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Earthquake rupture on multiple splay faults and its effect on tsunamis

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Key Points:

- Multiple splay faults can be activated during an earthquake by slip on the megathrust, dynamic stress transfer, or stress changes from waves
- Splay fault activation is partially facilitated by their alignment with the local stress field and closeness to failure
- The tsunami has a high crest due to slip on the longest splay fault and a second broad wave packet due to slip on multiple smaller faults

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Abstract

Detailed imaging of accretionary wedges reveal complex splay fault networks which could pose a significant tsunami hazard. However, the dynamics of multiple splay fault activation and interaction during megathrust events and consequent effects on tsunami generation are not well understood. We use a 2D dynamic rupture model with six complex splay fault geometries consistent with initial stress and strength conditions constrained by a geodynamic seismic cycle model. The dynamic seafloor displacements serve as input for a 1D shallow water tsunami propagation and inundation model. We find that all splay faults rupture coseismically due to either slip on the megathrust, dynamic stress transfer, or stress changes induced by seismic waves. The ensuing tsunami features one high-amplitude crest related to rupture on the longest splay fault and a second, broader wave packet resulting from slip on the other faults. This results in two episodes of flooding and 77% larger run-up length.

Plain Language Summary

In subduction zones, where one tectonic plate moves beneath another, earthquakes can occur on many different faults. Splay faults are steep faults that branch off the largest fault in a subduction zone (the megathrust). As they are steeper than the megathrust, the same amount of movement on them could result in more vertical displacement of the seafloor. Therefore, splay faults are thought to play an important role in the generation of tsunamis. Here, we use computer simulations to study if an earthquake can break multiple splay faults at once and what the effect of this is on the tsunami. We find that multiple splay faults can indeed fail during a single earthquake, due to the complicated stress changes that occur during the rupture. Rupture on splay faults result in larger seafloor displacements with smaller wavelengths, so the ensuing tsunami is bigger and results in two main flooding episodes at the coast.

1 Introduction

Splay faults branch off the megathrust in the accretionary wedge or overriding plate (e.g., Plafker, 1965; Fukao, 1979; Park et al., 2002). Earthquake ruptures originating on the megathrust can potentially transfer to splay faults. Apart from complicating rupture dynamics, this may lead to important ramifications for tsunamigenesis, as rupture

48 on splay faults increases the efficiency of tsunami generation (e.g., Fukao, 1979; Lotto
49 et al., 2018; Hananto et al., 2020). Several studies suggested that splay fault rupture played
50 an important role in large tsunamigenic megathrust earthquakes, such as the 2004 M_w 9.1–
51 9.3 Sumatra-Andaman and 2010 M_w 8.0 Maule earthquakes (DeDontney & Rice, 2012;
52 Melnick et al., 2012; Waldhauser et al., 2012). Tsunami earthquakes in which the ob-
53 served tsunami is larger than expected from surface wave magnitude analysis of the earth-
54 quake (e.g., Kanamori, 1972; Heidarzadeh, 2011), such as the 365 Crete, 1946 Nankai,
55 and 1964 Alaska earthquakes, have also been linked to splay fault rupture (e.g., Cum-
56 mins & Kaneda, 2000; Cummins et al., 2001; Shaw et al., 2008; Chapman et al., 2014;
57 Haeussler et al., 2015; von Huene et al., 2016; Fan et al., 2017; Martin et al., 2019; Hananto
58 et al., 2020; Suleimani & Freymueller, 2020).

59 Dynamic rupture modelling is a useful tool to understand the role of splay faults
60 in rupture dynamics (e.g., Kame et al., 2003; Wendt et al., 2009; Geist & Oglesby, 2009;
61 DeDontney et al., 2011; Tamura & Ide, 2011; DeDontney & Hubbard, 2012; Lotto et al.,
62 2018). These studies show that parameters such as the initial stress, branching angle,
63 frictional properties, strength of the accretionary wedge, and material contrasts along
64 the megathrust affect splay fault rupture. Building upon these insights, several coupled
65 models have been employed to solve for splay fault rupture dynamics and tsunamis se-
66 quentially or simultaneously (Wendt et al., 2009; Geist & Oglesby, 2009; Li et al., 2014;
67 Lotto et al., 2018).

68 Dynamic rupture models of branching faults typically use simple, planar fault ge-
69 ometries, even if observed splay fault geometries are much more complicated (e.g, Park
70 et al., 2002; G. Moore et al., 2007; Collot et al., 2008). Besides that, most dynamic rup-
71 ture studies include only a single splay fault, which is partly necessitated by the diffi-
72 culty of modelling fault junctions with numerical methods (e.g., Aochi et al., 2002; De-
73 Dontney et al., 2012). Observations of accretionary wedges in subduction zones show mul-
74 tiple splay faults with a range of sizes and dips, although not all of them are expected
75 to be seismically active simultaneously (G. F. Moore et al., 2001; Kimura et al., 2007;
76 Kopp, 2013; Fabbri et al., 2020; Hananto et al., 2020).

