

# 1        **Illuminating a Contorted Slab with a Complex Intraslab** 2        **Rupture Evolution during the 2021 $M_W$ 7.3 East Cape, New** 3        **Zealand Earthquake**

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## 11        **Key Points:**

- 12        • A moment magnitude 7.3 2021 East Cape, New Zealand intraslab earthquake
- 13               comprised multiple rupture episodes with different faulting styles
- 14        • The complex rupture comprises components of shallow trench-normal extension
- 15               and unexpectedly, deep trench-parallel compression in slab
- 16        • The trench-parallel compression likely reflects stress rotation at a buoyancy contrast
- 17               that drives slab contortion

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18 **Abstract**

19 The state-of-stress within subducting oceanic plates controls rupture processes of deep  
20 intraslab earthquakes. However, little is known about how the large-scale plate ge-  
21 ometry and the stress regime relate to the physical nature of the deep-intraslab earth-  
22 quakes. Here we find, by using globally and locally observed seismic records, that the  
23 moment magnitude 7.3 2021 East Cape, New Zealand earthquake was driven by a com-  
24 bination of shallow trench-normal extension and unexpectedly, deep trench-parallel  
25 compression. We find multiple rupture episodes comprising a mixture of reverse, strike-  
26 slip, and normal faulting. Reverse faulting due to the trench-parallel compression is  
27 unexpected given the apparent subduction direction, so we require a differential-buoyancy  
28 driven stress rotation which contorts the slab near the edge of the Hikurangi plateau.  
29 Our finding highlights that buoyant features in subducting plates may cause diverse  
30 rupture behavior of intraslab earthquakes due to the resulting heterogeneous stress  
31 state within slabs.

32 **Plain Language Summary**

33 A key type of tectonic boundary is where two plates collide with one sinking into the  
34 mantle beneath. These subduction zones generate the world's largest earthquakes. Quan-  
35 tifying stress in the subducting plate ("slab") is important because slabs drive the global  
36 plate-tectonic system, and large earthquakes can occur within them. These earthquakes  
37 can cause strong shaking, and, when occurring near cities, can lead to damage. How-  
38 ever, mapping stress is challenging as we cannot directly "see" inside deep slabs. Our  
39 best indications of slab stress come from earthquakes themselves. A magnitude 7.3  
40 earthquake north of New Zealand in 2021 generated a distinct pattern of seismic wave-  
41 forms at seismometers installed worldwide. We used these seismic records to probe  
42 the earthquake, providing a new view of stress in subduction zones. We found the earth-  
43 quake generated both vertical and horizontal motions along faults, driven by compres-  
44 sional and extensional stresses deep within the slab. The compressional part is ori-  
45 ented 90 degrees from the subduction direction, which is opposite to the usual com-  
46 pression in subduction zones, and has not been observed before. This unusual direc-  
47 tion of compression can be explained by subduction of a thickened and buoyant part  
48 of the Pacific plate, known as the Hikurangi plateau.

## 1 Introduction

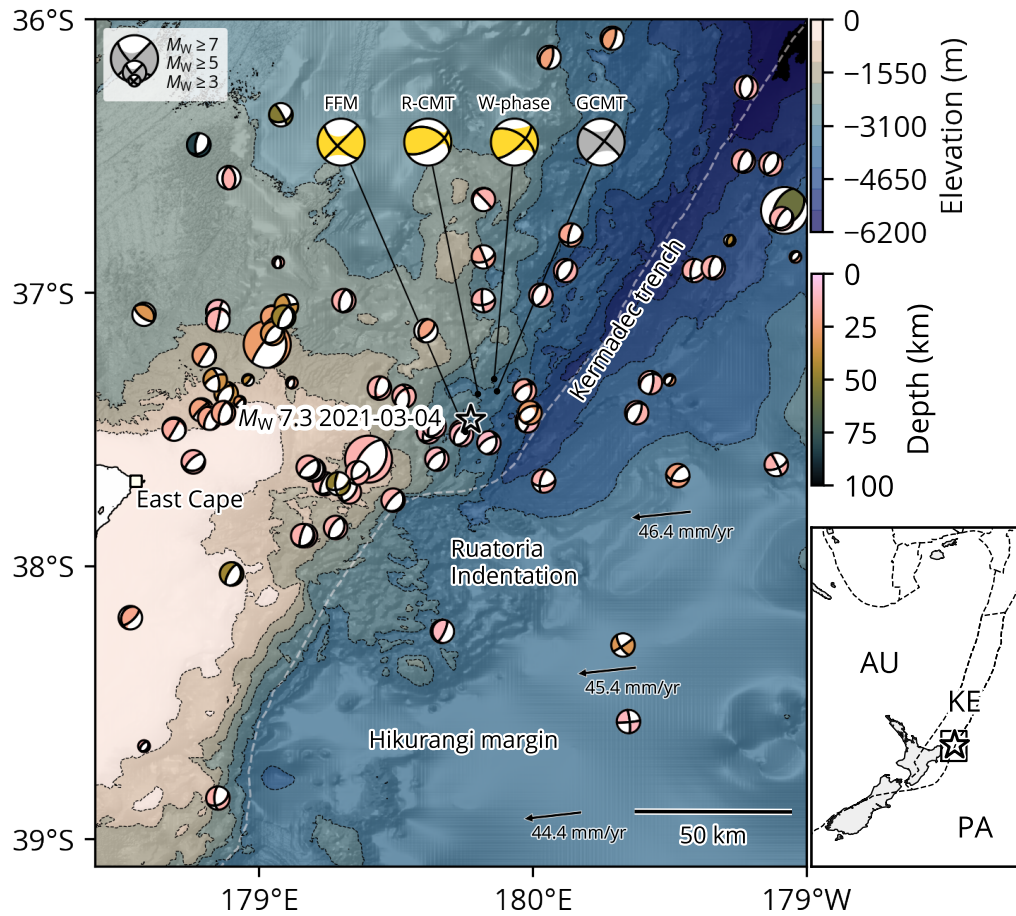
Complex fault configurations and heterogeneous fault conditions, i.e., stress and strength states, govern earthquake rupture development and propagation (Avouac et al., 2014; Floyd et al., 2016; Elliott et al., 2016; Hamling et al., 2017). Such relations can be inferred from the fault geometry and long-term geodetic observations for shallow active faults (Simons et al., 2002; Williams et al., 2013; Elliott et al., 2016; Arai et al., 2016; Hamling et al., 2017; Hayes et al., 2018; Sippl et al., 2018). However, for intraslab earthquakes occurring below  $\sim 50$  km depth, these physical controlling factors are difficult to assess because of challenges to map structure at such depths, and the general lack of seismicity there (Wiens, 2001; Ranero et al., 2005; Page et al., 2016; Dascher-Cousineau et al., 2020; Gomberg & Bodin, 2021). In particular, the internal stress state and its extensional-compression transition regime are often elusive in subducted slabs, although they directly impact intraslab earthquake occurrence and their faulting styles (Astiz et al., 1988; Ammon et al., 2008; Craig et al., 2014; Romeo & Álvarez-Gómez, 2018; Sandiford et al., 2019, 2020; Ye et al., 2021). Thus, imaging the rupture processes of large, deep intraslab earthquakes offers a rare window to investigate the slab configuration, and to understand fault interaction and rupture evolution of these earthquakes, illuminating heterogeneous stress fields.

