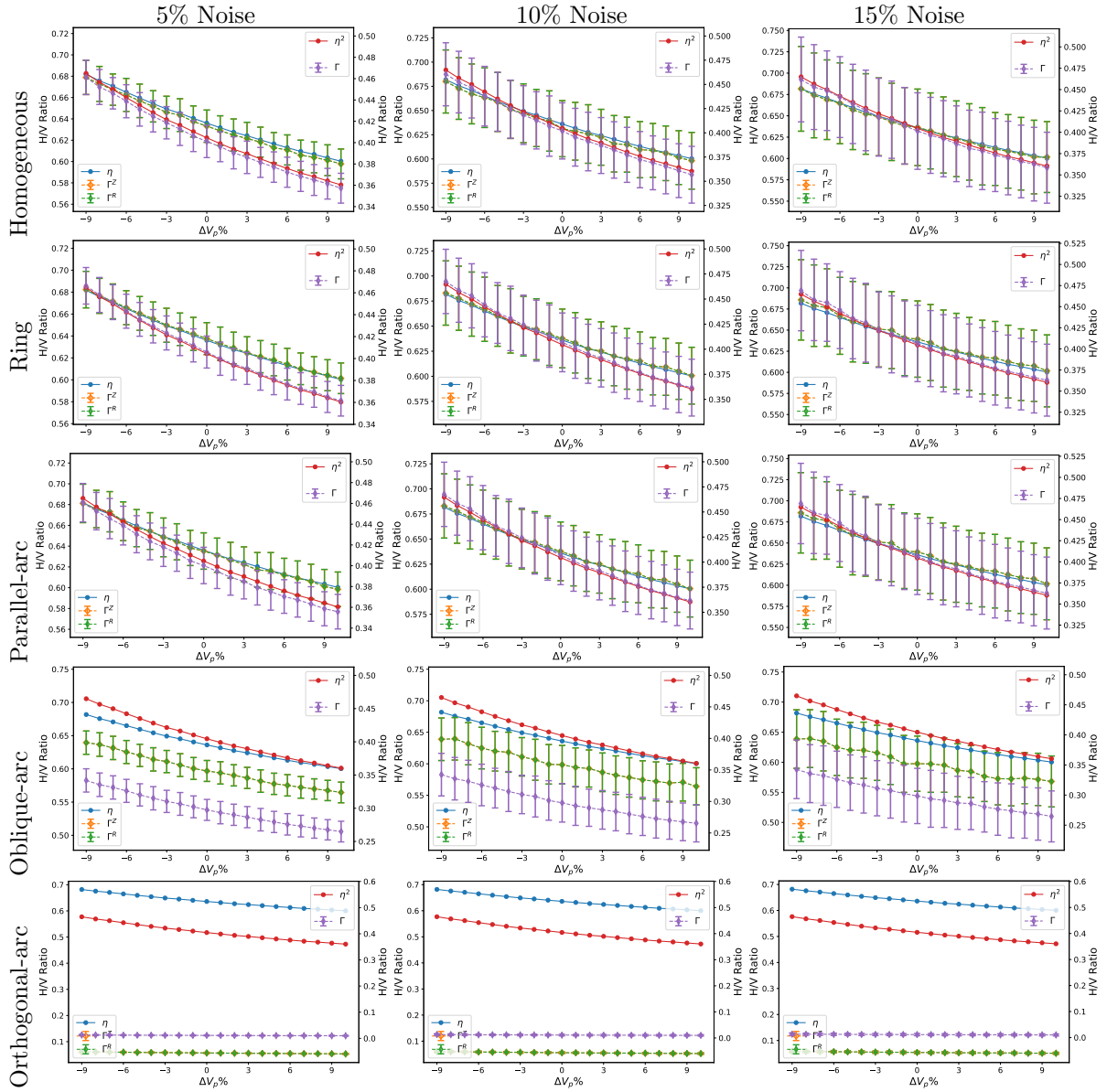


Figure 5: Similar to Fig. 4 but for measurements made with synthetic noise added to the CC. Noise levels vary across columns as indicated in the top panel, and rows correspond to source distributions as indicated on the extreme left.

