

---

This manuscript is accepted for publication in *ADVANCES IN GEOPHYSICS*.

The manuscript has undergone peer-review already but has no 'Peer-reviewed Publication DOI' link yet. As soon as possible the link will be made available. Please feel free to contact the author; I welcome feedback.

---

1 Revised submission to *Advances in Geophysics*

2 **Rotational Ground Motion Measurements for Regional Seismic Mo-**  
3 **ment Tensors: a Review**

4 Corresponding author:

5 Donner, Stefanie

6 Address: Bundesanstalt für Geowissenschaften und Rohstoffe (BGR), GeoZentrum Han-  
7 nover, Stilleweg 2, 30655 Hannover, Germany

8 E-mail: [stefanie.donner@bgr.de](mailto:stefanie.donner@bgr.de)

9 Telefon: +49 511 643 3904

10 Hannover, 8th June 2021

11	<b>Contents</b>	
12	<b>List of acronyms and symbols</b>	<b>3</b>
13	<b>Abstract</b>	<b>5</b>
14	<b>1 Introduction</b>	<b>5</b>
15	<b>2 A brief mathematical overview</b>	<b>8</b>
16	2.1 Mathematical description of the point source . . . . .	9
17	2.1.1 Definition of the seismic moment tensor . . . . .	9
18	2.1.2 Geometry of the seismic moment tensor . . . . .	11
19	2.1.3 Decomposition of the seismic moment tensor . . . . .	14
20	2.2 Introduction to rotational ground motion . . . . .	17
21	2.2.1 Fundamental theory . . . . .	17
22	2.2.2 Measuring rotational ground motions . . . . .	19
23	2.2.3 Rotations due to a double-couple point source . . . . .	21
24	2.2.4 Strain-rotation coupling and local side effects . . . . .	21
25	<b>3 Benefits of rotational ground motions for regional seismic moment tensors</b>	<b>22</b>
26	3.1 General benefits for the resolution of the moment tensor components . . . . .	23
27	3.2 Influence of the receiver distribution . . . . .	26
28	3.3 Influence of frequency range and structural model . . . . .	30
29	3.4 Resolution of the centroid depth . . . . .	33
30	3.5 Resolvability of the tectonic mechanism and DC/non-DC parts . . . . .	34
31	3.6 Influence of noise . . . . .	35
32	<b>4 Summary</b>	<b>36</b>
33	<b>5 Outlook</b>	<b>37</b>
34	<b>Acknowledgement</b>	<b>39</b>
35	<b>References</b>	<b>39</b>

## 36 List of acronyms and symbols

### 37 Acronyms

38	1D/2D/3D	1-/2-/3-dimensional
39	3C/6C	3/6 components of waveform data: translation vs. translation+rotation
40	CLVD	compensated linear vector dipole part of source mechanism
41	DC	double-couple (tectonic) part of source mechanism
42	DEV	deviatoric part of source mechanism
43	GF	Green's function
44	IG	Shannon's criterion of information gain
45	INSN	Iranian National Seismic Network
46	ISO	isotropic (volumetric) part of source mechanism
47	kde	(Gaussian) kernel density estimation
48	pdf	(prior/posterior) probability density function

### 49 Symbols

50	$\hat{\mathbf{r}}, \hat{\boldsymbol{\theta}}, \hat{\boldsymbol{\phi}}$	unit vectors of spherical polar coordinate system
51	$\mathbf{A}^P, \mathbf{A}^S, \mathbf{A}^R$	radiation pattern of translational P- and S-wave, and rotational S-wave
52	$\mathbf{a}_i, e_i$	eigenvectors and -values of the moment tensor
53	$\mathbf{d}$	displacement (or slip) vector on the rupture plane
54	$\mathbf{G}, G_{ij}, G_{ij,k}$	tensor of Green's functions and its spatial derivatives
55	$\mathbf{J}$	strain-rotation coupling vector
56	$\mathbf{M}, M_{jk}$	seismic moment tensor
57	$\mathbf{s}_k$	slowness vector
58	$\mathbf{t}, \mathbf{b}, \mathbf{p}$	tension/null/pressure axis of moment tensor
59	$\mathbf{u}, u_i$	translational displacement field, field component
60	$\mathbf{x}, t$	location and time of observation
61	$\boldsymbol{\omega}, \omega_i$	rotational ground motion, field components
62	$\boldsymbol{\omega}^{FS}$	rotational ground motion at the Earth surface

63	$\xi, \tau$	location and time of source origin
64	$\phi, \delta, \lambda$	strike, dip, and rake angles of DC part of the moment tensor; angles of
65		rupture plane and slip vector orientation
66	$F_j$	total force component exerted by the source
67	$f_j$	body force density component within source region, ' <i>stress glut</i> '
68	$M_0$	seismic moment
69	$S$	source time function

## Abstract

Seismic moment tensors are an important tool in geosciences on all spatial scales and for a broad range of applications. The basic underlying theory is established since decades. However, various factors influence the reliability of the inversion result, several of them are mutually dependent. Hence, a reliable retrieval of seismic moment tensors is still hampered in many cases, especially at regional event-receiver distances.

To sample the entire wavefield due to a seismic source we need six components: three translational and three rotational ones. Up to now, only translational ground motion recordings were used for moment tensor retrieval, missing out valuable information.

Using rotational in addition to the classical translational ground motions during waveform inversion for moment tensors mainly adds information on the vertical displacement gradient to the inversion problem. Furthermore, having available six instead of only three components per receiver location provides additional constraints on the sampling of the radiation pattern.

As a result, the moment tensor components are resolved with higher precision and accuracy, even when the number of recording receivers is considerably reduced. Especially, components with a dependence to depth as well as the centroid depth can benefit significantly from additional rotational ground motion.

Up to the time of writing this review only a few studies are published on the topic. Here, I summarise their findings and provide an overview over the possible capabilities of including rotational ground motion measurements to waveform inversion for seismic moment tensor retrieval.

## 1 Introduction

In an effort to mathematically describe the source processes during an earthquake, mainly three models have emerged over time: seismic moment tensors, kinematic, and dynamic source descriptions (Aki and Richards, 2002). They differ in their underlying assumptions and applied simplifications as well as in their information on the source processes. Seismic moment tensors assume all energy release in one point in space described by a system of body forces acting at that point. We can derive information on source geometry, strength and composition. The kinematic source model assumes a time-dependent displacement field but without considering the stresses and forces responsible for it. We get information on the rupture dimension and propagation as well as slip direction and slip rate function in addition to geometry and strength. The most complex model is the dynamic source model which aims at a complete physical understanding of the rupture physics including initial and boundary conditions for the stresses and forces involved as well as material properties. It is based on solving the elastodynamic equation of motion and, thus, is quite expensive in

106 storage and computational resources.

107 Seismic moment tensors are an integral and essential part of geosciences (D’Amico, 2018).

108 They help us to understand the mechanics of single earthquakes or earthquake sequences

109 (e.g. Kanamori and Given, 1982; Dreger and Helmberger, 1991; Braunmiller et al., 2002;

110 Krüger and Scherbaum, 2014). Using a comprehensive catalogue of moment tensor solutions,

111 they provide useful insight into the seismotectonics of a region (e.g. Herrmann et al., 2011;

112 Kinscher et al., 2013; Dahm et al., 2018; Schippkus et al., 2020). Also, such a catalogue of

113 moment tensors can be inverted again to obtain information on the stress condition of the

114 upper crust (e.g. Gephart and Forsyth, 1984; Heidbach et al., 2018). Lessons learned from

115 seismotectonic and crustal stress studies in turn are a fundamental base for seismic hazard

116 studies. In Tsunami warning systems seismic moment tensors are a crucial input to estimate

117 the likeliness of such a threat within a few minutes after a large earthquake (e.g. Kanamori

118 and Rivera, 2008; Inazu et al., 2016).

119 While we need some prior knowledge about Earth structure to determine moment tensors

120 (see Sec. 2.1.1) they also help us to gain an improved estimate on underground structures.

121 In tomographic studies, moment tensors are used to simulate seismic waveforms and study

122 their distortions while travelling through the underground. These distortions provide direct

123 evidence for structural details (e.g. Toyokuni and Takenaka, 2006; Nissen-Meyer et al.,

124 2014; Shi et al., 2018).

125 In contrast to focal solutions from first motion body wave polarities, seismic moment tensors

126 contain information beyond the pure shear motion. Hence, they are a useful tool for source

127 discrimination. Possible applications are the identification of an explosion, for example in

128 the frame of the Comprehensive Nuclear Test-Ban Treaty (e.g. Gaebler et al., 2019), the

129 interpretation of volcanic signals (e.g. Nettles and Ekström, 1998; Legrand et al., 2000), and

130 the monitoring of induced seismicity for example at geothermal facilities, mining areas or

131 within oil/gas production fields (e.g. Dahm et al., 2007; Cesca et al., 2013; Sen et al., 2013;

132 Kühn et al., 2020).

133 Almost 60 years ago, Haskell (1964) presented equations for the radiation pattern of surface

134 waves from double-couple (DC, see section 2.1.3) point sources in a layered medium. In

135 1970 Gilbert provided *‘a very compact and simple representation for the transient response*

136 *of the Earth to earthquakes’*, the first definition of the seismic moment tensor. He used it to

137 calculate the static displacement field caused by Earth’ normal mode eigenfunctions. Three

138 years later, he extended his theory to the formulation of a linear inverse problem with six

139 independent elements for the moment tensor (Gilbert, 1973). Dziewonski and Gilbert (1974)

140 and Gilbert and Dziewonski (1975) further extended the theory and applied it to determine

141 the source mechanisms of earthquakes. The seismic moment tensor is related to the inelastic

142 processes inside the focal region only and is zero outside of it (Backus and Mulcahy, 1976;

143 Backus, 1977a). Therefore, it is a perfect general concept to describe a variety of seismic  
144 sources.

145 The seismic point-source moment tensor is a low-frequency assumption, valid only below the  
146 corner frequency of the studied event (see section 2.1.1). In addition, several authors invest-  
147 igated early the relation between moment tensors of higher degree to seismic sources with  
148 finite extend (kinematic sources). Here, Backus (1977a), Backus (1977b), Stump and John-  
149 son (1982), Doornbos (1982), and Silver (1983) are to be mentioned for example. However,  
150 in this study, I focus on the point-source moment tensor.

151 Traditionally, the waveform inversion for seismic moment tensors is further classified in  
152 global, regional, and sometimes also local application. Yet, this classification is just a proxy  
153 for different length scales and the amount of heterogeneities involved. Although, there is  
154 no strict definition, we can say that 'global' starts beyond event-receiver distances of about  
155 1000-3000 km for moment tensor applications. The larger the event-receiver distance, a larger  
156 fraction of the wavefield passes through deeper parts of the Earth instead of the crust. The  
157 velocity structure of the Earth interior is much more homogeneous than than the crustal  
158 structure. Therefore, teleseismic recordings are easier to model, a processing step necessary  
159 in waveform inversion for moment tensors. As soon as distances become close enough that  
160 the wavefield fraction passing the highly complex structures of the crust is longer than the  
161 wavefield fraction passing deeper Earth, waveform inversion becomes more complicated. This  
162 is mainly due to the more complex waveforms compared to the teleseismic distance range.  
163 Several practical consequences for the waveform inversion can be derived from this general  
164 difference. They are explained in more detail in section 3.3. Keeping this generalisation in  
165 mind the classification is rather twofold between 'global' and 'regional', with 'local' being a  
166 subclass of regional.

167 On the global scale the implementation of waveform inversion schemes are well established.  
168 Since 1982 the Global CMT Project (formerly called the Harvard CMT Project) provides a  
169 global catalogue of moment tensor solutions, comprehensive for earthquakes with magnitudes  
170  $M > 5$  (Dziewonski et al., 1981; Ekström et al., 2012). The determination on a regional  
171 (or even local) scale is more complicated. The stability of the waveform inversion result  
172 is affected by less well-known structural models (e.g. Šílený, 2004; Vasyura-Bathke et al.,  
173 2021), influence of theoretical and measurement noise (e.g. Sipkin, 1986; Duputel et al., 2012;  
174 Mustać et al., 2020), unfavourable event-receiver geometries (e.g. Dreger and Helmberger,  
175 1993; Delouis and Legrand, 1999), ignored source complexities (e.g. Adamova and Šílený,  
176 2010), and limitations of methodological approaches (e.g. Fan and Wallace, 1991; Frohlich,  
177 1994; Julian et al., 1998; Cesca and Heimann, 2018).

178 The literature about the topic is so numerous that the citations given in here can cover only  
179 a small fraction of it. I hope that it provides an overview broad enough to serve as a good



180 starting point for own research. Providing a fully comprehensive review on all aspects of  
181 seismic moment tensors would include the complete theory, an overview on methodological  
182 approaches for inversion as well as codes and algorithms, discussing the limits and uncertainty  
183 estimation, backlashes, etc. That is a book-filling task and beyond the scope of this paper.  
184 Therefore, this review concentrates on some practical aspects during waveform inversion for  
185 seismic moment tensors in the regional distance range. These are probably also applicable  
186 to the local distance range because of similar reasons for complexities. The main focus is  
187 the integration of rotational ground motion recordings into the waveform inversion and how  
188 they can improve the reliability of the resulting seismic moment tensor.

189 A short comment on the wording: very often I read about '*moment tensor inversion*'. This  
190 is logically not entirely correct. Moment tensors are the output of the inversion. The inputs  
191 are waveforms, i. e. recordings of the wavefield or seismograms. Therefore, the logically  
192 correct phrasing should be '*waveform inversion for seismic moment tensors*' or '*moment  
193 tensor retrieval or determination*'.

194 The paper is structured in two main parts. After briefly introducing the theory of the seismic  
195 moment tensor and rotational ground motions in Section 2, Section 3 provides a review on  
196 the results of waveform inversion including rotational ground motions for seismic moment  
197 tensors. It is followed by a summary in Section 4 and an Outlook in Section 5.

## 198 **2 A brief mathematical overview**

199 In the following, I provide a brief overview of the theoretical background of the seismic  
200 moment tensor as well as rotational ground motions. The information given are restricted  
201 to what is necessary to understand this review article. For more in-depth theory about  
202 the seismic moment tensor, I suggest for beginners Jost and Herrmann (1989), Krüger and  
203 Bock (2009), Cesca and Heimann (2013), and Dahm and Krüger (2014). More advanced  
204 readers may prefer Udías, Madariaga, and Buforn (2014) and Aki and Richards (2002). An  
205 introduction into rotational ground motions for beginners can be found in Cochard et al.  
206 (2006), Li and van der Baan (2017), and Igel et al. (2015). For more advanced readers I  
207 suggest Aki and Richards (2002), Schmelzbach et al. (2018) and Sollberger et al. (2020).

208 In the following, tensors appear in bold face (for example  $\mathbf{u}$  for vectors and  $\mathbf{M}$  for matrices).  
209 Subscripts (for example  $u_i$ ) indicate components of tensors with  $i = x, y, z$  being the three  
210 space axes. Einstein's summation convention applies on repeated indices.

## 2.1 Mathematical description of the point source

### 2.1.1 Definition of the seismic moment tensor

For a general elastodynamic source, the linear relation between the observed displacement field component  $u_i$  at observation point  $\mathbf{x}$  and time  $t$  and the distribution of equivalent body force densities  $f_j$  within the source region  $\boldsymbol{\xi}$  at origin time  $\tau$  is given by (Gilbert, 1970; Aki and Richards, 2002):

$$u_i(\mathbf{x}, t) = \iiint_V G_{ij}(\mathbf{x}, t - \tau; \boldsymbol{\xi}, 0) * f_j(\boldsymbol{\xi}, t) d^3\xi \quad (1)$$

Displacement and traction are omitted. The  $*$  marks a temporal convolution.  $G_{ij}$  are the Green's functions (GF) defined as the response of the medium to a unidirectional unit  $\delta$ -Dirac impulse in space and time. They provide the  $i$ -th component of displacement at place  $\mathbf{x}$  and time  $t$  due to a force in direction  $j$  at place  $\boldsymbol{\xi}$  and time  $\tau$ . Because the boundary conditions at  $t < \tau$  are time-independent, the GFs depend only on the difference between origin and observation time  $t - \tau$  but not on the origin time  $\tau$  itself.

The spatial integral in Eq. 1 can be simplified by Taylor series expansion around the source  $\boldsymbol{\xi}_0$  as reference point. This reference point is defined as the centroid location of the source, the point of highest energy release. Usually, it does not coincide with the hypocenter, the point where the rupture starts. Applying the point source assumption, we assume that the GF do not change (much) within the source volume. That is, the considered wavelength must be larger than the source dimension. Then, we only need to consider the first two terms of the Taylor series and the equation modifies to:

$$u_i(\mathbf{x}, t) = G_{ij}(\mathbf{x}, t - \tau; \boldsymbol{\xi}_0, 0) * F_j(t) + G_{ij,k}(\mathbf{x}, t - \tau; \boldsymbol{\xi}_0, 0) * M_{jk}(t) \quad (2)$$

$F_j(t)$  is the total force exerted by the source. It is defined as the volume integral of the body-force density  $f_j(\boldsymbol{\xi}, t)$  arising from the difference between the model stress and the actual physical stress when describing the physical, non-linear source processes by an equivalent force system (Julian et al., 1998). Backus and Mulcahy (1976) called this body-force density the '*stress glut*'. Omitting effects of gravitation and mass advection, the stress glut vanishes outside the source medium and, hence, the total force  $F_j(t)$  is zero. It remains:

$$u_i(\mathbf{x}, t) = M_{jk}(t) * G_{ij,k}(\mathbf{x}, t - \tau; \boldsymbol{\xi}_0, 0) \quad (3)$$

This is the basic equation for the waveform inversion for seismic moment tensors. The (linearised) forward problem is given by  $\mathbf{u} = \mathbf{G}\mathbf{m}$ . It can be further simplified when we formally rewrite the tensor of GFs to  $G_{ij} = G_{ij}(\mathbf{x}(\xi), t(\xi))$ . Then, the spatial derivative in

239 Eq. 3 turns to:

$$\begin{aligned}
 G_{ij,k} &= \frac{\delta}{\delta \xi_k} G_{ij} \\
 &= \frac{\delta G_{ij}}{\delta x_n} \frac{\delta x_n}{\delta \xi_k} + \frac{\delta G_{ij}}{\delta t} \frac{\delta t}{\delta \xi_k}
 \end{aligned}
 \tag{4}$$

240 The first term of the right hand side is the near-field term and can be neglected at larger  
 241 distances. The second term is the far-field. The second factor of the second term is the  
 242 slowness vector  $s_k = \frac{\delta t}{\delta \xi_k}$ . Omitting near-field effects, equation 3 turns to:

$$\begin{aligned}
 u_i(\mathbf{x}, t) &= M_{jk}(t) * \dot{G}_{ij}(\mathbf{x}, t) s_k \\
 &= \dot{M}_{jk}(t) * G_{ij}(\mathbf{x}, t) s_k
 \end{aligned}
 \tag{5}$$

243 with the dot representing temporal derivative which can be interchanged between the GFs  
 244 and the moment tensor.

