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Abstract	debated. Using a fully Great Barrier Reef agai Solomon Islands eartho landslide source that ha Knolls Slide), and a po Great Barrier Reef acts bathymetric features (i. However, the buffering When coral cover is ren offshore wave amplitud where they tend to dou incited by higher-ampl coral. At a site-specific of protectiveness again	reefs may provide a beneficial first line of defence against tsunami hazards, though this is currently ed. Using a fully nonlinear, Boussinesq propagation model, we examine the buffering capacity of the Barrier Reef against tsunamis triggered by several hypothetical sources: a series of far-field, non Islands earthquake sources of various magnitudes ( $M_w$ 8.0, $M_w$ 8.5, and $M_w$ 9.0), a submarine ide source that has previously been documented in the offshore geological record (i.e. the Gloria s Slide), and a potential future landslide source (i.e. the Noggin Block). We show that overall, the Barrier Reef acts as a large-scale regional buffer due to the roughness of coral cover and the comple metric features (i.e. platforms, shoals, terraces, etc.) that corals construct over thousands of years. ever, the buffering effect of coral cover is much stronger for tsunamis that are higher in amplitude. coral cover is removed, the largest earthquake scenario ( $M_w$ 9.0) exhibits up to a 31% increase in ore wave amplitude and estimated run-up. These metrics increase even more for landslide scenarios, they tend to double. These discrepancies can be explained by the higher bed particle velocities d by higher-amplitude waves, which leads to greater frictional dissipation at a seabed covered by At a site-specific level, shoreline orientation relative to the reef platforms also determines the degre tectiveness against both types of tsunamis, where areas situated behind broad, shallow, coral-covere rms benefit the most. Additionally, we find that the platforms, rather than gaps in the offshore reef	

	structure, tend to amplify wave trains through wave focussing when coral cover is removed from simulations. Our findings have implications for future tsunami hazards along the northeastern Australian coastline, particularly as the physiological stressors imposed by anthropogenic climate change further exacerbate coral die-off and reductions in ecosystem complexity. Therefore, areas that experience a protective benefit by the Great Barrier Reef's platforms could be disproportionately more vulnerable in the future.
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# Examining the impact of the Great Barrier Reef on tsunami propagation using numerical simulations

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# 7 Abstract

8 Coral reefs may provide a beneficial first line of defence against tsunami hazards, though 9 this is currently debated. Using a fully nonlinear, Boussinesq propagation model, we exam-10 ine the buffering capacity of the Great Barrier Reef against tsunamis triggered by several 11 hypothetical sources: a series of far-field, Solomon Islands earthquake sources of various magnitudes (M<sub>w</sub> 8.0, M<sub>w</sub> 8.5, and M<sub>w</sub> 9.0), a submarine landslide source that has previ-12 13 ously been documented in the offshore geological record (i.e. the Gloria Knolls Slide), and 14 a potential future landslide source (i.e. the Noggin Block). We show that overall, the Great 15 Barrier Reef acts as a large-scale regional buffer due to the roughness of coral cover and 16 the complex bathymetric features (i.e. platforms, shoals, terraces, etc.) that corals construct 17 over thousands of years. However, the buffering effect of coral cover is much stronger for 18 tsunamis that are higher in amplitude. When coral cover is removed, the largest earthquake 19 scenario ( $M_{y}$ , 9.0) exhibits up to a 31% increase in offshore wave amplitude and estimated 20 run-up. These metrics increase even more for landslide scenarios, where they tend to dou-21 ble. These discrepancies can be explained by the higher bed particle velocities incited by 22 higher-amplitude waves, which leads to greater frictional dissipation at a seabed covered 23 by coral. At a site-specific level, shoreline orientation relative to the reef platforms also 24 determines the degree of protectiveness against both types of tsunamis, where areas situ-25 ated behind broad, shallow, coral-covered platforms benefit the most. Additionally, we find 26 that the platforms, rather than gaps in the offshore reef structure, tend to amplify wave 27 trains through wave focussing when coral cover is removed from simulations. Our findings 28 have implications for future tsunami hazards along the northeastern Australian coastline, 29 particularly as the physiological stressors imposed by anthropogenic climate change fur-30 ther exacerbate coral die-off and reductions in ecosystem complexity. Therefore, areas that 31 experience a protective benefit by the Great Barrier Reef's platforms could be dispropor-32 tionately more vulnerable in the future.

<sup>33</sup> Keywords Coral reef · Tsunami · Great Barrier Reef · Submarine landslide · Earthquake ·
 <sup>34</sup> Numerical simulation

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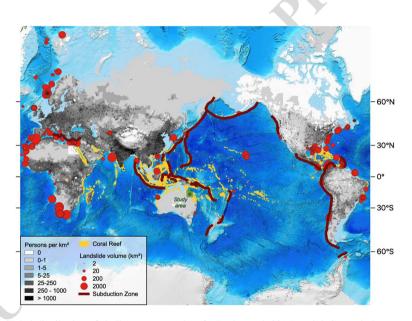
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### 35 1 Introduction

36 Tsunamis threaten low-lying coastal communities around the world. Coral reef ecosys-37 tems, many of which are positioned between tsunami source regions and densely populated 38 shorelines (Fig. 1), could provide a broad, cost-effective first line of defence for coastal 39 zones (Ferrario et al. 2014). While field-based studies suggest that coral reefs induce effi-40 cient energy attenuation in wind waves due to their structural complexity (Sheppard et al. 41 2005; Ferrario et al. 2014; Gallop et al. 2014), a lack of consensus endures surrounding 42 their protectiveness against tsunamis.

Following a similar logic, some post-inundation field surveys (Fernando et al. 2005; 43 McAdoo et al. 2011) and modelling studies (Shao et al. 2019) have concluded that, due to 44 their structural complexity, coral reef ecosystems impart similar drag-induced attenuation 45 of wave energy on tsunamis. Other field-based studies (McAdoo et al. 2009; Fritz et al. 46 2011; Gelfenbaum et al. 2011) and modelling work (Kunkel et al. 2006; Yao et al. 2012; 47 Roger et al. 2014) echo these conclusions, but with caveats. For instance, some authors 48 caution that the buffering effect of the reef depends on where the reef is located relative to 49 a coastal community or built asset (McAdoo et al. 2009; Fritz et al. 2011), and that wider 50 reefs, preferably those with an extensive reef flat, appear to dissipate tsunami energy more 51 effectively than narrower fringing reefs (Kunkel et al. 2006; Gelfenbaum et al. 2011; Yao 52



**Fig. 1** Global distribution of shallow-water coral reefs (Burke et al. 2011) and their proximity to tsunamigenic sources, including large submarine landslides or landslide complexes (>1 km<sup>3</sup>; see Online Resource 1 for table of landslide events) and submarine convergent plate boundaries that constitute source zones of major tsunamigenic earthquakes. Landslides are plotted as red circles sized proportionally to the natural log of a given landslide's volume. This compilation is based on several reviews (Hampton et al. 1996; Elvenhøi et al. 2002; Owen et al. 2007; Lee 2009; Urlaub et al. 2013; Harbitz et al. 2014; Papadopoulos et al. 2014; Moscardelli and Wood 2016), where landslides with estimated volumes of 1 km<sup>3</sup> were excluded. All original references documenting each of the plotted slides are provided in the reference list of this study. Landmasses are overlaid with gridded UN-adjusted population density for 2020 (CIESIN 2018), with ETOPO1 as the base map (Amante and Eakins 2009)

et al. 2012; Roger et al. 2014). Conversely, others have proposed that coral reefs offer marginal to no protective benefit against tsunamis (Baird et al. 2005; Uslu et al. 2010). Further still, some field-based (Nott 1997; Chatenoux and Peduzzi 2005, 2007; Fritz et al. 2011) and modelling work (Roeber et al. 2010; Gelfenbaum et al. 2011; Yao et al. 2012; Ford et al. 2014) suggest that reefs can actually exacerbate damage along neighbouring coastlines. While there is near-universal consensus that inter-reef passages (or "gaps/openings" between reefs) can amplify tsunami waves, some argue that these amplification effects, along with other effects such as intra-lagoon resonance and increased shoaling/bore formation over shallow reef platforms, undermine any protective benefit that the presence of the reef would otherwise offer (Chatenoux and Peduzzi 2005; Liu et al. 2005; Roeber et al. 2010; Gelfenbaum et al. 2011; McAdoo et al. 2011; Ford et al. 2014; Roger et al. 2014). 63 Despite the wide variety of methods and case studies employed to investigate this topic, the 64 impact of coral reef ecosystems on tsunami propagation remains unclear. 65

Ongoing threats to the health and longevity of coral reefs under a changing climate 66 (De'ath et al. 2012; Hughes et al. 2018) heighten these uncertainties. Decades-long field-67 based studies reveal declines in both coral cover and ecosystem structural complexity as 68 critical reef-building species disappear from coral communities, leading to a progressive 69 "flattening" of reefs (Alvarez-Filip et al. 2009; Bozec et al. 2015; Spalding and Brown 70 2015). It has been proposed that this decline in coral cover will reduce the protectiveness 71 of coral reefs against other common coastal hazards, such as flooding, wind-wave expo-72 sure (both under fair weather and stormy conditions), and rising sea levels (Quataert et al. 73 2015; Harris et al. 2018; Storlazzi et al. 2018). The literature surrounding the impact of 74 anthropogenically mediated coral decline on tsunami hazards is less conclusive. How-75 ever, some evidence from post-tsunami field surveys suggests that direct coral removal by 76 means of mining and poaching intensifies tsunami wave heights and inundation extents at 77 a local level (Fernando et al. 2005). In light of recent coral reef decline, and in the wake 78 of recent significant tsunami events (e.g., the 2004 Indian Ocean tsunami, the 2009 South 79 80 Pacific tsunamis, and the 2011 Tohoku tsunami), a concerted effort has emerged to more rigorously assess both the present and future coastal buffering role of coral reef ecosystems 81 against tsunamis (Chatenoux and Peduzzi 2007; Ferrario et al. 2014; Spalding et al. 2014), 82 and this study is a contribution to that effort. 83