77 To understand the effect of multiple splay fault rupture with non-planar geome-
78 tries on the surface displacements and the ensuing tsunami, we model dynamic rupture

79 constrained by a geodynamic model of long-term subduction and the subsequent tsunami
80 propagation and inundation.

81 **2 Modelling approach**

82 We use the modelling approach presented in Van Zelst et al. (2019), where a geo-
83 dynamic seismic cycle (SC) model is used to constrain the initial conditions of a dynamic
84 rupture (DR) model. We extend this approach by using the resulting surface displace-
85 ments of the DR model as input for a tsunami propagation and inundation (TS) model.
86 Our modelling framework accounts for the varying temporal and spatial scales from geo-
87 dynamics to tsunami inundation (see also Madden et al., 2020). We apply this frame-
88 work to the problem of multiple splay fault rupture by including six splay fault geome-
89 tries constrained by the SC model in the DR model setup.

90 **2.1 Geodynamic seismic cycle model**

91 The SC model solves for the conservation of mass, momentum, and energy with
92 a visco-elasto-plastic rheology (Gerya & Yuen, 2007). It models 4 million years of sub-
93 duction followed by a seismic cycle phase with a 5-year time step with spontaneous slip
94 events driven by a strongly rate-dependent seismo-thermo-mechanical (STM) modelling
95 approach (van Dinther et al., 2013). We observe widespread visco-plastic shear bands
96 in the accretionary wedge in the SC model during slip events, which we interpret as faults
97 (Figure 1a). For one event, we use the output of the SC model as input for the DR model
98 according to Van Zelst et al. (2019). We pick six splay fault geometries according to the
99 highest accumulated visco-plastic strain during the event visualised as the accumulated
100 visco-plastic slip in Figure 1a (Supplementary Material Section S1; Figures S1-S7). The
101 splay faults generally align with the local stress field (Figure 1b) and are close to fail-
102 ure, apart from splay fault (SF) 6 and the deeper parts of SF4 and SF5 (Figures S8-15).
103 The branch angles (average 14.4°) and dips (average 24.0°) of our splay fault geometries
104 are in line with observations (Park et al., 2002) and other modelling studies (Table S1;
105 Wendt et al., 2009; DeDontney et al., 2011; Tamura & Ide, 2011; DeDontney & Hubbard,
106 2012).

