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9 The predictability of shallow landslides: lessons from a
10 natural laboratory

11 **R. Bainbridge¹, M. Lim², S. Dunning¹, M.G. Winter³, A. Diaz-Moreno¹, J. Martin²,**
12 **H. Torun², B. Sparkes⁴, M. Khan², N. Jin²**

13 ¹ *Department of Geography, Newcastle University, Newcastle, NE1 7RU, UK*

14 ² *Department of Geography, Northumbria University, Newcastle, NE1 8SB, UK*

15 ³ *Winter Associates, Kirknewton, Midlothian, EH27 8AF, UK*

16 ⁴ *Richard Allitt Associates Ltd, The Forge Offices, Haywards Heath, RH17 6ET, UK*

17

18 *Corresponding author: rupert.bainbridge@ncl.ac.uk*

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24 ¹ Department of Geography, Newcastle University, Newcastle, NE1 7RU, UK

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28

29 **ABSTRACT**

30 Shallow landslides are a significant hillslope erosion mechanism and can
31 transform into destructive debris-flows. Limited understanding of the controls on
32 debris-flow initiation, development and deposition results in persistent risk and high
33 impacts where linear infrastructure is affected. Here, we analyse steep slopes above
34 a key road, the A83 Rest and be Thankful, Scotland, where near-real-time rain gauge
35 data, time-lapse camera deformation tracking and seismics allow us to define
36 thresholds for increased debris-flow risk, examine long-term slope creep and, detect
37 debris-flow occurrence. We show the patterns and development of channelized and
38 hillslope debris-flows that act as a key geomorphic agent, accounting for 58% of
39 landslide source volume over 13-years. On-slope rainfall data allow us to quantify the
40 effect of antecedent rainfall and storm intensity-duration on landslide triggering and
41 develop new local thresholds over which landslides are likely to occur. To better equip
42 asset managers, we use time-lapse imagery vector tracking to detect slope
43 instabilities, and deformation rates to calculate inverse-velocity values to indicate if

44 failure is imminent. Low-cost seismometers are used to detect when a debris-flow has
45 occurred and locate the source area. The suite of sensors has provided vital
46 information both prior to failure, and during debris-flows to support operational
47 decision-making for authorities dealing with complex slope hazards.

48

49 **INTRODUCTION**

50 Debris-flows are extremely rapid (>5 m/s), saturated debris landslides from
51 hillslopes (Hungri et al., 2014). Shallow landslides translate into debris-flows given
52 favourable material and fluidisation conditions (Zimmerman et al., 2020). Debris-flow
53 runout potential and capacity to entrain water and sediment make them a significant
54 global hazard, particularly where linear infrastructure traverses affected slopes
55 (Geertsema et al., 2009; Meyer et al., 2015). They can be broadly grouped into
56 channelized debris-flows (CDFs) that are constrained for their flow path and hillslope
57 debris-flows (HDFs) that occur on non-incised slopes (Chen et al., 2009). CDFs and
58 HDFs can transition into one another where HDFs meet gullies or CDFs breach
59 channels and flow over slope; hillslope-gully coupling controls the hazard potential
60 (Milne et al., 2009). CDFs often occur in torrent systems, such as the Illgraben,
61 Switzerland (Badoux et al., 2009) where the repeated flow path removes some of the
62 risk uncertainty.

63 Where debris-flows source across large areas with uncertain runout, a
64 combination of active mitigation (physically controlling site aspects using engineering
65 infrastructure) and passive mitigation (reducing impacts via land-use planning,
66 closures and warning systems) methods can be used (Huebl and Fiebiger, 2005;
67 Vagnon, 2020).

68 In Scotland, debris-flows have repeatedly damaged linear infrastructure
69 resulting in economic and social costs (Winter et al. 2019a). Here we demonstrate the
70 use of near-real-time, on-site data to supplement Landslide Management Plans (LMP)
71 and enhance alert capabilities for stakeholders at a debris-flow prone slope in the west
72 of Scotland.