The Great Barrier Reef (GBR), the world's largest coral reef system, is an iconic fea-84 ture of Australia's coastal landscape. Despite Australia's proximity to the seismically active 85 source regions (Dominey-Howes 2007; Davies and Griffin 2018), the manner in which 86 tsunami behaviour is regulated by the GBR, which partitions Australia's coastline from 87 these convergent margins, is not well understood (Webster et al. 2016). Additionally, the 88 discovery of large (volume >  $30 \text{ km}^3$ ) landslide scars and slumps on the nearby continental 89 slope (Puga-Bernabéu et al. 2016, 2019) warrants an investigation into the GBR's ability to 90 protect against landslide-generated tsunamis. Though believed to occur less frequently than 91 their coseismic counterparts, landslide-generated tsunamis such as the 1998 Sissano, Papua 92 New Guinea event (Synolakis et al. 2002) can occur suddenly within close proximity to 93 the shoreline, causing significant localized damage and limiting opportunities for warning 94 and swift response. This, along with the existence of possible paleo-tsunami deposits along 95 the adjacent coastline (Nott 1997), underscores an urgency to quantify the GBR's widely 96 speculated role as a regional buffer from these hazards (Baba et al. 2008; Puga-Bernabéu 97 et al. 2013a; Wei et al. 2015; Xing et al. 2015; Webster et al. 2016). However, like most 98 coral reefs worldwide, the GBR has not escaped the consequences of anthropogenic cli-99 mate change (De'ath et al. 2012; Hughes et al. 2018), and therefore, the buffering capacity 100 of the GBR remains uncertain. 101

Thus far, a large portion of the debate surrounding coral reef protectiveness against

102

tsunamis is based on findings from post-tsunami field surveys and anecdotal eye-witness 103 accounts (Baird et al. 2005; Fernando et al. 2005; Liu et al. 2005). However, the degree of 104 а coral reef's influence cannot be quantified solely from these field-based techniques. As 105 many others have highlighted (Chatenoux and Peduzzi 2005; Kunkel et al. 2006; McAdoo 106 et al. 2009; Uslu et al. 2010; Roger et al. 2014; Dilmen et al. 2018), several confounding 107 factors can influence tsunami run-up, such as the extent of coral cover, the nature and prox-108 imity of the tsunami triggering source, and site-specific variability in coastal bathymetry 109 and topography. Therefore, following a tsunami event, it is difficult to retrospectively ascer-110 tain the impact of coral reefs in isolation from these other site-specific factors. Numeri-111 cal simulations can provide additional insights into tsunami behaviour (e.g., Kunkel et al. 112 2006), where experiments can be designed to systematically test the impact of coral cover 113 and reef platform bathymetry on tsunami attenuation while keeping all other parameters, 114 initial conditions, and boundary conditions constant (e.g., Kunkel et al. 2006). Previous 115 studies have aimed to assess the overall impact of the GBR on tsunami propagation using 116 numerical simulations (Baba et al. 2008; Wei et al. 2015; Xing et al. 2015; Webster et al. 117 2016). However, they do not account for smaller-scale structural complexity introduced by 118 coral cover on reef platforms, and they only consider one type of tsunami source at a time. 119

Using numerical modelling, we evaluate the GBR's ability to shield the northeast-120 ern Australian coastline from a range of hypothetical, though plausible tsunami sources. 121 Firstly, we consider a Solomon Islands earthquake source over various magnitudes ( $M_w$ ) 122 8.0,  $M_w$  8.5, and  $M_w$  9.0). Additionally, we consider two near-field landslide tsunami 123 sources: (1) the largest documented submarine landslide event on the GBR margin (i.e. the 124 Gloria Knolls landslide complex; Puga-Bernabéu et al. 2016), and (2) a potential collapse 125 of a feature on the upper continental slope known as the Noggin Block (Puga-Bernabéu 126 127 et al. 2013a).

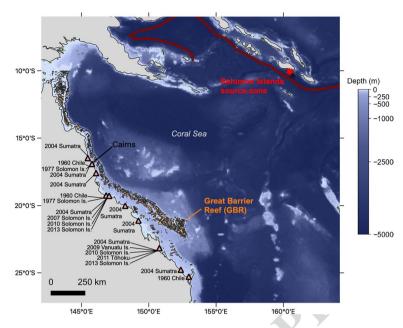
In the first of a series of tsunami propagation model runs, for each tsunami source, we 128 129 numerically simulate the tsunamis assuming healthy coral cover conditions (i.e. "coralcovered platforms" scenarios), where reef platforms are prescribed high roughness to 130 reflect their structural complexity (Nelson 1996). Then, we simulate the tsunamis with 131 smoothed reef platforms (i.e. "smooth platforms" scenarios), where we isolate the impact 132 of live coral cover on wave attenuation (Sheppard et al. 2005). Following the methods of 133 Baba et al. (2008), we further sequester the region's bathymetric complexity by completely 134 excising the reef platforms from the shelf and simulating tsunami propagation with altered 135 bathymetry (i.e. "no reef platforms" scenarios), allowing us to assess the platform-scale 136 buffering capacity of the entire reef structure. We further test the impact of tidal phase 137 on the buffering capacity of the GBR. We then draw upon these findings to consider the 138 broader implications regarding present and future coral reef defence to densely inhabited, 139 low-lying coastal areas. 140

#### 141 2 Study area

#### 142 2.1 Regional setting

The central northeastern Australian margin is a passive margin characterised by a relatively broad (~60 km) continental shelf (Fig. 2). The spring tidal range varies from north to south, but the region is generally meso- to macro-tidal (Andrews and Bode 1988). Several

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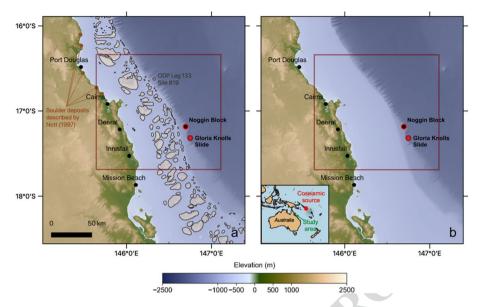
**Fig. 2** Regional view of the Solomon Islands source zone, the Coral Sea, and the northeastern Australian margin, which includes the GBR (orange). Also plotted are the locations along the Australian coastline where historical tsunamis that exceeded maximum water heights of 10 cm have been observed using tide gauges (triangles; NGDC/WDS 2020). The red line indicates the subduction zones that traverse the Solomon Islands source zone

environmental factors favour coral reef growth on the mid- to outer-continental shelf, 146 including the region's tropical climate, shallow seas, far proximity from terrestrial run-off, 147 and nutrient-poor oceanographic conditions. Over hundreds of thousands of years of eus-148 tatic sea level fluctuations, these coral reef ecosystems have constructed large (up to  $\sim 300$ 149 km<sup>2</sup>) submerged and semi-submerged carbonate platforms, pinnacles, and terraces, which 150 comprise the offshore reef structure (Hopley et al. 2007; Hinestrosa et al. 2016). This reef 151 structure, which underlies the modern generation of living coral cover, extends roughly 152 2,300 km along the mid- to outer shelf (Hopley et al. 2007). On the central margin, broad, 153 arcuate patch reef platforms are separated by relatively wide (up to ~10 km) inter-reef pas-154 sages, or "gaps" (Fig. 3). While these passages are wide enough to allow some wind waves 155 to propagate through to the inner shelf, much of the energy transferred by wind waves is 156 attenuated atop the reef platforms (Young 1989; Gallop et al. 2014). 157

#### 158 2.2 Historical and pre-historic tsunami record

Historically, northeastern Australia has been affected by tsunamis originating from multiple regions contained within the Pacific Ring of Fire (e.g. Chile, Tonga, and more recently, Sumatra and Japan; see Fig. 2). Notably, a large proportion of these historical tsunami events were triggered within subduction zones in the Solomon Islands region, which lies to the northeast of Australia across the Coral Sea (Dominey-Howes 2007; Australian Bureau of Meteorology 2020; NGDC/WDS 2020). A nationwide, probabilistic tsunami hazard assessment revealed that the Solomon Islands source zone poses the greatest hazard to the

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**Fig. 3** a Bathymetry used in the "coral-covered platforms" and "smooth platforms" simulations. **b** Bathymetry used in the "no reef platforms" simulations. Also shown are the Gloria Knolls Slide, Noggin Block, ODP Leg 133 Site 819, the locations of the boulder deposits described by Nott (1997) and the location of the hypothetical Solomon Islands coseismic sources

northeastern Australian town of Cairns and the surrounding area (Davies and Griffin 2018).
Therefore, the Solomon Islands source zone was selected to simulate a range of hypothetical earthquake-generated tsunami events for this study. In contrast, the pre-historic tsunami
record in northeastern Australia is much more sparse (Dominey-Howes 2007). Nonetheless, previous work has described boulder deposits that were speculated to have been
emplaced by tsunami waves (Nott 1997; Fig. 3).

### 172 2.3 Submarine landslides and areas of potential future collapse

Since the collection of high-resolution multibeam bathymetry in 2007 (Webster et al. 173 2008), a wide variety of submarine landslides have been described on the shelf-edge, 174 upper, mid, and lower-slope (Puga-Bernabéu et al. 2016, 2019; Webster et al. 2016). These 175 slides exhibit a range of different sizes and morphologies (e.g. rotational slumps, transla-176 tional slides, shovel slides, carbonate terrace collapses, etc.). While they are distributed 177 along the entirety of the margin, landslides are more commonly found on the north and 178 central sections of the margin, where the continental slope gradient is moderate to high 179 (4°–10°, Puga-Bernabéu et al. 2011, 2013b). 180

The present study focuses on two notable features on the central GBR margin. The first is the Gloria Knolls landslide complex (Puga-Bernabéu et al. 2016), which is the largest among the documented submarine landslide cases on the northeastern Australian margin (total estimated volume  $\approx 32 \text{ km}^2$ ). The entire complex is believed to have failed in multiple phases, with the estimated age of the first event pre-dating 300 ka (Puga-Bernabéu et al. 2016). Debris from the slide is visible in both sub-bottom profiles and in bathymetry, where the debris field extends ~20 km from the slide scarp. Roughly 8 km northwest of

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the Gloria Knolls slide complex lies the Noggin Block, a 4.9×3.5 km upper-slope feature that was previously identified as a potential area of future collapse (Puga-Bernabéu et al. 2013a). Pockmarks and adjacent landslide scars have also been described around the block (Puga-Bernabéu et al. 2013a). Slope stability modelling indicates that while the block is presently stable, seismic loading could potentially trigger a future failure (Puga-Bernabéu et al. 2013a).

We should note that it lies beyond the scope of this work to include a detailed catalogue, and thus a detailed hazard assessment, of landslide tsunami risk on this margin. A complete catalogue of all submarine landslides on the GBR margin is currently the subject of future work (Puga-Bernabéu et al., in prep).