An intraslab moment magnitude ( $M_W$ ) 7.3 earthquake occurred offshore the East Cape in northern New Zealand on 4th March 2021, which was followed  $\sim 4$  hours later by a series of the  $M_W$  7.4 and  $M_W$  8.1 earthquakes in the Kermadecs ( $\sim 900$  km to the north) (GeoNet, 2021). The  $M_W$  7.3 2021 East Cape earthquake, which is the focus of this paper, may offer insight into the regional slab geometry because of its location and complex rupture process. The 2021 East Cape earthquake locates at the boundary between the southern end of Kermadec trench and the northern end of Hikurangi margin, where the Pacific plate subducts beneath the Australian plate and its convergence decreases and progressively rotates to oblique motion toward the south (Fig. 1) (Collot et al., 1996, 2001; Lewis et al., 1998; Wallace et al., 2009). The earthquake produced observable tsunami signals at tide gauges at the northern coast of New Zealand (GeoNet News, 2021), indicating seafloor deformation due to possible shallow slip. However, the reported centroid depth of the earthquake was  $\sim 50$  km (U.S. Geological Survey Earthquake Hazards Program, 2017; Duputel et al., 2012; Dziewonski et al., 1981; Ekström et al., 2012), and the focal mechanism indicates oblique-thrust motion, with the compressional axis oriented towards the north-south direction (Fig. 1) (U.S. Geological Survey Earthquake Hazards Program, 2017; Duputel et al., 2012; Dziewonski et al., 1981; Ekström et al., 2012). This compressional axis suggests the earthquake

85 was not a simple shallow normal- or reverse-faulting event with the strike angle ori-  
86 ented parallel to the trench axis, as is typically seen in many subduction zones (Fig.  
87 1) (U.S. Geological Survey Earthquake Hazards Program, 2017; Duputel et al., 2012;  
88 Dziewonski et al., 1981; Ekström et al., 2012). All these apparently inconsistent ob-  
89 servations (GeoNet, 2021; GeoNet News, 2021) suggest a complex rupture process of  
90 the East Cape earthquake, possibly involving multiple faults at different depths.

91 Although the subduction-related deformation processes in region south of East  
92 Cape have received a lot of scientific attention (e.g., Eberhart-Phillips & Reyners, 1999;  
93 Reyners et al., 2006; Wallace et al., 2009; Mochizuki et al., 2021), the northern seg-  
94 ment of Hikurangi margin, where it transitions to the Tonga-Kermadec arc, is less well  
95 understood. In the region north of East Cape, sporadic deep seismicity (>80-km depth)  
96 contrasts with abundant shallow seismicity (<50-km depth) (Dziewonski et al., 1981;  
97 Ekström et al., 2012; GeoNet Moment Tensors, 2021; U.S. Geological Survey Earth-  
98 quake Hazards Program, 2017; GeoNet, 2021). Most of the shallow earthquakes are  
99 normal faulting events within the top of the oceanic plate due to trench-normal ex-  
100 tensional stress due to slab bending into the trench (Reyners & McGinty, 1999; Hen-  
101 rrys et al., 2006; Bassett et al., 2010). With these shallow earthquakes, the plate inter-  
102 face and the surrounding materials have been imaged down to ~20 km depth (Davey  
103 et al., 1997; Bell et al., 2010; Bassett et al., 2010, 2016), but the lithospheric structure  
104 of the deep slab is poorly resolved. The apparent complex rupture process of the 2021  
105 East Cape earthquake offers a unique opportunity to image the stress regime associ-  
106 ated with the deeper subduction process.