245 We assume that all components of the moment tensor  $M_{jk}(t)$  have the same time dependence  
 246 which corresponds to the source time function  $S(t)$ . With the point source assumption, the  
 247 source time function is modelled as a Dirac  $\delta$ -pulse and, thus, becomes unity in the far-field.  
 248 This approach is valid as long as the real source duration is shorter than the shortest periods  
 249 (that is highest frequencies) considered during inversion. With another Taylor expansion of  
 250 the GFs around the centroid time  $\tau_0$  and again neglecting terms of higher order we obtain  
 251 (Dahm, 1993; Dahm and Krüger, 2014):

$$\begin{aligned}
 u_i(\mathbf{x}, t) &= M_{jk} \cdot \left[ \dot{S} * G_{ij}(\mathbf{x}, t) s_k \right] \\
 &= M_{jk} \cdot G_{ij,k}(\mathbf{x}, t)
 \end{aligned}
 \tag{6}$$

252 The second factor in this equation is a rephrase of the spatial derivatives of the far-field GFs  
 253 with respect to the centroid.

254 From the seismic moment tensor, we not only obtain information about the physical source  
 255 processes (see section 2.1.3) but also on the strength of the source. The seismic moment is  
 256 defined directly on the moment tensor components Silver and Jordan (1982):

$$M_0 = \sqrt{\frac{\sum M_{kj}^2}{2}}
 \tag{7}$$

257 It has the unit of energy (Nm) and we can derive the moment magnitude from it. In addition,

258 the waveform inversion for the seismic moment tensor provides us with an estimate for the  
 259 centroid depth. The pre-calculated GFs needed for the inversion are based on a specific  
 260 depth. In practice, the waveform inversion is repeated with GFs for different depths and the  
 261 inversion with the best residual is assumed to be in the correct depth.

### 262 2.1.2 Geometry of the seismic moment tensor

263 The seismic moment tensor  $M_{ij}$  is the most general description of equivalent body forces for  
 264 a seismic point source. It is a tensor of second order with nine components (Fig. 1). Each  
 265 represents the strength (moment) of an elementary force couple.

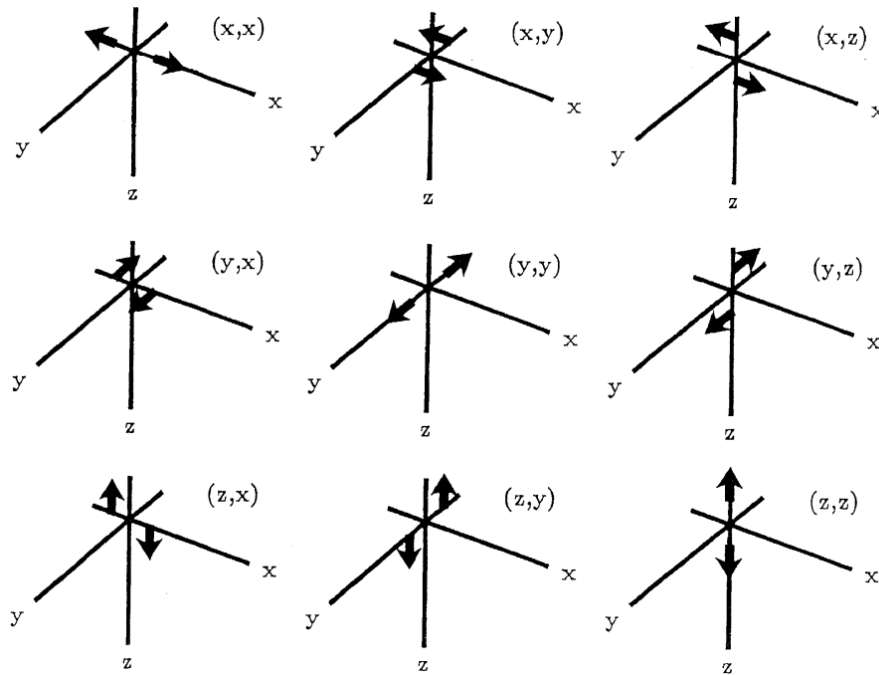


Figure 1: The nine components of the seismic moment tensor representing generalised force couples (from Jost and Herrmann, 1989).

266 The diagonal elements represent linear dipoles causing no torque. The off-diagonal elements  
 267 correspond to force couples ('double-couples'). They represent shear dislocation with three  
 268 different orientations. They can be connected to the displacement (or slip) vector  $\mathbf{d}$  on the  
 269 rupture plane and its normal vector  $\mathbf{n}$ :

$$M_{jk} = \mu A(d_k n_j + d_j n_k) \quad (8)$$

270 with  $\mu$  and  $A$  being the shear modulus of the source area and the area of the rupture plane,  
 271 respectively (Fig. 2). Because switching  $\mathbf{d}$  and  $\mathbf{n}$  has no consequences on the resulting tensor  
 272 element, it follows that the moment tensor is symmetric and, therefore, also the off-diagonal

273 elements exert no torque. As a consequence, only six of the nine moment tensor components  
 274 are independent which can be inverted for from wavefield recordings.

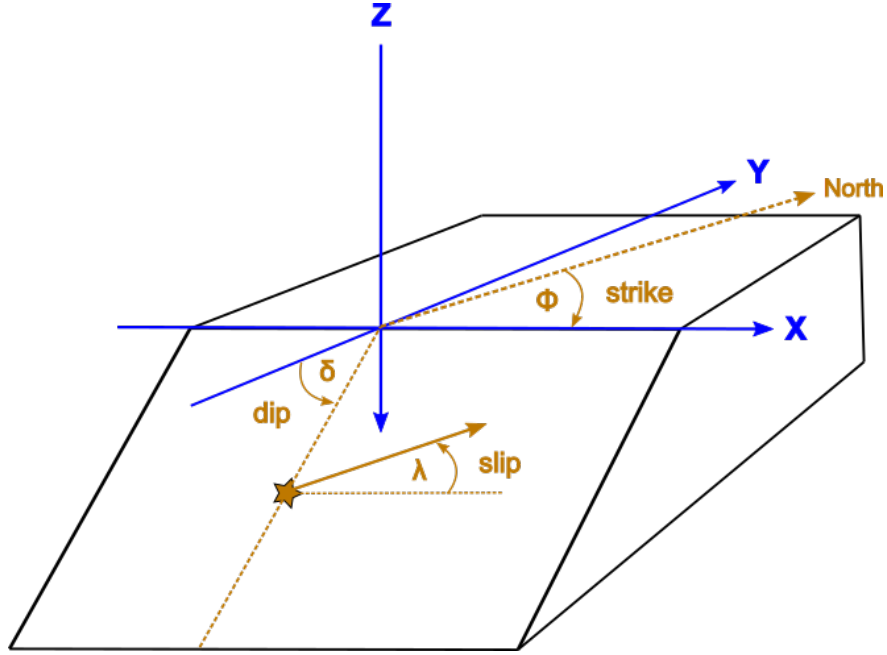


Figure 2: Block model of a shear rupture plane showing the three angles strike, dip, and slip or rake defining the orientation of the rupture plane and of the displacement (or slip) vector. These angles are related to the seismic moment tensor via Eq. 11. The star on the rupture plane marks the centroid location.

275 It also follows that the displacement and normal vector can not be separated from each other.  
 276 Therefore, the source solution contains two nodal planes and it needs further information to  
 277 distinguish the fault from the auxiliary plane. For example, these information be aftershock  
 278 distribution, known fault orientation, or borehole breakouts.

279 In an infinite, homogeneous and isotropic medium we can describe the ground motion due to a  
 280 point shear dislocation (DC) with an analytical solution. Aki and Richards (2002) have given  
 281 the expressions for the vertical, radial and transversal components of the displacement  $\mathbf{u}(\mathbf{x}, t)$   
 282 in spherical polar coordinates centered on the source (Fig. 3). These expressions include  
 283 terms for the energy radiation pattern for the P- and S-wavefield in the near, intermediate,  
 284 and far-field. For the far-field these radiation pattern terms are:

$$\begin{aligned} \mathbf{A}^P &= \sin 2\theta \cos \phi \hat{\mathbf{r}} \\ \mathbf{A}^S &= \cos 2\theta \cos \phi \hat{\boldsymbol{\theta}} - \cos \theta \sin \phi \hat{\boldsymbol{\phi}} \end{aligned} \quad (9)$$

285 The vectors  $\hat{\mathbf{r}}$ ,  $\hat{\boldsymbol{\theta}}$ , and  $\hat{\boldsymbol{\phi}}$  are the unit vectors of the spherical polar coordinate system in

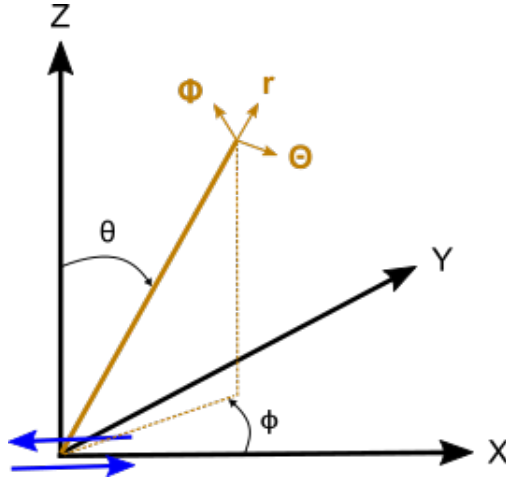


Figure 3: Cartesian (black) and spherical polar (orange) coordinates to describe double-couple displacement components. Blue indicates a point shear dislocation in the x-y plane related to Eqs. 9 and 19 for radiation patterns of translation and rotation.

286 the vertical, radial, and transverse directions, respectively (see Fig. 3). Mathematically, the  
 287 moment tensor can be rotated in any coordinate system. Thus, we always find a system where  
 288 the tensor comprise only three orthogonal linear force dipoles. Then, the eigenvectors of the  
 289 moment tensor correspond to the principal axes which can be defined via the displacement  
 290 and normal vector (Jost and Herrmann, 1989):

$$\mathbf{t} = \frac{1}{\sqrt{2}}(\mathbf{n} + \mathbf{d}) \quad \text{tension axis} \quad (10a)$$

$$\mathbf{b} = \mathbf{n} \times \mathbf{d} \quad \text{null axis} \quad (10b)$$

$$\mathbf{p} = \frac{1}{\sqrt{2}}(\mathbf{n} - \mathbf{d}) \quad \text{pressure axis} \quad (10c)$$

291 Using these equations, we can derive the connection between the moment tensor components  
 292  $M_{jk}$  and the geological faulting geometry, meaning the three angles strike  $\phi$ , dip  $\delta$ , and rake

293 (or slip)  $\lambda$  of a shear (DC) mechanism (Fig. 2, Jost and Herrmann, 1989):

$$\begin{aligned}
M_{xx} &= -M_0(\sin \delta \cos \lambda \sin 2\phi + \sin 2\delta \sin \lambda \sin^2 \phi) \\
M_{yy} &= M_0(\sin \delta \cos \lambda \sin 2\phi - \sin 2\delta \sin \lambda \cos^2 \phi) \\
M_{zz} &= M_0(\sin 2\delta \sin \lambda) \\
M_{xy} &= M_0(\sin \delta \cos \lambda \cos 2\phi + 0.5 \sin 2\delta \sin \lambda \sin 2\phi) \\
M_{xz} &= -M_0(\cos \delta \cos \lambda \cos \phi + \cos 2\delta \sin \lambda \sin \phi) \\
M_{yz} &= -M_0(\cos \delta \cos \lambda \sin \phi - \cos 2\delta \sin \lambda \cos \phi)
\end{aligned}
\tag{11}$$

294 Figure 4 provide some examples of moment tensors and their corresponding focal mechanism  
295 in beachball representation.

### 296 **2.1.3 Decomposition of the seismic moment tensor**

297 Equation 11 relates the moment tensor components to a pure shear rupture, a DC mech-  
298 anism. Such a moment tensor is characterised by eigenvalues summing up to zero and one  
299 of the eigenvalues being zero itself. The largest and smallest eigenvalue correspond to the  
300 tension and pressure axes, respectively (Eqs. 10). However, we usually have no pure DC  
301 mechanisms but seismic sources include opening/closing fractures, volume changes, or other  
302 complexities. They are connected with physical mechanisms beyond pure shear earthquakes,  
303 such as volcanic or induced seismicity. The full seismic moment tensor represents a linear  
304 combination of such effects. There are several ways to separate the different mechanisms  
305 from each other. A good overview about such 'decomposition' schemes can be found in Jost  
306 and Herrmann (1989) and Dahm and Krüger (2014).

307 The most common and widely used scheme is the decomposition into physical (geological)  
308 sources. These are namely the already mentioned DC part representing shear rupture, the  
309 isotropic (ISO) part representing volume changes within the source, and the compensated  
310 linear vector dipole (CLVD, Knopoff and Randall, 1970; Fitch et al., 1980):

$$\mathbf{M}_{full} = \mathbf{M}_{DC} + \mathbf{M}_{ISO} + \mathbf{M}_{CLVD}.
\tag{12}$$

311 The CLVD part has no verified geological interpretation. When inverting waveforms for  
312 earthquake mechanisms, it is often interpreted as residual radiation from the DC source  
313 part. A low CLVD part is then interpreted as a confirmation of the model assumptions.  
314 However, several studies suggest that it might be more than just a mathematical leftover.  
315 Tensile faulting, where the displacement discontinuity is normal instead of parallel to the  
316 fault plane, or deep earthquakes caused by phase transformation (in subduction zones) can

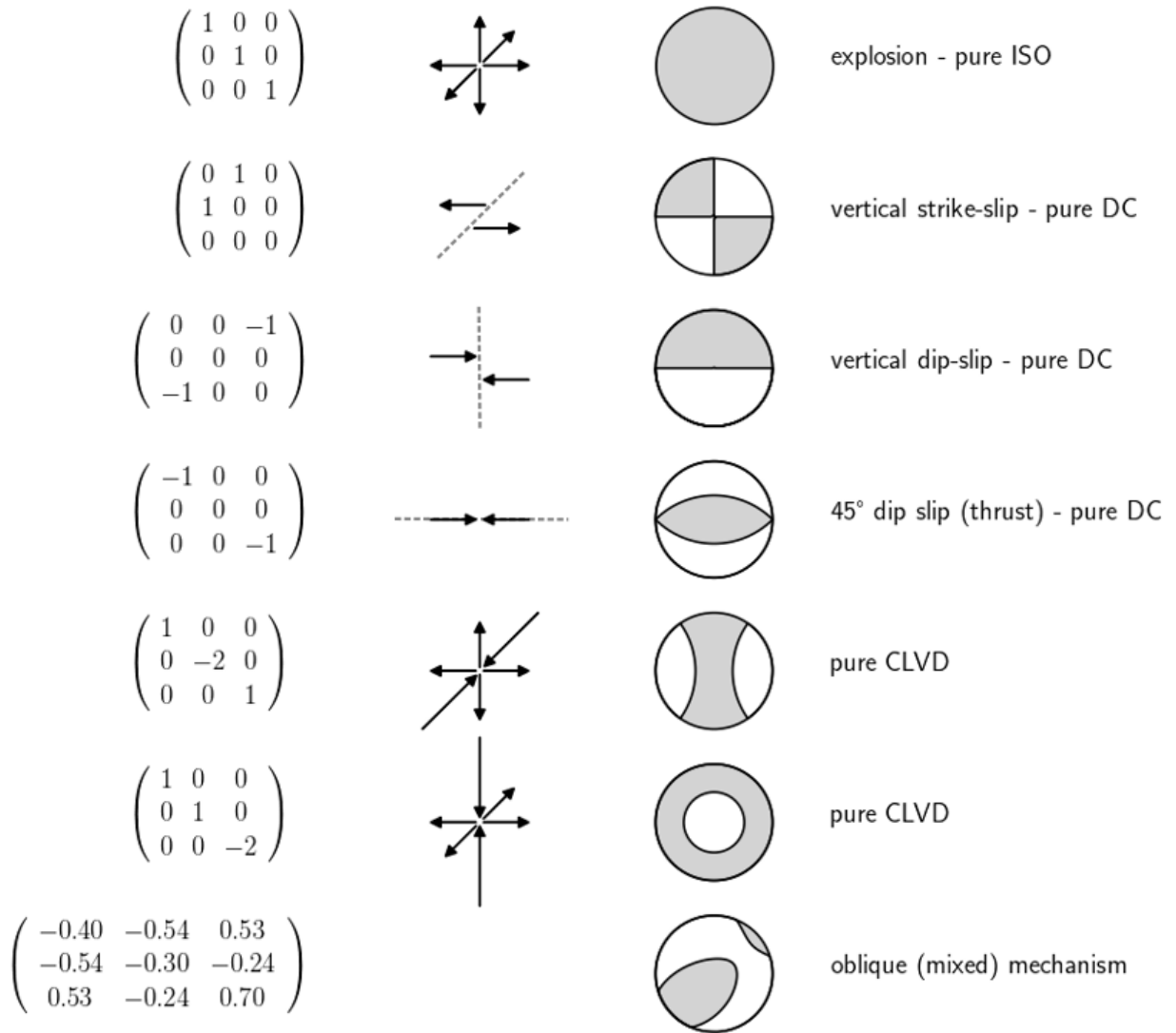


Figure 4: Examples of seismic moment tensors and their corresponding force couples and focal mechanisms. Grey dotted lines mark the axes on which the force couple acts. The arrows mark the force direction of the couple. The moment tensor components are given in the NWU (North-West-Up) coordinate system.

317 be explained with CLVD mechanisms (e.g. Julian et al., 1998). Fault complexities such as  
 318 curvatures can also cause CLVD source components (e.g. Frohlich, 1990). Furthermore, in  
 319 volcano seismology a CLVD can explain ring-faulting mechanisms associated with caldera  
 320 collapse (e.g. Shuler et al., 2013; Gudmundsson et al., 2016).