73

74 **STUDY AREA**

75 The A83 Rest and be Thankful (RabT), a key road into west Scotland, has the
76 highest landslide frequency on the Scottish road network (McMillan and Holt, 2019). It
77 bisects the south-western slope of Beinn Luibhean above Glen Croe. The bedrock is
78 Schist, with overlying till up to 3 m thick, interspersed with gullies, scars, levees and
79 debris cones (Sparkes et al., 2017, Finlayson, 2020, BGS, 2020). Past debris-flows
80 have been linked to high-intensity rainfall (Winter et al., 2019b).

81 On average 4,000 vehicles cross the RabT per day (Winter et al. 2019a).
82 Closures divert traffic ~88 km, if the Old Military Road (OMR), a one-way convoy
83 diversion below the A83 is closed, casting a vulnerability shadow over 4,300 km² (Fig
84 1A). A full road closure costs ~£90k per day (2012 prices; Winter et al. 2019a) and
85 £13.3m has been spent on protecting the A83 and improving the OMR (Scottish
86 Parliament, 2020). Some debris-flows still exceed mitigation measures and impact the
87 A83 and OMR. Quantified RabT risk studies justified measures for the LMP (Winter at
88 al., 2008; Winter and Wong, 2020) which sends out daylight patrols and activates
89 warning 'wig-wag' lights on the RabT approach if forecast rainfall is ≥ 25 mm in a 24-
90 hour period or ≥ 4 mm in a 3-hour period (Winter et al. 2020).

91

92 **LANDSLIDE ACTIVITY**

93 A new RabT landslide inventory has been collated from road reports (2003-
94 2015), quarterly and event responsive terrestrial laser scans (TLS; 2015-2019) and
95 time-lapse imagery (2017-2020). Post-2015 it is unlikely events are missing as TLS
96 (0.1 m resolution) and time-lapse imagery was used (Sparkes et al., 2017 and this
97 study). Pre-2015, debris-flows that reached the A83 are recorded, but smaller
98 landslides may not be. From 2003 to 2019 there were 63 landslides (Fig. 1); 43 were
99 debris-flows (19 HDFs, 21 CDFs, three of unknown type), 11 slope creeps, and nine
100 soil falls. 15 debris-flows closed the A83, on average nearly once a year since 2003;
101 six reached the OMR.

102 60 landslides have known source areas (Fig. 1B), 45% (n=27) are in till, 35%
103 (n=21) in debris cones and 20% (n=12) in regolith. 50 of these have source volumes
104 derived from TLS (2015-2019) or estimates from reports (2007-2015). Debris cones
105 cover 22% of the slope and account for 27% of the landslide volume; regolith (18% of
106 the slope) and till (61% of the slope) account for 10% and 62% of the landslide volume
107 respectively. Volumetric contributions from different materials reflect failure processes
108 and depth to bedrock. Debris cone sources have deep scarps which shallow
109 downslope, indicative of rotational slides. Till and regolith sources have a regular depth
110 profile indicating translational failures. Modelling over a TLS derived DEM shows
111 coupling of source areas and stream flow (Fig. 1B).

112

113 **MANAGING DEBRIS-FLOW RISK - MONITORING STRATEGIES FOR ALERT,**
114 **TRACKING AND DETECTION**

115 Here we use 2018, an active year with 19 of the 63 landslides (Fig 1C), as a
116 case study for pro-active, near-real-time monitoring to alerting stakeholders to

117 increased landslide risk based on rainfall thresholds, tracking slope creep and
118 detecting debris-flows occurrence.

119 Rainfall on seasonal, daily and 15-minute timescales are used to indicate raised
120 landslide risk. The 2013-2019 seasonal rainfall trend was examined for Scottish
121 Environment Protection Agency (SEPA) RabT rain gauge data (SEPA, 2020) using
122 the Bayesian Estimator of Abrupt change, Seasonality and Trend (BEAST) analysis
123 package (Zhao et al., 2019). BEAST uses ensemble modelling, where multiple
124 competing models analyze data, and Bayesian statistics derive a model average with
125 associated probabilities that detect if seasonal and trend changes are ‘true’.

126 An Antecedent Precipitation Index (API; Fedora and Beschta, 1989), a proxy
127 for ground saturation (Segoni et al., 2018), was calculated for daily rainfall totals using
128 Equation 1, as an indicator of raised debris-flow risk.

$$129 \quad API_i = k(API_{i-1}) + P_i \quad (1)$$

130 Where API_i is the API at time i , P_i is the daily rainfall total at i and k is a constant decay
131 function defined by the user ($k=0.8$). Rainfall was measured with an on-slope Davis
132 Vantage Pro 2 gauge, better reflecting on-slope conditions than the off-slope SEPA
133 gauge.