# 198 3 Methods

### 199 3.1 Tsunami generation

### 200 3.1.1 Earthquake sources

To simulate tsunami generation by an earthquake source, the code Geowave (Watts et al. 201 2003) was used to produce the initial ocean free surface deformation for the hypothetical 202  $M_{w}$  8.0, 8.5, and 9.0 coseismic events in the Solomon Islands source zone. Tsunami gen-203 eration is specifically handled in the TOPICS module of Geowave (Watts et al. 2003). The 204 code incorporates the widely implemented Okada elastic half-space formulation, which 205 relates earthquake geometric source parameters (e.g. fault width, length, strike, dip, etc.) 206 to the initial free surface deformation (Okada 1985). The Okada method has been shown to 207 adequately reproduce free surface deformation for coseismic events exhibiting an abrupt, 208 mostly vertical slip of the seafloor (Kowalik et al. 2005; Fujii et al. 2011) and specifically 209 for past events that originated in the Solomon Islands (Baba et al. 2008). Source param-210 eters were selected from the Enhanced Tsunami Scenario Database T2 (Greenslade et al., 211 2009; see Table 1), a suite of earthquake tsunami scenarios developed by the Joint Austral-212 ian Tsunami Warning Centre and the Centre for Australian Weather and Climate Research. 213 For simplicity, magnitude was altered by modifying the maximum fault slip parameter (see 214 Table 1). 215

### 216 3.1.2 Submarine landslide sources

To simulate tsunami generation by the Gloria Knolls Slide and the potential collapse of 217 the Noggin Block, we used NHWAVE (Ma et al. 2013), a non-hydrostatic wave model that 218 has been successfully validated in laboratory settings (Enet and Grilli 2007; Tehranirad 219 et al. 2012) and has been used for several case studies of submarine mass failure-induced 220 tsunamis (Tappin et al. 2014; Grilli et al. 2015; Li et al. 2015; Schnyder et al. 2016). The 221 code numerically approximates the solutions to non-hydrostatic Navier-Stokes equations 222 for incompressible flow in three dimensions, implementing a terrain-following (i.e. sigma-223 layered) vertical coordinate system. For simplicity and computational efficiency, a three-224 dimensional, rigid, translational failure was assumed for both cases, where the bottom 225 boundary condition is dictated by a time-varying change in depth imparted by an approxi-226 mately Gaussian-shaped slide. 227

**Author Proof** 

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Hypothetical Solomon Islands earthquake cases	cases		Landslide cases		
	8			Gloria Knolls slide (worst-case scenario)	Noggin block potential land- slide
Mw	8.0	8.5 9.0	Latitude	17°19'21.9"S	18°46'48"S
Maximum slip distance (m)	0.8	4.4 24.7	Longitude	146°45'07.4"E	148°12'01"E
Centroid latitude	9°50'13.2"S		Length $b$ (m)	3947	4900
Centroid longitude	160°37'55.2"E		Width $w$ (m)	19,200	3500
Strike (°)	300		Maximum thickness $T(m)$	288	150
Dip (°)	30		Slide volume (km <sup>3</sup> )	6.51	0.767
Slip rake (°)	06		Initial submergence depth $d(m)$	420	600
Fault length (km)	400		Mean slope $\theta$ (°)	18.6	5.00
Fault centroid depth (km)	10		Slide density (kg/m <sup>3</sup> )	2000	2000
Fault width perpendicular to strike (km)	80		Slide terminal velocity (m/s)	25.0	25.0
Shear modulus (Pa)	$4.5\cdot 10^{10}$		Initial acceleration $a_{\alpha}$ (m/s <sup>2</sup> )	0.966	0.280

slide volumes were calculated using the formulas of Enet and Grilli (2007), which are incorporated into NHWAVE

NHWAVE requires approximate landslide dimensions (i.e., length, width, thickness) 228 to construct the Gaussian-shaped slide that generates the initial tsunami. For both land-229 slide cases, these dimensions were determined in previous work (Puga-Bernabéu et al. 230 2013a, 2016, 2019), and were thus adopted here (see Table 1). For the Gloria Knolls Slide, 231 slide dimensions were determined using bathymetry data containing the slide scar (Puga-232 Bernabéu et al. 2016, 2019). The slide is believed to have failed sequentially in multiple 233 phases, forming what is known as a larger "slide complex". Here, we modelled what was 234 determined to be the worst-case scenario of these failure phases (i.e., "Event 2, Worst-Case 235 Scenario", see Puga-Bernabéu et al. 2019). This case was selected to represent one of the 236 most severe submarine landslide cases for this region, as the Gloria Knolls Slide is, thus 237 far, the largest documented slide complex (total volume  $\approx 32 \text{ km}^3$ ) on the northeastern 238 Australian margin (Puga-Bernabéu, in prep). For the Noggin Block, the initial dimensions 239 were determined from a rigorous, modelling-based slope stability analysis conducted for 240 the block (Puga-Bernabéu et al. 2013a). This feature is comparatively small; the estimated 241 slide volume is ~0.77 km<sup>3</sup> (using the volume formulas of Enet and Grilli 2007). However, 242 the block is relatively shallow, resting on the upper slope ( $\sim 400$  m). An additional sensitiv-243 ity analysis was conducted to test the impact of failure depth on the initial tsunami wave 244 height (see Sect. 4.2). 245

For both landslide cases, kinematic parameter  $a_0$  was determined using the semi-empir-246 ical formulations of Enet and Grilli (2007), and the peak slide velocity was prescribed a 247 value of 25 m/s. This peak velocity is of similar magnitude to those recorded by submarine 248 cable breaks during the Grand Banks Event (i.e., 20-25 m/s; Fine et al., 2005). A landslide 249 density of 2000 kg/m3 was informed by sediment core measurements obtained by Ocean 250 Drilling Program (ODP) Leg 133 Site 819, which was drilled ~70 km north of the Nog-251 gin Block and the Gloria Knolls Slide (Davies et al. 1991). Each simulation was run for a 252 landslide failure duration of 3 min at 100 m resolution horizontally and at 5 sigma layers 253 vertically. 254

#### 255 3.2 Tsunami propagation

The resulting ocean free surface elevations, as well as the depth-averaged zonal and meridi-256 onal velocities, were smoothed and re-interpolated from the tsunami generation model out-257 puts to set the initial conditions for the wave propagation model. Tsunami propagation was 258 modelled using FUNWAVE-TVD (Shi et al. 2012), a widely used, fully nonlinear Bouss-259 inesq tsunami propagation code that has been validated against NOAA's National Tsunami 260 Mitigation Program benchmark requirements (NTHMP, 2012). The model captures wave 261 behaviours such as shoaling, dissipation via bottom friction and wave breaking, and fre-262 quency dispersion (Shi et al. 2012). 263

For the earthquake scenarios, tsunami propagation was simulated across the Coral Sea 264 using a 1 arcminute ETOPO1 grid (Amante and Eakins 2009). Smaller nested grids of 265  $200 \times 200$  m resolution were used to resolve the earthquake-generated waves upon arrival 266 to the continental shelf. These grids were generated from a 100 m resolution bathymet-267 ric dataset spanning the entire northeastern Australian margin, including the GBR (i.e. 268 269 "3DGBR", Beaman 2010; see Fig. 3a). Waves were introduced into the smaller nested grids via a one-way coupling scheme. Near-field landslide scenarios were also simulated 270 with grids generated from the 3DGBR bathymetric dataset. Bathymetry for all cases was 271 smoothed using a Gaussian filter to prevent numerical instability incited by steep bathym-272 etric slopes. 273

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The spatial resolution of the model domains was carefully selected using a range of sensitivity analyses (see Online Resource 2). For the earthquake scenarios, a  $200 \times 200$  m grid is deemed sufficient to resolve interactions between the propagating waves and the seafloor. The Gloria Knolls Slide and the Noggin Block potential failure necessitated finer resolution grids to adequately resolve shoaling and scattering processes (100 m and 50 m resolution, respectively).

It is important to note here that although Geowave also has the ability to simulate 280 tsunami generation and propagation by both coseismic slip and landslide sources, we 281 opted to use updated models that more explicitly resolve processes involved in landslide 282 tsunami generation (i.e. the non-hydrostatic formulations of NHWAVE) and more accu-283 rately represent frequency dispersion of propagating gravity waves (i.e. the improved 284 fully nonlinear, Boussinesq formulations of FUNWAVE-TVD). Dispersive effects 285 become more critical to simulate for far-field and landslide tsunami sources (Tehranirad 286 et al. 2015). 287

#### 288 3.3 Run-up estimation

In the absence of the nearshore high-resolution bathymetric and topographic data (< 50 m) required to accurately resolve onshore tsunami inundation, final estimated run-up distributions were calculated using virtual tide gauges placed along the shoreline in ~25 m water depth *d* using the following equation:

293 294

$$R = A(d)^{\frac{4}{5}} \cdot d^{\frac{1}{5}}$$
(1)

where *R* is the estimated run-up and A(d) is the maximum wave amplitude at a virtual gauge location at depth *d*. This formula is based on the conservation of wave energy flux and applies to both breaking and non-breaking waves (Ward and Asphaug 2003).

k

# 298 3.4 Testing the impact of the GBR on tsunami propagation

A major objective of this study is to test whether the structural complexity of the GBR 299 300 plays a role in attenuating tsunami wave energy. The GBR exhibits structural complexity at two predominant spatial scales. Firstly, due to the morphological diversity of individual 301 species, coral cover is structurally complex on the meter to sub-meter scale (Nelson 1996; 302 Graham and Nash 2013). We hereafter refer to the structural complexity of coral cover 303 as "ecosystem-scale" complexity. In a modelling context, this "ecosystem-scale" com-304 plexity cannot be resolved in the computational domain and must be parameterized (see 305 Sect. 3.4.1). Secondly, the GBR exhibits structural complexity at the > 1 km scale. The 306 reef structure itself is composed primarily of completely submerged or semi-submerged 307 carbonate platforms. These features create complex positive relief on the submerged con-308 tinental shelf, and much of this relief (aside from smaller, deeper pinnacles and terraces) 309 is resolved by the 100 m resolution 3DGBR bathymetric dataset (Beaman 2010). Thus, the 310 reef structure can be adequately resolved in the computational domain. We hereafter refer 311 to complexity introduced by the reef structure as "bathymetric-scale" complexity. 312

The following sections detail how the impact of GBR's structural complexity at both the ecosystem scale and bathymetric scale was tested.