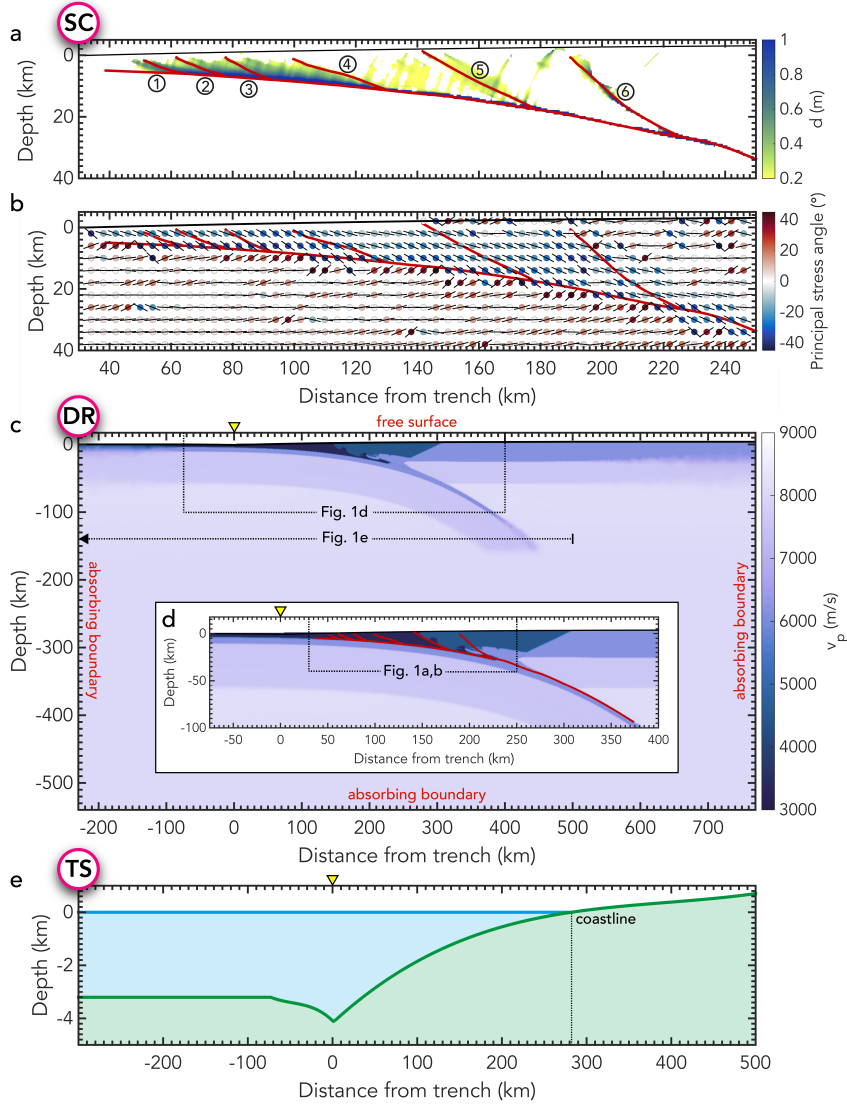


Figure 1. (a) Accumulated slip d in the accretionary wedge after the SC slip event from Van Zelst et al. (2019). Picked splay fault geometries (red) are numbered for easy reference. (b) Orientation of the principal stress σ_1 in the SC model. The angle is indicated in colour and by the bar originating in each dot. Complete (c) and zoomed (d) model setup of the DR model with P -wave velocity v_p , boundary conditions (red) and megathrust and splay fault geometries. (e) Model setup of the tsunami propagation and inundation model with bathymetry (green) and initial sea surface height (blue). The coastline is located at $x = 282.25$ km. Note that the x -axis differs for each panel depending on the model setup size (trench indicated by the yellow triangle).

107

2.2 Dynamic rupture model

108

We use the two-dimensional version of the software package SeisSol (<http://www.seissol.org>; Dumbser & Käser, 2006; de la Puente et al., 2009; Pelties et al., 2014)

109

110 to model dynamic rupture in the model setup described by Van Zelst et al. (2019) with
 111 six additional splay fault geometries in the mesh (Figure 1c,d). We model mode II frac-
 112 ture, which is a simplification that is also used by other studies (e.g., Ramos & Huang,
 113 2019). The on-fault element edge length is 200 m, which combined with polynomial de-
 114 gree $p = 5$ (spatio-temporal order 6 accuracy for wave propagation) results in an ef-
 115 fective resolution of 28.6 m on the fault, which is sufficient to resolve the cohesive zone
 116 size. At the top of the DR model setup, we employ a free surface boundary condition
 117 with topography derived from a 3rd order polynomial approximation of the rock-sticky
 118 air (Cramer et al., 2012) interface in the SC model from $x = -72.8$ km to $x = 499.6$ km,
 119 beyond which we assign constant topography values (Figure 1e). We run the model for
 120 180 s, which ensures smooth coupling to the TS model, as the surface displacements do
 121 not vary significantly after that time. To obtain the surface displacements of the DR model,
 122 we place 601 seismometers from -100 km to 500 km near the free surface with a spac-
 123 ing of 1 km to record the velocity field.

124 **2.3 Tsunami propagation and inundation model**

125 To model tsunami propagation, we use the one-dimensional shallow water equa-
 126 tions (SWE), which consist of the conservation of mass and momentum and consider the
 127 hydro-static pressure caused by gravitational acceleration (Madden et al., 2020). Other
 128 tsunami studies sometimes use the hydrodynamic shallow water equations (e.g., Wendt
 129 et al., 2009; Saito et al., 2019). We choose a hydrostatic approach, since we are specif-
 130 ically interested in the combination of dynamic tsunami generation and inundation.

131 To solve the SWEs, we employ a first order finite volume scheme (LeVeque et al.,
 132 2002) and we use a well-tested augmented Riemann solver to solve for inundation (George,
 133 2008). To incorporate dynamic surface displacements, we consider the bathymetry as a
 134 time-dependent parameter. We define the bathymetry as the unperturbed topography
 135 from the SC model which has an average beach angle of $7.2 \cdot 10^{-6}$. Then we add the seafloor
 136 deformation $\Delta b(x, t)$, caused by the displacements from the DR model. To compute the
 137 seafloor deformation from the DR model we use the method by Tanioka and Satake (1996),
 138 which adds the vertical displacement to a linear approximation of the contribution of the
 139 horizontal displacement. The resulting displacement field contains fast travelling seis-
 140 mic waves, which are radiating from the earthquake source during the DR simulation.
 141 We remove the seismic waves from all displacements used as tsunami sources. To this

142 end, we apply a Fourier filter to the seafloor displacements which removes transient dis-
 143 placements resulting from waves with a frequency/wavelength ratio higher than 300 m/s
 144 (Figures S18-19).

145 We consider a model domain from $x = -300$ km to $x = 500$ km, with the initial
 146 bathymetry from the SC model (Figure 1e). We set the coastline at $x = 282.25$ km to
 147 coincide with the downdip limit of the seismogenic zone (Klingelhoefer et al., 2010). This
 148 results in a maximum water depth of 4117 m. To discretise the model, we use 20,000 points,
 149 which translates to an average spacing of 40 m. We use adaptive time stepping and run
 150 the model for a total simulation time of 2 hours with maximum time steps of 0.5 s and
 151 minimum time steps of 0.08 s. We consider cells with a water column of less than 10^{-6} m
 152 as dry.