321 To decompose the full seismic moment tensor according to Eq. 12, it first need to be trans-  
 322 formed into its principal axes coordinate system (see Eq. 10) by determining its eigenvalues



323  $e_i$  and eigenvectors  $\mathbf{a}_i$  (Jost and Herrmann, 1989):

$$\mathbf{M} = \begin{pmatrix} \mathbf{a}_1 & \mathbf{a}_2 & \mathbf{a}_3 \end{pmatrix} \mathbf{e} \begin{pmatrix} \mathbf{a}_1^T \\ \mathbf{a}_2^T \\ \mathbf{a}_3^T \end{pmatrix} = \begin{pmatrix} a_{1x} & a_{2x} & a_{3x} \\ a_{1y} & a_{2y} & a_{3y} \\ a_{1z} & a_{2z} & a_{3z} \end{pmatrix} \begin{pmatrix} e_1 & 0 & 0 \\ 0 & e_2 & 0 \\ 0 & 0 & e_3 \end{pmatrix} \begin{pmatrix} a_{1x} & a_{1y} & a_{1z} \\ a_{2x} & a_{2y} & a_{2z} \\ a_{3x} & a_{3y} & a_{3z} \end{pmatrix}. \quad (13)$$

324 The elements of  $\mathbf{e}$ , the diagonalised moment tensor, correspond to the eigenvalues of  $\mathbf{M}_{full}$ .  
 325 In the next step, we separate the ISO moment tensor, which is defined as 1/3 the trace of  
 326  $\mathbf{M}_{full}$ :

$$\mathbf{M}_{ISO} = \frac{1}{3} \begin{pmatrix} tr(\mathbf{M}) & 0 & 0 \\ 0 & tr(\mathbf{M}) & 0 \\ 0 & 0 & tr(\mathbf{M}) \end{pmatrix}. \quad (14)$$

327 What remains is the deviatoric moment tensor  $\mathbf{M}_{DEV} = \mathbf{M}_{full} - \mathbf{M}_{ISO}$  with eigenvalues  $e_i^{dev}$ .  
 328 Assuming  $|e_3^{dev}| \geq |e_2^{dev}| \geq |e_1^{dev}|$  the deviatoric moment tensor  $\mathbf{M}_{DEV}$  can be rewritten to:

$$\begin{aligned} \mathbf{M}_{DEV} &= e_3^{dev} \begin{pmatrix} -K & 0 & 0 \\ 0 & (K-1) & 0 \\ 0 & 0 & 0 \end{pmatrix} \\ &= e_3^{dev}(1-2K) \begin{pmatrix} 0 & 0 & 0 \\ 0 & -1 & 0 \\ 0 & 0 & 1 \end{pmatrix} + e_3^{dev}K \begin{pmatrix} -1 & 0 & 0 \\ 0 & -1 & 0 \\ 0 & 0 & 2 \end{pmatrix} \end{aligned} \quad (15)$$

329 with  $K = -e_1^{dev}/e_3^{dev}$  and  $(K-1) = e_2^{dev}/e_3^{dev}$  and  $K$  being in the range  $0 \leq K \leq 0.5$ . The  
 330 first term on the RHS in Eq. 15 represents the DC source component while the second term  
 331 stands for the CLVD part.

332 Visualising all source components in one plot is not a trivial task. Tape and Tape (2012)  
 333 and Aso et al. (2016) provide overviews about different source-type plots. Nowadays, the  
 334 most common one in use is the Hudson plot (Fig. 5, Hudson et al., 1989). It provides 'a  
 335 two-dimensional graphical display of all possible relative sizes of the three principal moments'  
 336 using a projection onto a cube. It has the advantage of an equal-area source-type plot.

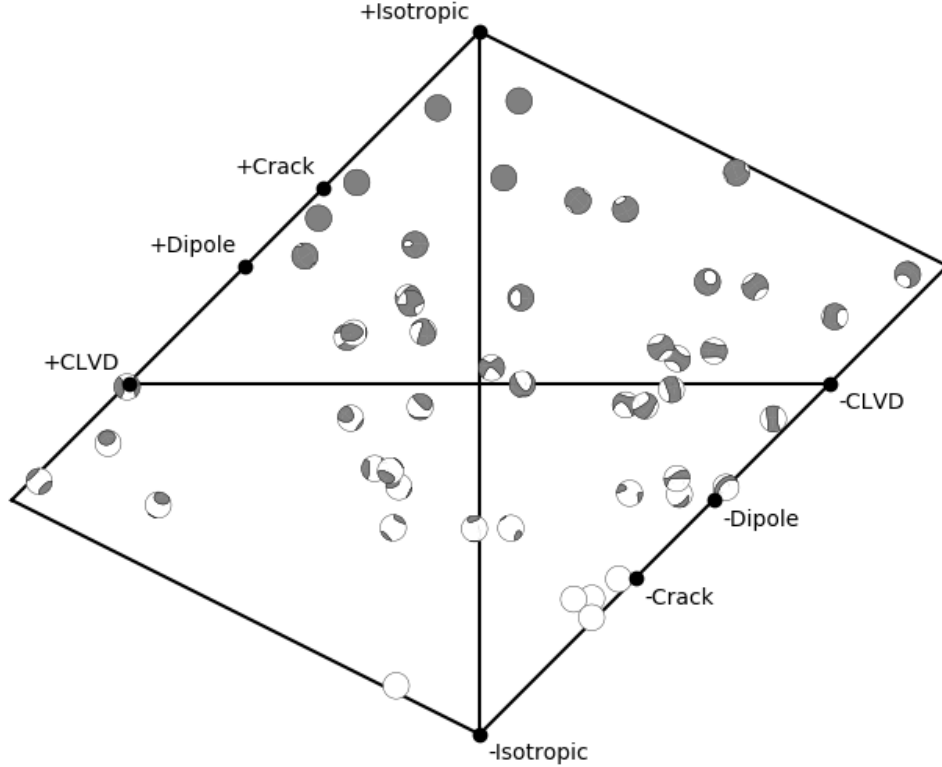


Figure 5: Source-type plot according to Hudson et al. (1989). Pure DC sources are plotted in the center spot. As an example, 50 random moment tensors are shown.

## 337 2.2 Introduction to rotational ground motion

### 338 2.2.1 Fundamental theory

339 The complete seismic wavefield due to a seismic source is fully described by six compon-  
 340 ents (6C), three components of translational and three components of rotational ground  
 341 motion; plus six components of strain when considering entire ground deformation. Rota-  
 342 tional ground motions  $\boldsymbol{\omega}$  are related to the curl of the deformation field and can be obtained  
 343 through spatial derivatives of the translational wavefield  $\mathbf{u}$ :

$$\boldsymbol{\omega} = \frac{1}{2} \nabla \times \mathbf{u} = \frac{1}{2} \begin{pmatrix} u_{z,y} - u_{y,z} \\ u_{x,z} - u_{z,x} \\ u_{y,x} - u_{x,y} \end{pmatrix}, \quad (16)$$

344 where  $u_{i,j}$  denote the spatial derivative along the three space axes  $j$ . It is a vector which  
 345 represents the angle of rigid rotation of the medium caused by a small deformation.

346 When we measure ground motion at the Earth surface, we have to consider that normal and  
 347 shear traction vanish. This leads to a simplification of the equation where only horizontal

348 spatial derivatives remain (Robertsson and Curtis, 2002; Cochard et al., 2006):

$$\omega^{FS} = \begin{pmatrix} u_{z,y} \\ -u_{z,x} \\ \frac{1}{2}(u_{y,x} - u_{x,y}) \end{pmatrix}. \quad (17)$$

349 In Eq. 17 the horizontal components are defined by spatial derivatives of the vertical trans-  
350 lation. They are known as tilt or rocking and provide us with information on the spatial  
351 wavefield gradient of the vertical displacement with depth. This information is not available  
352 from translational point measurements at the surface. It would need large receiver arrays  
353 and data processing to access this information. The vertical component of rotational ground  
354 motion is defined by spatial derivatives of the horizontal translations and represents torsion.  
355 These relations are important to understand where the additional information with depth is  
356 coming from, mentioned later in the text several times.

357 In the linearised, time-domain inversion scheme for moment tensors (Eqs. 3 and 6) the  
358 ground motion components are linear combinations of the moment tensor components with  
359 the matrix of spatial derivatives of GFs. Therefore, it is straight forward to include rota-  
360 tional ground motion into the waveform inversion for seismic moment tensors. With the  
361 appropriate, pre-calculated GFs simply similar linear combinations need to be set-up. The

362 long version of the inversion equation based on Eq. 6 then looks like:

$$\underbrace{\begin{pmatrix} u_1^{rec1} \\ u_2^{rec1} \\ \dots \\ u_k^{rec1} \\ u_1^{rec2} \\ u_2^{rec2} \\ \dots \\ u_k^{rec2} \\ [\dots] \\ \omega_1^{rec1} \\ \omega_2^{rec1} \\ \dots \\ \omega_k^{rec1} \\ \omega_1^{recN} \\ \omega_2^{recN} \\ \dots \\ \omega_k^{recN} \end{pmatrix}}_{N \cdot k} = \underbrace{\begin{pmatrix} G_{11}^{u_{rec1}} & G_{12}^{u_{rec1}} & G_{13}^{u_{rec1}} & G_{14}^{u_{rec1}} & G_{15}^{u_{rec1}} & G_{16}^{u_{rec1}} \\ G_{21}^{u_{rec1}} & G_{22}^{u_{rec1}} & G_{23}^{u_{rec1}} & G_{24}^{u_{rec1}} & G_{25}^{u_{rec1}} & G_{26}^{u_{rec1}} \\ \vdots & \vdots & \vdots & \vdots & \vdots & \vdots \\ G_{k1}^{u_{rec1}} & G_{k2}^{u_{rec1}} & G_{k3}^{u_{rec1}} & G_{k4}^{u_{rec1}} & G_{k5}^{u_{rec1}} & G_{k6}^{u_{rec1}} \\ G_{11}^{u_{rec2}} & G_{12}^{u_{rec2}} & G_{13}^{u_{rec2}} & G_{14}^{u_{rec2}} & G_{15}^{u_{rec2}} & G_{16}^{u_{rec2}} \\ G_{21}^{u_{rec2}} & G_{22}^{u_{rec2}} & G_{23}^{u_{rec2}} & G_{24}^{u_{rec2}} & G_{25}^{u_{rec2}} & G_{26}^{u_{rec2}} \\ \vdots & \vdots & \vdots & \vdots & \vdots & \vdots \\ G_{k1}^{u_{rec2}} & G_{k2}^{u_{rec2}} & G_{k3}^{u_{rec2}} & G_{k4}^{u_{rec2}} & G_{k5}^{u_{rec2}} & G_{k6}^{u_{rec2}} \\ [\vdots & \dots & \vdots] \\ G_{11}^{\omega_{rec1}} & G_{12}^{\omega_{rec1}} & G_{13}^{\omega_{rec1}} & G_{14}^{\omega_{rec1}} & G_{15}^{\omega_{rec1}} & G_{16}^{\omega_{rec1}} \\ G_{21}^{\omega_{rec1}} & G_{22}^{\omega_{rec1}} & G_{23}^{\omega_{rec1}} & G_{24}^{\omega_{rec1}} & G_{25}^{\omega_{rec1}} & G_{26}^{\omega_{rec1}} \\ \vdots & \vdots & \vdots & \vdots & \vdots & \vdots \\ G_{k1}^{\omega_{rec1}} & G_{k2}^{\omega_{rec1}} & G_{k3}^{\omega_{rec1}} & G_{k4}^{\omega_{rec1}} & G_{k5}^{\omega_{rec1}} & G_{k6}^{\omega_{rec1}} \\ G_{11}^{\omega_{recN}} & G_{12}^{\omega_{recN}} & G_{13}^{\omega_{recN}} & G_{14}^{\omega_{recN}} & G_{15}^{\omega_{recN}} & G_{16}^{\omega_{recN}} \\ G_{21}^{\omega_{recN}} & G_{22}^{\omega_{recN}} & G_{23}^{\omega_{recN}} & G_{24}^{\omega_{recN}} & G_{25}^{\omega_{recN}} & G_{26}^{\omega_{recN}} \\ \vdots & \vdots & \vdots & \vdots & \vdots & \vdots \\ G_{k1}^{\omega_{recN}} & G_{k2}^{\omega_{recN}} & G_{k3}^{\omega_{recN}} & G_{k4}^{\omega_{recN}} & G_{k5}^{\omega_{recN}} & G_{k6}^{\omega_{recN}} \end{pmatrix}}_{N \cdot k \cdot 6} \begin{pmatrix} M_1 \\ M_2 \\ M_3 \\ M_4 \\ M_5 \\ M_6 \end{pmatrix} \quad (18)$$

363 with  $N$  and  $k$  being the number of total recordings (translation plus rotation) and samples  
 364 per recording, respectively. In Eq. 18 [...] on the LHS and  $[\vdots \quad \dots \quad \vdots]$  on the RHS stand for  
 365 possible further entries. They are not shown to keep the equation as compact as possible.  
 366 Ichinose et al. (2021) also have demonstrated this fact based on the analytical expressions for  
 367 the translational and rotational ground motion components based on four fundamental source  
 368 types and corresponding coefficients defined on the source-receiver azimuth and moment  
 369 tensor components. The fundamental source types are vertical strike-slip, vertical dip-slip,  
 370 45° dip-slip, and explosion.

### 371 2.2.2 Measuring rotational ground motions

372 Although the benefits of measuring "inclination" have been mentioned quite early (Schlüter,  
 373 1903), seismology for a long time was limited to the translational part of the wavefield, with  
 374 no access to the other part of the available information. Even in 2002 Aki and Richards  
 375 stated: "... note the utility of measuring rotation ..., but as of this writing seismology still  
 376 awaits a suitable instrument for making such measurements." This is reasoned by the very  
 377 small amplitudes of rotational ground motions. Compared with translational ground motions

378 they are smaller by roughly a factor of 1000, depending on the local phase velocity. Thus,  
379 for quite a while appropriate measurement facilities were missing.

380 A short summary about early attempts of observational rotational seismology can be found  
381 in Lee et al. (2011). Some of the first direct measurements have been done with highly  
382 sensitive ringlasers gyroscopes, an instrument originally developed for geodesy to monitor  
383 Earth's rotation (McLeod et al., 1998; Pancha et al., 2000; Igel et al., 2005; Schreiber et al.,  
384 2009). It is an interferometer, the measurement principle based on the Sagnac effect (Lefèvre,  
385 2014). However, ringlasers are massive structures at fixed locations which need a huge effort  
386 in absolutely rigid construction to provide stable measurements. That makes them very  
387 expensive and limits the number of available measurements. Up to today only five ringlasers  
388 exist worldwide of which four measure the vertical component of rotation only.

389 As early as the 1990s attempts have been made to measure rotational ground motion with  
390 portable sensors (Nigbor, 1994; Takeo, 1998). Since then, several portable sensors based  
391 on very different measure principles were developed. They include the principle of torsion  
392 balance (Cowsik et al., 2009), the pairwise combination of geophones (Brokešová et al.,  
393 2012; Brokešová and Málek, 2013), liquid-based rotational motion sensors (Jedlička et al.,  
394 2012; Huang et al., 2013), magnetohydrodynamic sensors (Pierson et al., 2016), and micro-  
395 electromechanical systems (MEMS)-based gyroscopes (Nigbor, 1994). Partly, these sensors  
396 were successfully used for strong motion studies (Lee et al., 2009; Nigbor et al., 2009).  
397 However, for a broad application in seismology, a higher sensitivity in a wider bandwidth  
398 is needed. A promising development with respect to that point was the usage of fibre-  
399 optic gyroscopes (Jaroszewicz et al., 2006; Velikoseltsev et al., 2012; Bernauer et al., 2021).  
400 Bernauer et al. (2018) showed that we now have the first portable rotation sensor developed  
401 for seismology which is commercially available.

402 According to Eqs. 16 and 17 we can derive rotational ground motions from translational  
403 surface array measurements (array-derived-rotation - ADR). The seismogeodetic method  
404 is one way to do so (Spudich et al., 1995; Bodin et al., 1997; Huang, 2003; Spudich and  
405 Fletcher, 2008, 2009). Here, the best-fitting spatially uniform strain and rigid body rotation  
406 is determined to fit the instantaneous deformation of an array of seismic recorders and, thus,  
407 provides a spatial average of rotational ground motions over the area of the surface array. P-  
408 and S-wave velocities beneath the array must be known and the method assumes that the  
409 deformation is linear over the array area. Therefore, the validity of the resulting rotational  
410 ground motion is limited to lower frequencies, depending on the spatial extend of the array.  
411 Suryanto et al. (2006) also stated, that although the method needs measurements of only  
412 three stations, the accuracy of the derived rotation is considerably influenced by noise within  
413 the translational data. However, the more recordings are used to derive rotational ground  
414 motions, the better this influence is cancelled out. Other factors influencing the accuracy

415 of derived rotational ground motions are topography, structural heterogeneities, receiver  
416 location uncertainties, uncertainties in the seismometer response function, strain-rotation-  
417 coupling, and inaccuracies in the plane wave assumption. Nevertheless, comparisons between  
418 ADR and direct measurements showed excellent fit between both with correlation coefficients  
419 up to 98% (Suryanto et al., 2006; Wassermann et al., 2009; Lin et al., 2012; Donner et al.,  
420 2017). Therefore, it should be possible to use them as an addendum to direct measurements  
421 for waveform inversion. The method of Spudich and Fletcher (2008) is implemented in the  
422 Python-based seismological analysis toolbox ObsPy (Beyreuther et al., 2010; Megies et al.,  
423 2011; Krischer et al., 2015).

424 Langston (2007a,b,c, 2018) developed a very similar method complemented by a weighting  
425 scheme and coined the term '*wave gradiometry*' for it. Instead on the resulting array-  
426 derived rotation and strain, he rather focuses on determining the wavefield gradient with  
427 high precision (Liang and Langston, 2009).

### 428 **2.2.3 Rotations due to a double-couple point source**

429 Applying the same notation as for Eq. 9 and given in Fig. 3 for the translational rotation  
430 pattern, we can find a likewise expression for the rotational radiation pattern (Cochard et  
431 al., 2006; Igel et al., 2015):

$$\mathbf{A}^R = \cos \theta \sin \phi \hat{\boldsymbol{\theta}} + \cos \phi \cos 2\theta \hat{\boldsymbol{\phi}} \quad (19)$$

432 Another way to obtain the rotational radiation pattern is to calculate the curl of the trans-  
433 verse far-field radiation pattern (Eq. 9, Cochard et al., 2006). That is  $\nabla \times \mathbf{A}^{FS} = \mathbf{A}^R/r$ .  
434 Hence, it becomes clear, that these two radiation patterns are orthogonal to each other (see  
435 also Sec. 3.2).