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# 315 3.4.1 Ecosystem-scale complexity: coral cover parameterization

316 In FUNWAVE-TVD, bottom shear stress  $\tau$  is calculated using the standard quadratic 317 drag law (Shi et al. 2016):

318

$$\tau = \frac{1}{2}\rho C_D U^2 \tag{2}$$

320 where  $C_D$  is the non-dimensional bottom friction coefficient,  $\rho$  is the density of water, and U is the particle velocity at the seabed. A variable bottom friction coefficient was 321 established throughout the domain, where it was altered according to the presence or 322 absence of coral cover on reef platforms. A value of  $C_D = 0.1522$  was prescribed to reef 323 platforms to simulate coral cover (average depth of platforms  $\approx 14.9$  m). This value was 324 obtained from a prior field investigation of the hydraulic roughness of coral reefs, which 325 was conducted at John Brewer Reef, a reef platform within the GBR that lies close to 326 the study region (Nelson 1996; ~80 km from the computational domain). Additionally, 327 this coefficient falls well within the range of values obtained for other reefs (Monismith 328 et al. 2013). All other areas of the computational domain where prescribed the con-329 ventional value of  $C_D = 0.0025$ , which is representative of sand-covered seafloor (Grilli 330 et al. 2015). This approach was used to create the "coral cover" scenarios, where the 331 ecosystem-scale structural complexity of the GBR was taken into account in tsunami 332 propagation simulations (Fig. 3a). 333

To test the impact of coral cover on tsunami attenuation, the "coral cover" scenarios were then compared to "smooth platform" scenarios, where coral cover was effectively removed. In the "smooth platform" scenarios, all areas of the bottom boundary, reef platforms included, were prescribed a standard bottom friction coefficient value of  $C_D = 0.0025$ .

### 339 3.4.2 Bathymetric-scale complexity: testing the impact of the reef platforms

Larger-scale, bathymetric complexity is introduced by the reef structure itself, which is 340 composed primarily of reef platforms. Testing the impact of these platforms on tsunami 341 propagation requires artificial bathymetry, where the positive relief formed by the plat-342 forms is removed from the shelf (Fig. 3b). Platforms were removed by "cookie-cutting" the 343 bathymetry, removing areas of the mid- to outer-shelf containing the reef platforms. The 344 bathymetry was then linearly interpolated and smoothed over the cookie-cut areas employ-345 ing a Gaussian filter. This modified bathymetry was then used in the "no reef platforms" 346 scenarios. 347

# 348 3.5 Testing the additional effect of tidal phase

As the central northeastern Australian margin is a meso-tidal environment, water depths over the reef platforms can vary significantly over several hours. Consequently, tidal phase has been shown to modulate the degree of wind wave attenuation (Young and Hardy 1993). To test the impact of tidal phase on tsunami propagation, two additional scenarios were configured: one where the highest spring tide (+1.75 m above MSL) and one where the lowest spring tide (-1.75 m above MSL) coincided with tsunami arrival at the GBR.

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# 355 4 Results

# 356 4.1 Earthquake tsunami generation and regional propagation

For the hypothetical  $M_w$  8.0, 8.5, and 9.0 Solomon Islands earthquake scenarios, the generation model simulates initial peak wave amplitudes of 0.32 m, 1.7 m, and 9.7 m, respectively (Fig. 4). The tsunamis in each case then propagate across the Coral Sea to the outer GBR margin after an approximately 3.5 h travel time, which is consistent with previous travel times observed for the Solomon Islands source zone (NGDC/WDS 2020). Upon

Fig. 4 Maximum wave ampli-M<sub>w</sub> 8.0 Solomon Islands Coseismic Source tudes simulated by FUNWAVE-5°S TVD for the hypothetical M., 8.0 Solomon **a**, M<sub>w</sub> 8.5 **b**, M<sub>w</sub> 9.0 **c** Solomon Islands 10°S Islands earthquake sources. Initial maximum wave amplitudes at the source are 0.32 m, 15°S 1.7 m, and 9.7 m, respectively. The simulated propagation time 20°S represented here is ~ 8 h to allow Nested domain waves to reach all parts of the Australia 25°S bathymetric domain 2.00 a 500 km 150°E 160°E 170°E 1.75 M<sub>w</sub> 8.5 Solomon Islands Coseismic Source 1.50 laximum wave amplitude 5°S Solomon Islands 10°S 1.25 15°S 1.00 20°S Nested 0.75 domain Australia 25°S b 500 km 0.50 150°E 160°E 170°E 0.25 M<sub>w</sub> 9.0 Solomon Islands Coseismic Source 5°S Solomon 0.00 Islands 10°S 15°S 20°S Nested domain Australia 25°S С 500 km 150°E 160°E 170°E

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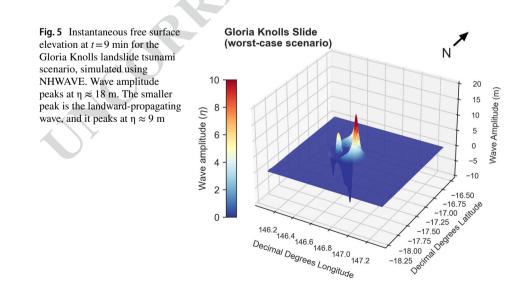
arrival to the outer Australian continental shelf within the nested domain, wave amplitudes range from ~ 1–2 cm for the  $M_w$  8.0 case, ~ 6–10 cm for the  $M_w$  8.5 case, and ~ 30–60 cm for the  $M_w$  9.0 case.

#### 365 4.2 Landslide tsunami generation

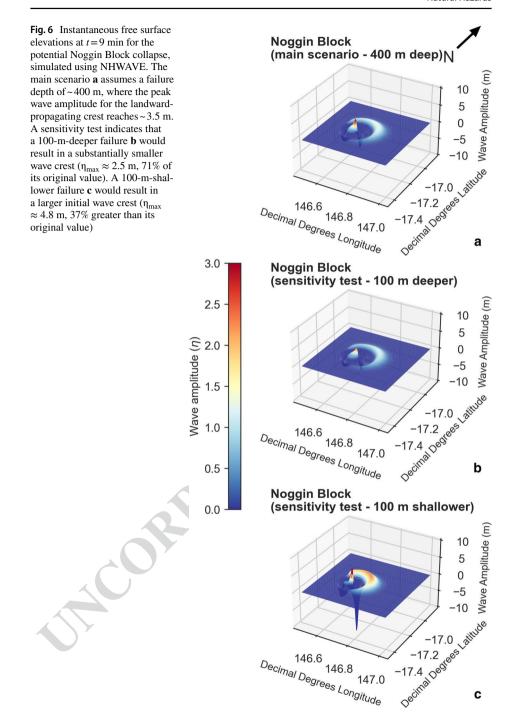
The landslide generation model NHWAVE simulates ~18 m-high seaward-propagating 366 wave crest and~9 m-high landward-propagating wave crest for the Gloria Knolls Slide 367 (Fig. 5), assuming the previously determined worst-case scenario (Puga-Bernabéu et al. 368 2019). For the potential collapse of the Noggin Block, the landslide generation model 369 simulates a~1.3 m-high seaward-propagating crest and a~3.5 m-high landward-prop-370 agating crest (Fig. 6a). Sensitivity analyses indicate that initially generated wave ampli-371 tudes are responsive to moderate changes in depth ( $\pm 100$  m). If the block was to initially 372 fail 100 m deeper (500 m depth), the wave amplitude of the landward-propagating crest 373 reaches  $\sim 2.5$  m, about 71% of its original value. On the other hand, should the block fail 374 at a 100 m-shallower depth (300 m depth), the wave amplitude peaks at ~4.8 m, grow-375 ing roughly 37%. For the subsequent simulations of tsunami propagation, the main Noggin 376 Block scenario (failure depth = 400 m) is implemented. 377

### 378 4.3 Nearshore earthquake tsunami propagation

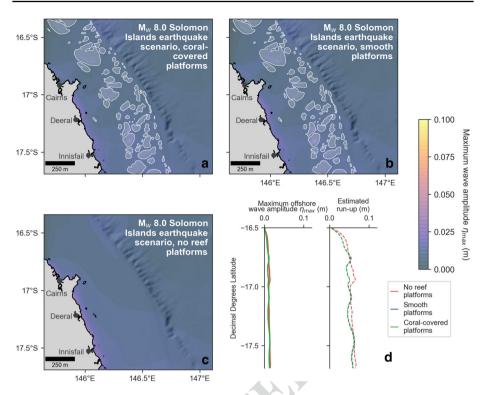
Results indicate that the GBR's buffering impact on the earthquake-generated tsunami, 379 380 which originates in the Solomon Islands source zone, depends on the magnitude of the initial earthquake. Turning firstly to the hypothetical  $M_w$  8.0 earthquake scenario (Fig. 7a), 381 maximum wave amplitudes across the domain remain under 5 cm when coral cover is pre-382 sent atop the reef platforms (i.e. when ecosystem-scale complexity is high), where maxi-383 mum estimated run-up R<sub>max</sub> reaches ~ 6.2 cm. When coral cover is removed (Fig. 7b), max-384 imum wave amplitudes increase marginally or remain the same, growing 2% on average 385 along the 25 m isobath (Fig. 7c). Estimated run-ups follow a similar trend ( $R_{max} \approx 6.4$  cm). 386



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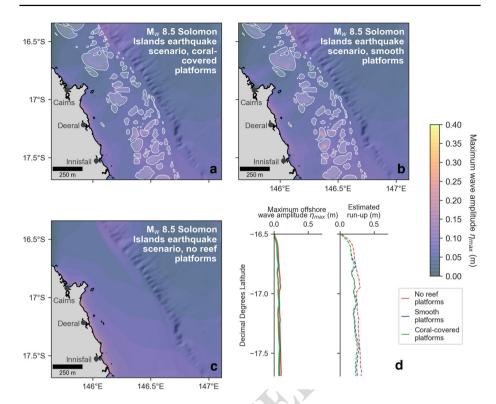
**Fig. 7** Maximum wave amplitude distributions for the hypothetical  $M_w$  8.0 Solomon Islands earthquake scenario simulated with **a** the modern "coral-covered platforms" (bottom friction coefficient  $C_D = 0.1522$  on platforms, shown in white) **b** "smooth platforms" ( $C_D = 0.025$ ), and **c** "no reef platforms". **d** Corresponding maximum offshore wave amplitude and estimated run-up distributions. Maximum run-up estimates are 6.2 cm for the "coral-covered platforms" scenario, 6.4 cm for the "smooth platforms" scenario, and 6.7 cm for the "no reef platforms" scenario. Offshore wave amplitudes were interpolated along the 25 m isobath

Finally, when reef platforms are removed from bathymetry (Fig. 7c), offshore wave amplitudes increase a bit more substantially (17% on average), but still fall below ~5 cm across the domain. The maximum run-up estimate remains at a similar elevation ( $R_{max} \approx 6.7$  cm, Fig. 7d).