153 **3 Results**

154 **3.1 Dynamic earthquake rupture**

155 We compare a model in which only the megathrust is allowed to rupture (Figure 2a;
 156 Van Zelst et al. (2019)) to the model in which six splay faults are theoretically allowed
 157 to break. The ruptures show similar rupture speeds, but different rupture duration with
 158 the model including splay faults rupturing for longer (89 s instead of 82 s). Approximat-
 159 ing the magnitude of the ruptures with the empirical rupture width-magnitude scaling
 160 by Blaser et al. (2010), results in $M_w = 9.4$ for the model without splays and $M_w =$
 161 9.8 for the model including them. However, this does not take the amount of slip into
 162 account, which differs significantly between the two ruptures with the model including
 163 splay faults exhibiting lower slip and slip velocities (Figure 2).

164 After a non-prescribed two-stage nucleation at very low slip rate (a 4 s period of
 165 low rupture speed, followed by a 2 s high speed phase), spontaneous rupture emerges on
 166 the megathrust ((1) in Figure 2b) and the rupture propagates both updip and downdip,
 167 where the rupture is spontaneously arrested at the brittle-ductile transition (2) in both
 168 models (Figure 2a,b). In the updip direction, the main rupture front in the splay fault
 169 model encounters SF6 after 14.1 s. While the dynamic activation of SF6 appears to re-
 170 semble rupture branching (DeDontney et al. (2011); Movie 1, 2 in Supplementary Ma-
 171 terial), we observe a high degree of complexity on smaller scales. The passing megath-
 172 rust rupture dynamically unclamps SF6, i.e., there is a decrease in the normal stress σ_n

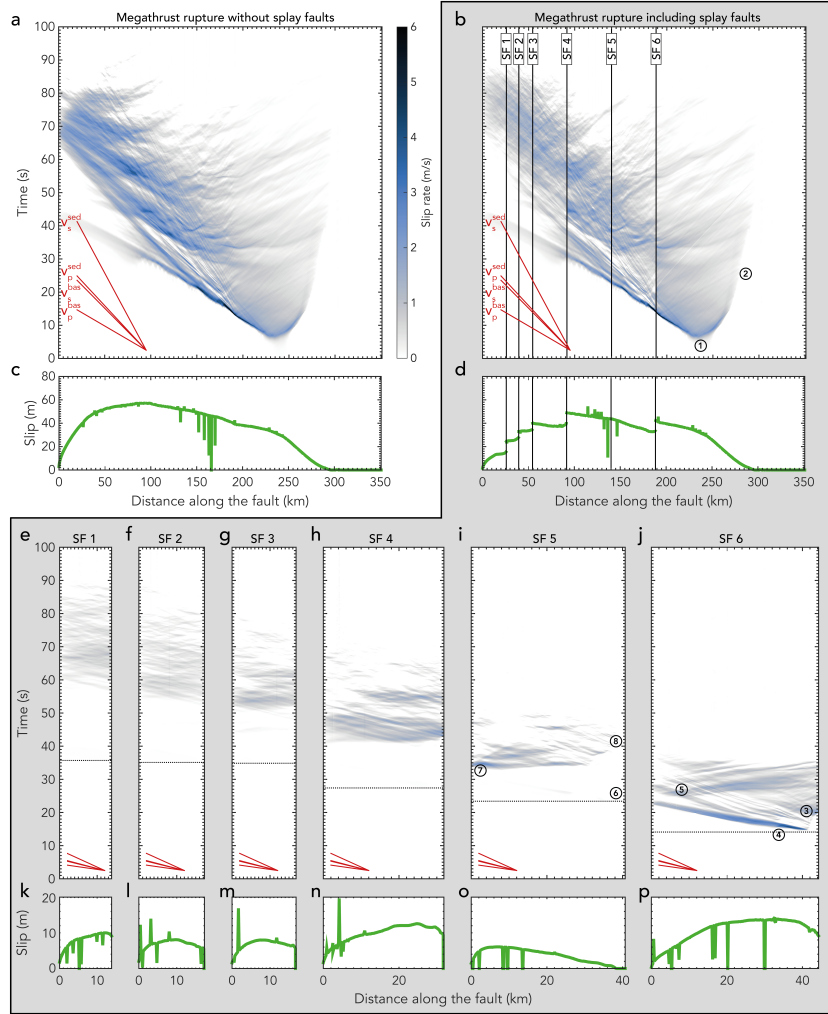


Figure 2. (a,b) Slip rate evolution with time along the megathrust fault for the model (a) without splay faults and (b) including the six splay fault geometries. The splay fault branching points on the megathrust are indicated by black lines. (c,d) Accumulated slip on the megathrust. (e-j) Slip rate evolution and (k-p) accumulated slip on each of the six splay faults for the model including the splay faults. The splay faults connect to the megathrust at the right of each panel. Horizontal black dotted lines indicate the passing of the megathrust rupture front at the branching point. The P - and S -wave velocities for the basalt and sediment are indicated in red: $v_p^{\text{bas}} = 6164$ m/s, $v_s^{\text{bas}} = 3559$ m/s, $v_p^{\text{sed}} = 4429$ m/s, $v_s^{\text{sed}} = 2557$ m/s. See text for an explanation of the numbers.