134 An intensity-duration (I-D) threshold was developed using 15-minute rainfall
135 intensity data. Duration and mean rain intensity for all storms in the study period were
136 plotted (Brunetti et al., 2010; Guzzetti et al., 2008), with a six-hour inter-event period.
137 An I-D threshold above which landslides occur was visually derived from the results.
138 Mean rain intensity over an entire storm was used as not all landslide timings were
139 known.

140 Alerts of slope changes allow stakeholders to be on stand-by, pre-position
141 resources, or proactively manage risk. Processing of time-lapse imagery in a particle

142 image velocimetry tool (PIVLab; Thielicke and Stamhuis, 2014; Thielicke, 2020)
143 detected creep on the 19/09/2018. Displacement vectors and velocity were
144 established between consecutive slope-wide images at 16x16 pixel resolution (~2.7
145 m²). Cumulative deformation was derived for a point tracked through the photo
146 sequence. Inverse velocity (I-V), a tool used to predict failure in brittle materials (Carlà
147 et al., 2017), was used as a tentative metric for till failure prediction despite the non-
148 brittle materials involved. Imminent failure is predicted when I-V values reach zero
149 (infinite velocity). Time between images was not uniform due to poor visibility, so
150 velocity data from PIVLab were interpolated to 12h intervals, with a moving average
151 smoothing of 24h. I-V was calculated for smoothed data using Equation 2 (Manconi
152 and Giordan, 2016), where I_v is inverse velocity and V_w is velocity (V) over the defined
153 time window (w).

$$154 \quad I_v = \frac{1}{V_w} \quad (2)$$

155 Seismics were used to detect debris-flow onset. Seismics are widely used in
156 torrent debris-flows systems (Walter et al., 2017), but here a Raspberry Shake 3D
157 seismometer (Raspberry Shake, 2020; Manconi et al., 2018) was deployed for
158 detection on a hillslope with uncertain flow routing. The seismogram trace shows
159 characteristic debris-flow signals, generated through clast-clast and flow-substrate
160 interactions, above the long-term average. Hodograms (plotting signal direction
161 through time) were used to confirm the direction of debris-flow signals to the
162 seismometer. Hodograms are seldom used in geosciences but have been used in
163 rockfall monitoring (Borella et al., 2019).

164

165 **RAINFALL THRESHOLDS**

166 BEAST identified three rainfall seasonal change points (SCP) in winter periods
167 from 2013 to 2016 (Fig. 2A). SCP3 (Fig. 2A) is Storms Desmond and Frank which
168 caused debris-flows at the RabT. No SCPs are seen from 2016-2019. However,
169 debris-flows are coincident with abrupt rainfall trend change points (TCPs) 2, 6 and 7,
170 their subsequent falling trends and in long period high trends (TCP1; Fig. 2B). TCP7
171 starts the 2018 landslide period. For this period Fig. 2C shows when LMP forecast
172 rainfall thresholds were exceeded and 'wig-wag' warning lights were operating, along
173 with the same thresholds plotted using on-slope, live rain data. False alarms and
174 missed landslides account for 6.9% of the study period for wig-wags and 12.2% for
175 on-slope data (Fig. 2D). Wig-wags are human operated, reducing false alarms through
176 expert judgement. However, on-slope data would raise alert levels two times where
177 landslides occurred, that are not fully covered by the wig-wags (Fig. 2C i and ii).

178 Landslide producing storms were medium (>10h) to long duration (max. 72h;
179 Fig. 2E); for two storms it is not known in which the landslide happened. Mean rain
180 intensity for landslide initiation ranges from 2.95 mm/hr to 8.15 mm/hr. Landslides
181 occur above the threshold described by Equation 3.

182
$$I = 4.75D^{-0.18} \quad (3)$$

183 Where I is mean rain intensity and D is duration. As all confirmed landslide storms
184 were >10h duration, the threshold may not apply to <10h storms. The I-D threshold
185 gives a false alarm for 5.7% of the study period (Fig. 2G).