107 Here we show that the rupture process of the 2021 East Cape earthquake involves  
108 multiple rupture episodes with a mixture of reverse, strike-slip, and normal faulting  
109 mechanisms. These episodes ruptured multiple faults through the subducted oceanic  
110 lithosphere at various depths. The earthquake initiated at 70 km depth with an un-  
111 expected trench-parallel compressional reverse faulting mechanism, and followed by  
112 a slip episode at 30 km depth, which is likely governed by more usual slab-bending  
113 trench-normal down-dip extensional stresses. Such a rupture process reflects a het-  
114 erogeneous stress regime within the subducted slab, in response to a possible geomet-  
115 ric change of the slab in depth due to either the subduction of a seamount associated  
116 with the Ruatoria debris slide (Lewis et al., 1998; Collot et al., 2001; Lewis et al., 2004),  
117 or a sharp change in slab buoyancy at the northern end of the subducting Hikurangi  
118 oceanic plateau.



**Figure 1.** Seismo-tectonic overview of the study region in the north of East Cape, New Zealand. The star shows the relocated hypocenter of the  $M_W$  7.3 2021 East Cape earthquake. Beach balls are the lower-hemisphere stereographic projection of the moment tensor solutions before the 2021 East Cape earthquake, colored by depth (Dziewonski et al., 1981; Ekström et al., 2012). Yellow beach balls are the moment tensor solutions for the 2021 East Cape earthquake obtained by this study (FFM; Finite-fault model, R-CMT; regional centroid moment tensor,  $W$ -phase;  $W$ -phase moment tensor). Background contours display the bathymetry (Mitchell et al., 2012). The arrows show the relative plate motions with the convergence rate of the Pacific plate (PA) towards the fixed Australian plate (AU) (DeMets et al., 2010). The dashed line gives the approximate location of the subduction trench (e.g., Bassett et al., 2010). The right map shows the wider setting of the study region. The rectangle shows the area of the left map. The star marks the epicenter. The dashed lines are the plate boundaries (Bird, 2003) between the Pacific (PA), the Australian (AU) and the Kermadec (KE) plates.

## 119 2 Hypocenter, aftershock relocation, and initial source estimates

120 We first determined the hypocenter of the East Cape earthquake by non-linear  
121 inversion of *P*- and *S*-wave arrival times at regional distances using a 1D velocity model  
122 appropriate for the region north of East Cape (Text S1; Fig. S1). Our relocated epi-  
123 center lies along the trench axis, and is within 10 km of the GeoNet solution (GeoNet,  
124 2021), and ~35 km ENE of the U.S. Geological Survey National Earthquake Informa-  
125 tion Center (USGS-NEIC) solution (U.S. Geological Survey Earthquake Hazards Pro-  
126 gram, 2017) which is consistent with the USGS-NEIC epicenters being systematically  
127 shifted to the down-dip direction in subduction zones (e.g., Ye et al., 2017). Our maximum-  
128 likelihood hypocenter depth is 72 km. Although this hypocenter depth may be thought  
129 to be inherently uncertain due to the sub-optimal station coverage, it provides an ini-  
130 tial hypothesis for testing our results of the more complex rupture configuration later.  
131 If we instead fix our hypocentral depth at the fixed GeoNet/USGS estimates of 10–  
132 12 km (GeoNet, 2021; U.S. Geological Survey Earthquake Hazards Program, 2017),  
133 the root-mean-square (RMS) residual of arrival times at the closest stations (<200 km)  
134 increases by 0.3 s. Although the deeper hypocentral depth led to lower RMS value,  
135 the lower RMS value only represents a better data fit and does not reduce the nonunique-  
136 ness of the inverse problem, hence not equivalent to location uncertainty itself. The  
137 68% confidence ellipsoid of our solution corresponds to an epicentral uncertainty of  
138 0.03° and 0.02° in longitude and latitude, respectively; the depth uncertainty is ±9  
139 km (Fig. S1). However, no depth phases were reported in the International Seismo-  
140 logical Centre Bulletin for this earthquake (International Seismological Centre, 2021),  
141 presumably due to interference with the long source-time function.

142 Next, we located aftershocks of the 2021 East Cape earthquake the same way as  
143 for the mainshock. We focus on events reported by GeoNet (2021) occurring from March  
144 4, 2021 to April 11, 2021 (1 week from the mainshock); (Fig. S2), which yields 622  
145 events with magnitudes ranging from 1.5–6.2. To assure the robustness of the solu-  
146 tions, we remove earthquakes and their arrivals that: (1) were not manually reviewed  
147 by GeoNet (2021), (2) have maximum azimuthal gaps of more than 295 degrees, and  
148 (3) have fewer than at least 10 phase arrivals (Fig. S2). The median of uncertainty of  
149 these aftershocks is 22 km (with 6 km standard deviation), and the median epicen-  
150 tral uncertainties are 0.05° and 0.08° in latitude and longitude, respectively. The af-  
151 tershocks suffer large depth uncertainty due to their location outside of the regional  
152 network, which hampers an unambiguous determination of the total rupture area. How-  
153 ever, we broadly identify both shallow (<30 km) and deep (>50 km) aftershocks, and