173 (Oglesby et al., 2008), which results in negligible slip over 1 km of the splay fault close
 174 to the fault junction without spontaneously propagating rupture. Subsequently the rup-
 175 ture jumps from the megathrust to SF6 due to dynamic triggering, omitting the deep-

176 est 3 km of the splay fault, which only ruptures in a down-dip direction after 18 s ((3)
 177 in Figure 2j). Unilateral dynamic rupture then propagates updip on the splay fault with
 178 slip velocities of 4.7 m/s. Simultaneously, in front of this rupture front, secondary rup-
 179 tures are dynamically triggered by the main megathrust rupture (4) leading to an ap-
 180 parently very high updip splay rupture speed. Behind the first, apparently fast splay rup-
 181 ture front, we observe fault reactivation due to multiple passing rupture fronts on the
 182 megathrust and free surface reflected seismic waves (5), resulting in a static slip max-
 183 imum of 13.8 m. Due to the splay fault rupture, the slip velocities on the megathrust
 184 updip of the splay fault are sharply reduced compared to a model which only ruptures
 185 the megathrust. This leads to a slip discontinuity on the megathrust (Figure 2d).

186 The main rupture front on the megathrust passes SF5 without activating it (6),
 187 i.e., neither by branching nor dynamic triggering (Figure 2i). Instead, SF5 is activated
 188 at ~ 5 km depth at 32.8 s due to waves reflecting from the surface (7). Multiple rup-
 189 ture fronts then propagate downdip on SF5, but the deepest 2.5 km of SF5 never fully
 190 ruptures (8). Since the passing of the primary megathrust rupture front does not trig-
 191 ger slip on SF5, there is no decrease in slip rate on the megathrust after it passes SF5.

192 Although the passing of the main rupture front induces small slip rates on SF1–
 193 4 on the order of ~ 0.02 m/s due to unclamping, they only rupture self-sustained af-
 194 terwards at slip rates larger than 1 m/s due to the static and dynamic stress changes in-
 195 duced by secondary rupture front complexity on the megathrust as well as on SF5 and
 196 SF6 and multiple reflected (trapped) waves within the accretionary wedge. The long rup-
 197 ture duration on these shallow splay faults leads to a maximum slip of 12.6 m for SF4
 198 and 10.0 m, 8.1 m, and 8.0 m for SF1–3, respectively, barring any numerical outliers. Since
 199 slip occurs on the splay faults and the slip velocity on the megathrust is reduced when
 200 the rupture interacts with a splay fault, the maximum slip on the megathrust in the model
 201 including splay fault rupture (48.9 m) is lower than in the model without splay fault rup-
 202 ture (57.6 m). Besides that, the slip profile on the megathrust is discontinuous and cor-
 203 responds to rupture on the splay faults.

204 The maximum stress drop on the megathrust on the order of ~ 17 MPa is compa-
 205 rable in the models with and without splay faults (Figure S16). Splay fault 6 shows the
 206 largest stress drop of all splay faults on the order of ~ 19 MPa. The other splay faults