### 436 **2.2.4 Strain-rotation coupling and local side effects**

437 Similarly to translational ground motions, direct measurements of rotational ground motions  
438 are biased due to local side effects. Small-scale heterogeneities and rough topography, for  
439 example, can cause a conversion of strain into rotation (strain-rotation-coupling or strain-  
440 induced rotation, King and Bilham, 1973; Harrison, 1976; Kohl and Levine, 1995; van Driel  
441 et al., 2012, 2015). This effect can significantly contribute to the measurement of rotational  
442 ground motion on all distances and in the low-frequency spectrum (van Driel et al., 2012).  
443 The same authors also found a dependence on the relative magnitude of strain and rotation.  
444 In turn, the relative magnitude of strain and rotation is influenced by the radiation pattern,  
445 source-receiver-distance, or seismic phases.

446 The effects of local side conditions, that means small scale heterogeneities of the structure,

447 on rotational ground motion is more significant than for translational data. For example,  
448 Fichtner and Igel (2009) and Bernauer et al. (2012) could show that the finite-frequency  
449 sensitivity kernels of rotational ground motion are influenced only by structure in close  
450 vicinity of the receiver but not along the path or in the vicinity of the source. Thus, they  
451 could be used for single receiver local tomography.

452 These findings have important implications when working with direct measurements of rota-  
453 tional ground motion. Under specific circumstances the data are usable only when they are  
454 corrected for local side effects, especially strain-rotation-coupling. (Singh et al., 2020) in-  
455 vestigated the coupling in more detail using the theory of homogenisation (Capdeville et al.,  
456 2020). They introduced the coupling vector  $\mathbf{J}$  which is a characteristic of the receiver loca-  
457 tion and not dependent on source or time. Therefore, it is possible to invert for the coupling  
458 vector  $\mathbf{J}$  and subsequently use it to correct the measured data of a specific receiver location.

### 459 **3 Benefits of rotational ground motions for regional** 460 **seismic moment tensors**

461 When including recordings of rotational ground motions into the waveform inversion for  
462 seismic moment tensors, we extend the number of observations of the seismic wavefield.  
463 Intuitively, we understand this addition in information alone should improve the resulting  
464 moment tensor solution. Because portable rotational sensors are quite new instruments, so  
465 far, there are no studies based on real, direct measurements of rotational ground motion.  
466 The studies summarised in this review worked with either synthetic waveforms or with ADR  
467 measurements.

468 This section is structured as follows: At first, some general benefits are presented (section 3.1)  
469 before the influences of receiver number and geometry are explained (section 3.2). Section  
470 3.3 discusses the influence of structural model and its relation to inverted frequencies as well  
471 as the relation between frequencies, magnitudes, distance ranges and used waveform types.  
472 Section 3.4 focuses on the resolvability of centroid depth. A discussion on the resolvability  
473 of different source parts can be found in section 3.5 before findings on the influence of noise  
474 are presented in section 3.6.

475 In the following, the term '*resolution*' is used to describe the quality, or reliability, of the  
476 resulting moment tensor from waveform inversion. In this review, the term refers to both,  
477 the accuracy and the precision with which the moment tensor components are determined.

### 3.1 General benefits for the resolution of the moment tensor components

Donner et al. (2016) investigated the waveform inversion results from six component (6C, translation+rotation) synthetic waveforms in a scenario based on a 1-dimensional (1D) structural model of northern Iran. The synthetic waveforms are calculated based on a synthetic shallow strike-slip source in 6 km depth with a moment magnitude of  $M_w$  4.0 and with 80% DC. The seismograms were calculated up to 0.1 Hz with a minimum wavelength of 27 km. Therefore, the dominant wave type are surface waves as it is standard in regional waveform inversion for moment tensors. For the receiver locations the authors chose two scenarios: one based on the real distribution of broadband stations of the Iranian National Seismic Network (INSN) operated by the Institute of Earthquake Engineering and Seismology, and a second scenario based on a regular grid of virtual receivers covering almost entire Iran (Fig. 6). To obtain an unbiased solution selection and also consider possible trade-offs the authors performed a Bayesian (probabilistic) inversion based on equations from Tarantola (2005). A *prior probability density function* ( $\rho(\mathbf{m})$ , *prior pdf*) on the parameter space  $\mathbf{m}$  (moment tensor components and centroid depth) is connected with a Likelihood function to obtain the *posterior probability density function* ( $\sigma(\mathbf{m})$ , *posterior pdf*). The likelihood function provides a measure of how well a model is fitting the data and is basically defined as the L2 norm between the synthetic and theoretical observations. The parameter space is randomly sampled using the Metropolis-Hastings algorithm testing one million start solutions (Metropolis and Ulam, 1949; Metropolis et al., 1953; Hastings, 1970). The *posterior pdf* is quantified relative to the *prior pdf* using Shannon’s measure of information gain (IG, Shannon, 1948):

$$IG(\rho, \sigma) = \int \rho(x) \log \left[ \frac{\rho(x)}{\sigma(x)} \right] dx. \quad (20)$$

The unit of the information gain is termed a *bit* due to the logarithm base 2. In their first scenario, Donner et al. (2016) compared the three component (3C) versus six component (6C) inversion results based on two rings of virtual recorders distributed around the source. To keep the amount of data constant during inversion, they halved the number of recorders when including the rotational data to the inversion (black dots with white crosses in Fig. 6a). Hence, the improvement of the result does not come from purely increasing the amount of data but actually from adding new information. In this case, the IG increased by 53% ( $(IG_{6C} - IG_{3C}) / IG_{3C} \times 100\%$ ). Especially, components including spatial derivatives with respect to depth are significantly better resolved. For component  $M_{zz}$  the IG increased by 161%. The same comparison based on the real station distribution (second scenario of this study) confirmed the findings with an overall increase of IG of 136%. That means,



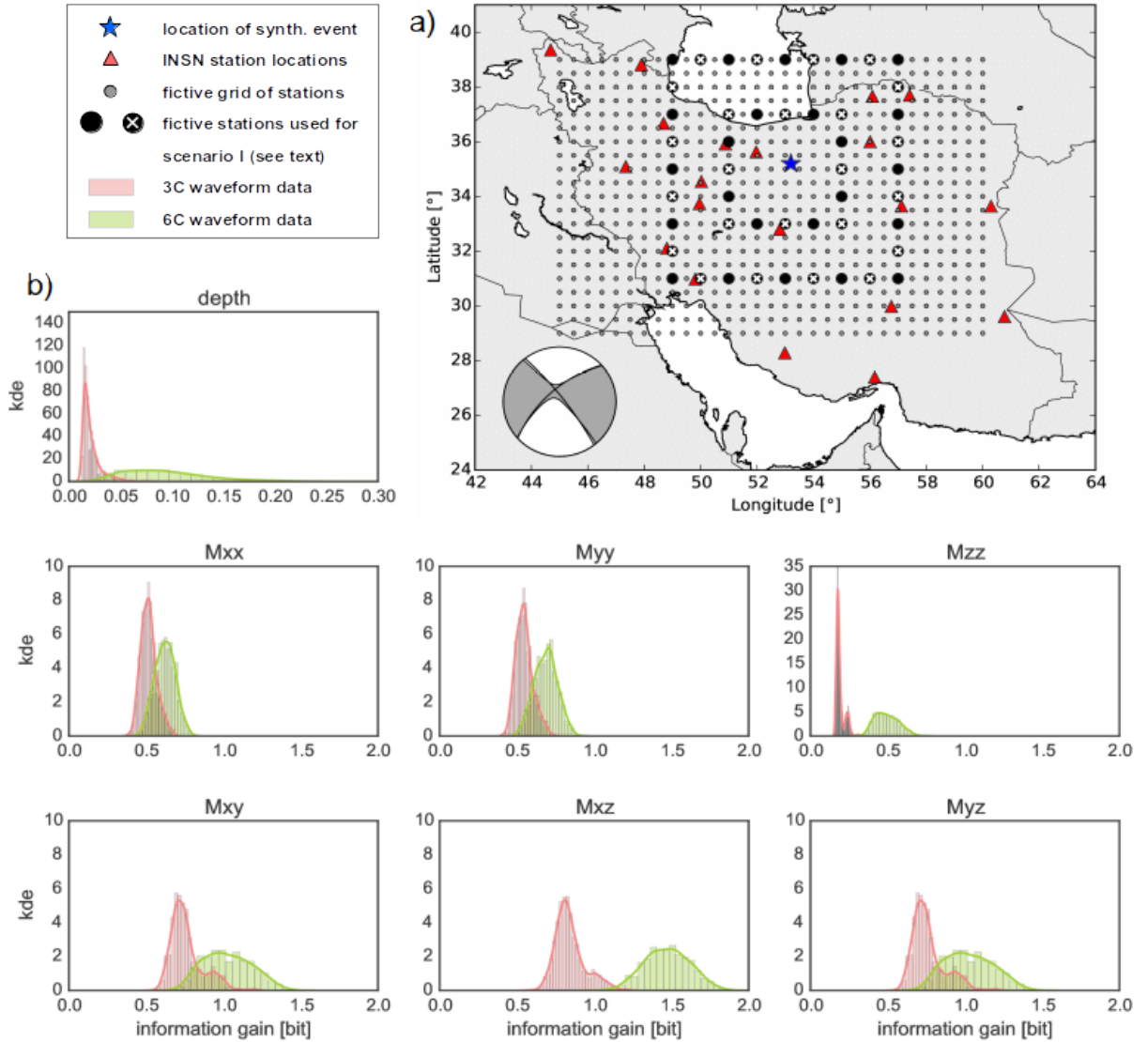


Figure 6: Summarised study results of Donner et al. (2016, 2018). a) Overview map for the study area. Blue star shows the location of a synthetic source with its mechanism given by the beachball (grey: full moment tensor; black: DC part). Red triangles mark the real station locations of the Iranian National Seismic Network (INSN) while dots represent a virtual grid of receivers. Black and white-crossed dots (6C and 3C receivers, respectively) are the receivers used in their scenario one. b) Gaussian kernel density estimations for the IG corresponding to 1000 runs based on the virtual grid of receivers. Coral and green distributions show the IGs from inverting 3C and 6C waveform data from randomly chosen receivers for the given parameters, respectively. The higher the IG, the more the inverted parameter benefits from using rotational motions. Same IG means same inversion resolution using half the number of receivers but the same amount of data. (Modified after Figs. 1 and 3 of Donner et al. (2016).)

512 with half the number of receivers the resulting moment tensor is better resolved using 6C  
513 compared with only 3C waveform data. Most probably, the benefits come from the horizontal  
514 components of the rotation (tilt) holding information on the vertical displacement gradient  
515 (see also section 2.2.1).

516 This assumption could be confirmed by a study on the kinematic source solution of a buried  
517 fault (Reinwald et al, 2016). Here, the authors applied the same Bayesian inversion scheme  
518 inverting for slip on the rupture plane, rupture velocity and rise time. They compared the  
519 inversion results for a strike-slip and a dip-slip source with exactly the same synthetic set-  
520 up and source-receiver-geometry for both synthetic sources. For the strike-slip source the  
521 increase in IG due to adding rotational recordings to the inversion was in total 10% while  
522 for the dip-slip source the increase in IG was 32%. Especially, the resolution of the rupture  
523 velocity, rise time, and the slip closest to the Earth surface benefited significantly from the  
524 rotational ground motions. In addition, already Bernauer et al. (2014) could show that the  
525 well-known trade-off between rupture velocity and rise time can be reduced substantially.  
526 Applying the same inversion scheme, the authors tested a synthetic strike-slip source only.  
527 They showed the 2D marginal *posterior pdf* of rupture velocity and rise time for the 3C and  
528 6C scenario. The area where variations in both parameters compensate each other is about  
529 twice as large for the 3C case than for the 6C case. Also, in the 3C case the expected values  
530 from the *posterior pdf* missed the target value considerably, the inaccuracy being larger for  
531 the rise-time than for the rupture velocity. For the 6C case, the increase in IG for rupture  
532 velocity and rise time was 25% and 60%, respectively.

533 A study with real, ADR-based measurements was performed by Ichinose et al. (2021). They  
534 used translational measurements from the Piñon Flat Observatory Array and the Golay Ar-  
535 ray in the US to derive rotational ground motion (see Sec. 2.2.2). The authors performed a  
536 waveform inversion for the full moment tensor (long period, time-domain, and linear inver-  
537 sion) and a Network Sensitivity Solution (NSS) analysis (Ford et al., 2010) to investigate the  
538 resolution of the resulting moment tensors. In addition, they intentionally reduced the num-  
539 ber of measurements for inversion to three receivers because they argue that adding more  
540 data to an already large dataset would not necessarily improve the solution (without apply-  
541 ing weighting schemes). Ichinose et al. (2021) found similar improvement for the moment  
542 tensor resolution as Donner et al. (2016, 2017) which manifest in a reduction of the non-DC  
543 components (as discussed in Sec. 3.5) and a decrease of the area of certain percentage of  
544 variance reduction level in the NSS analysis.

545 Most generally, we know that some moment tensor components are very difficult to resolve  
546 from translational ground motion in the regional distance range. Some specific source char-  
547 acteristic cannot be determined from Love or Rayleigh surface waves alone (for a discussion  
548 on body versus surface waves see section 3.3). For example, the component  $M_{zz}$  can only

549 be determined in combination with  $M_{xx}$  and  $M_{yy}$  from Rayleigh waves alone, affecting the  
550 resolution of the ISO source part (Julian et al., 1998). Furthermore, because for shallow  
551 sources some moment tensor components ( $M_{xz}$ ,  $M_{yz}$ ) do not contribute to the surface wave  
552 radiation pattern due to the free surface condition (Bukchin, 2006; Bukchin et al., 2010).  
553 Yet, due to their dependence on the vertical displacement gradient, these components are  
554 also the ones benefiting most from including rotational ground motion into the waveform  
555 inversion.

## 556 **3.2 Influence of the receiver distribution**

557 Fig. 6b summarises the generalised inversion results based on the virtual grid of receivers  
558 from Donner et al. (2016). They repeated the Bayesian inversion a 1000 times randomly  
559 selecting receivers out of the regular grid to further investigate the effect of the receiver  
560 distribution. Fig. 6b shows the Gaussian kernel density estimation (*kde*) over the IG from  
561 these 1000 inversions with one million start solutions each for the seven parameters inverted  
562 for. That means, the further the distribution stretches to the right side of the panels, the  
563 better is the parameter resolved. The coral and green distributions correspond to inversion  
564 results of 3C and 6C waveform data, respectively. Again, for the 6C case only half the  
565 number of receivers but the same amount of data was inverted. For the moment tensor  
566 components  $M_{zz}$  and  $M_{xz}$  it shows, no matter how the receivers are distributed around the  
567 source, the parameters are always better resolved when including rotations into the inversion.  
568 For the other moment tensor components it depends on the receiver distribution whether  
569 the component is equally well or better resolved. In Fig. 6b, these two cases correspond to  
570 both distributions partially overlapping or the 6C distribution being shifted to the right to  
571 higher IG, respectively.

572 Theoretically, it should be possible to determine the full seismic moment tensor from a single  
573 3C recording when all seismic wave types are recorded because in the time domain it is an  
574 overdetermined inversion problem (see Eqs. 3 and 6). Ekström et al. (1986) has shown it  
575 for the teleseismic distance range. However, in practise the attempt is rarely successful in  
576 the regional distance range, mainly due to more complex waveforms and, hence, a higher  
577 necessity for detailed structural models compared with the teleseismic distance range (see  
578 also section 3.3). Therefore, often only a constrained moment tensor or even just the DC part  
579 can be obtained from a single 3C recording. Donner et al. (2018) have analysed this issue  
580 including rotational ground motions using the same inversion scheme and set-up as in their  
581 2016 study (see Fig. 6). They investigated the outcome from one, two, and three receiver  
582 locations. They conclude that the probability to retrieve a reliable full moment tensor  
583 solution from the 6C recordings of only two or three receivers is very high. The increase in  
584 IG compared with inverting 3C recordings only was 178% and 181%, respectively. However,

585 from only one 6C recording alone the *full* moment tensor is probably still not retrievable in  
586 many cases. The possibility to resolve a constrained moment tensor, for example the DEV  
587 moment tensor or only DC part, was not tested but the authors argue that it might be  
588 possible. The IG from inverting a single 6C recording for the full moment tensor increases  
589 by 105% compared with inverting a single 3C recording.

590 In their study based on ADR data, Ichinose et al. (2021) inverted data of three receivers, of  
591 which only one is a 6C receiver, for the full moment tensor. The authors demonstrated a  
592 significant increases in the DC part of the source mechanisms compared to inverting trans-  
593 lational recordings alone.

594 In the study of Donner et al. (2018), a second reason for the improved resolution of the mo-  
595 ment tensor due to including rotations into the inversion could be identified. Fig. 7 shows  
596 the radiation pattern for the theoretical earthquake source used in the mentioned studies,  
597 that means the normalised maximum energy for each receiver of the virtual grid. It is cal-  
598 culated as the square root of the sum of the squared amplitudes divided by the maximum  
599 amplitude of the trace:  $E = \sqrt{\sum tr_i^2 / A_{max}(tr)}$ . It is clearly visible that an optimum choice  
600 of receiver location within this radiation pattern provides strongly varying amplitude ratios,  
601 constraining the waveform inversion for the seismic moment tensor effectively. From the  
602 three components of translational ground motion alone only three amplitude ratios are pos-  
603 sible. When including the rotational ground motion this number increases to 15 amplitude  
604 ratios providing significantly more constraint for the inversion (enumerative combinatorics:  
605 two out of six without multiple selection and without considering order). Of course, we  
606 can perform this analysis only after the earthquake occurred and then it is hardly possible  
607 anymore to decide for the perfect receiver location for this specific earthquake. However,  
608 seismological observatories usually have a good overview of their monitored region and know  
609 where to expect seismic activity and what general kind of earthquake mechanisms, at least  
610 approximately. In addition, in some settings we know quite well which kind of seismicity  
611 to expect at which location, for example, when monitoring geothermal facilities, mining,  
612 or volcanic areas. Hence, for some cases it is possible to roughly determine which receiver  
613 location would be more optimal than others in advance.