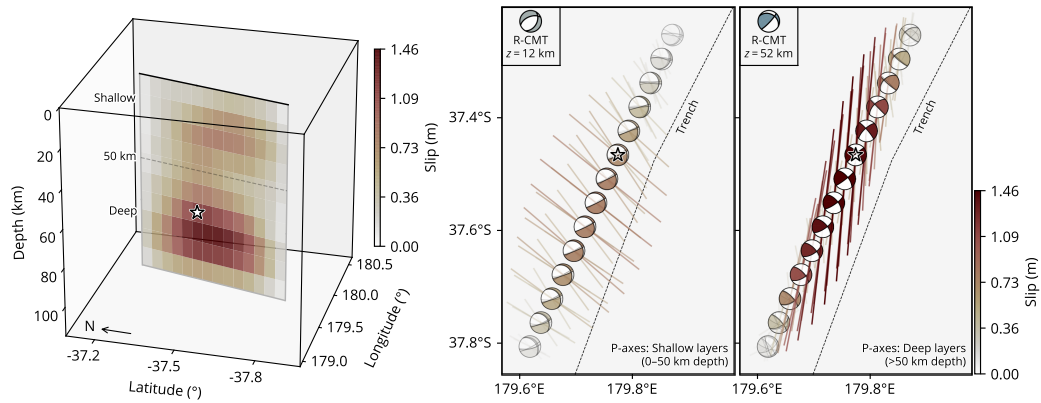
154 such a depth distribution could be explained by our preferred rupture model of both  
155 shallow and deep ruptures in the downgoing lithosphere.

156 Using a Bayesian bootstrapping centroid-moment tensor (CMT) inversion of low-  
157 frequency (2.0–8.5 mHz) teleseismic waveforms for a single-point source (Text S2),  
158 we find a mean centroid depth of 53 km, with a centroid position shifted 18 km NNE  
159 of our relocated epicenter, and time shift from the origin time of +5 s (Fig. S3). How-  
160 ever, the CMT solution has a large non-double couple component (DC=15%). Such  
161 a low DC component is likely caused by geometric complexities of the earthquake that  
162 may involve multiple faults within the subducted Pacific plate near the Hikurangi trench.

163 Finally, to test the hypothesised rupture complexity, we investigated the rupture  
164 process of the earthquake with a multi-point centroid moment tensor (R-CMT) inver-  
165 sion method using regional seismic waveforms (Text S3; Figs. S4 to S6). The approach  
166 can resolve the first-order features of a complex rupture with few assumptions. The  
167 later part of the <25 s period surface waves on the horizontal components at stations  
168 within ~400 km epicentral distance are poorly fit (Figs. S5 and S6) due to basin res-  
169 onance effects (Kaneko et al., 2019). We find that the East Cape event can be best ex-  
170 plained by two sub-events, with the largest sub-event ( $M_W \sim 7.3$ ) at 50–70 km depth  
171 occurring 8–10 s after the origin time, and the second sub-event at 7–12 km depth  
172 and 6–8 s after the first sub-event. The second sub-event significantly increases wave-  
173 form variance reduction by 16–23%. The first sub-event has an oblique-reverse mech-  
174 anism. Conversely, the second sub-event has a normal faulting mechanism. Overall,  
175 our R-CMT solution corroborates a complex rupture scenario involving at least two  
176 sub-events separated by ~40 km in depth: one in the top of the Pacific plate, the other  
177 deep within the slab.

### 178 **3 Intermittent complex multiple rupture episodes with various focal mechanisms**

179 To better understand the rupture development, we applied a finite-fault potency-  
180 density inversion method (Shimizu et al., 2020) to estimate the rupture evolution of  
181 the 2021 East Cape earthquake (Text S4). The method can flexibly accommodate mul-  
182 tiple faults with different geometries rupturing during the same event, which are in-  
183 ferred from the spatiotemporal distribution of five-basis double-couple components  
184 of the potency-density tensors (Kikuchi & Kanamori, 1991; Ampuero & Dahlen, 2005).  
185 In our inversion formulation, the model parameters are objectively determined by min-  
186 imizing Akaike’s Bayesian Information Criterion (ABIC) (Akaike, 1980; Yabuki & Matsu’ura,  
187 1992), and we do not adopt non-negative constraints for slip vectors. Such a proce-  
188 dure can effectively prevent over- or under-smoothing of the source model as theo-



**Figure 2.** Static slip distribution. The left panel shows the total slip distribution in a 3D view, viewed from the south-west. The star represents our hypocenter. The black line shows the top of the model fault. The right panels show the map view of the slip distribution from shallow (<50 km) and deep depths ( $\geq 50$  km), with beach balls representing double-couple components of the moment tensor solution (Fig. S7), and corresponding P-axis azimuths (bars scaled by slip). The moment tensor is calculated by integrating the slip-rate function for each basis component of moment tensor with respect to time at each sub-fault. The P-axis azimuth is extracted from the resultant double-couple solution for each sub-fault, which is represented by a lower-hemisphere stereographic projection. We show the beach balls from the slip patch corresponding to the fault element with the maximum slip within each given depth range. The inset shows the corresponding R-CMT solutions annotated with their depths ( $z$ ). The dashed line is the subduction trench (Bird, 2003).