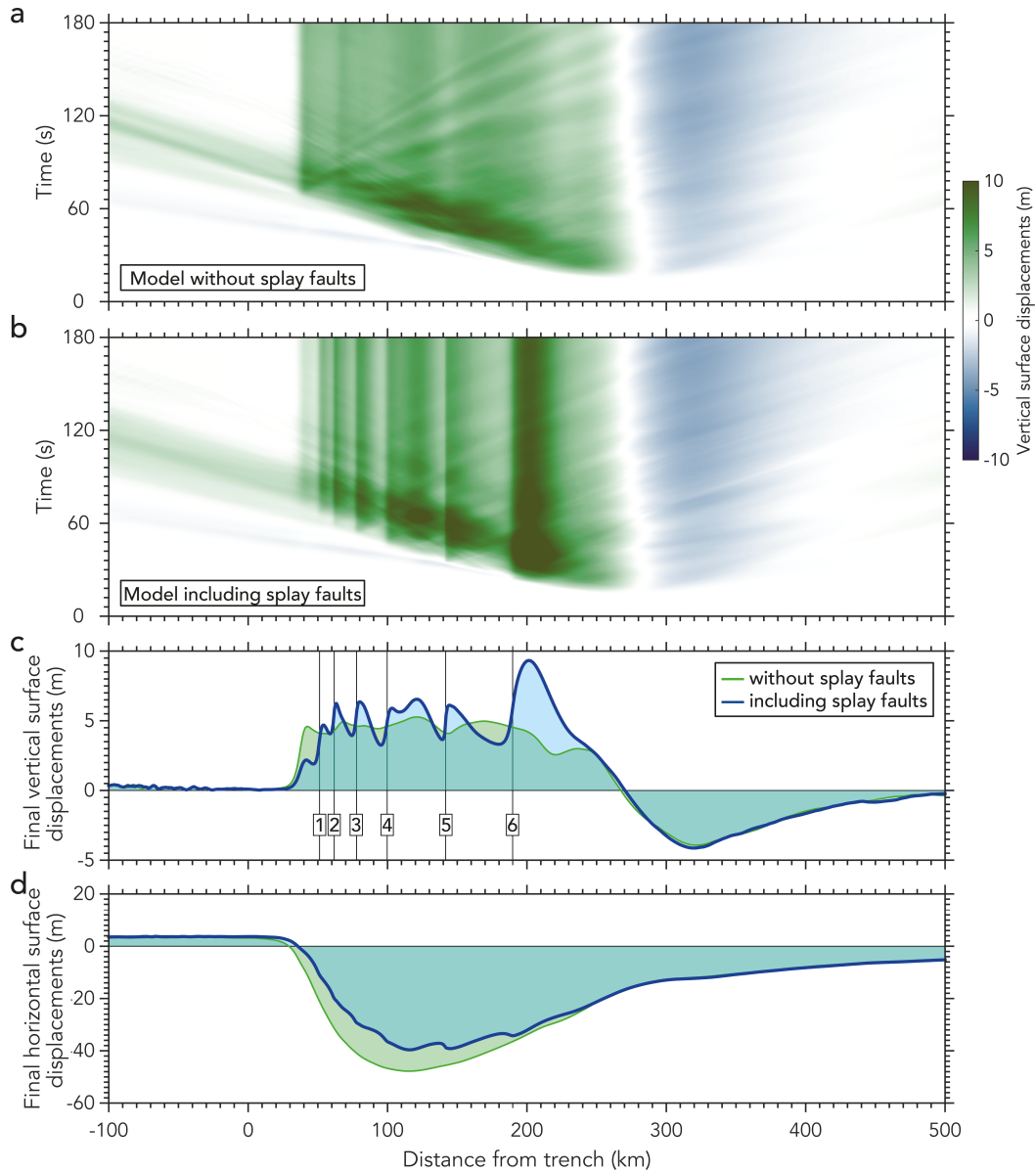


Figure 3. (a,b) Temporal evolution of the vertical surface displacements in the model (a) without splay faults and (b) including all six splay fault geometries. The static vertical (c) and horizontal (d) surface displacements of the two models after 180 s are compared in (c,d) with splay fault numbers indicating the x -coordinates of the shallow splay fault tips near the surface.

207 show maximum stress drops of 2.5–6.5 MPa, with the deeper splay faults exhibiting larger
 208 stress drops than the shallow splay faults.

209 The model without splay faults has relatively uniform static vertical surface dis-
 210 placements of ~ 5 m and a smooth profile of horizontal displacements of 47.8 m sea-

wards (Figure 3). In contrast, the model with splay faults shows clear vertical surface displacement peaks corresponding to the shallow tips of the splay faults near the surface (Figure 3b,c). The wavelengths of these peaks are $\sim 80\text{--}95\%$ smaller than the wavelengths of the vertical surface displacements due to rupture purely on the megathrust. The largest peak of 9.3 m at 180 s is associated with SF6, whereas the other peaks with amplitudes ranging from 4.7–6.5 m are associated with SF1–5. Hence, rupture on splay faults increases the amplitude of the vertical displacements with up to 86%. The amounts of vertical displacement and slip are not linearly correlated (Figure S17) as other factors, such as the dip angle and slip distribution on the fault also play a role. The effect of splay fault rupture is less pronounced in the horizontal displacements with a 17% lower amplitude of the horizontal displacements compared to the model without splay faults (Figure 3d).

3.2 Tsunami propagation and inundation

The tsunami resulting from the model without splay faults consists of a single wave with a wavelength of 300 km and a maximum sea surface height of 6.5 m (Figure 4a). It arrives at the beach after 11 min and it takes a total of 74.5 min for the whole wave to arrive at the coast. There is one episode of flooding at the coast with a run-up length of 1250 m. In the model including splay fault rupture, the tsunami consists of one high wave crest corresponding to slip on SF6 ((7) in Figure 4b) and a broad wave packet resulting from slip on the other splay faults and shallow limit of the megathrust ((1-6) in Figure 4b). Similar to the tsunami of the model without splay faults, the waves span a region of 300 km, but have smaller individual wavelengths. The tsunami first reaches the coast after 11 min and impacts the coast until 71.3 min. It reaches a maximum sea surface height of 12.2 m, which is almost double the height of the model without splay faults. Besides that, the flooding at the coast occurs in two episodes (Figure 4e) in contrast to one flooding episode for the model without splay faults. The first episode is related to the large wave resultant from rupture on SF6, whereas the second episode relates to a wave originating from the interference of the smaller waves related to the other splay faults and shallow megathrust. The run-up length of the tsunami is 2210 m, which is 77% larger than that of the tsunami sourced by a rupture without splay faults.