614 This argumentation was also demonstrated by Ichinose et al. (2021) using a finite difference  
615 simulation of the curl and displacement wavefields for regional distance receivers and arguing  
616 on the orthogonality of the rotational and far-field SH radiation patterns (see Sec. 2.2.3  
617 and Cochard et al., 2006). They summarised the relation as follows: *'One 6-C sensor*  
618 *gathers the same information on long-period radiation pattern as two 3-C at 90° azimuth*  
619 *from one another on the focal plane'*. Fig. 8 demonstrates the effect with synthetic, noise-free  
620 waveforms of a dip-slip event (strike=45°, dip=50°, and rake=-70°) in a depth of 6 km based  
621 on a local 1D structural model. The theoretical receivers are located in the same distance

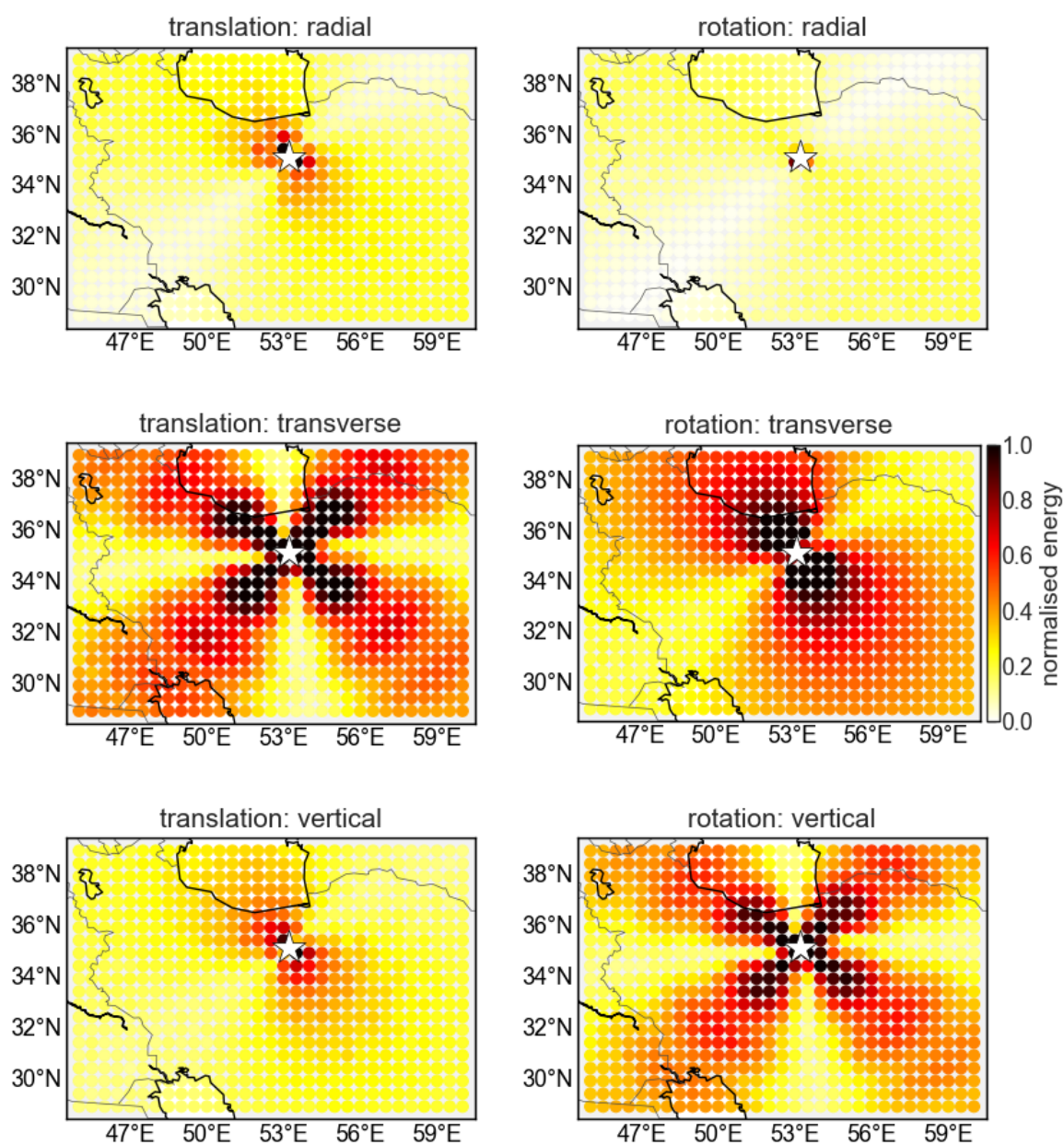


Figure 7: Radiation pattern for the synthetic earthquake scenario in Fig. 6. Upper and lower row show the normalised energy amplitudes for translation and rotation while from left to right the radial, transverse and vertical components are shown, respectively. White star marks the epicenter of the theoretical source. Modified after Fig. 8 of Donner et al. (2018).

622 with varying azimuths in steps of  $30^\circ$  around the source. The waveforms are normalised to one  
 623 over all components, evaluating translations and rotations separately because of their large  
 624 amplitude difference. The dominant wave is the S-wave, the P-wave is only lightly visible  
 625 on the vertical translation data. The increase/decrease of the amplitudes with increasing  
 626 azimuth clearly show the difference in azimuth for the maximum amplitudes between both  
 627 types of waveform data. This information leads to meaningful amplitude ratios which are  
 628 exploited during waveform inversion.

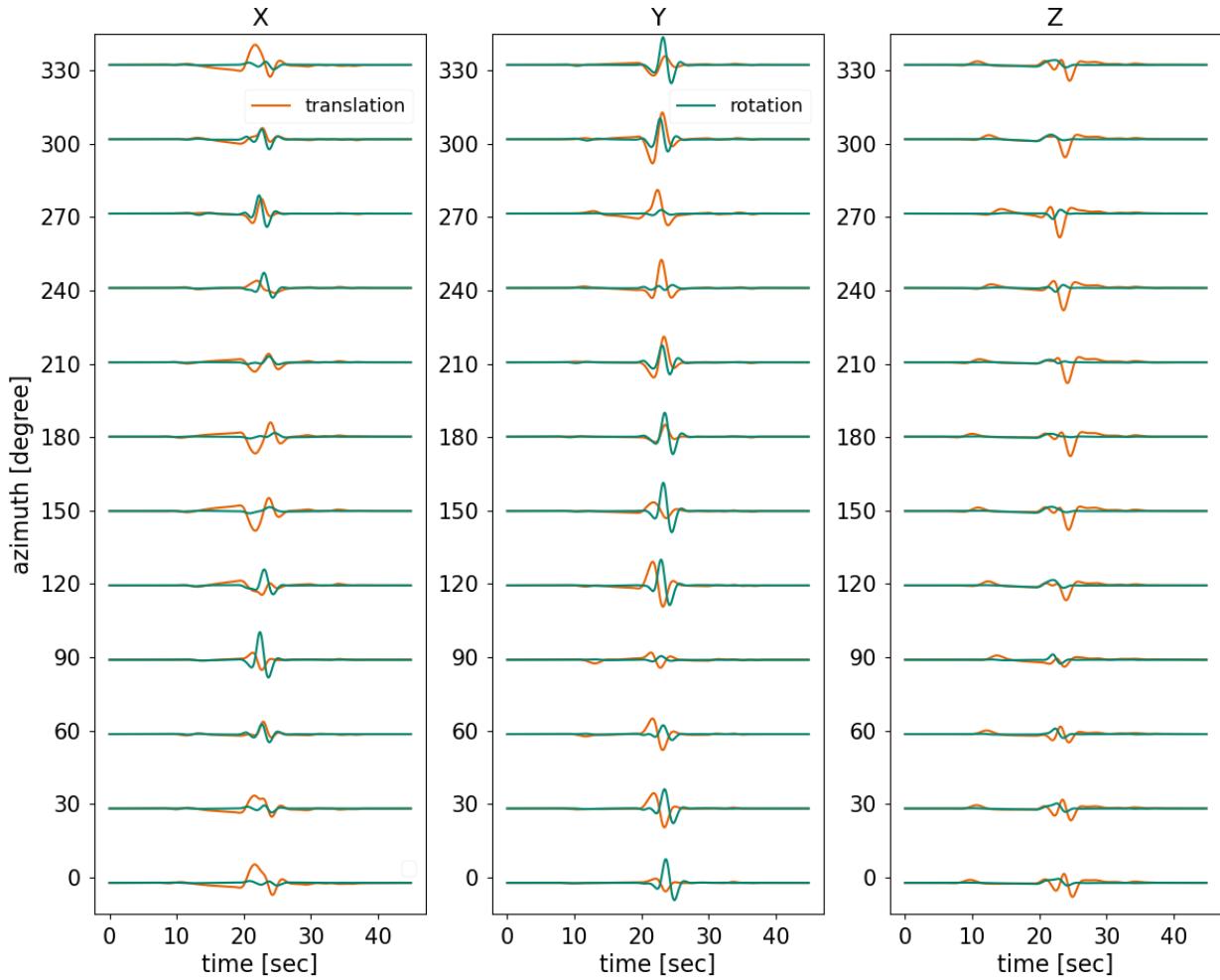


Figure 8: Synthetic waveforms for a dip-slip event (strike= $45^\circ$ , dip= $50^\circ$ , and rake= $-70^\circ$ ) with 6 km depth recorded at the same distance but with different azimuths in steps of  $30^\circ$ . Amplitudes are normalised to one, evaluating translations (orange) and rotations (turquoise) separately. The dominant amplitudes are the S-wave. The varying amplitudes over azimuth clearly show the orthogonality of the radiation pattern between translations and rotations.

### 629 3.3 Influence of frequency range and structural model

630 In the regional distance range, it is standard to invert the waveforms in a frequency range  
 631 appropriate to cover the surface waves, which is roughly between 0.01 and 0.1 Hz (10- 100 sec)  
 632 with a focus between 0.02 and 0.05 Hz (20- 50 sec). In this frequency range it is the surface  
 633 waves carrying most of the energy and, thus, yielding a lot of information into the inversion.  
 634 The choice of frequencies is also related to the magnitudes of the analysed events. The lower  
 635 the magnitude, the higher is the corner frequency of the event and the radiated frequency  
 636 content (Fig. 9). In the regional distance range, we usually analyse earthquakes with a  
 637 magnitude roughly between Mw 4.0 and Mw 6.5. For these events, the frequency content of  
 638 the radiated surface waves is safely below the corner frequency of the events. Above the  
 639 corner frequency the simplifying assumption of a point source (see Sec. 2.1.1) and thus  
 640 the mathematical equation for the waveform inversion is no longer valid. Below and above  
 641 these approximate magnitude thresholds, we rather speak of local and teleseismic waveform  
 642 inversion, respectively. Though, the boundaries between these categories are not defined  
 643 precisely.

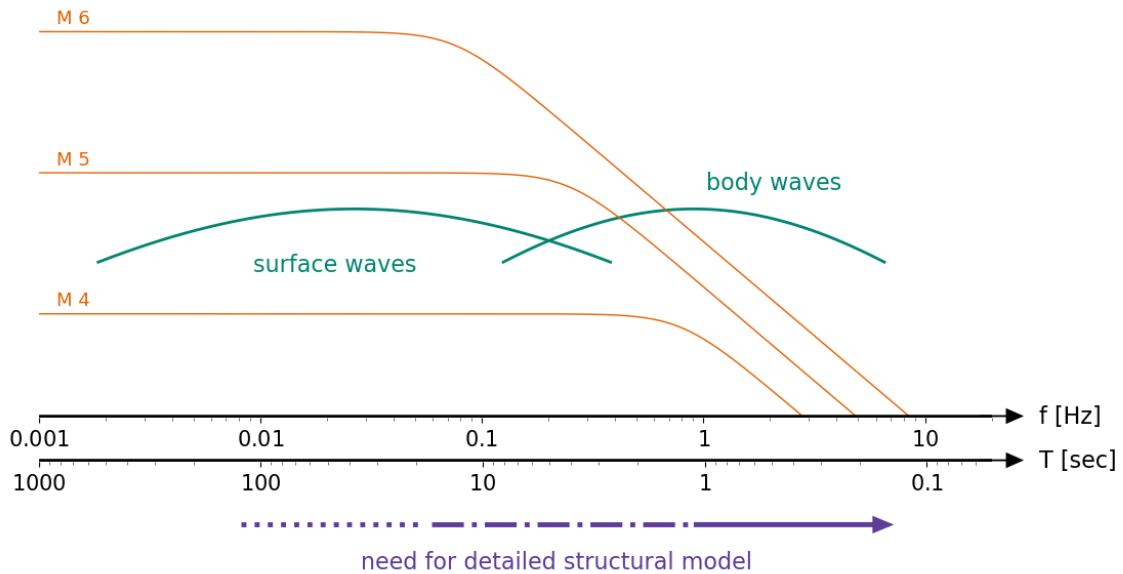


Figure 9: Schematic representation of the relationships between earthquake magnitude and corresponding corner frequency (orange), seismic wave type (turquoise), and structural model accuracy (purple) with respect to frequency and period range. The given values represent approximate guidelines and no exact limits.

644 The choice of frequencies is also connected to the accuracy of the structural model on which  
 645 the calculation of the GFs for the inversion is based. Low frequencies are related to rather  
 646 long wavelengths. In the case of surface waves the wavelength is several tens of kilometres as

647 a minimum. As a consequence, the seismic wave is 'blind' for smaller details of the underlying  
648 structure. Very often, a 1D structural model, where seismic properties vary only with depth  
649 but not laterally, is sufficient to reliably invert for seismic moment tensors in the regional  
650 distance range. According to Šílený (2004) for the inversion in the frequency range 0.02-  
651 0.05 Hz an uncertainty of the crustal structure up to 30% is harmless before it starts to bias  
652 the inversion result for the event-receiver geometry he tested. Also Vasyura-Bathke et al.  
653 (2021) concluded that uncertainties in the structural model can affect the moment tensor  
654 resolution profoundly. Especially, the resulting decomposition suffered from structural model  
655 errors.

656 For a lot of regions such 1D structural models meanwhile exist, for example, from local  
657 earthquake tomography (e. g. Eberhart-Phillips, 1990; Thurber, 1993; Haberland et al., 2009;  
658 Mousavi et al., 2015). However, seismic waveforms are influenced the most from the upper  
659 crust, which is the most complex part of the Earth's structure and includes strong lateral  
660 heterogeneities on all spatial scales. A structural model perfectly describing arrival times of  
661 seismic body wave phases is not necessarily sufficient for surface wave waveform inversion  
662 but in the best case can be adapted (e. g. Donner et al., 2013).

663 Since a couple of years, the progress in computational and storage resources allowed to  
664 investigate the usage of 3-dimensional (3D) structural models for various studies, including  
665 regional waveform inversion for moment tensors (e. g. Hingee et al., 2011; Zhou et al., 2016;  
666 Hejrani et al., 2017). Several authors have shown that the usage of 3D structural models can  
667 be strongly beneficial for the reliability of the inversion result, that means the seismic moment  
668 tensor (e. g. Fichtner and Tkalčić, 2010; Kim et al., 2011; Covellone and Savage, 2012; Kühn  
669 and Vavryčuk, 2013; Hejrani and Tkalčić, 2020). It allows to extend the waveform inversion  
670 to higher frequency ranges, but still below the corner frequency, because the chances to  
671 decipher the more complex waveforms due to more detailed structure increase. This instance  
672 shifts the focus from surface waves to include body wave energy adding physical information  
673 to the inversion and, thus, can improve the resolution of the resulting moment tensor. It also  
674 allows to lower the magnitude threshold for which waveform inversion for seismic moment  
675 tensors are possible because smaller events have a higher corner frequency.

676 Fig. 9 suggests that the radiated energy of seismic events is constant and easy to use at  
677 the lower end of the frequencies but this is not entirely true. Real world observations show  
678 that the plateau of the displacement amplitude spectrum does not spread endlessly to lower  
679 frequencies but rises again below a certain frequency. This is due to the influence of noise  
680 superimposing the earthquake signal. Thus, it is difficult to resolve the moment tensor of  
681 small events from low frequencies and more detailed models are needed to fit the higher  
682 frequencies. Nevertheless, 3D structural models and GFs calculated on them need to be  
683 carefully validated against the true structure. If they do not represent the real conditions



684 properly, they rather harm the inversion result than improve it (e. g. Graves and Wald, 2001;  
685 Hjörleifsdóttir and Ekström, 2010).

686 These relationships have long been known from the inversion of translational ground motions.  
687 They are still just as valid when including the rotational ground motions into the waveform  
688 inversion. The question remains what factor improves the reliability of the resulting moment  
689 tensor more: inverting 6C waveforms or GFs based on 3D structural models? Donner et al.  
690 (2020) tried to answer this question, again based on the same Bayesian inversion scheme as  
691 before comparing 3C versus 6C waveform inversion. This time, the set-up is a scenario on the  
692 Korean Peninsula with synthetic waveforms based on a shallow strike-slip Mw 5.4 earthquake  
693 in the Republic of Korea (ROK) and based on an Mw 5.8 explosive source in the Democratic  
694 People’s Republic of Korea (DPRK). They calculated two sets of GFs based on a 1D and  
695 a 3D structural model and compared the inversion results for both sets in three different  
696 frequency ranges: 0.02 - 0.05 Hz (20 - 50 sec), 0.02 - 0.1 Hz (10 - 50 sec), and 0.02 - 0.16 Hz (6 -  
697 50 sec). Their main conclusion is that for both event scenarios the combination of 6C with  
698 3D improves the reliability of the result the most. This effect can even be increased when  
699 broadening the frequency range to higher frequencies.

700 However, they found differences for the two source types. For the explosive event the usage  
701 of a 3D model turned out to be superior than adding the rotational ground motion to the  
702 inversion, especially in the higher frequency range. This is explained by the type of radiated  
703 energy. Explosive sources radiate most of their energy as compressional (P-) wave energy  
704 and only very few shear-wave energy, i. e. S- and surface wave energy. They contain much  
705 higher frequencies than surface waves, which strengthens the preference for 3D instead of  
706 6C for explosive sources. In addition, compressional waves cannot excite rotations in a  
707 homogeneous medium and considering the far-field energy radiation. Though, Pham et al.  
708 (2010) showed with real data examples that we do see rotations in the P-wave train. It  
709 is assumed that scattering and P-to-S conversion due to anisotropy in the upper crust is  
710 responsible for the effect. As a consequence, the rotational ground motions indeed do add  
711 physical information to the waveform inversion of explosive sources but being able to model  
712 crustal details and invert higher frequencies is more relevant here.

713 Finally, as already mentioned in Sec. 2.2, the distortions of the recorded waveforms due  
714 to local site effects are more severe for rotational than for translational ground motions  
715 (though not negligible here as well). Most likely it will not be possible to invert real, direct  
716 recordings of rotational ground motion without carefully considering the coupling vector  $\mathbf{J}$ .  
717 The verification is pending.