189 retically shown in Fukuda and Johnson (2008). Particularly, we flexibly solve the po-  
190 tency density in a finite-fault domain instead of regularizing the model with possi-  
191 ble inaccurate subjective assumptions (e.g., positivity constraints, and the prescribed  
192 fault geometry). The method has proven effective at resolving complex earthquake rup-  
193 tures in a variety of tectonic settings (Shimizu et al., 2020, 2021; Okuwaki et al., 2020;  
194 Hicks et al., 2020; Tadapansawut et al., 2021; Yamashita et al., 2021). In practice, we  
195 parametrize a 2D vertical model domain along a  $200^\circ$  strike extending from 7- to 107-  
196 km depth with a total of 140 source elements (sub-faults) (Fig. 2). This parameter-  
197 ization is guided by the observed cluster of the near-trench-parallel aftershocks (Fig.  
198 S2). Although it is difficult to resolve the absolute locations of slip surfaces due to in-  
199 sufficient spatial resolution of the teleseismic body waves used in our finite-fault mod-  
200 eling, in the 2D model domain, we solve the fault-normal and shear-slip vectors at each  
201 source element, which are independent of the model domain geometry. In other words,  
202 we solve for distributed sources in the model domain that may have any type of fault-  
203 ing mechanism required by the data. The model domain therefore allows multiple fault-  
204 ing episodes of the earthquake and does not necessarily indicate a single fault plane  
205 cutting through the lithosphere in a continuous rupture. Our preferred slip model sug-  
206 gests that the earthquake initiated at 72 km depth (Fig. S12), which yields variance  
207 reduction (VR) of waveform fitting 74%, corroborating the relocated hypocenter and  
208 the R-CMT solution. We test possible model domain geometries that only cover some  
209 specific depths, but the finite-fault models of such model setups cannot adequately  
210 explain the observed waveforms (Fig. S12). We note that a 3-D parameterization would  
211 have been ideal for imaging this earthquake, but it is currently infeasible due to com-  
212 putational limits. To further test our model, we also use the same dataset and model  
213 domain to invert a finite-fault model but restrict the subfaults to have the same strike  
214 and dip (Fig. S14). The results of our test show that in comparison to our preferred  
215 finite-fault model, fixing the focal mechanisms to the prescribed model plane has a  
216 much lower VR of 25%. This exercise highlights the importance of permitting a com-  
217 plex rupture scenario when modeling this earthquake and shows that an overly sim-  
218 plified model would fail to explain even the first few seconds the direct  $P$  waves (for  
219 example, first 5 s  $P$  waves of XMAS and CRZF stations). These early  $P$  waves are un-  
220 likely to be affected by water phases given the source depth. The water multiples should  
221 be incoherent with azimuth, given the variation in water depth around the source re-  
222 gion. Such incoherent phases, that are not represented in the Green's functions used  
223 in our inversion, cannot translate into complexity in source time function. We also  
224 note that using a 1D velocity model for Green's functions without considering the sim-  
225 plification effects may introduce erroneous biases. Further, even using 3D velocity mod-

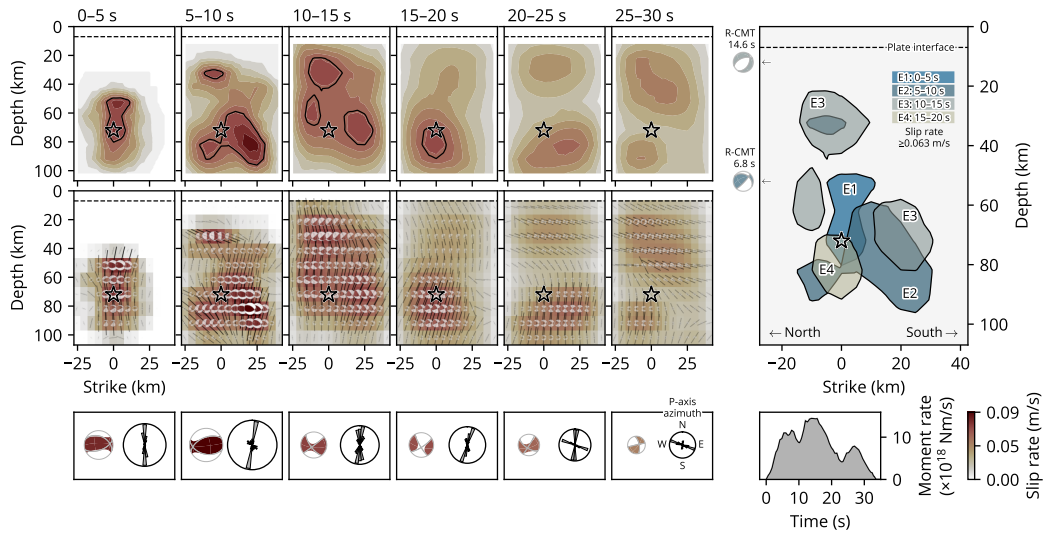
226 els to compute the Green's functions, the fidelity of the velocity models remains a source  
227 of uncertainty. For example, the local 3D velocity model (e.g., Eberhart-Phillips et al.,  
228 2010, 2020) may suffer uncertainties for the area near the 2021 event because of a lack  
229 of offshore stations for tomographic inversions. Our approach can address such as-  
230 sumption induced errors. We explicitly consider these effects by introducing an un-  
231 certainty term of the Green's function into the data covariance matrix in the inversion  
232 formulation (Yagi & Fukahata, 2011). Such an approach has proven effective in reduc-  
233 ing solution errors that are due to model oversimplifications (Yagi & Fukahata, 2011;  
234 Minson et al., 2013; Duputel et al., 2014; Ragon et al., 2018).