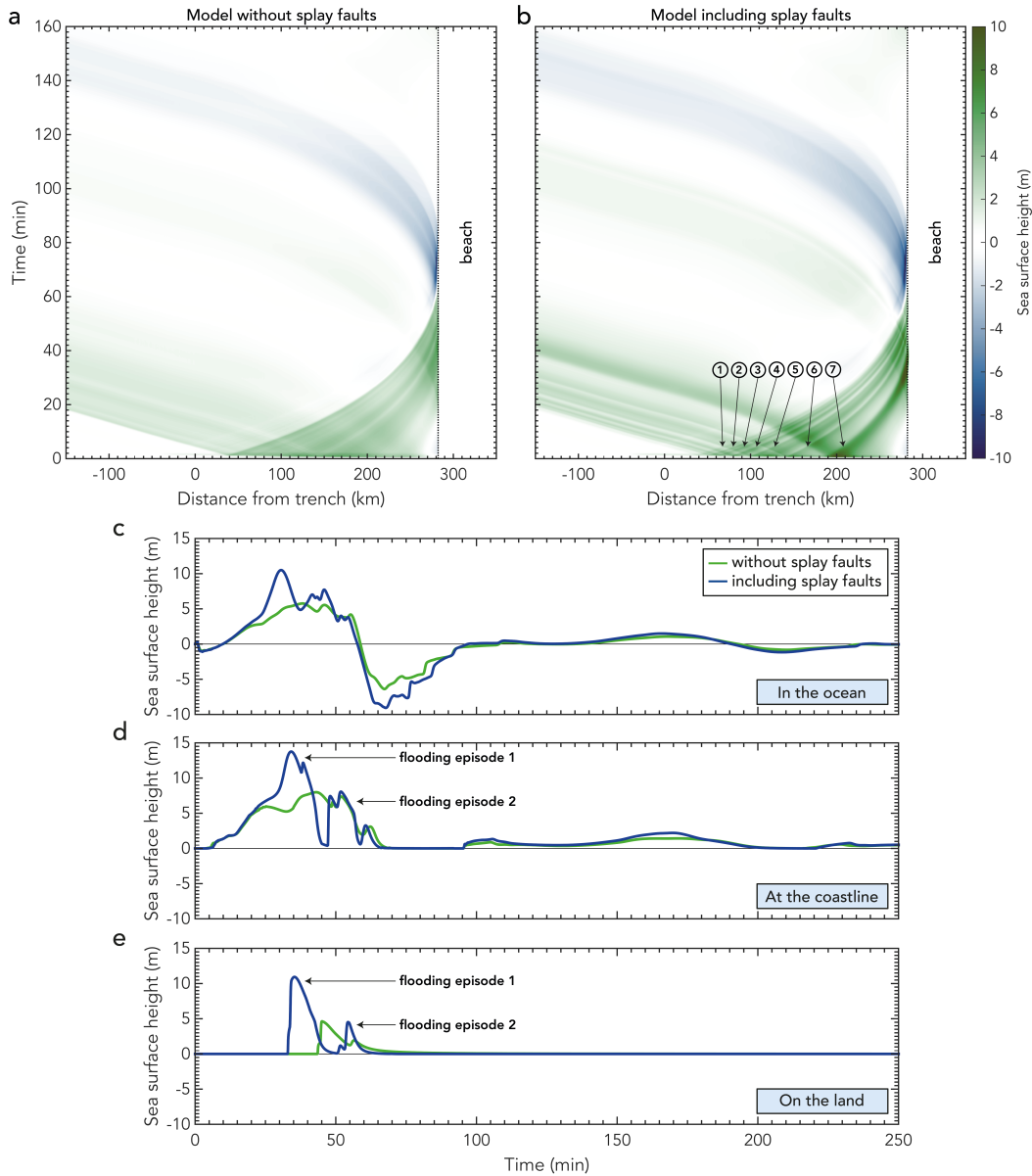


Figure 4. Temporal evolution of the sea surface height for (a) the model without splay faults and (b) the model including all six splay faults. (c,d,e) Sea surface height with time at three different locations for both the model without (green) and with (blue) splay faults: (c) $x = 278.46$ km, in the ocean; (d) $x = 282.46$ km, at the coastline; (e) $x = 283.46$ km, on the beach. As the measurements are taken on land in (d,e), the sea surface height should be interpreted as inundation depth.