391 For the hypothetical Mw 8.5 Solomon Islands earthquake scenario, the GBR, both in terms of its ecosystem-scale and bathymetric-scale complexity, appears to have slightly 392 more impact on offshore tsunami amplitudes and estimated run-up. When coral cover is 393 present (Fig. 8a), wave amplitudes landward of the GBR range from  $\sim 5-10$  cm, with an 394 Rmax estimate of  $\sim 26$  cm. When platforms are smoothed (Fig. 8b), these amplitudes grow, 395 increasing 7% on average along the 25 m isobath. The maximum run-up estimate also 396 increases slightly (Rmax  $\approx 28$  cm). Wave amplitudes similarly increase when reef plat-397 forms are removed (Fig. 8c; 13% average increase along the 25 m isobath; Rmax  $\approx$  32 cm). 398 Overall, the changes in the amplitude and run-up distributions are moderate for this case 399 (Fig. 8d). 400

The GBR has a much more substantial impact on the propagating tsunami when considering the hypothetical Mw 9.0 Solomon Islands earthquake source. Overall, the Mw 9.0-generated tsunami is significantly larger in amplitude than its smaller-magnitude

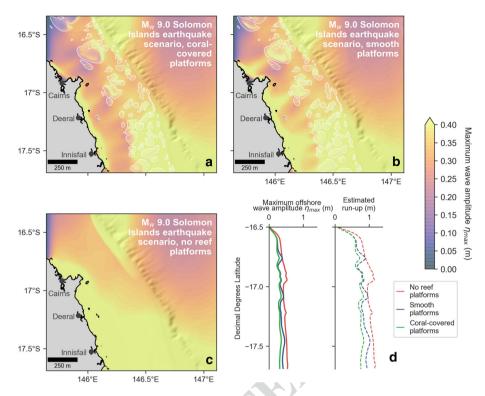
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**Fig. 8** Maximum wave amplitude distributions for the hypothetical  $M_w$  8.5 Solomon Islands earthquake scenario simulated with **a** the modern "coral-covered platforms" (bottom friction coefficient  $C_D = 0.1522$  on platforms, shown in white) **b** "smooth platforms" ( $C_D = 0.0025$ ), and **c** "no reef platforms". **d** Corresponding maximum offshore wave amplitude and estimated run-up distributions. Maximum run-up estimates are 26 cm for the "coral-covered platforms" scenario, 28 cm for the "smooth platforms" scenario, and 32 cm for the "no reef platforms" scenario. Offshore wave amplitudes were interpolated along the 25 m isobath. For animations of tsunami propagation for the "coral-covered platforms" and "no reef platforms" scenarios, see Online Resources 3 and 4

counterparts. When coral cover is present on reef platforms, maximum offshore wave 404 405 amplitudes range from about 0.2–0.4 m landward of the GBR (Fig. 9a), resulting in a maximum estimated run-up of~0.85 m. When platforms are smoothed (Fig. 9b), ampli-406 tudes increase (18% on average along the 25 m isobath), particularly directly landward of 407 broad reef platforms. Likewise, the maximum estimated run-up increases when platforms 408 are smoothed, reaching 1 m. Finally, when reef platforms are removed from bathymetry, 409 amplitudes increase substantially on the shelf (51% on average along the 25 m isobath), 410 leading to a maximum estimated run-up of  $\sim 1.2$  m (Fig. 9d). 411

Figure 10 shows the percentage increase exhibited by both offshore wave amplitude 412 and predicted run-up when both the ecosystem-scale and bathymetric-scale complexity of 413 the GBR is removed. This gives an indication of the relative degree to which the GBR 414 415 attenuates tsunami wave energy. Firstly, considering ecosystem-scale complexity isolation, 416 when coral cover is removed, under the Mw 8.0 scenario (Fig. 10a), wave amplitudes are slightly larger on a percentage-wise basis compared to when coral cover is present, rang-417 ing from 0–4% increase within the study area. For the Mw 8.5 scenario, this percentage 418 increase heightens, ranging from 1-15%. Finally, for the largest earthquake scenario (Mw 419



**Fig. 9** Maximum wave amplitude distributions for the hypothetical  $M_w$  9.0 Solomon Islands earthquake scenario simulated with **a** the modern "coral-covered platforms" (bottom friction coefficient  $C_D = 0.1522$  on platforms, shown in white) **b** "smooth platforms" ( $C_D = 0.0025$ ), and **c** "no reef platforms". **d** Corresponding maximum offshore wave amplitude and estimated run-up distributions. Maximum run-up estimates are 0.85 m for the "coral-covered platforms" scenario, 1.0 m for the "smooth platforms" scenario, and 1.2 m for the "no reef platforms" scenario. Offshore wave amplitudes were interpolated along the 25 m isobath

9.0), amplitudes increase substantially, ranging from 3-31% higher compared to when 420 coral cover is present. Percentage increases in the estimated run-up distributions follow 421 similar patterns. Amplitude and run-up increases are highly variable alongshore, with the 422 largest peaks occurring directly behind shelf areas with broad, shallow reef platforms. For 423 424 instance, the city of Cairns (latitude  $\approx 16.8^{\circ}$ S) seems to benefit from being situated behind a wide, shallow reef platform that lies in the path of the tsunami. The overall trend indi-425 cates that the attenuating effect of coral cover increases with the magnitude of the earth-426 quake source. 427

The second panel of Fig. 10 reflects the very substantial combined attenuative impact 428 of ecosystem-scale and bathymetric-scale complexity (i.e. coral cover and reef plat-429 forms). When coral cover and reef platforms are removed, wave amplitudes and run-ups 430 increase considerably for the Mw 8.0 scenario (range 0-48%). Notably, at a few locations, 431 this percentage dips marginally below zero (-5% maximum), indicating that these areas 432 would experience a decrease in offshore amplitudes and estimated run-ups if reef platforms 433 were not present. Amplitude and run-up distributions follow a similar pattern, increasing 434 overall for the Mw 8.5 (range 7–70%), and again for the Mw 9.0 (range 20–90%). These 435 results reflect the significant combined attenuative impact of both coral cover and the reef 436

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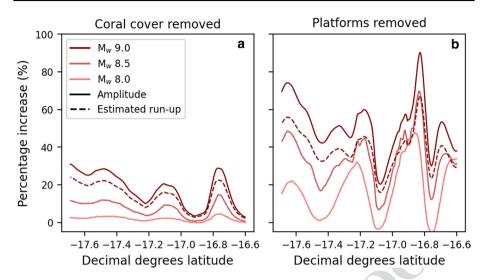


Fig. 10 Percentage increases in both earthquake tsunami amplitude and estimated run-up when **a** coral cover is removed and **b** reef platforms are removed. Amplitudes, which were also used to calculate run-up, were extracted along the 25 m isobath

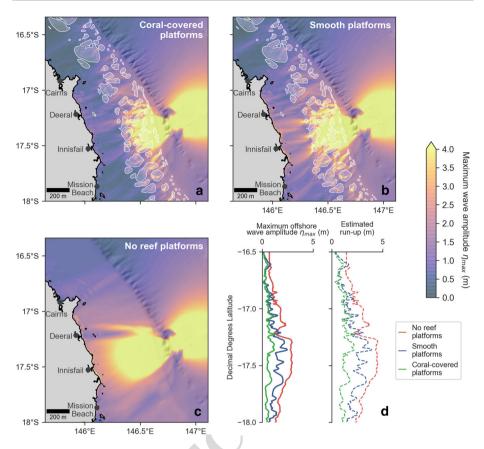
platforms on the propagating tsunamis, which increases with earthquake source magnitude.
We again note the immense variability of the amplitude and run-up increases alongshore
for each earthquake scenario.

For all cases, the first tsunami waves arrive at the coast after an approximately 4 h travel time from the Solomon Islands source zone. When passing over the shelf, the tsunami experiences diffraction, shoaling, and focusing. In particular, broad, moderately deep platforms tend to focus tsunami wave energy towards shore (e.g., Fig. 9b). When platforms are removed, this behaviour disappears. For animations of the Mw 8.5 scenario simulated with coral cover and no reef platforms, see Online Resources 3 and 4.

#### 446 4.4 Nearshore landslide tsunami propagation

Simulations indicate that the impact of ecosystem-scale and bathymetric-scale complex-447 ity on tsunami attenuation is sizeable for the landslide-generated cases considered on 448 this margin. Turning firstly to the previously termed "worst-case scenario" for the Gloria 449 Knolls Slide (Puga-Bernabéu et al. 2016), when reef platforms are covered by coral, off-450 shore amplitudes markedly decline from over  $\sim 4$  m to under  $\sim 2$  m landward of the plat-451 forms (Fig. 11a), and maximum estimated run-up is estimated reaches up to  $\sim 2.2$  m. When 452 coral cover is removed (Fig. 11b), offshore amplitudes along the 25 m isobath nearly dou-453 ble, increasing by a factor of  $\sim 1.9$  on average. Maximum estimated run-up rises to  $\sim 3.9$  m 454 under the "smooth platforms" simulation. When reef platforms are removed (Fig. 11c), off-455 shore amplitudes more than quadruple on average (fold change:  $\sim 4.6$ ), when compared to 456 the "coral-covered platforms" scenario. When platforms are absent, estimated maximum 457 run-up increases again, reaching 4.6 m (Fig. 11d). The total elapsed time between tsunami 458 generation and the arrival of the first waves is ~ 1.5 h. 459

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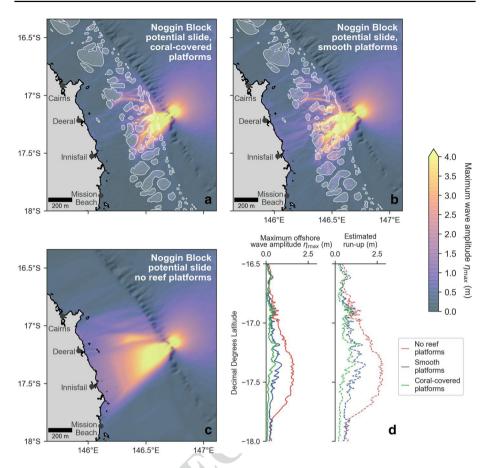