186 All landslides (n=18) occur over an API threshold of 37 mm, with three false
187 alarms and long periods of alert with no landslides (Fig. 2F). A 62 mm API threshold
188 covers 90% of landslides (n=16), reduces false alarms to 0.8% of the study period
189 (Fig. 2G), but misses two mid-December events. A combination of I-D and API

190 thresholds maximizes landslide detection and minimizes false alarms (Fig 2G). All
191 landslide inducing storms exceed the I-D threshold with five false alarms (Fig. 2F i to
192 v) which API thresholds can reduce to two (Fig. 2F iv, v).

193

194 **TIME-LAPSE VECTOR TRACKING**

195 Creep of Failure 2 (Fig. 2B) was monitored via time-lapse image vector tracking
196 from initiation (19/09/2018) to arrest (27/09/2018) using PIVLab (Thielicke and
197 Stamhuis, 2014; Thielicke, 2020). Vectors of change and a velocity heat map between
198 consecutive images are shown in Figures 3A and 3B.

199 Creep initiation coincides with a rainstorm on the 18/09/2018 (Fig. 3C i). Half of
200 the total cumulative deformation occurs in the first 2.5 days. Inverse velocity (I-V)
201 rapidly decreases towards zero on the 19-20/09/18; extrapolation of the I-V trend
202 predicts failure on the 21/09/2018. However, I-V values increase on the 21/09,
203 indicating reduced velocity after rainfall ceases. The deformation rate slows until arrest
204 and subsequent rainfall does not affect the deformation rate (Fig. 3C ii and iii).
205 Operationally, alert levels would be raised in Phase i when imminent failure seemed
206 likely but lowered after the 21/09.

207

208 **PASSIVE SEISMICS DEBRIS-FLOW DETECTION**

209 Seismics identified a HDF (Figs. 4A and 4B) on the 09/10/2018 and located the
210 source area. The z-axis seismogram (Fig. 4C) shows a high-amplitude signal lasting
211 ~15s, corresponding with the failure time derived from time-lapse imagery, which is
212 likely the HDF in motion. Short duration, lower amplitude signals follow and are likely
213 post-landslide sediment and boulder reworking. Hodograms show very little activity at
214 first (Fig. 4C i), but signal strength increases as the HDF signal arrives (ii) before

215 subsiding (iii). Stacked hodograms, overlain on a DEM, point to the HDF source area
216 as the direction of the incoming signal (Fig. 4D).

217 RabT debris-flow seismic signals are brief due to short, steep flow paths, with
218 boulder and sediment reworking post-event. Another deposit on Fig. 4B, which is a
219 thin, fine-grained drape but has a large deposit footprint, was not detected by seismics;
220 indicating that whilst high debris content flows can be detected, hyper-concentrated
221 flows may need larger station arrays for detection.

222

223 **DISCUSSION AND CONCLUSIONS**

224 This paper presents on-site monitoring at the RabT, aimed at supplementing
225 the existing LMP (Winter et al., 2008). Between 2003 and 2019 there are 63 landslides
226 recorded, including 43 debris-flows. Two landslide processes lead to debris-flows,
227 shallow translational failures (mean depth c.1 m), generally below hydrological
228 convergence zones in regolith and till, and deep-seated (>2 m) rotational failures in
229 debris-cones. Material type exerts control on landslide volumes. Total material losses
230 from the slope are 6,829 m³, with debris cones accounting for 27% (1,853 m³), regolith
231 10% (697 m³) and till the remaining 63% (4,278 m³).

232 BEAST rainfall analysis shows that landslides are primarily associated with
233 abrupt rainfall trend changes. In the 2018 study period, antecedent, and medium- to
234 long-duration, high-intensity rainfall is shown to be an important factor in debris-flows
235 initiation. New local API and I-D rainfall thresholds, identify all landslide inducing
236 storms and minimize false alarms, improve on the LMP and provide road authorities
237 time to consider actions. 90% of RabT landslides occurred over a 62mm API,
238 indicating a critical antecedent rainfall threshold. Rainstorm I-D >10h is key for
239 landslide initiation with largely higher mean rain intensity than non-landslide storms.