241 **4 Discussion**

242 Observational studies of accretionary wedges image multiple splay faults which pose
 243 a tsunami hazard (Kopp, 2013). However, it is difficult to assess if multiple splay faults

244 will rupture during a single earthquake and how that would affect the ensuing tsunami.
 245 The choice of numerical discretisation method typically hampers the geometric complex-
 246 ity in dynamic rupture models (e.g., DeDontney & Hubbard, 2012). Here, we explicitly
 247 account for the complex geometries of a shallowly dipping megathrust intersecting with
 248 several splay faults.

249 Our models show that all six splay faults rupture when we use the self-consistent
 250 initial conditions from the SC model. This is partly due to the predominantly optimal
 251 orientation of the splay faults with respect to the local stress field (Figure 1b). In line
 252 with this, the splay faults exhibit low strength excess (Figures S10-S15) — particularly
 253 at shallow depths — indicating that they are close to failure (Li et al., 2014). Here, we
 254 define strength excess as $\sigma_{\text{yield}}^{\text{dr}} - \tau$, where $\sigma_{\text{yield}}^{\text{dr}}$ is the fault yield stress and τ is the ini-
 255 tial shear stress. The low strength excess of the shallow splay faults partly results from
 256 the weak, i.e., low static friction coefficient, sediments of the accretionary wedge where
 257 high pore-fluid pressures are prevalent (van Dinther et al., 2014). The deeper splay faults
 258 SF4–6 are not as close to failure as the shallower splay faults, but still rupture due to
 259 the energetic rupture and wave reflections and the resulting stress changes. SF5 in par-
 260 ticular does not rupture at the branching point due to the large strength excess and high
 261 branching angle (21.8°). Instead, it is activated at shallow depth due to reflecting waves
 262 from the surface where the strength excess on the fault is small. Hence, our results sug-
 263 gest that multiple splay faults rupture during an energetic event with reflecting waves
 264 when they are well orientated with respect to the local stress field, i.e., they are strong
 265 faults according to Andersonian faulting theory, and have a low strength excess, i.e., they
 266 are close to failure.

267 In the tsunami models, the effect of slip on splay faults is visible in the propagat-
 268 ing wave and the inundation pattern at the coast (Figure 4; Goda et al. (2014)). The
 269 tsunami model without splay fault rupture also shows localised crests (Figure 4a), al-
 270 though to a lesser extent. This indicates that crests in the tsunami data cannot exclu-
 271 sively be contributed to splay fault rupture. Similarly, the absence of complexity in the
 272 tsunami data or source inversion, particularly with regards to the second wave packet,
 273 does not necessarily mean that rupture only occurred on one splay fault. Indeed, the ef-
 274 fect of rupture on other, smaller splay faults might not be distinguishable based on tsunami
 275 data alone. To relate our findings to tsunami data, the here found splay fault effects should
 276 be analysed with more complex bathymetry and 3D complexity in future studies (Matsuyama

277 et al., 1999; Bletery et al., 2015; Ulrich et al., 2019; Madden et al., 2020; Tonini et al.,
278 2020).

279 **5 Conclusions**

280 In this study, we develop and use one of the first modelling frameworks that com-
281 bines geodynamics, seismic cycles, dynamic rupture, and tsunamis. We can therefore con-
282 strain the geometry, stress, and strength of the domain, megathrust, and six splay faults
283 in a physically self-consistent manner. We find that the splay faults are optimally ori-
284 entated with respect to the local stress field — unlike the shallow megathrust — which
285 contributes to splay fault rupture. The splay faults are activated by various mechanisms,
286 such as the passing of the megathrust rupture front and stress changes from reflected waves
287 in the accretionary wedge. Rupture on the largest splay fault in our simulations results
288 in a short-wavelength increase in tsunami height. A second, broad wave packet in the
289 tsunami is due to slip on multiple smaller faults and the shallow megathrust, making it
290 difficult to distinguish from the tsunami data alone if multiple splay faults ruptured. In
291 order to better understand tsunami hazard, future studies should take the possibility of
292 rupture on multiple splay faults into account as it has an effect on the tsunami height
293 and flooding pattern at the coast.

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299 originally wrote the tsunami code.

300 We use scientific colour maps by Crameri (2018b) to prevent visual distortion of
301 the data and exclusion of readers with colour-vision deficiencies (Crameri, 2018a).

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Author contribution statement

IvZ conceived the study, designed and ran the DR models, analysed the DR and TS results, and wrote the article. LR designed the tsunami models together with IvZ and ran them. YvD and AAG supervised IvZ and contributed to the analysis of the SC and DR models. All authors discussed the results and contributed to the final manuscript.

Data availability statement

We use the data of the geodynamic seismic cycle model provided in Van Zelst et al. (2019) to set up our dynamic rupture model. The additional six splay fault geometries can be found in the supplementary material of this article and will be uploaded to Zenodo. We use the two-dimensional version of the open source software package SeisSol to model dynamic rupture (<http://www.seissol.org>). We use the one-dimensional version of the open source code SWE to model the tsunami (<https://github.com/TUM-I5/SWE>), which will also be made available on Zenodo.

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