**Fig. 11** Maximum wave amplitude distributions for the Gloria Knolls Slide (worst-case scenario) simulated with **a** the modern "coral-covered platforms" (bottom friction coefficient  $C_D = 0.1522$  on platforms, shown in white) **b** "smooth platforms" ( $C_D = 0.0025$ ), and **c** "no reef platforms". **d** Corresponding maximum off-shore wave amplitude and estimated run-up distributions. Maximum run-up estimates are ~2.2 m for the "coral-covered platforms" scenario, ~3.9 m for the "smooth platforms" scenario, and ~4.6 m for the "no reef platforms" scenario. Offshore wave amplitudes were interpolated along the 25 m isobath. For animations of the "coral-covered platforms" and "no reef platforms" scenarios, see Online Resources 5 and 6

Results for the Noggin Block potential slide are very similar to that of the Gloria Knolls 460 Slide, though it produces a smaller tsunami (see Sect. 4.2). Assuming healthy reef growth 461 (Fig. 12a), offshore amplitudes remain under  $\sim 1$  m, where they sharply decline upon pass-462 ing over the GBR platforms. Maximum estimated run-up for this scenario is  $\sim 1.4$  m. When 463 coral cover is removed (Fig. 12b), offshore amplitudes along the 25 m isobath increase by a 464 factor of  $\sim 2$  on average, with the maximum run-up rising to 1.8 m. Finally, when platforms 465 are removed from the simulations (Fig. 12c), offshore amplitudes along the 25 m isobath 466 are, on average, 4.5 times larger than the original "coral cover" scenario. Peak estimated 467 run-up reaches ~ 2.8 m under the "no reef platforms" scenario (Fig. 12d). The total time 468 between tsunami generation and the arrival of the first waves is similar to the Gloria Knolls 469 landslide tsunami (~1.5 h). 470

Figure 10 shows the overall change in offshore wave amplitude and estimated run-up when coral cover and reef platforms are removed from simulations, this time represented

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**Fig. 12** Maximum wave amplitude distributions for the Noggin Block potential landslide scenario simulated with **a** the modern "coral-covered platforms" (bottom friction coefficient  $C_D = 0.1522$  on platforms, shown in white) **b** "smooth platforms" ( $C_D = 0.0025$ ), and **c** "no reef platforms". **d** Corresponding maximum offshore wave amplitude and estimated run-up distributions. Maximum run-up estimates are ~1.4 m for the "coral-covered platforms" scenario, ~1.8 m for the "smooth platforms" scenario, and ~2.9 m for the "no reef platforms" scenario. Offshore wave amplitudes were interpolated along the 25 m isobath. For animations of the "coral-covered platforms" and "no reef platforms" scenarios, see Online Resources 7 and 8

473 in terms of fold change rather than percentage change. For each landslide case, offshore 474 amplitudes along the 25 m isobath, along with estimated run-ups, tend to double when 475 coral cover is removed (Fig. 10a). When platforms are removed, the amplitudes and run-476 ups increase significantly for each case, but more so for the Noggin Block potential slide 477 (Fig. 10b). Again, we highlight the enormous along-shore variability in amplitude and run-478 up change across simulations.

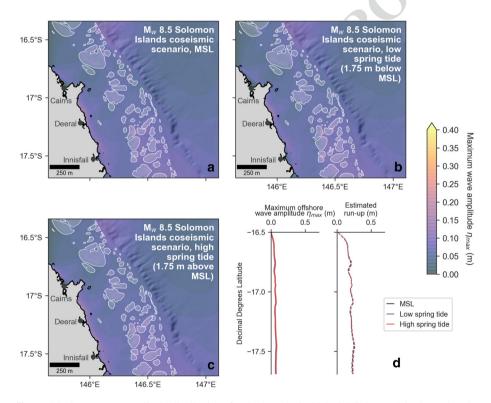
Landslide tsunamis across both cases exhibit common behaviours. Amplitude and runup distributions follow a localized bell-curve due to radial damping, a standard process undergone by point-source tsunamis (Brune et al. 2010; Harbitz et al. 2006). Additionally, reef platforms greatly interfere with these comparably shorter waves as they traverse the shallow continental shelf (Harbitz et al. 2006). For animations of both the Gloria Knolls slide scenario simulated with coral-covered platforms and no reef platforms, see Online

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Resources 5 and 6. For the same corresponding Noggin Block landslide tsunamis, see Online Resources 7 and 8.

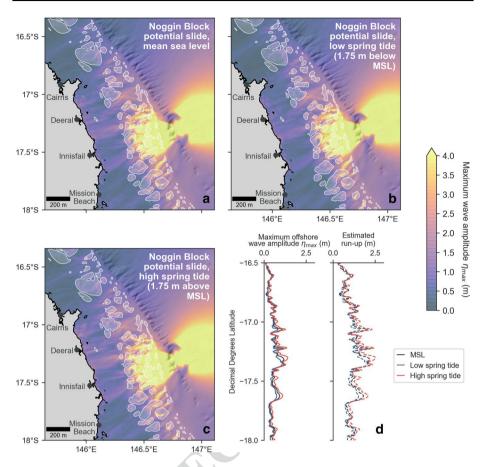
#### 487 4.5 Tidal impacts on tsunami propagation

The additional impact of tide level was tested for the  $M_w$  8.5 Solomon Islands earthquake 488 scenario, the Gloria Knolls Slide scenario, and the Noggin Block potential slide scenario. 489 Results indicate a minimal impact of tide level on the degree of attenuation of the  $M_w$  8.5 490 earthquake-triggered tsunami (Fig. 13a), where amplitudes were 1.6% lower on average at 491 low spring tide (1.75 m below MSL; Fig. 13b) and 2.6% higher on average at high spring 492 tide (1.75 m above MSL; Fig. 13c). Offshore amplitude and run-up distributions along the 493 494 25 m isobath are very similar for all tide cases (Fig. 13d). For the Gloria Knolls Slide, the effect of tides is more pronounced, where amplitudes decrease 11% on average during low 495 spring tide and increase 17% on average at high spring tide (Fig. 14). Similarly, for the 496 Noggin Block, potential slide scenario (Fig. 15a), amplitudes were 16% lower on average 497 at low spring tide (Fig. 15b) and 6% higher on average at high spring tide (Fig. 15c). 498



**Fig. 13** Maximum wave amplitude distributions for the hypothetical  $M_w$  8.5 Solomon Islands earthquake scenario simulated at **a** mean sea level (MSL, bottom friction coefficient  $C_D = 0.1522$  on platforms, shown in white) **b** low spring tide (1.75 m below MSL,  $C_D = 0.1522$  on platforms), and **c** high spring tide (1.75 m above MSL,  $C_D = 0.1522$  on platforms). **d** Corresponding maximum offshore wave amplitude and estimated run-up distributions. Maximum run-up estimates are 26 cm for the MSL scenario, 25 cm for the low spring tide scenario, and 26 cm for the high spring tide scenario. Offshore wave amplitudes were interpolated along the 25 m isobath

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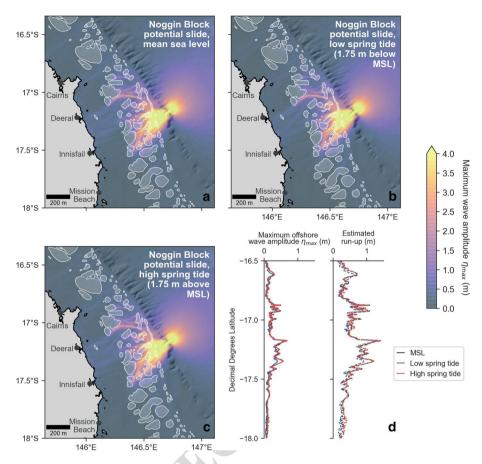


**Fig. 14** Maximum wave amplitude distributions for the Gloria Knolls Slide scenario simulated at **a** mean sea level (bottom friction coefficient  $C_D = 0.1522$  on platforms, shown in white) **b** low spring tide (1.75 m below MSL,  $C_D = 0.1522$  on platforms), and **c** high spring tide (1.75 m above MSL,  $C_D = 0.1522$  on platforms). **d** Corresponding maximum offshore wave amplitude and estimated run-up distributions. Maximum run-up estimates are 1.4 m for the MSL scenario, 1.4 m for the low spring tide scenario, and 1.3 m for the high spring tide scenario. Offshore wave amplitudes were interpolated along the 25 m isobath

# 499 5 Discussion

### 500 5.1 The impact of the GBR's ecosystem-scale complexity on tsunami propagation

Our results show that tsunamis are strongly impacted by the presence of coral cover in 501 the GBR. Across many of the "coral-covered platforms" simulations, maps showing maxi-502 mum wave amplitude distributions show clear "shadow zones" landward of reef platforms, 503 where amplitudes markedly decrease. These impacts are especially pronounced for the  $M_W$ 504 9.0 Solomon Islands earthquake scenario (Fig. 9), the Gloria Knolls submarine landslide 505 scenario (Fig. 11) and the Noggin Block potential submarine landslide scenario (Fig. 12). 506 These declines in wave amplitude are driven by elevated frictional dissipation over coral-507 covered reef platforms. We eliminate the possibility that wave breaking contributed to 508



**Fig. 15** Maximum wave amplitude distributions for the Noggin Block potential slide scenario simulated at **a** mean sea level (bottom friction coefficient  $C_D = 0.1522$  on platforms, shown in white) **b** low spring tide (1.75 m below MSL,  $C_D = 0.1522$  on platforms), and **c** high spring tide (1.75 m above MSL,  $C_D = 0.1522$  on platforms). **d** Corresponding maximum offshore wave amplitude and estimated run-up distributions. Maximum run-up estimates are 1.4 m for the MSL scenario, 1.4 m for the low spring tide scenario, and 1.3 m for the high spring tide scenario. Offshore wave amplitudes were interpolated along the 25 m isobath

energy dissipation, as wave-breaking was not detected in any of the simulations due to the 509 tsunamis' large wavelengths in comparison to their amplitudes. These results reaffirm the 510 prevailing notion that the GBR acts as a regional buffer to tsunamis (Baba et al. 2008; 511 Wei et al. 2015; Xing et al. 2015; Webster et al. 2016; Puga-Bernabéu et al. 2019). They 512 are also consistent with previous findings from other modelling studies, especially those 513 that include wider reef platforms in their assessments (Kunkel et al. 2006; Gelfenbaum 514 et al. 2011; Yao et al. 2012), which allows the cumulative impact of frictional dissipation 515 to dominate. Therefore, we propose that the effect of live coral cover should be directly 516 incorporated into future hazard assessments of the northeastern Australian margin, as we 517 anticipate it will have a detrimental impact on propagating tsunamis. 518