240 Shadow trials with confusion matrices against LMP thresholds are needed before full
241 deployment.

242 Time-lapse vector tracking located and quantified creeping deformation in
243 response to rainfall drivers. I-V calculations forecast imminent failure in the initiation
244 phase, however creep slowed when rainfall ceased and arrested despite further
245 rainfall. This method can detect slope movement and indicate times of heightened risk
246 of failure for management authorities.

247 24-7 passive seismic detection and hodograms were used to identify a HDF. In
248 this instance, and likely others due to short RabT flow paths, the 15 second event
249 duration is too brief for live warnings but allows for 24/7 event detection and rapid
250 response, outside of time-lapse image capture. Additional seismometers (now
251 deployed) extend the range of detection and allow more traditional geo-location.

252 On-site sensor systems can indicate raised risk levels and landslide detection
253 for authorities, improving their ability to act. Low-cost sensors can be replicated at
254 high-risk sites and lower risk sites where cost-benefit would normally prevent
255 monitoring. Increased high-intensity rainfall due to climate warming is expected in
256 Scotland (UKCP, 2018) and more sites will have increased debris-flow risk; greater
257 low-cost monitoring capacity is a necessary advancement.

258

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265

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381

382 **FIGURE CAPTIONS**

383 **Figure 1. RabT landslide inventory. (A) Site regional context. Vulnerability**
384 **shadow outlined in orange (modified from Winter et al. 2019a). (B) TLS derived**
385 **hillshade and 2007 to 2019 landslide source areas, coloured by autumn-winter**
386 **season (Sept-Feb), Spring (Spr) or Summer (Sum). Dashed lines delineate**

387 surface material (modified from Finlayson, 2020). Landslide numbers refer to
388 Figure 2. (C) 2003 to 2019 cumulative landslide timeseries and yearly totals.

389

390 Figure 2. (A) BEAST seasonal rainfall trend. (B) BEAST rainfall trend. (C)
391 01/09/18 to 31/12/18 landslide timeline. (D) Wig-wag and on-slope alert
392 operation confusion matrix. (E) September to December rainstorm intensity-
393 duration (I-D) plot. (F) Antecedent Precipitation Index (API) with 37 mm and 62
394 mm thresholds. Rainfall intensity (data loss 13/11-05/12) with storms >10h
395 duration exceeding the I-D threshold. (G) API and I-D threshold confusion
396 matrix.

397

398 Figure 3. (A) PIVLab deformation vector plot (Thielicke and Stamhuis, 2014). (B)
399 Velocity heat map. (C) Cumulative rainfall, cumulative deformation and I-V.

400

401 Figure 4. (A) Pre-failure HDF source and seismometer location. (B) Post-failure.
402 (C) Fifteen-minute seismogram with HDF signal (red box) and three hodogram
403 time-steps (i, ii, iii). (D) Hillshade with HDF location and ten second stacked
404 hodogram.