235 Our preferred finite-fault model suggests that most slip occurred at 55 to 100  
236 km depth and  $\sim 15$  km south of the hypocenter, releasing 69% of the total moment  
237 (Fig. 2). Another patch of slip is observed at 20–40 km depth, much shallower than  
238 the hypocentral depth and comprising 31% of the total moment. The deeper slip is  
239 dominated by an oblique strike-slip faulting mechanism. The shallow slip involves  
240 a mixture of normal and strike-slip faulting mechanisms. The finite-fault model leads  
241 to a moment estimate of  $1.7 \times 10^{20}$  Nm ( $M_W$  7.4). We evaluated the robustness and  
242 uncertainty of the finite-fault model by performing synthetic tests (Fig. S13). The re-  
243 sult shows that both the slip pattern and the variation of faulting mechanism in the  
244 model domain are well reproduced. We will discuss in detail in a later section, but  
245 the focal mechanisms of the shallow and deep domains agree with the R-CMT solu-  
246 tions (Fig. 2), which show shallow normal faulting with the likely fault plane orient-  
247 ing along the trench axis and deep reverse faulting with the compressional axis ori-  
248 enting along the trench axis.

249 The rupture process of the East Cape earthquake involved deep- and shallow-  
250 slip corresponding to different faulting types, which may be expressed as a few bursts  
251 of rupture episodes (e.g., E1 to E4). The earthquake initiated as a reverse faulting with  
252 a strike-slip component for the first 5 s (E1, Fig. 3). The rupture then propagated to-  
253 wards the south at 60–100 km depth, releasing 20% of the total moment and lasting  
254 for about 5 s (E2, Fig. 3). This episode was dominated by thrust faulting. The third  
255 episode (E3) simultaneously might have ruptured several fault patches from 5 s to 15  
256 s, including a shallow patch at  $\sim 25$  km depth and a deep patch  $\sim 70$  km depth (Fig.  
257 3). The shallow part of E3 ruptured with a normal faulting mechanism, while the deep  
258 patch of E3 had a strike-slip mechanism. The last major episode (E4) ruptured a fault  
259 patch beneath the hypocenter for about 5 s with a dominant strike slip focal mech-  
260 anism (Fig. 3). We note that E4 is unique as its dominant mechanism suggests a strike-  
261 slip faulting style, whilst the E1 and E2 show reverse mechanisms (Fig. 3). The remain-

262 ing 26% of the total moment was released by slips at both shallow and deep regions,  
263 and the earthquake lasted for about  $\sim 30$  s. Most of the seismic moment was released  
264 within  $\sim 20$  s in our finite-fault solution, consistent with the half-duration of the GCMT  
265 solution (10 s) (Dziewonski et al., 1981; Ekström et al., 2012), which seems typical as  
266 for other similar sized earthquakes (e.g., Duputel et al., 2013).

267 The four rupture episodes appear compact in size and seem to involve multi-  
268 ple faulting mechanisms at different depths. Given the varying focal mechanisms, the  
269 chaotic episodes likely do not result from the same continuous rupture front, but more  
270 likely represent segmented slip on different faults that may have interacted with, and  
271 triggered, each other.



**Figure 3.** Slip evolution. The left panels show the cross sections of the spatio-temporal distribution of slip rate and the resultant moment-rate tensor solution, given in 5 s long windows. The moment tensor is calculated by integrating the slip-rate function for each basis component of moment tensor with respect to the corresponding time window at each sub-fault. The star represents the hypocenter. The dashed line is the top of the subducting plate (Bassett et al., 2010). The black contour highlights faster slip rates ( $\geq 0.063$  m/s;  $\geq 70\%$  of maximum slip rate). The centroid moment tensor for each time window is shown at the bottom, together with the rose diagram of P-axis azimuths weighted by slip rate. The centroid moment tensor is calculated by integrating the slip-rate function for each basis component of moment tensor of all the sub-faults with respect to the corresponding time window and then constructing a final moment tensor from the integrations by spatially integrating the moment tensors from all the subfaults. All the beach balls of the moment-tensor solution are represented as a lower-hemisphere stereographic projection, not rotated according to the model geometry, but in map view. The right panel summarizes the slip-rate evolution. The color for each episode (E1 to E4) corresponds to the time window. The minor slip-rate events within the final two time windows (20–30 s) are not slipping fast enough to plot a contour on the right panel. R-CMT solutions are also shown at the corresponding depths, with their time shift given relative to the hypocentral time. The right-bottom inset is the total moment-rate function from the finite-fault model.

272 Our preferred finite-fault solution suggests a non-uniform moment release of the  
273 earthquake, which could be due to spatiotemporally disconnected rupture episodes  
274 (Figs. 3 and S15). Alternatively, the results could also represent two sub-events with  
275 longer durations. In this case, the deep sub-event initiates at the hypocenter and prop-  
276 agates toward south at  $<2.5$  km/s until 15 s from the origin. The higher slip rate, seen  
277 during 15–20 s located around the hypocenter, can be a result of faster  $<5$  km/s back-  
278 propagation from south to north. The shallow sub-event can be rather a continuous  
279 rupture propagating from deep (50 km) to shallow (30 km) depths during 0–15 s at  
280 a speed of  $<2$  km/s.