### 3.4 Resolution of the centroid depth

For a long time, it is well known that the focus on surface wave frequencies in the regional distance range comes with a major drawback. The equations for the radiation patterns of Love and Rayleigh surface waves contain terms including spatial derivatives of the eigenfunctions with respect to depth. The terms in question affect the moment tensor components  $M_{xz}$  and  $M_{yz}$ . They are proportional to the shear traction on a horizontal plane. At the free surface, the shear traction vanishes. As a consequence, the connected moment tensor components are badly resolved for shallow sources (centroid depth  $\ll$  considered wavelength, Dufumier and Cara, 1995; Bukchin, 2006; Bukchin et al., 2010).

In their second scenario based on the real station distribution of the INSN (red triangles in Fig. 6a) Donner et al. (2016) found a bimodal distribution for the *kde* of the centroid depth for both inversions, based on 3C and 6C waveform data; one for a shallow depth of 4-8 km and one for a deeper depth of 16-20 km (target centroid depth: 6 km). The 3C *kde* distribution showed the highest peak at the deeper and wrong depth, while the 6C *kde* distribution resulted in the correct depth. Interestingly, Donner et al. (2013) and Donner et al. (2014) found a similar bimodal sensitivity for centroid depth when inverting real translational measurements for the moment tensor. So, the cause might be in the event-receiver geometry for the Iranian setting. Based on the two rings of virtual receivers around the source the inversion resulted in unimodal *kde* distributions. However, again from 3C waveform data the possibility to end up with a wrong centroid depth is high. Including rotational data increase the chances to determine a reliable centroid depth. Here, the increase in IG is 175%.

From the summarised results of the generalised inversion in Fig. 6a the panel for the centroid depth is of particular interest. It shows the well-known problem of resolving this parameter from the inversion of 3C waveform data alone. No matter how well the receivers are distributed around the source, the results always have a low IG. When adding rotations to the inversion, the *kde* distribution stretches over a wide range of IG. That means, the centroid depth is almost always more reliably resolved. Depending on the receiver distribution the gain in information can reach a multiple of the one from 3C data. The reader should note that these are results from a synthetic strike-slip source which includes mainly horizontal slip. For an event including vertical slip the benefit will probably be even better because of the information on the vertical displacement gradient adding valuable constraint on the inversion.

### 751 **3.5 Resolvability of the tectonic mechanism and DC/non-DC parts**

752 As explained in Sec. 2.1.3 the full seismic moment tensor contains information on several  
753 source components, only part of them having a tectonic origin. Depending on the goal of a  
754 scientific study, either the DC (tectonic) or the non-DC (ISO and CLVD) part of the moment  
755 tensor is the focus. From inverting recordings of translational ground motion alone it is  
756 sometimes not possible to resolve the full moment tensor. Scientists constrain the inversion,  
757 for example by setting the ISO part to zero or even invert only for the DC part. Other  
758 constraints are also possible. When the reliability of the full moment tensor solution can  
759 benefit from recordings of rotational ground motions then the different source components  
760 should as well.

761 Based on their 1000 inversions for the generalisation of their study based on the Iranian  
762 setting, Donner et al. (2016) have calculated the decomposition of these  $1e9$  moment tensor  
763 solutions ( $1e6$  start solutions for each inversion) and determined DC, ISO, and CLVD per-  
764 centages as well as strike, dip, and rake angles of the DC part. The overall distribution for  
765 the 3C and the 6C case were similar. In both cases the *kde* peak values for each parameter  
766 did not match the value of the target model. Though, for the 6C case, they found sub-peaks  
767 of the *kde* distribution at the target values for DC and ISO part as well as for the dip and  
768 rake angles.

769 The entire decomposition result depends on the reliable estimation of the ISO part (diagonal  
770 elements of the moment tensor) because this is the very first step in the chosen decomposition  
771 scheme (see Sec. 2.1.3). For the scenarios tested (based on a real station distribution and  
772 on a virtual grid of receivers), two of the three diagonal moment tensor components showed  
773 flaws in their reliability in the 3C and 6C case and, hence, the ISO part is flawed as well. The  
774 peak values of the *kde* distribution for the 3C and the 6C case are off by about 35-45%. As a  
775 result, all other decomposition parameters do not fit the target value neither. Nevertheless,  
776 the reliability of estimating the ISO part still could be improved. Comparing the IG values  
777 for the diagonal moment tensor elements from 3C versus 6C there is an increase by 35%  
778 for the virtual grid of receivers and by 130% for the real station distribution scenario. In  
779 summary that means, adding recordings of rotation into the inversion indeed brings a benefit  
780 for the decomposition of the full moment tensor.

781 This conclusion is particularly significant for non-tectonic events, such as explosions, mining  
782 collapse, and volcanic or geothermally induced events. Sometimes this question is connected  
783 with a certain political sensitivity, for example in the frame of the Comprehensive Nuclear-  
784 Test-Ban Treaty (CTBT). Several studies have already addressed this question from transla-  
785 tional ground motion alone (e.g. Dreger and Woods, 2002; Barth, 2014; Vavrycuk and Kim,  
786 2014; Gaebler et al., 2019; Mustac et al., 2020, and many more). For the DPRK nuclear test  
787 of 2016 Cesca et al. (2017) showed a trade-off between the ISO, vertical CLVD, and DC part.

788 Within the ISO part, it is a trade-off between the horizontal ( $M_{xx}$  and  $M_{yy}$ ) and vertical  
789 ( $M_{zz}$ ) diagonal moment tensor elements (see also Julian et al., 1998). For tectonic events,  
790 several authors could show that the low resolution of the ISO part is inherently related to  
791 the often low resolution of the centroid depth (e. g. Sipkin, 1986; Šílený et al., 1992; Křížová  
792 et al., 2013). Rotational ground motion measurements can address all of these aspects.

### 793 **3.6 Influence of noise**

794 Studies on synthetic data always lack real world complexities in many ways. One of it is  
795 the influence of noise contained in real observations. It can arise from inaccuracies in the  
796 measurement, for example noise in the seismogram, or from inaccuracies in the theory, for  
797 example hypocenter uncertainties, structural model uncertainties. The latter one often can  
798 be taken into account by appropriate inversion strategies. For example, by adjusting the  
799 inverted frequency range to match uncertainties in the structural model or by grid-searching  
800 a specific range of likely values for parameters such as coordinates and centroid depth.

801 Noise due to measurement inaccuracies is more difficult to take into account due to its cor-  
802 related nature (Yagi and Fukahata, 2008). Mustač and Tkalčić (2017) showed that erroneous  
803 inversion solutions can be the result of unaccounted noise during inversion which leads to  
804 overfitting waveform data. In their 2020 study they demonstrated that the non-ISO part  
805 of the moment tensor is affected most from this effect. It has direct consequences for the  
806 analysis of non-tectonic sources such as explosions.

807 In the synthetic studies including rotational ground motions summarised here, the synthetic  
808 waveform data were biased with Gaussian noise of 10% of the maximum amplitude observed  
809 in the synthetic waveforms. Because the maximum amplitude between translations and  
810 rotations differ by several orders of magnitude they were evaluated separately. To investigate  
811 the effect of different noise levels during inversion including rotations, Bernauer et al. (2014)  
812 have repeated their Bayesian inversion for kinematic source parameters with varying noise  
813 levels. Because the study approach provides a relative comparison on 3C versus 6C inversion  
814 results, it is controlled only by the ratio of the noise level between rotational and translational  
815 synthetics. Therefore, they kept the noise level for the translational data constant while  
816 increasing the noise level for the rotational data up to five times the level of the translational  
817 noise. They conclude that the signal-to-noise ratio just need to be similar in both types of  
818 waveform data for the inversion result to benefit from including rotational ground motion  
819 measurements.

## 4 Summary

Most difficulties with the resolution of the seismic moment tensor components during waveform inversion are connected with depth: specific moment tensor components are badly resolved for shallow sources, centroid depth itself, several trade-offs somehow related to depth or depth-dependent components, and sensitivity to the structural model with depth. This is exactly what rotational ground motion can provide: information on the spatial wavefield gradient of the vertical displacement (see Eqs. 16 and 17). As a consequence, when including rotational ground motion into inversion, the resolution (here, meaning accuracy and precision) of the seismic moment tensor components are significantly increased, in some cases by more than 100%. As to be expected, especially the depth-dependent components and the centroid depth could benefit the most. From finite source studies, we also know that the benefit is even increased when we analyse earthquake sources which include vertical rupture instead of a pure strike-slip source mainly rupturing horizontally.

The benefits for the moment tensor resolution was shown on both, synthetic studies and real ADR data. The benefits for the centroid depth and for sources including vertical rupture was shown with synthetic studies only. So far missing but in progress is a study validating the findings on real, direct measurements.

If the single moment tensor components are more reliably determined, then also the decomposition into different source parts is more reliable. Especially the ISO part (volume changes within the source) is fundamental for the entire decomposition process but also the hardest part to resolve from translational waveform data alone.

In summary, the benefits for the moment tensor resolution mainly are due to two reasons:

- Rotational ground motion recordings contain information on the vertical displacement gradient. This information is not available from classical translational surface station recordings. That is an added information to the waveform inversion (beyond simply adding more data).
- Having available six components of ground motion per observation point instead of only three, the amount of amplitude ratios between the components increases by a factor of five (from 3 to 15, enumerative combinatorics). These ratios uniquely reflect the radiation pattern of the source which is hence better constrained. Or to put it differently: With respect to the radiation pattern, one 6C observation is equivalent to two 3C observations at  $90^\circ$  azimuth from one another.

From inversion theory we know that the inversion result is generally improved when more data of the same type is added to the inversion, even for generally overdetermined inversion problems (Tarantola, 2005). In the few studies performed so far this effect was considered.

855 Having six components per observation only half the number of receivers were used for  
856 waveform inversion. Still, the same if not higher solution quality was obtained. This result  
857 has important implications for hardware installation and maintenance efforts. At some  
858 regions of Earth it is simply not possible to establish a dense station network, even more in  
859 planetary seismology. Here, recording the entire wavefield in six components can be highly  
860 beneficial, not only for source inversion.

861 Finally, I want to comment on the question whether ADR and direct measurements of  
862 rotation are redundant. No, they are not. ADR is valid only in a specific, rather long-  
863 period range of frequencies, depending on the spatial extent of the receiver array used to  
864 calculate them. In contrast, direct measurements cover a very broad range of frequencies,  
865 meanwhile even with portable devices. Also, ADR is a spatial averaged measure and it is not  
866 entirely clear if it contains the same physical information than a direct point measurement,  
867 for example local side effects are averaged out during the calculation. Due to the same reason  
868 ADR measurements can not be used for tilt corrections.

## 869 5 Outlook

870 The findings from the currently few studies are very promising concerning the improved reli-  
871 ability of the resulting moment tensor from inverting rotational and translational waveforms  
872 together. They suggest that some well- and long-known difficulties in regional waveform  
873 inversion for seismic moment tensors can be tackled quite well with the relatively new meas-  
874 urement of rotational ground motion. However, some aspects have not yet been investigated.  
875 The most important aspect is the question whether the results can be replicated from real,  
876 directly measured data. The study using ADR data is a pointer in this direction. However,  
877 as already explained ADR data is not entirely comparable with direct measurements. One  
878 specific aspect of ADR data is their spatial averaging over the array area. Thus, they average  
879 out local side effects. In contrast, meanwhile we know that rotational ground motion are  
880 much more sensitive to small-scale structural heterogeneities in the vicinity of the receiver.  
881 While we often can ignore or compensate local side effects when analysing translational  
882 ground motion, we probably need to correct rotational ground motion for these effects before  
883 we can analyse them. The introduction of the strain-rotation coupling vector  $\mathbf{J}$  is a good  
884 approach to do so. However, it was not applied yet on real data as preparation for further  
885 studies such as waveform inversion for moment tensors.

886 Another aspect of ADR data is their reliable range of frequencies, depending on the spatial  
887 extend of the translational receiver array used to calculate them (see Sec. 2.2.2). Real arrays,  
888 i.e. particularly designed for array processing purposes, usually have quite small inter-  
889 receiver distances of a few kilometres, resulting in relatively high reliable frequency ranges,

890 roughly higher than 0.005 Hz. These frequencies are still quite small for regional waveform  
891 inversion. Using 'normal' receiver networks to calculate ADR the network extend quickly  
892 becomes large and the resulting reliable frequencies very small. This is in contradiction  
893 to the frequencies usually used in regional waveform inversion for moment tensors ( $f \leq$   
894 0.01 Hz). Nevertheless, it is not investigated yet whether both types of measurement could  
895 complement each other in waveform inversion for moment tensors. If done with proper care  
896 for the limitations of the method, ADR data might be a useful addendum to the waveform  
897 inversion for moment tensors.

898 Most of the findings summarised in this article are from studies based on synthetic data.  
899 They are lacking real world complexities in many ways, mainly due to missing correlated noise  
900 (see Secs. 3.3 and 3.6). Therefore, the most important next step in investigating the benefits  
901 of rotational ground motion for waveform inversion for moment tensors is the validation from  
902 real, direct measurements. Effects of uncertainties in structural model, local side effects and  
903 strain rotation coupling, uncertainties in epicenter versus hypocenter location, measurement  
904 errors, and used frequency range can be investigated thoroughly only on real data.

905 In addition, the studies so far investigated the benefits of rotational ground motion either in a  
906 setting with an entire network of 6C receivers or a sparse network of only two or three 6C re-  
907 ceivers. Not answered yet is the question how much benefit it will bring to expand an existing  
908 network of translational receivers with only one or two rotational receivers. This question is  
909 interesting not only for the regional but also for the local distance range. Given the promising  
910 findings so far, it might be possible to circumvent limitations due to relations between fre-  
911 quency, structure, and magnitude (see Sec. 3.3) and expand the waveform inversion to much  
912 lower magnitude thresholds. Such expanded catalogues of earthquake mechanisms broadens  
913 the underlying data base for subsequent seismotectonic studies enormously. Particularly in  
914 regions with low seismicity rate, where the number of medium to large sized earthquakes  
915 over time is low, this is a possibility to gain further insights into tectonic processes.

916 Further investigation is also needed on the topic of moment tensor decomposition, especially  
917 on the reliable determination of the difficult to obtain ISO part. Thus, we can learn more  
918 about the physical processes within the source beyond the pure tectonic shear rupture; that is  
919 in volcanic areas and areas with swarm activity as well as induced source processes connected  
920 to geothermal facilities, mining activities, and oil/gas production. Increasing the reliability  
921 of the decomposition by incorporating rotational ground motion contributes strongly to  
922 distinguishing between tectonic, explosive and induced sources and analysing them.

923 In Sec. 2.1.1 I show that the equation for the general elastodynamic source (Eq. 1) is  
924 simplified when external forces such as gravitation are neglected. That is net forces and  
925 torques are vanishing and thus the moment tensor becomes symmetric. Several authors  
926 showed that these are overly restrictive assumptions and real sources indeed include net

927 forces and torque components. Abreu et al. (2018) have developed a framework for a more  
928 realistic, asymmetric moment tensor using micropolar theory. It allows an independent  
929 rotation within the source (spin) which is different from the continuum, rigid body rotation.  
930 The theory enables to better account for deformation by including material rotations during  
931 the rupture and thus better constrains physical processes within the source. The theory still  
932 needs to be validated against real measurements.

## 933 **Acknowledgement**

934 I thank the editor C. Schmelzbach for the opportunity to write this review and for his support  
935 throughout the writing and publishing process. Reviewer G. Hillers' constructive comments  
936 considerably helped to improve the accessibility of the manuscript.

## 937 **References**

- 938 R. Abreu, S. Durand, and C. Thomas. The asymmetric seismic moment tensor in micropolar  
939 media. Bull. Seismol. Soc. Am., 108(3A):1160–1170, 2018.
- 940 P. Adamova and J. Šilený. Non-double-couple earthquake mechanism as an artefact of the  
941 point-source approach applied to a finite-extent focus. Bull. Seismol. Soc. Am., 100:447–  
942 457, 2010.
- 943 K. Aki and P. G. Richards. Quantitative seismology. University Science Book, second  
944 edition, 2002.
- 945 N. Aso, K. Ohta, and S. Ide. Mathematical review on source-type diagrams. Earth, Planets,  
946 and Space, 68:52, 2016.
- 947 G. Backus and M. Mulcahy. Moment tensors and other phenomenological descriptions of  
948 seismic sources - I. Continuous displacements. Geophys. J. R. astr. Soc., 46:341–361, 1976.
- 949 G. Backus. Interpreting the seismic glut moments of total degree two or less. Geophys. J.  
950 R. astr. Soc., 51:1–25, 1977a.
- 951 G. Backus. Seismic sources with observable glut moments of spatial degree two. Geophys.  
952 J. R. astr. Soc., 51:27–45, 1977b.
- 953 A. Barth. Significant release of shear energy of the North Korean nuclear test on February  
954 12, 2013. J. Seismol., 18(3):605–615, 2013.