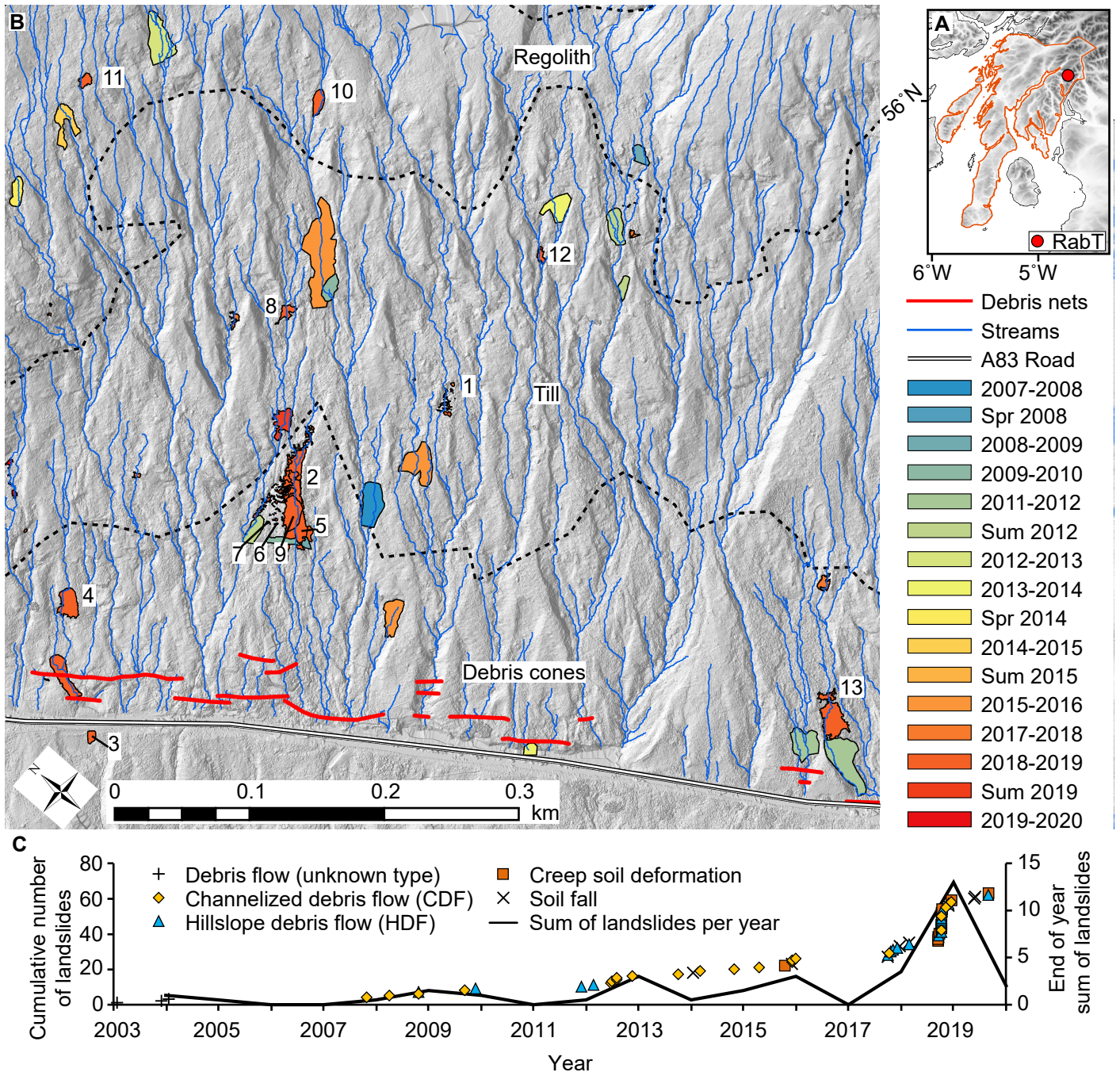


FIGURE 1
 Author - Bainbridge et al.,

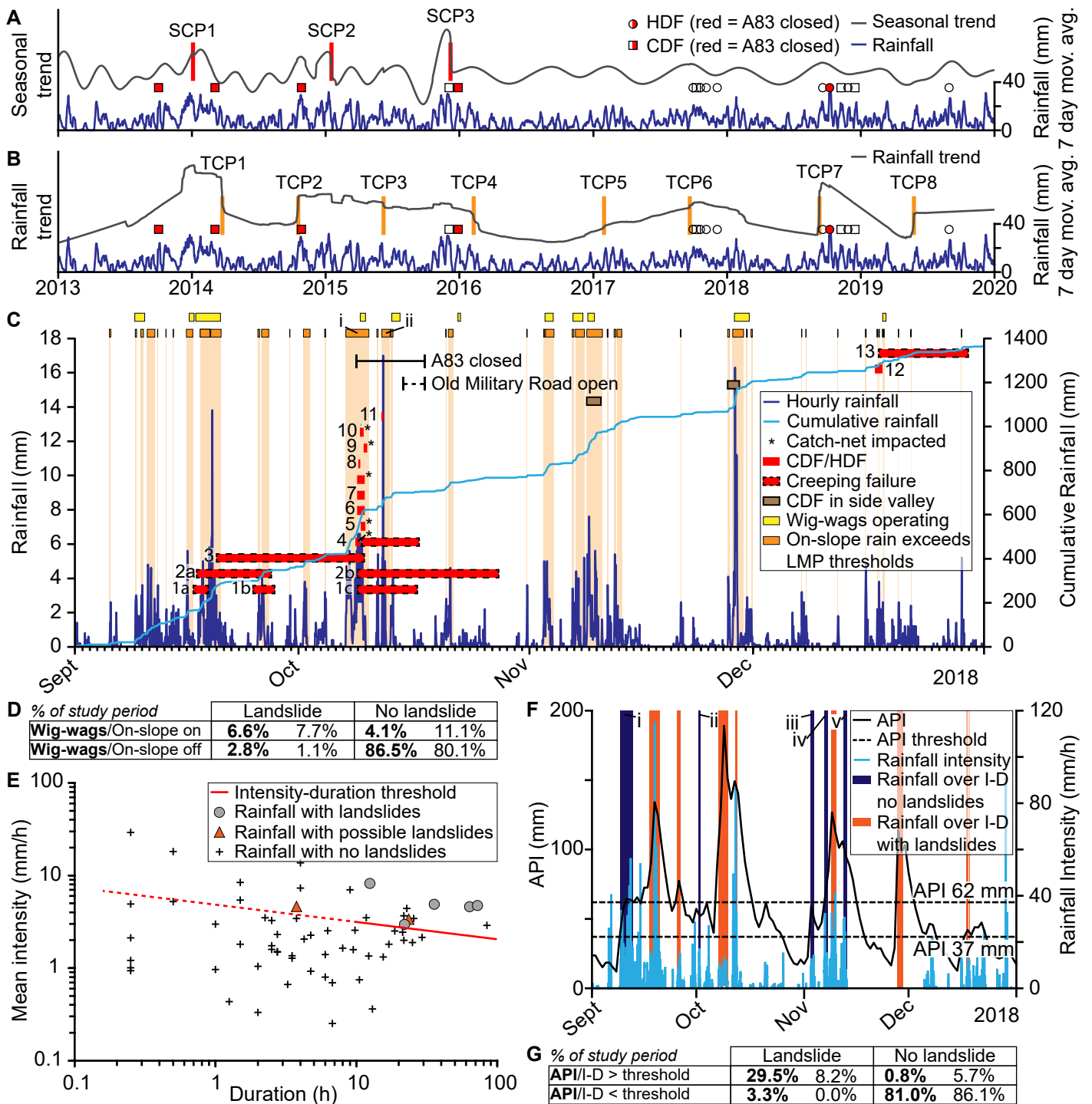