#### 281 **4 Intralab stress rotation in depth**

282 The source process of the 2021 East Cape earthquake could be characterized as  
283 multiple episodes rupturing from deep to shallow within the subducted slab (Fig. 2).  
284 The multi-fault rupture may have caused the small double-couple percentage in the  
285 moment tensor solution for the 2021 East Cape earthquake (e.g., 32% in the GCMT  
286 solution), which is particularly evident for the deeper rupture domain in our finite-  
287 fault solution (Figs. 3 and S7). Such a rupture process would involve a mixture of re-  
288 verse and strike-slip slips, which is akin to the 2000  $M_W$  7.9 Enggano intralab earth-  
289 quake that ruptured multiple faults at a similar depth leading to a 33% double-couple  
290 component in its GCMT solution (Abercrombie et al., 2003). For the shallow slip episode  
291 of the 2021 East Cape earthquake, its focal mechanism shows a mixture of the nor-  
292 mal faulting with a strike-slip component. The general trend of the aftershock dis-  
293 tribution (Fig. S2) suggests that the fault plane striking toward the northeast-southwest  
294 direction likely ruptured during the later phase of the earthquake. Although the lim-  
295 ited station azimuth coverage could cause an artificially elongated aftershock distri-  
296 bution, the major axis of the uncertainty ellipse of the mainshock relocation, which  
297 shares the similar station coverage, is oriented W-E rather than SW-NE (Fig. S1). It  
298 is noteworthy that some aftershocks (U.S. Geological Survey Earthquake Hazards Pro-  
299 gram, 2017; Dziewonski et al., 1981; Ekström et al., 2012; GeoNet Moment Tensors,  
300 2021) share similar focal mechanisms to the shallow rupture episode (Fig. S8). Given  
301 the near-trench location of the East Cape earthquake, there is some ambiguity regard-  
302 ing the exact faulting configuration. However, the aftershock distribution indicates  
303 that the shallow slip episode likely ruptured a normal fault within the downgoing plate.  
304 Additionally, in the absence of clear shallow slip with a reverse-faulting mechanism,  
305 this normal faulting episode likely caused the observed tsunami.

306 The varying focal-mechanisms of the four slip episodes (E1–E4) show the com-  
307 pressional stress orientation (the P-axis orientation) of the East Cape earthquake ro-  
308 tated from the northwest-southeast direction to the north-south direction with a gap  
309 in slip and approximate stress transition depth at  $\sim 50$  km (Figs. 2 and 3). The nor-  
310 mal faulting of the shallow slip episodes striking toward the northeast-southwest di-  
311 rection agrees well with the extensional stress in the upper part of the subducted plate  
312 due to the expected plate bending and pulling process (e.g., Astiz et al., 1988; Am-  
313 mon et al., 2008; Craig et al., 2014; Romeo & Álvarez-Gómez, 2018; Sandiford et al.,  
314 2020). Such a bending process seems to have caused most of the background seismic-  
315 ity in this region, which has predominant normal faulting mechanisms (Fig. 1; Reyn-  
316 ers & McGinty, 1999; Bassett et al., 2010). If the deep slip at 50–100-km depth dur-  
317 ing the East Cape earthquake was driven by the same bending-related process, we would  
318 expect a trench-normal P-axis orientation, which is typical for similar events at other  
319 subduction zones, where deep trench-parallel reverse faulting is observed (e.g., Okada  
320 & Hasegawa, 2003; Ohta et al., 2011; Ye et al., 2012; Todd & Lay, 2013; Ye et al., 2021).  
321 However, the deep slip patches of the East Cape earthquake (E1 and E2, and R-CMT  
322 Sub-event 1) have oblique-thrusting mechanisms, resulting in a trench-parallel com-  
323 pression. This perplexing P-axis orientation indicates an additional regional factor that  
324 may have modulated the rupture process of the East Cape earthquake.

325 The interactivity between various faulting episodes is a puzzling part of the East  
326 Cape earthquake. Subduction zone earthquakes may involve multiple disconnected  
327 subevents with different faulting types that can trigger and interact with each other  
328 (Ammon et al., 2008; Lay et al., 2013; Hicks & Rietbrock, 2015; Lay et al., 2020). For  
329 the East Cape earthquake, our preferred finite-fault model does not show a contin-  
330 uous rupturing path from the deep to shallow episodes (Figs. 2 and 3). The shallow  
331 rupture E3 is separated by  $\sim 40$  km from the deep episodes and started  $\sim 5$  s later (Fig.  
332 3), suggesting an apparent rupture speed of  $\sim 8$  km/s if the rupture was continuous.  
333 Such a rupture speed would be close to the local  $P$ -wave speed (Table S1), which is  
334 unlikely. More likely, slip episodes E1 and E2 triggered the following shallow episode  
335 E3 due to either the static and/or dynamic stress change from the initial deep rup-  
336 ture. A stress transition or strength contrast within the slab can work as an inhom-  
337 ogeneous barrier (Das & Aki, 1977; Aki, 1979) to smooth propagation from deep to shal-  
338 low rupture during the East Cape earthquake. Therefore, the rupture evolution of the  
339 earthquake may have developed as discontinuous jumps by means of stress trigger-  
340 ing (Miyazawa & Mori, 2005; Sleep & Ma, 2008; Fischer, Sammis, et al., 2008; Fischer,  
341 Peng, & Sammis, 2008) across the apparent stress/strength barrier between the deep  
342 and shallow rupture areas.