- 955 M. Bernauer, A. Fichtner, and H. Igel. Measurements of translation, rotation and strain:  
956 new approaches to seismic processing and inversion. J. Seismol., 16:669–681, 2012.
- 957 M. Bernauer, A. Fichtner, and H. Igel. Reducing nonuniqueness in finite source inversion  
958 using rotational ground motions. J. Geophys. Res., 119:4860–4875, 2014.
- 959 F. Bernauer, J. Wassermann, F. Guattari, A. Frenois, A. Bigueur, A. Gaillot, E. de Toldi, D.  
960 Ponceau, K. U. Schreiber, and H. Igel. BlueSeis3A - full characterization of a 3C broadband  
961 rotational seismometer. Seismol. Res. Lett., 89(2A):620–629, doi: 10.1785/0220170143.
- 962 F. Bernauer, K. Behnen, J. Wassermann, S. Egdorf, H. Igel, S. Donner, K. Stammler, M.  
963 Hoffmann, P. Edme, D. Sollberger, C. Schmelzbach, J. Robertsson, P. Paitz, J. Igel,  
964 K. Smolinski, A. Fichtner, Y. Rossi, G. Izgi, D. Vollmer, E. P. S. Eibl, S. Buske, C.  
965 Veress, F. Guattari, T. Laudat, L. Mattio, O. Sébe, S. Olivier, C. Lallemand, B. Brun-  
966 ner, A. T. Kurzych, M. Dudek, L. R. Jaroszewicz, J. K. Kowalski, P. A. Bońkowski, P.  
967 Bobra, Z. Zembaty, J. Vackář, J. Málek, and J. Brokesova. Rotation, strain, and trans-  
968 lation sensors performance tests with active seismic sources. Sensors, 21(1):264, 2021,  
969 <https://doi.org/10.3390/s21010264>.
- 970 M. Beyreuther, R. Barsch, L. Krischer, T. Megies, Y. Behr, and J. Wassermann. ObsPy: A  
971 Python toolbox for seismology Seismol. Res. Lett., 81:530–533, 2010.
- 972 P. Bodin, J. Gomberg, S. K. Singh, and M. Santoyo. Dynamic deformations of shallow  
973 sediments in the Valley of Mexico, Part I: three-dimensional strains and rotations recorded  
974 on a seismic array. Bull. Seismol. Soc. Am., 87:528–539, 1997.
- 975 J. Braunmiller, U. Kradolfer, M. Baer, and D. Giardini. Regional moment tensor determ-  
976 ination in the European-Mediterranean area - initial results. Tectonophysics, 356:5–22,  
977 2002.
- 978 J. Brokešová, J. Málek, and J. r. Evans. Note: Rotaphone, a new self-calibrated six-degree-  
979 of-freedom seismic sensor. Rev. Sci. Instrum., 83(8):086108-1–086108-3, 2012.
- 980 J. Brokešová and J. Málek. Rotaphone, a self-calibrated six-degree-of-freedom seismic sensor  
981 and its strong-motion records. Seismol. Res. Lett., 84(5):737–744, 2013.
- 982 B. Bukchin. Specific features of surface wave radiation by shallow sources. Phys. Solid Earth,  
983 42:712–717, 2006.
- 984 B. Bukchin, E. Clévédé, and A. Mostinskiy. Uncertainty of moment tensor determination  
985 from surface wave analysis for shallow earthquakes. J. Seismol., 14:601–614, 2010.

- 986 Y. Capdeville, P. Cupillard, and S. Singh. An introduction to the two-scale homogenization  
987 method for seismology. Advances in Geophysics, 61:217–306, 2020.
- 988 S. Cesca and S. Heimann. A practical on moment tensor inversion using the Kiwi tools. In:  
989 P. Bormann, editor, New Manual of Seismological Observatory Practice 2 (NMSOP-2),  
990 EX 3.6. Potsdam: Deutsches GeoForschungsZentrum GFZ, 2013.
- 991 S. Cesca, A. Rohr and T. Dahm. Discrimination of induced seismicity by full moment tensor  
992 inversion and decomposition. J. Seismol., 17:147–163, 2013.
- 993 S. Cesca, S. Heimann, M. Kriegerowski, J. Saul, and T. Dahm. Moment tensor inversion of  
994 nuclear explosions: what can we learn from the 6 January and 9 September 2016 nuclear  
995 tests, North Korea? Seismol. Res. Lett., 88(2A):300-310, 2017.
- 996 C. Cesca and S. Heimann. Challenges in regional moment tensor resolution and interpreta-  
997 tion. In: S. D’Amico, editor, Moment tensor solutions - A useful tool for seismotectonics,  
998 pages 163–181. Springer International Publishing, 2018.
- 999 A. Cochard, H. Igel, B. Schuberth, W. Suryanto, A. Velikoseltsev, U. Schreiber, J. Wasser-  
1000 mann, F. Scherbaum, D. Vollmer. Rotational motions in seismology: theory, observa-  
1001 tion, simulation. In: R. Teisseyre, E. Majewski, M. Takeo, editors, Earthquake source  
1002 asymmetry, structural media and rotation effects, pages 391–411. Springer Verlag, Ber-  
1003 lin/Heidelberg, 2006.
- 1004 B. M. Covellone and B. Savage. A quantitative comparison between 1D and 3D source inver-  
1005 sion methodologies: Application to the Middle East. Bull. Seism. Soc. Am., 102(5):2189–  
1006 2199, 2012.
- 1007 R. Cowsik, T. Madziwa-Nussinov, K. Wagoner, D. Wiens, and M. Wyssession. Performance  
1008 characteristics of a rotational seismometer for near-field and engineering applications. Bull.  
1009 Seismol. Soc. Am., 99(2B):1181–1189, 2009.
- 1010 T. Dahm. Relativmethoden zur Bestimmung der Abstrahlcharakteristik von seismischen  
1011 Quellen. PhD Thesis, University of Karlsruhe, Germany, 1993.
- 1012 T. Dahm, G. Manthei, and J. Eisenblätter. Automated moment tensor inversion to estimate  
1013 source mechanisms of hydraulically induced micro-seismicity in salt-rock. Tectonophysics,  
1014 306:1–17, 1999.
- 1015 T. Dahm, F. Krüger, K. Stammer, K. Klinge, R. Kind, K. Wylegalla and J.-R. Grasso. The  
1016 2004 Mw 4.4 Rotenburg, northern Germany, earthquake and its possible relationship with  
1017 gas recovery. Bull. seism. Soc. Am., 97(3):691–704, 2007.

- 1018 F. Krüger and T. Dahm. Moment tensor inversion and moment tensor interpretation. In:  
1019 P. Bormann, editor, New Manual of Seismological Observatory Practice 2 (NMSOP-2),  
1020 IS 3.9. Potsdam: Deutsches GeoForschungsZentrum GFZ, 2014.
- 1021 T. Dahm, S. Heimann, S. Funke, S. Wendt, I. Rappsilber, D. Bindi, T. Plenefisch, and F.  
1022 Cotton. Seismicity in the block mountains between Halle and Leipzig, central Germany:  
1023 centroid moment tensors, ground motion simulation, and felt intensities of two  $M \sim 3$   
1024 earthquakes in 2015 and 2017. J. Seismol., 22:985–1003, 2018.
- 1025 S. D’Amico. Moment tensor solutions - A useful tool for seismotectonics. Springer  
1026 International Publishing, 2018.
- 1027 B. Delouis and D. Legrand. Focal mechanism determination and identification of the fault  
1028 plane of earthquakes using only one or two near-source seismic recordings. Bull. Seismol.  
1029 Soc. Am., 89:1558–1574, 1999
- 1030 S. Donner, D. Rößler, F. Krüger, A. Ghods, and M. R. Strecker. Segmented seismicity of  
1031 the Mw 6.2 Baladeh earthquake sequence (Alborz mountains, Iran) revealed from regional  
1032 moment tensors. J. Seismol., 17:925–959, 2013.
- 1033 S. Donner, F. Krüger, D. Rößler, and A. Ghods. Combined inversion of broad-band and  
1034 short-period waveform data for regional moment tensors: A case study in the Alborz  
1035 mountains, Iran. Bull. Seismol. Soc. Am., 104:1358–1373, 2014.
- 1036 S. Donner, M. Bernauer, and H. Igel. Inversion for seismic moment tensors combining  
1037 translational and rotational ground motions. Geophys. J. Int., 207:562–570, 2016.
- 1038 S. Donner, C.-J. Lin, C. Hadziioannou, A. Gebauer, F. Vernant, D. C. Agnew, H. Igel, K.  
1039 U. Schreiber, and J. Wassermann. Comparing direct observation of strain, rotation, and  
1040 displacement with array estimates at Piñon Flat Observatory, California. Seismol. Res.  
1041 Lett., 88(4):1107–1116, 2017.
- 1042 S. Donner, H. Igel, C. Hadziioannou, and the Romy group. Retrieval of the seismic moment  
1043 tensor from joint measurements of translational and rotational ground motions: Sparse  
1044 networks and single stations. In: S. D’Amico, editor, Moment tensor solutions: A useful  
1045 tool for seismotectonics, Springer International Publishing, pp. 263–280, 2018.
- 1046 S. Donner, M. Mustać, B. Hejrani, H. Tkalčić, and H. Igel. Seismic moment tensors from  
1047 synthetic rotational and translational ground motion: Green’s functions in 1-D versus 3-D.  
1048 Geophys. J. Int., 223:161–179, 2020.

- 1049 D. Doornbos. Seismic moment tensors and kinematic source parameters. Geophys. J. R.  
1050 astr. Soc., 69:235–251, 1982.
- 1051 D. Dreger and D. Helmberger. Source parameters of the Sierra Madre earthquake from  
1052 regional and local body waves. Geophys. Res. Lett., 18(11):2015–2018, 1991.
- 1053 D. Dreger and D. Helmberger. Determination of source parameters at regional distances  
1054 with three-component sparse network data. J. Geophys. Res., 98:8107–8125, 1993.
- 1055 D. Dreger and B. Woods. Regional distance seismic moment tensors of nuclear explosions.  
1056 Tectonophysics, 356:139–156, 2002.
- 1057 H. Dufumier and M. Cara. On the limits of linear moment tensor inversion of surface wave  
1058 spectra. Pure appl. Geophys., 145:235–257, 1995.
- 1059 Z. Duputel, L. Rivera, Y. Fukahata, and H. Kanamori. Uncertainty estimations for seismic  
1060 source inversion. Geophys. J. Int., 190:1243–1256, 2012.
- 1061 A. M. Dziewonski and F. Gilbert. Temporal variation of the seismic moment tensor and the  
1062 evidence of precursive compression for two deep earthquakes. Nature, 247:185–188, 1974.
- 1063 A. M. Dziewonski, T.-A. Chou, and J. H. Woodhouse. Determination of earthquake source  
1064 parameters from waveform data for studies of global and regional seismicity. J. Geophys.  
1065 Res., 86(B4):2825–2852, 1981.
- 1066 D. Eberhart-Phillips. Three-dimensional P and S velocity structure in the Coalinga region,  
1067 California. J. Geophys. Res., 95:15,343–15,363, 1990.
- 1068 G. Ekström, A. M. Dziewonski, and J. M. Steim. Single station CMT: application to the  
1069 Michoacan, Mexico, earthquake of September 19, 1985. Geophys. Res. Lett., 13:173–176,  
1070 1986.
- 1071 G. Ekström, M. Nettles, and A. M. Dziewonski. The global CMT project 2004-2010:  
1072 Centroid-moment tensors for 13,017 earthquakes. PEPI, 200-201:1-9, 2012.
- 1073 G. Fan and T. Wallace. The determination of source parameters for small earthquakes from  
1074 a single, very broadband seismic station. Geophys. Res. Lett., 18:1385–1388, 1991.
- 1075 A. Fichtner and H. Igel. Sensitivity densities for rotational ground-motion measurements.  
1076 Bull. Seismol. Soc. Am., 99(2B):1302–1314, 2009.
- 1077 A. Fichtner and H. Tkalčić. Insights into the kinematics of a volcanic caldera drop: Probab-  
1078 ilitistic finite-source inversion of the 1996 Bardarbunga, Iceland, earthquake. Earth Planet.  
1079 Sci. Lett. 297(3–4):607–615, 2010.

- 1080 T. J. Fitch, D. W. McCowan, and M. W. Shields. Estimation of the seismic moment tensor  
1081 from teleseismic body wave data with application to intraplate and mantle earthquakes.  
1082 J. Geophys. Res., 85:3817–3828, 1980.
- 1083 S. R. Ford, D. S. Dreger, and W. R. Walter. Network sensitivity solutions for regional  
1084 moment tensor inversions. Bull. Seismol. Soc. Am., 100(5A):1962–1970, 2010.
- 1085 C. Frohlich. Note concerning non-double-couple source components from slip along surfaces  
1086 of revolution. J. Geophys. Res., 95(B5):6861–6866, 1990.
- 1087 C. Frohlich. Earthquakes with non-double-couple mechanisms. Science, 264:804–809, 1994.
- 1088 P. Gaebler, L. Ceranna, N. Nooshiri, A. Barth, S. Cesca, M. Frei, I. Grünberg, G. Hartmann,  
1089 K. Koch, C. Pilger, J. O. Ross, and T. Dahm. A multi-technology analysis of the 2017  
1090 North Korean nuclear test. Solid Earth, 10(1):59–78, 2019.
- 1091 J. W. Gephart and D. W. Forsyth. An improved method for determining the regional stress  
1092 tensor using earthquake focal mechanism data: Application to the San Francisco Earth-  
1093 quake Sequence. J. Geophys. Res., 89(B11):9305–9320, 1984
- 1094 F. Gilbert. Excitation of the normal modes of the Earth by earthquake sources. Geophys.  
1095 J. R. astr. Soc., 22:223–226, 1970.
- 1096 F. Gilbert. Derivation of source parameters from low-frequency spectra. Phil. Trans. R.  
1097 SOC., 274:369–371, 1973.
- 1098 F. Gilbert and A. M. Dziewonski. An application of normal mode theory to the retrieval  
1099 of structural parameters and source mechanisms from seismic spectra. Philosophical  
1100 Transactions of the Royal Society of London; Series A, Mathematical and Physical  
1101 Sciences, 278(1280):187–269, 1975.
- 1102 R. W. Graves and D. J. Wald. Resolution analysis of finite fault source inversion us-  
1103 ing one- and three-dimensional Green’s functions 1. Strong motions. J. Geophys. Res.,  
1104 106(B5):8745–8766, 2010.
- 1105 M. T. Gudmundsson, K. Jónsdóttir, A. Hooper, E. P. Holohan, S. A. Halldórsson, B. G.  
1106 Ófeigsson, S. Cesca, K. S. Vogfjörd, F. Sigmundsson, T. Högnadóttir, P. Einarsson, O.  
1107 Sigmarsson, A. H. Jarosch, K. Jónasson, E. Magnússon, S. Hreinsdóttir, M. Bagnardi, M.  
1108 M. Parks, V. Hjörleifsdóttir, F. Pálsson, T. R. Walter, M. P. J. Schöpfer, S. Heimann, H.  
1109 I. Reynolds, S. Dumont, E. Bali, G. H. Gudfinnsson, T. Dahm, M. J. Roberts, M. Hensch,  
1110 J. M. C. Belart, K. Spaans, S. Jakobsson, G. B. Gudmundsson, H. M. Fridriksdóttir, V.  
1111 Drouin, T. Dürig, G. Aðalgeirsdóttir, M. S. Riishuus, G. B. M. Pedersen, T. van Boeckel,

- 1112 B. Oddsson, M. A. Pfeffer, S. Barsotti, B. Bergsson, A. Donovan, M. R. Burton, and A.  
1113 Aiuppa. Gradual caldera collapse at Bárðarbunga volcano, Iceland, regulated by lateral  
1114 magma outflow. Science, 353(6296), aaf9899-1–aaf8988-8, 2016.
- 1115 C. Haberland, A. Rietbrock, D. Lange, K. Bataille, and T. Dahm. Structure of the seis-  
1116 mogenic zone of the southcentral Chilean margin revealed by local earthquake travelttime  
1117 tomography. J. Geophys. Res., 114:B01317, 2009.
- 1118 J. C. Harrison. Cavity and topographic effects in tilt and strain measurement. J. geophys.  
1119 Res., 81(2):319–328, 1976.
- 1120 N. A. Haskell. Radiation pattern of surface waves from point sources in a multi-layered  
1121 medium. Bull. Seism. soc. Am., 54(1):377–393, 1964.
- 1122 W. K. Hastings. Monte Carlo sampling methods using Markov chains and their applications.  
1123 Biometrika, 57:97–109, 1970.
- 1124 O. Heidbach, M. Rajabi, X. Cui, K. Fuchs, B. Müller, J. Reinecker, K. Reiter, M. Tingay,  
1125 F. Wenzel, F. Xie, M. Ziegler, M.-L. Zoback, and M. Zoback. The World Stress Map  
1126 database release 2016: Crustal stress pattern across scales. Tectonophysics, 744:484–498,  
1127 2018.
- 1128 B. Hejrani, H. Tkalčić and A. Fichtner. Centroid moment tensor catalogue using a 3-D  
1129 continental scale Earth model: Application to earthquakes in Papua New Guinea and the  
1130 Solomon Islands. J. Geophys. Res., 122:5517–5543, doi: 10.1002/2017JB014230, 2017.
- 1131 B. Hejrani and H. Tkalčić. Resolvability of the centroid-moment-tensors for shallow seismic  
1132 sources and improvements from modelling high-frequency waveforms. J. Geophys. Res.,  
1133 125(7):e2020JB019643, 2020.
- 1134 R. Herrmann, H. Benz, and C. Ammon. Monitoring the earthquake source process in North  
1135 America. Bull. Seismol. Soc. Am., 101:2609–2625, 2011.
- 1136 M. Hingee, H. Tkalčić, A. Fichtner and M. Sambridge. Seismic moment tensor inversion  
1137 using a 3-D structural model: applications for the Australian region. Geophys. J. Int.,  
1138 184:949–964, doi: 10.1111/j.1365-246X.2010.04897.x, 2011.
- 1139 V. Hjörleifsdóttir and G. Ekström. Effects of three-dimensional Earth structure on CMT  
1140 earthquake parameters. PEPI, 179:178–190, 2010.
- 1141 H. Huang, V. Agafonov, and H. Yu. Molecular electric transducers as motion sensors: A  
1142 review Sensors, 13(4):4581–4597, 2013.

- 1143 B. S. Huang. Ground rotational motions of the 1991 Chi-Chi, Taiwan, earthquake as inferred  
1144 from dense array observations. Geophys. Res. Lett., 30(6):1307–1310.
- 1145 J. A. Hudson, R. G. Pearce, and R. M. Rogers. Source type plot for inversion of the moment  
1146 tensor. J. Geophys. Res., 94(B1):765–774, 1989.
- 1147 G. A. Ichinose, S. R. Ford, and R. J. Mellors. Regional moment tensor inversion using  
1148 rotational observations. J. Geophys. Res., 126:e2020JB020827, 2021.
- 1149 H. Igel, K. U. Schreiber, B. Schuberth, A. Flaws, A. Velikoseltsev, and A. Cochard. Obser-  
1150 vation and modelling of rotational motions induced by distant large earthquakes: the M  
1151 8.1 Tokachi-oki earthquake September 25, 2003. Geophys. Res. Lett. 32:L08309, 2005.
- 1152 H. Igel, M. Bernauer, J. Wassermann, and K.U. Schreiber. Rotational Seismology: Theory,  
1153 Instrumentation, Observations, Applications. In: R.A. Meyers, editor Encyclopedia of  
1154 Complexity and Systems Science, pages 391–411. Springer, Berlin, Heidelberg, 2015.
- 1155 D. Inazu, N. Pulido, E. Fukuyama, T. Saito, J. Senda, and H. Kumagai. Near-field tsunami  
1156 forecast system based on near real-time seismic moment tensor estimation in the regions  
1157 of Indonesia, the Philippines, and Chile. Earth, Planets and Space, 68:73, 2016.
- 1158 P. Jedlička, J. T. Kozák, J. R. Evans, and C. R. Hutt. Designs and test results for three new  
1159 rotational sensors. J. Seismol., 16(4):639–647, 2012.
- 1160 L. R. Jaroszewicz, Z. Krajewski, L. Solarz, and R. Teisseyer. Application of the fibre-optic  
1161 Sagnac interferometer in the investigation of seismic rotational waves. Institute of Physics  
1162 Publishing, 17:1186-1193.
- 1163 M. L. Jost and R. B. Herrmann. A student’s guide to and review of moment tensors. Seismol.  
1164 Res. Lett., 60:37–57, 1989.
- 1165 B. R. Julian, A. D. Miller, and G. R. Foulger. Non-double-couple earthquakes - 1. Theory.  
1166 Reviews of Geophysics, 36(4):525–549, 1998.
- 1167 H. Kanamori and J. W. Given. Use of long-period surface waves for rapid determination  
1168 of earthquake source parameters - 2. Preliminary determination of source mechanisms of  
1169 large earthquakes ( $M_S \leq 6.5$ ) in 1980. PEPI, 30:260–268, 1982.
- 1170 H. Kanamori and L. Rivera. Source inversion of W phase: speeding up the seismic tsunami  
1171 warning. Geophys. J. Int., 175:222–238, 2008.
- 1172 Y. Kim, Q. Liu and J. Tromp. Adjoint centroid-moment tensor inversions. Geophys. J. Int.  
1173 186(1):264–278, 2011.