FIGURE 2
Author - Bainbridge et al.,

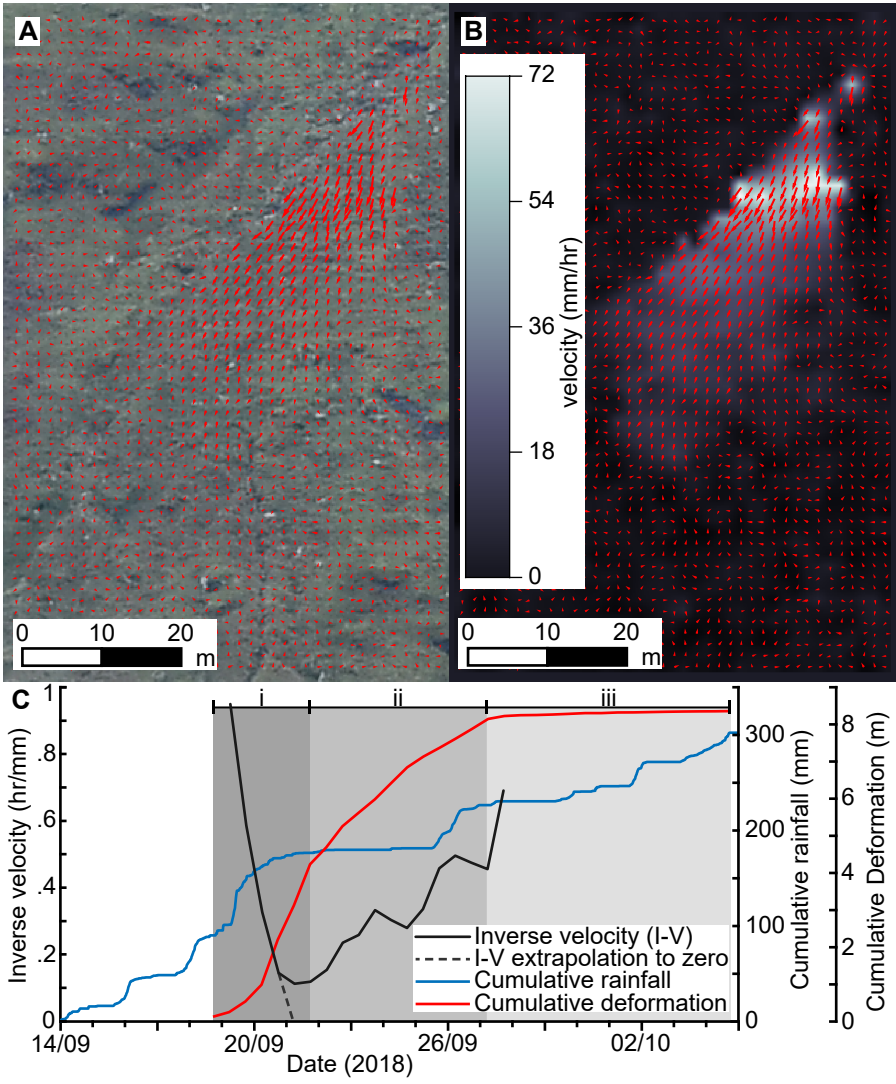


FIGURE 3