The energy-diminishing impact of coral cover becomes most apparent when comparing the "coral-covered platforms" simulations with the "smooth platforms" simulations. When coral cover is removed, amplitudes increase across each source scenario tested here. 522 Notably, run-up projections increase as much as 24% for the  $M_{w}$  9.0 earthquake source 523 (Fig. 10), and they exhibit a maximum of a nearly fourfold change for the Noggin Block potential slide (Fig. 16). These increases in amplitude and run-up imply that while coral 524 cover in the GBR may currently have a buffering effect on tsunami wave energy, this 525 effect may diminish as reef ecosystems in the GBR continue to decline under the physi-526 ological stressors (e.g., heat stress, acidity stress) that accompany anthropogenic climate 527 change (Hughes et al. 2018). Generally speaking, the structural complexity of coral reefs 528 is expected to deteriorate as reef-building species are lost and as ecosystems transition to 529 algal-dominated states (Bellwood et al. 2004; Alvarez-Filip et al. 2009; Wild et al. 2011). 530 This deterioration of structural complexity is expected to lessen frictional dissipation of 531 wind wave energy (Harris et al. 2018; de Lalouvière et al. 2020). Based on our results, we 532 expect a similar outlook for tsunami wave hazards. This loss of buffering capacity may be 533 further compounded by the effects of sea level rise, where some assessments have fore-534 casted heightened tsunami hazard under current projections (Li et al. 2018; Nagai et al. 535 2020). 536

Across source scenarios, there are prominent discrepancies in the magnitude of the 537 amplitude and run-up increases when coral cover is removed. For instance, while the  $M_{\rm w}$ 538 8.0 earthquake scenario experiences marginal increases (4% maximum, see Fig. 10),  $M_w$ 539 9.0 scenario experiences substantial jumps in offshore amplitude (up to 31%) when plat-540 forms are smoothed. This implies that the degree of coral-induced frictional dissipation 541 at bed is different across source scenarios. Our findings demonstrate that these differences 542 in frictional dissipation are directly related to wave amplitude (and thus, wave energy). 543 Particle velocity (note: this is different to wave *celerity*) is a function of wave amplitude 544 (Nielsen 1992), and therefore, waves of differing amplitudes experience different degrees 545 of dissipation due to shear stress at bed. This amplitude-mediated discrepancy in parti-546 cle velocity is best exemplified by comparing earthquake scenarios, where tsunami ampli-547 tude was altered by changing the magnitude and slip displacement of the initial coseismic 548

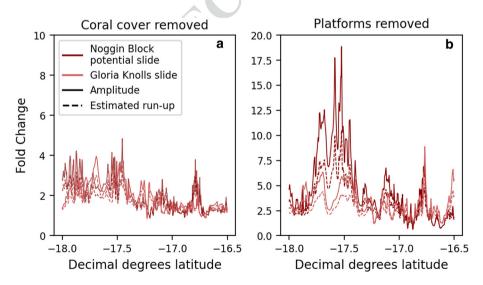


Fig. 16 Fold-change increase in both landslide tsunami amplitude and estimated run-up when  $\mathbf{a}$  coral cover is removed and  $\mathbf{b}$  reef platforms are removed. Amplitudes, which were also used to calculate run-up, were extracted along the 25 m isobath

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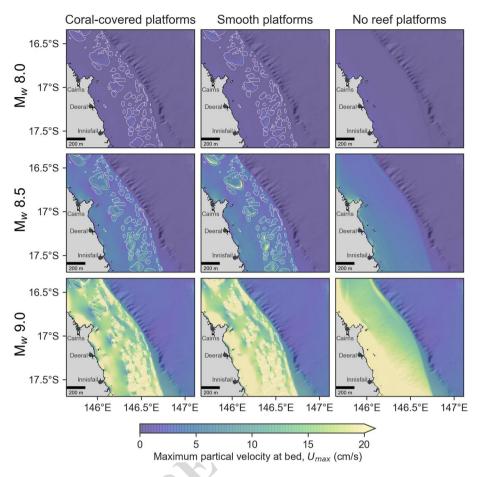
source (Fig. 4, see Table 1 for source parameters). For the  $M_{w}$  8.0 Solomon Islands earthquake scenario, bed particle velocities are relatively low (<1 cm/s) throughout the computational domain given the relatively low tsunami amplitudes produced by the source. However, for the  $M_w$  8.5 and  $M_w$  9.0 earthquake scenarios, particle velocities are much higher on the shelf (> 5 cm/s). Moreover, in their corresponding "smooth platforms" simulations, particle velocities are more elevated atop the reef platforms than in the "coral-covered platforms" simulations, which further reflects the dissipative effect of coral cover. As wave energy dissipation through shear stress is proportional to the square of the particle velocity (see Eq. 1), the higher velocities computed for higher-magnitude earthquake tsunamis result in greater overall wave energy dissipation via bottom friction when coral cover is present. This also explains why a relatively large degree of attenuation is observed for the 559 landslide-generated tsunamis, both of which produce similarly high waves (9 m and 3.5 m 560 for the landward-propagating waves, respectively). Our results show that tsunami ampli-561 tude, which ultimately depends on the magnitude and proximity of the triggering source, 562 should also be considered when examining the buffering capacity of natural defences such 563 as coral reefs (Fig. 17). 564

While the GBR generally acts as a buffer to tsunami wave energy, despite its namesake, 565 the GBR itself does not form a continuous barrier on the mid- to outer shelf, especially 566 in the central region (Fig. 3). As a result, the buffering effect offered by coral cover var-AQ2567 ies considerably alongshore. Turning again to the Solomon Islands earthquake scenarios 568 (Fig. 10), when coral cover is removed, the largest increases in wave amplitude and run-up 569 tend to occur landward of broad reef platforms (see also Fig. 9a, b). On the other hand, 570 areas that lie between inter-reef passages, or gaps, exhibit smaller increases in amplitude 571 and run-up. This phenomenon is consistent across source scenarios, and it is particularly 572 pronounced in cases where tsunami amplitudes are relatively high. This implies that the 573 574 protectiveness offered by coral cover varies alongshore because of platform placement; if coral-covered platforms (particularly broad platforms) are positioned between the incom-575 ing tsunami and the shoreline, they are more inclined to dampen the tsunami. 576

To summarise, reef cover contributes substantially to the overall buffering capacity of 577 the GBR, which is consistent with previous findings (e.g., Kunkel et al. 2006). However, 578 the GBR's buffering capacity for any given location alongshore depends on various site-579 specific factors, including the presence of coral cover, the relative positioning of the plat-580 forms, and tsunami amplitude. 581

#### 5.2 The impact of the GBR's bathymetric-scale complexity on tsunami propagation 582

Our simulations reveal the remarkably complex ways in which tsunami waves interact with 583 the larger-scale bathymetric features (i.e., platforms, shoals, etc.) that comprise the GBR. 584 Of particular note is the platforms' ability to focus tsunami wave energy towards shore (see 585 Fig. 8 and Online Resource 3 for the M<sub>w</sub> 8.5 Solomon Islands earthquake simulations). In 586 a manner analogous to a convex lens focussing light, platforms cause the incoming tsu-587 588 nami waves to refract inwards towards their shallower depths, inciting shoaling, positive wave interference, and subsequent heightening of wave trains. Shoaling and heightening of 589 590 tsunami waves over shallow reefs has been observed by others, both from field-based and modelling evidence (Chatenoux and Peduzzi 2005; Gelfenbaum et al. 2011). Interestingly, 591 frictional dissipation by coral cover appears to fully or partially counteract these focussing 592 effects, where waves subsequently dampen after growing in amplitude over the platforms 593 (e.g., Fig. 9). Consequently, smoothing the domain tends to enhance the platforms' ability 594



**Fig. 17** Maximum bed particle velocities (in cm/s) across the computational domain for each the  $M_w$  8.0 Solomon Islands earthquake scenario (top row), the  $M_w$  8.5 scenario (middle row), and the  $M_w$  9.0 scenario (bottom row). Columns are aligned based on their corresponding "coral-covered platforms" simulations (left column), "smooth platforms" simulations (middle column), and "no reef platforms" simulations (right column)

to focus wave energy. This is demonstrated by the higher-amplitude, landward wave trains shown in wave amplitude distributions (e.g., Fig. 9). Some platforms appear to more effectively focus wave energy than others, and we suspect this is due to factors such as reef morphology, size, and submergence depth. A more systematic investigation of platform characteristics warranted to test this hypothesis, particularly as coral reef cover, is expected to decline in the future.

In addition to focussing effects, simulated tsunamis exhibit a complex interplay of additional behaviours when interacting with platforms, such as diffraction, reflection, and scattering of wave trains (see Online Resource 5 for example). These effects are most pronounced for the landslide-generated tsunami cases (see Sect. 4.4), and we tentatively suggest that this is due to their shorter wavelengths. Our simulations further reinforce the important role that local bathymetry plays in modulating tsunami behaviour, particularly in shallow reef environments (Baba et al. 2008; Dilmen et al. 2018). This potent, complex, and site-specific control on tsunami propagation further underscores the need to evaluate tsunami hazard on a case-by-case basis.