Noise %		Uniform	Ring	Parallel-arc (-30° to 30°)	Oblique-arc (15° to 75°)	Orthogonal-arc (60° to 120°)
0%	$A^+ = A^-$	✓	✓	×	×	×
0%	$T_R = T_{CC}$	✓	✓	✓	✓	×
0%	$\eta - \Gamma^Z$	0.4%	0.2%	0.2%	61%	91%
0%	$\eta - \Gamma^R$	0.4%	0.2%	0.2%	61%	91%
0%	$\eta^2 - \Gamma$	0.8%	0.4%	1.2%	26%	97%
Range of estimated H/V (Threshold $\Delta\eta_{DR} = 0.085$, $\Delta\eta_{DR}^2 = 0.104$)						
2%	$\Delta\Gamma^Z = \Delta\Gamma^R$	0.012 ↓	0.012 ↓	0.014 ↓	0.013 ↓	NA
	$\Delta\Gamma$	0.008 ↓	0.008 ↓	0.009 ↓	0.007 ↓	NA
5%	$\Delta\Gamma^Z = \Delta\Gamma^R$	0.030 ↓	0.030 ↓	0.035 ↓	0.033 ↓	NA
	$\Delta\Gamma$	0.019 ↓	0.019 ↓	0.022 ↓	0.016 ↓	NA
10%	$\Delta\Gamma^Z = \Delta\Gamma^R$	0.060 ↓	0.060 ↓	0.067 ↓	0.063 ↓	NA
	$\Delta\Gamma$	0.037 ↓	0.038 ↓	0.042 ↓	0.031 ↓	NA
15%	$\Delta\Gamma^Z = \Delta\Gamma^R$	0.090 ~	0.090 ~	0.096 ↑	0.091 ~	NA
	$\Delta\Gamma$	0.057 ↓	0.058 ↓	0.061 ↓	0.045 ↓	NA

Table 1: A tabular representation of results. First row shows whether the amplitude on positive and negative branch are equal. Second row show if the rayleigh wave travel time matches with waveform in CC. Third to fifth row shows the difference between the theoretical H/V ratio for Rayleigh wave and the one calculated using CC. Rest of the rows below represent measurement uncertainties, i.e. the size of error bars, estimated with added random noise. Up/down-arrows represent higher/lower values than the theoretical dynamic range threshold and ~ represents close to the threshold.

5 Discussion and conclusions

We have presented a synthetic study that critically examines measurements commonly used to estimate the Rayleigh-wave ellipticity or H/V amplitude ratio from multi-component CCs. The study focuses on two aspects of these measurements: the extent to which they are degraded on account of anisotropic distributions of ambient noise sources, and their variations with model V_P . Both aspects are analysed empirically, by modelling cross-correlations for some simple distributions of noise sources, and a suite of 1-D Earth models that differ in V_P . Our results demonstrate that the absolute values of CC-based H/V measurements are adversely affected by strongly anisotropic noise sources (off the receiver line), and that the sensitivity to V_P can be marginally enhanced by taking the ratio of the \mathcal{C}_{RR} and \mathcal{C}_{ZZ} components of the cross-correlation tensor. This measurement, Γ , defies conventional Green’s function interpretations for cross-correlations because it cannot be associated with a common virtual source. It however recovers the square of the Rayleigh H/V ratio when noise sources are not strongly anisotropic. Finally, uncertainty analysis reveals that V_p structure may be resolved in the presence of noise in the correlation measurements (up to 10%).

It should be borne in mind that our results are qualified by the modelling assumptions

256 we have used (Section 2). For example, because we assume only vertically directed
257 sources, we have excluded Love-wave contributions in our analysis. In general, Love
258 waves from laterally (horizontally) directed noise sources will additionally contribute
259 to the radial-component displacement, impacting the corresponding cross-correlations
260 and therefore the H/V-ratio measurements. However, this requires reliably determining
261 the true orientations of noise sources (i.e. horizontal or vertical and their directionality
262 with respect to the network), a challenging problem; we defer these modelling tasks to
263 a future effort.

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