 Author - Bainbridge et al.,

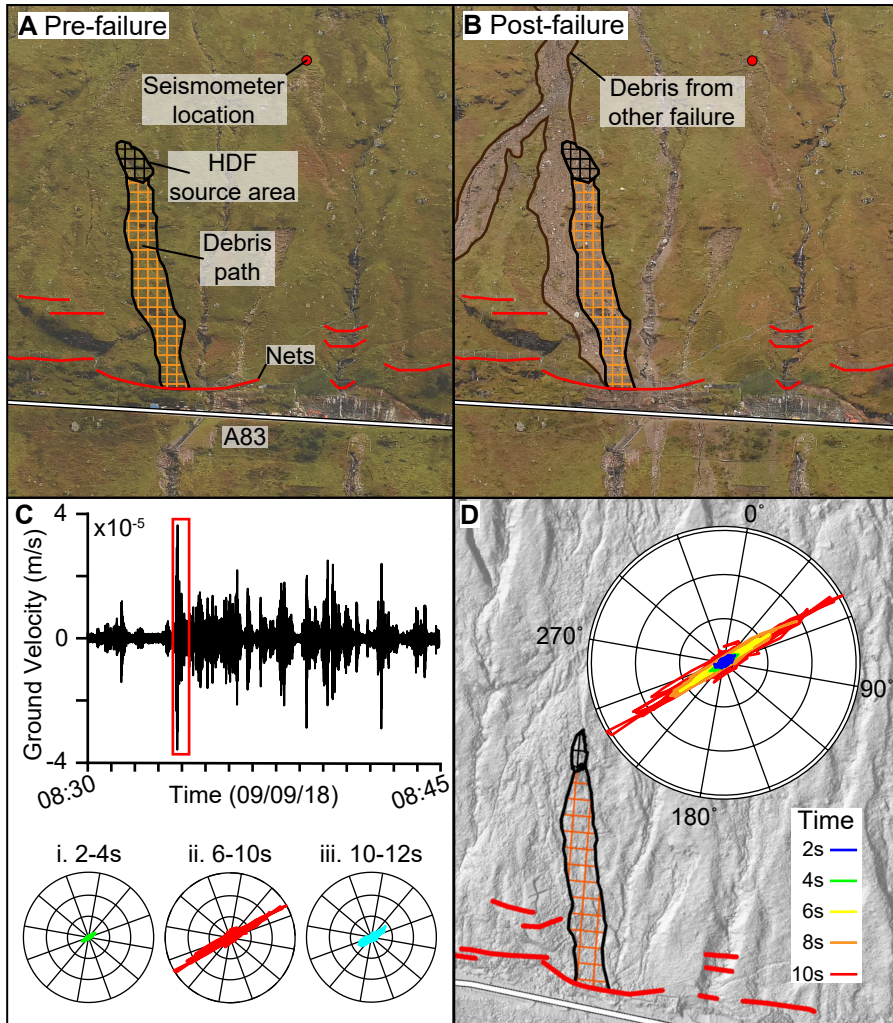


FIGURE 4
 Author - Bainbridge et al.,