We also highlight the intriguing role of inter-reef passages, or gaps, in modulating tsu-610 nami behaviour as it crosses the shelf. Many have hypothesized that gaps in the reef struc-611 ture worsen the tsunami hazard, as the gaps act as low-resistance conduits that amplify 612 wave energy (Nott 1997; Liu et al. 2005; Gelfenbaum et al. 2011; McAdoo et al. 2011; 613 Roger et al. 2014). In our simulations, porous gaps in the reef structure certainly permit 614 wave energy to pass through to the coastline. However, there is little evidence to support 615 the notion that the gaps amplify waves. In fact, due to focussing, amplification of wave 616 amplitudes occurs over the platforms rather than between them (e.g., Figs. 9, 11). In the 617 case of the GBR, many of the platforms appear to be wide enough, deep enough, far 618 enough apart, and far enough from the coastline such that the inter-reef gaps do not pose 619 a significant hazard. This is in contrast to many fringing reef systems, where gaps can be 620 quite narrow, shallow, and close to shore. We therefore suggest that for the GBR, the wave 621 focussing ability of platforms may be of greater concern for the northeastern Australian 622 coastline than the presence of gaps in the reef structure. 623

Overall, the GBR's underlying bathymetric structure contributes significantly to its 624 buffering capacity, and this becomes apparent when platforms are removed from simula-625 tions (see Figs. 10 and 16). When platforms are removed, waves are permitted to prop-626 agate smoothly and uninterruptedly across the shelf, highlighting the highly obstructive 627 nature of the platforms themselves. Offshore wave amplitudes and run-up distributions 628 increase alongshore across all source scenarios when platforms are removed. These find-629 ings are consistent with previous work which suggests that bathymetric irregularities on 630 the shelf exert large control on the eventual run-up distribution at the coast (Baba et al. 631 2008; Schambach et al. 2018). Even as the GBR is interrupted by gaps, the presence reef 632 633 structure appears to provide at least some benefit to nearly all areas of the coastline examined in this study. 634

#### 635 5.3 Broader implications surrounding the GBR's impact on tsunami hazard

This study has revealed wider implications for communities situated along the northeastern 636 Australian coastline. Firstly, from a mitigation perspective, the GBR may offer greater pro-637 tection for more severe tsunami events. In particular, the GBR may offer natural protection 638 against near-field landslide sources, which are notoriously difficult to predict and forecast 639 (Tappin et al. 1999; Harbitz et al. 2014). While this may take some pressure off warning 640 systems, we stress that coastal communities should not rely upon the GBR alone to reduce 641 their vulnerability to tsunami hazards. A holistic strategy for tsunami hazard preparedness 642 ultimately should include risk awareness, hazard education, resilient infrastructure, and 643 robust early warning systems (Baird et al. 2005; Liu et al. 2005; Dominey-Howes et al. 644 2007; Mori et al. 2011). 645

Secondly, from a *future* mitigation perspective, our work suggests that the declining 646 647 coral health, which is associated with globally mediated anthropogenic climate change (De'ath et al. 2012; Hughes et al. 2018), will have an overall adverse effect on the GBR's 648 649 defensive capability. In this context, today's reef-buffering asset may be tomorrow's liability. Areas of shoreline that are best-protected by broad, expansive coral-covered platforms 650 may experience the highest inundation risk in the future as coral die-off continues and as 651 architectural complexity deteriorates (Alvarez-Filip et al. 2009), enhancing the platforms' 652 ability to focus energy towards shore rather than attenuating it. These local differences 653

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reinforce the need for site-specific hazard assessments when considering tsunami hazard on the northeastern Australian margin in the future.

#### 656 5.4 Reconciling differing interpretations of coral reef impact on tsunamis

In light of our results, we address some of the contrasting interpretations in the literature 657 around the impact of coral reefs on tsunami hazard. Firstly, while the GBR, being an off-658 659 shore barrier system, buffers the tsunami hazard for the more distant Australian coastline. other reef environments (in particular, narrow fringing reefs that surround populated inner 660 islands) could exacerbate tsunami hazard through behaviours such as shoaling, focussing, 661 and bore formation (Chatenoux and Peduzzi 2005; Fritz et al. 2011; Gelfenbaum et al. 662 2011; Yao et al. 2012). Indeed, our simulations showcase shoaling and focussing on plat-663 forms, which locally augment wave amplitudes at the intra-platform scale. A more rigorous 664 inundation study would be needed to confirm whether this translates to increased hazard 665 within the lagoons, shoals, and islands that rest within the platforms. Therefore, coral reefs 666 could have either beneficial or detrimental effects on the overall hazard depending on the 667 type reef system in question and the proximity of coastal communities and assets to the 668 site of the most severe shoaling/focussing. In the debate surrounding reef protectiveness 669 against tsunamis, a distinction must be made between fringing reef systems and offshore 670 barrier systems, as they have different implications for proximity to wave focussing effects, 671 and therefore, exposure. 672

On the other hand, we also note potential ambiguities around the ways in which the 673 impact of coral reefs is reported in post-tsunami field surveys. From our simulations and 674 others (Kunkel et al. 2006; Uslu et al. 2010; Gelfenbaum et al. 2011), there is evidently 675 a strong theoretical basis to support the fact that coral reefs can dissipate tsunami wave 676 energy, reducing the tsunami hazard. However, this overall reduction in hazard may not 677 be sufficient to completely reduce the *physical vulnerability* and *exposure* of coastal com-678 munities (Uslu et al. 2010). When discussing the buffering role of reefs, many have high-679 lighted that despite being within close proximity to reefs, coastal assets have nonetheless 680 been destroyed during tsunami events (e.g., Baird et al. 2005), leading some to conclude 681 that coral reefs provide no protective benefit to coastal communities. In these cases, the 682 reefs could very well have buffered the overall tsunami hazard, reducing the overall inun-683 dation and run-up extent. However, this protective benefit may not have been sufficient 684 to completely shield coastal communities that were situated close to shore. Care must be 685 686 taken when retrospectively interpreting the role that coral reefs may have played in reducing tsunami hazard along a shoreline, and a clear distinction should be made between haz-687 ard reduction and risk reduction, which lies at the intersection between hazard, exposure, 688 and vulnerability. 689

#### 690 5.5 Study limitations and future work

Uncertainties persist that could complicate such future tsunami hazards assessments in coral reef environments. Firstly, at the ecosystem scale, the relationship between coral rugosity and community composition requires more precise quantification on an intra-reef platform scale (Rogers et al. 2016). This will continue to be a pressing task in the future, as profound ecological shifts may be precipitated by both the immediate aftermath of the tsunami impact and longer-term environmental changes, thus affecting ecosystem-scale structural complexity (Madin and Connolly 2006; Alvarez-Filip et al. 2009; Ferrari et al.

2016; Hughes et al. 2018). While platform degradation and bioerosion is largely antici-698 pated to flatten coral reefs (Alvarez-Filip et al. 2009), the shorter-term impact of these and 699 other stressors on ecosystem-scale rugosity is still not precisely known. These ecosystems 700 should be stringently monitored to better assess how coastal hazard severity as a whole 701 will be transformed in these areas. Additionally, the approach used to parameterize bottom 702 shear stress, though very common both in the field and in modelling studies, may need to 703 be reconfigured to account for more complex tsunami interactions and subgrid turbulent 704 dissipation within the 3D reef structure (Lowe et al. 2008; Kim et al. 2009; Rosman and 705 Hench 2011). Moreover, these more complex interactions may be better represented by a 706 Navier–Stokes model rather than a depth-averaged wave model (Kazolea et al. 2019). 707

On a larger scale, it is worth exploring the potential impact of undular bores that could 708 arise and break on the platforms themselves, as they could play an additional role in dis-709 sipating wave energy offshore (Grilli et al. 2012; Glimsdal et al. 2013). These wave fea-710 tures would not have been resolved in our coarser-resolution runs (Schambach et al. 2018), 711 as capturing them quickly becomes very demanding computationally (< 10 m resolution 712 required, Grilli et al. 2012). Also, while our study emphasizes the effect of the GBR on 713 offshore amplitudes and projected run-up distributions, ultimately, tsunami-induced surges 714 and bores deliver the force and high water levels that cause destruction to coastal commu-715 nities onshore (Koshimura et al. 2009; Nistor et al. 2009; Nouri et al. 2010). Further work 716 is warranted to establish whether the reduction in offshore wave amplitude translates to a 717 reduced hazard onshore, and this would necessitate the deployment of higher-resolution 718 inundation simulations. 719

Finally, our study was not designed to provide a reappraised, comprehensive hazard 720 assessment for the northeastern Australian coastline although our findings suggest that the 721 reef's role should be considered in future assessments. That being said, we stress the need 722 723 for a robust parameterization of reef roughness (Nelson 1996; Rosman and Hench 2011). Furthermore, as indicated by sensitivity analyses (see Online Resource 2), these propaga-724 725 tion simulations require high spatial resolution (200 m for earthquake sources and 100 m or less for landslide sources) in order to properly capture the reef structure and to resolve 726 complex tsunami-reef interactions. While this increases computational demand, we none-727 theless deem it worthwhile to consider the role of the reef, as current assessments may 728 be over-estimating tsunami risk in northeast Australia. Additionally, a more meaningful 729 assessment of the submarine landslide tsunami hazard is needed to better understand the 730 timing, frequency, and magnitude of these events. In the future, it may be worth consid-731 ering more complex failure dynamics (i.e. landslide deformation and two-way coupling 732 with the water column), which could alter the run-up results (Masson et al. 2006; Geist 733 et al. 2009; Abadie et al. 2010), but we anticipate that accounting for these dynamics will 734 not alter the overall conclusions established here about the buffering effect of the GBR. 735 Addressing these limitations will enable more reliable forecasting as the fate of the world's 736 coral reefs becomes clearer with time. 737

#### 738 6 Conclusions

This study demonstrates the nuanced interactions between tsunamis and coral reef systems. In agreement with previous work we find that the Great Barrier Reef (GBR), both in terms of coral cover and larger-scale bathymetric complexity, acts as a large-scale regional buffer against tsunamis. However, the reef appears to provide greater protection against

higher-amplitude tsunamis due to the larger computed particle velocities at bed, which 743 directly dictates the degree of frictional dissipation through shear stress. Additionally, we 744 find that the protectiveness offered by the GBR locally depends on coral cover and plat-745 form distribution. We also find that wave focussing by reef platforms could pose a greater 746 hazard than the gaps between platforms, which have been previously thought to amplify 747 waves. In the context of the larger debate about whether coral reefs reduce tsunami hazards 748 for coastal communities, we conclude that differing interpretations can be reconciled when 749 considering site-specific factors. AQ3 750

751 Supplementary information The online version contains supplementary material available at https://doi.
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764 Data availability The bathymetry of the Great Barrier Reef region can be found here: http://eatlas.org.
765 au/data/uuid/200aba6b-6fb6-443e-b84b-86b0bbdb53ac. The Great Barrier Reef Banks shapefile can be
766 obtained here: https://data.gov.au/dataset/ds-ga-c00ab093-f02d-5b03-e044-00144fdd4fa6/details?q=great%
767 20barrier%20reef%20banks. The global reef dataset can be downloaded here: www.wri.org/resources/data768 sets/reefs-risk-revisited.

769 Code availability The code Geowave can be downloaded here: http://www.appliedfluids.com/geowave.
 770 html. The codes NHWAVE and FUNWAVE.TVD can be downloaded from GitHub (github.com/JimKirby/
 771 NHWAVE; fengyanshi.github.io/build/html/index.html).

- 772 Declarations
- 773 Conflicts of interest The authors have none to declare.

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