- 1174 G. King and R. Bilham. Tidal tilt measurement in Europe. Nature, 243(5402):74–75, 1973.
- 1175 J. Kinscher, F. Krüger, H. Woith, B. G. Lühr, E. Hintersberger, T. S. Irmak, and S. Bariş.  
1176 Seismotectonics of the Armutlu peninsula (Marmara Sea, NW Turkey) from geological field  
1177 observation and regional moment tensor inversion. Tectonophysics, 608:980–995, 2013.
- 1178 L. Knopoff and M. J. Randall. The compensated linear-vector dipole: a possible mechanism  
1179 for deep earthquakes. J. Geophys. Res., 75:4957–4963, 1970.
- 1180 M. L. Kohl and J. Levine. Measurement and interpretation of tidal tilts in a small array. J.  
1181 geophys. Res., 100(B3):3929–3941,1995.
- 1182 L. Krischer, T. Megies, R. Barsch, M. Beyreuther, T. Lecocq, C. Caudron, and J. Wasser-  
1183 mann. ObsPy: A bridge for seismology into the scientific Python ecosystem. Comput.  
1184 Sci. Disc., 8:014003, 2015.
- 1185 D. Křížová, J. Zahradníck, and A. Kiratzi. Resolvability of isotropic component in regional  
1186 seismic moment tensor inversion. Bull. seism. Soc. Am., 103:2460–2473, 2013.
- 1187 F. Krüger and G. Bock. Moment-tensor determination and decomposition. In: P. Bormann,  
1188 editor, New Manual of Seismological Observatory Practice 2 (NMSOP), EX 3.5. Potsdam:  
1189 Deutsches GeoForschungsZentrum GFZ, 2009.
- 1190 F. Krüger and F. Scherbaum. Short Note: The 29 September 1969, Ceres, South Africa,  
1191 earthquake: Full waveform moment tensor inversion for point source and kinematic source  
1192 parameters. Bull. Seism. soc. Am., 140(1):576–581, 2014.
- 1193 D. Kühn and V. Vavryčuk. Determination of full moment tensors of microseismic events in  
1194 a very heterogeneous mining environment. Tectonophysics, 589:33–43, 2013.
- 1195 D. Kühn, S. Heimann, M. P. Isken, E. Ruigrok, and B. Dost. Probabilistic moment tensor  
1196 inversion for hydrocarbon-induced seismicity in the Groningen gas field, The Netherlands,  
1197 Part 1: Testing. Bull. Seismol. soc. Am., 110(5):2095–2111, 2020.
- 1198 C. A. Langston. Spatial gradient analysis for linear seismic arrays. Bull. Seismol. soc. Am.,  
1199 97:265–280, 2007a.
- 1200 C. A. Langston. Wave gradiometry in two dimensions. Bull. Seismol. soc. Am., 97:401–416,  
1201 2007b.
- 1202 C. A. Langston. Wave gradiometry in the time domain. Bull. Seismol. soc. Am., 97:926–933,  
1203 2007c.



- 1204 C. A. Langston. Calibrating dense spatial arrays for amplitude statics and orientation errors.  
1205 J. Geophys. Res., 123:3849–3870, 2018.
- 1206 W.H.K. Lee, B.-S. Huang, C. A. Langston, C.-J. Lin, C.-C. Liu, T.-C. Shin, T.-L. Teng, and  
1207 C.-F. Wu. Review: progress in rotational ground motion observations from explosions and  
1208 local earthquakes in Taiwan. Bull. Seismol. soc. Am., 99(2b):958–967, 2009.
- 1209 W.H.K. Lee, J.R. Evans, B.-S. Huang, S.R. Hutt, C.-J. Lin, C.-C. Liu, and R.L. Nigbor.  
1210 Measuring rotational ground motions in seismological practice. In: P. Bormann, ed-  
1211 itor, New Manual of Seismological Observatory Practice 2 (NMSOP-2), IS 5.3. Potsdam:  
1212 Deutsches GeoForschungsZentrum GFZ, 2011.
- 1213 H. C. Lefèvre. The fibre-optic gyroscope. Artech House, London, United Kingdom, 2014.
- 1214 D. Legrand, S. Kaneshima and H. Kawakatsu. Moment tensor analysis of near-field broad-  
1215 band waveforms observed at Aso Volcano, Japan. J. Volc. Geotherm. Res., 101(1-2):155–  
1216 169, 2000.
- 1217 Z. Li and M. van der Baan. Tutorial on rotational seismology and its applications in explor-  
1218 ation geophysics. Geophysics, 82(5):W17–W30, 2017.
- 1219 C. Liang and C. A. Langston Wave gradiometry for USArray: Rayleigh waves J. Geophys.  
1220 Res., 114:B02308, 2009.
- 1221 C.-J. Lin, W.-G. Huang, H.-P. Huang, B.-S. Huang, C.-S. Ku, and C.-C. Liu. Investigation  
1222 of array derived rotation in TAIPEI 101. J. Seismol., 16:1–11, 2012.
- 1223 T. Megies, M. Beyreuther, R. Barsch, L. Krischer, and J. Wassermann. ObsPy - What can  
1224 it do for data centers and observatories. Ann. Geophys., 54:47–58, 2011.
- 1225 N. Metropolis and S. Ulam. The monte carlo method. Journal of the American Statistical  
1226 Association, 44:335–341, 1949.
- 1227 N. Metropolis, M. N. Rosenbluth, A. H. Teller, and E. Teller. Equation of state calculations  
1228 by fast computing machines. Journal of Chemical Physics, 21:1087–1092, 1953.
- 1229 D. P. McLeod, G. E. Stedman, T. H. Webb, and K. U. Schreiber. Comparison of standard  
1230 and ring laser rotational seismograms. Bull. Seismol. Soc. Am., 88:1495–1503,1998.
- 1231 S. Mousavi, K. Bauer, M. Korn, and B. Heijrani. Seismic tomography reveals a mid-crustal  
1232 intrusive body, fluid pathways and their relation to the earthquake swarms in West Bo-  
1233 hemia/Vogtland. Geophys. J. Int., 203:1113–1127, 2015.

- 1234 M. Mustać and H. Tkalčić. On the use of data noise as a site-specific weight parameter in  
1235 a hierarchical Bayesian moment tensor inversion: the case study of the Geysers and Long  
1236 Valley Caldera earthquakes. Bull. seism. Soc. Am., 107:1914-1922, 2017.
- 1237 M. Mustać, B. Hejrani, H. Tkalčić, S. Kim, S.-J. Lee, and C. S. Chow. Large isotropic com-  
1238 ponent in the source mechanism of the 2013 Democratic People’s Republic of Korea nuclear  
1239 test revealed via a hierarchical Bayesian inversion. Bull. seism. Soc. Am., 110(1):166–177,  
1240 2020.
- 1241 M. Nettles and G. Ekström. Faulting mechanism of anomalous earthquakes near Bádarbunga  
1242 Volcano, Iceland. J. Geophys. Res., 103(B8):17973–17983, 1998.
- 1243 R. L. Nigbor. Six-degree-of-freedom ground-motion measurement. Bull. Seismol. Soc. Am.,  
1244 84(5):1665-1669, 1994.
- 1245 R. L. Nigbor, J. R. Evans, and C. R. Hutt. Laboratory and field testing of commercial  
1246 rotational seismometers. Bull. Seismol. Soc. Am., 99(2b):1215–1227, 2009.
- 1247 T. Nissen-Meyer, M. van Driel, S. C. Stähler, K. Hosseini, S. Hempel, L. Auer, A. Colombi,  
1248 and A. Fournier. AxiSEM: broadband 3-D seismic wavefield in axisymmetric media. Solid  
1249 Earth, 5:425–445, 2014.
- 1250 A. Pancha, T. H. Webb, G. E. Stedman, D. P. McLeod, and K. U. Schreiber. Ring laser  
1251 detection of rotations from teleseismic waves. Geophys. Res. Lett., 27:3553–3556, 2000.
- 1252 N. D. Pham, H. Igel, J. de la Puente, M. Käser, and M. A. Schoenberg. Rotational motions  
1253 in homogeneous anisotropic elastic media. Geophysics, 75:D47–D56, 2010.
- 1254 B. Pierson, D. Laughlin, and B. Brune. Seismic MHD (SMHD) - Rotational sensor develop-  
1255 ment and deployment. 4th IWGoRS Meeting, Tutzing Germany, 20–23 June 2016.
- 1256 M. Reinwald, M. Bernauer, H. Igel, and S. Donner. Improved finite-source inversion through  
1257 joint measurements of rotational and translational ground motions: a numerical study.  
1258 Solid Earth, 7:1467–1477, 2016.
- 1259 J. O. A. Robertsson and A. Curtis. Wavefield separation using densely deployed  
1260 three-component single-sensor groups in land surface-seismic recordings. Geophysics,  
1261 67(5):1624–1633, 2002.
- 1262 S. Schippkus, H. Hausmann, Z. Duputel, G. Bokelmann and AlpArray Working Group. The  
1263 Alland earthquake sequence in Eastern Austria: Shedding light on tectonic stress geometry  
1264 in a key area of seismic hazard. Austrian Journal of Earth Sciences, 112(2):182–194, 2020.

- 1265 W. Schlüter. Schwingungsart und Weg der Erdbebenwellen. Beiträge zur Geophysik, 5:314–  
1266 359, 1903.
- 1267 C. Schmelzbach, D. Donner, H. Igel, D. Sollberger, T. Taufiqurrahman, F. Bernauer,  
1268 M. Häusler, C. van Renterghem, J. Wassermann, and J.O.A. Robertsson. Advances  
1269 in 6C seismology: Applications of combined translational and rotational motion meas-  
1270 urements in global and exploration seismology. Geophysics, 83(3):WC53–WC69, doi:  
1271 10.1190/GEO2017-0492.1, 2018.
- 1272 K. U. Schreiber, J. N. Hautmann, A. Velikoseltsev, J. Wassermann, H. Igel, J. Otero, F.  
1273 Vernon, and J.-P. R. Wells. Ring Laser Measurements of Ground Rotations for Seismology.  
1274 Bull. Seismol. Soc. Am., 99(2b):1190–1198, 2009.
- 1275 C. E. Shannon. A mathematical theory of communication. Bell System Tech. J., 27:379–423,  
1276 1948.
- 1277 A. Shuler, G. Ekström, and M. Nettles. Physical mechanisms for vertical-CLVD earthquakes  
1278 at active volcanoes. J. Geophys. Res., 118:1569–1586, 2013.
- 1279 A. T. Sen, S. Cesca, M. Bischoff, T. Meier and T. Dahm. Automated full moment tensor  
1280 inversion of coal mining-induced seismicity. Geophys. J. Int., 195(2):1267–1281, 2013.
- 1281 P. Shi, D. Angus, A. Nowacki, S. Yuan, and Y. Wang. Microseismic full waveform modeling  
1282 in anisotropic media with moment tensor implementation. Surveys in Geophysics, 39:567–  
1283 611, 2018.
- 1284 J. Šílený. Regional moment tensor uncertainty due to mismodeling of the crust.  
1285 Tectonophysics, 383:133–147, 2004.
- 1286 P. G. Silver and T. H. Jordan. Optimal estimation of scalar seismic moment. Geophys. J.  
1287 R. astr. Soc., 70:755–787, 1982.
- 1288 P. Silver. Retrieval of source-extent parameters and the interpretation of corner frequency.  
1289 Bull. seism. Soc. Am., 73:1499–1511, 1983.
- 1290 S. Singh, Y. Capedeville, and H. Igel. Correcting wavefield gradients for the effects of local  
1291 small-scale heterogeneities. Geophys. J. Int., 220:996–1011, 2020.
- 1292 J. Šílený, G. F. Panza, and P. Campus. Waveform inversion for point source moment tensor  
1293 retrieval with variable hypocentral depth and structural model. Geophys. J. Int., 109:259–  
1294 274, 1992.

- 1295 S. A. Sipkin. Interpretation of non-double-double earthquake mechanisms derived from  
1296 moment tensor inversion. J. Geophys. Res., 91:531–547, 1986.
- 1297 D. Sollberger, H. Igel, C. Schmelzbach, P. Edme, D.-J. van Manen, F. Bernauer, S. Yuan,  
1298 J. Wassermann, U. Schreiber und J. O. A. Robertsson. Seismological processing of six  
1299 degree-of-freedom ground-motion data. Sensors, 20:6904, 2020.
- 1300 P. Spudich and J. B. Fletcher. Observation and prediction of dynamic ground strains, tilts,  
1301 and torsions caused by the Mw 6.0 2004 Parkfield, California, earthquake and aftershocks,  
1302 derived from UPSAR array observations. Bull. Seismol. Soc. Am., 98:1898–1914, 2008.
- 1303 P. Spudich and J. B. Fletcher. Short Note: Software for Inference of Dynamic Ground  
1304 Strains and Rotations and Their Errors from Short Baseline Array Observations of Ground  
1305 Motions. Bull. Seismol. Soc. Am., 99(2b):1480–1482, 2009.
- 1306 P. Spudich, L. K. Steck, M. Hellweg, J. B. Fletcher, and L. M. Baker. Transient stresses  
1307 at Parkfield, California, produced by the M 7.4 Landers earthquake of June 28, 1992  
1308 observations from the UPSAR dense seismograph array. J. Geophys. Res., 100:675–690,  
1309 1995.
- 1310 B. Stump and L. Johnson. Higher-degree moment tensors - the importance of source finiteness  
1311 and rupture propagation on seismograms. Geophys. J. R. astr. Soc., 69:721–741, 1982.
- 1312 W. Suryanto, H. Igel, J. Wassermann, A. Cochard, B. Schuberth, D. Vollmer, F. Scherbaum,  
1313 U. Schreiber, and A. Velikoseltsev. First comparison of array-derived rotational ground  
1314 motions with direct ring laser measurements. Bull. Seismol. Soc. Am., 96:2059–2071, 2006.
- 1315 M. Takeo. Ground rotational motions recorded in near-source region of earthquakes.  
1316 Geophys. Res. Let., 25(6):789–792, 1998.
- 1317 W. Tape and C. Tape. A geometric comparison of source-type plots for moment tensors.  
1318 Geophys. J. Int., 190(1):499-510, 2012.
- 1319 A. Tarantola. Inverse problem theory and methods for model parameter estimation, 2nd  
1320 edn. Society for Industrial and Applied Mathematics, Philadelphia, Penn., 2005.
- 1321 C. H. Thurber. Local earthquake tomography: velocities and  $V_p/V_s$  - theory. In: H. M.  
1322 Iyer and K. Hirahara, editors, Seismic Tomography: Theory and Practice, pp. 563–583,  
1323 Chapman and Hall, London, 1993.
- 1324 G. Toyokuni and H. Takenaka. FDM computation of seismic wavefield for an axisymmetric  
1325 Earth with a moment tensor point source. Earth, Planets and Space, 58:e29-e32, 2006.

- 1326 A. Udías. *Principles of Seismology*. Cambridge University Press, ISBN 978-0-521-62478-7,  
1327 1999.
- 1328 A. Udías, R. Madariaga, and E. Buforn. *Source Mechanisms of Earthquakes: Theory and*  
1329 *Practice*. Cambridge University Press, ISBN 978-1-107-04027-4, 2014.
- 1330 M. van Driel, J. Wassermann, M. F. Nader, B. S. A. Schuberth, and H. Igel. Strain rota-  
1331 tion coupling and its implications on the measurement of rotational ground motions. J.  
1332 Seismol., 16(4):657–668, 2012.
- 1333 M. van Driel, J. Wassermann, C. Pelties, A. Schiemenz, and H. Igel. Tilt effects on moment  
1334 tensor inversion in the nearfield of active volcanoes. Geophys. J. Int., 202(3):1711–1721,  
1335 2015.
- 1336 H. Vasyura-Bathke, J. Dettmer, R. Dutta, P. M. Mai, and S. Jónsson. Accounting for  
1337 theory errors with empirical Bayesian noise models in nonlinear centroid moment tensor  
1338 estimation. Geophys. J. Int., 225:1412–1431, 2021.
- 1339 V. Vavryčuk and S. G. Kim. Nonisotropic radiation of the 2013 North Korean nuclear  
1340 explosion. Geophys. Res. Lett., 41:7048-7056, 2014.
- 1341 A. Velikoseltsev, K. U. Schreiber, A. Yankovsky, J.-P. R. Wells, A. Boronachin, and A.  
1342 Tkachenko. On the application of fiber optic gyroscopes for detection of seismic rotations.  
1343 Journal of Seismology, 16:623–637, 2012.
- 1344 J. Wassermann, S. Lehndorfer, H. Igel, and U. Schreiber. Performance test of a commercial  
1345 rotational sensor. Bull. Seismol. Soc. Am., 99:1449–1456, 2009.
- 1346 Y. Yagi and Y. Fukahata. Importance of covariance component in inversion analyses of  
1347 densely sampled observed data: an application to waveform data inversion of seismic  
1348 source processes. Geophys. J. Int., 175(1):215–221, 2008.
- 1349 L. Zhou, W. Zhang, Y. Shen, X. Chen, and J. Zhang. Location and moment tensor inver-  
1350 sion of small earthquakes using 3D Greens functions in models with rugged topography:  
1351 application to the Longmenshan fault zone. Earthquake Science, 29(3):139–151, 2016.