343 Large intraplate earthquakes within the downgoing plate in subduction zones  
344 are typically caused either by the down-dip bending and unbending of the slab (e.g.,  
345 Astiz et al., 1988; Craig et al., 2014; Sandiford et al., 2020), the reactivation of ma-  
346 jor oceanic fabrics, including fracture zones (e.g., Abercrombie et al., 2003; Meng et  
347 al., 2012; Yue et al., 2012), or the tearing of the slab (e.g., Tanioka et al., 1995). How-  
348 ever, the orientation and rupture complexity of the 2021 East Cape event deviates from  
349 these typical events. Two events with apparently similar deep trench-parallel com-  
350 pression in the slab include 2000  $M_W$  7.9 Enggano and 2009  $M_W$  7.6 Padang earth-  
351 quakes, offshore Sumatra (Abercrombie et al., 2003; Wiseman et al., 2012). However,  
352 these events likely ruptured pre-existing fabrics in the downgoing plate (Abercrombie  
353 et al., 2003), such as fracture zones (Wiseman et al., 2012). Both earthquakes poten-  
354 tially represent the continuation of the diffuse deformation within the Wharton basin,  
355 and both consistently ruptured orthogonal fabrics toward the top of the downgoing  
356 plate both updip and downdip from the trench, where highly oblique convergence in-  
357 herently causes a rotated state of the stress in the slab. In contrast, the 2021 East Cape  
358 earthquake, which occurred deeper beneath the top of the slab, does not align with  
359 the expected oceanic fabric, and is not obviously part of a wider, plate-scale, defor-  
360 mation field, where there is no obvious oblique convergence nor are fracture zones  
361 of an orientation consistent with the observed mechanisms subducted (Fig. 1). Instead,  
362 the rupture processes may represent a unique case, highlighting a different type of  
363 stress transition within the subducted slab.

## 364 **5 A contorted slab structure due to slab buoyancy variations?**

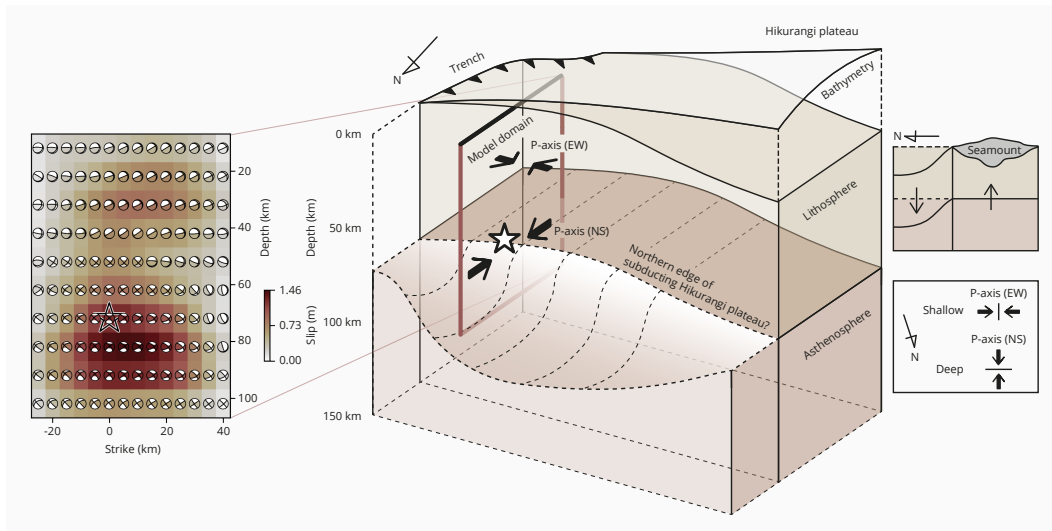
365 A key question is why does this part of the Hikurangi subduction zone exhibit  
366 an atypical stress regime, as manifested in the rupture process of the 2021 East Cape  
367 earthquake? Slab models of this region (Hayes, 2018; Hayes et al., 2018; Williams et  
368 al., 2013) show a homogeneous planar structure (Fig. S9) which would be expected  
369 to lead to a trench-normal compression in the deeper part of the slab. However, these  
370 slab models are poorly constrained near the East Cape earthquake, largely because of  
371 a lack of plate interface thrust earthquakes in the region (Fig. 1). The rupture pro-  
372 cess of the East Cape earthquake therefore potentially offers new insight into the lo-  
373 cal slab structure.

374 One possible explanation is that the slab surface warps downward north of the  
375 hypocenter, forming a depression at the plate interface (Fig. 4). The warping is likely  
376 a response to the buoyancy gradients in the subducting plate, which allows the less  
377 buoyant parts of the slab to sink more rapidly than the buoyant parts. The internal

378 stress field from such a slab topology would be complex, leading to strong 3-D stress  
379 rotations around the localized downwarp in a manner as shown in the 2021 East Cape  
380 earthquake (Fig. 2). One contribution to the buoyancy gradients might be the sub-  
381 duction of a large-scale seamount. About 30 km south-west from the epicenter, the  
382 Quaternary Ruatoria seamount was obliquely subducted at the margin (Lewis et al.,  
383 1998; Collot et al., 2001; Lewis et al., 2004), forming the characteristic bathymetry of  
384 the Ruatoria indentation (Fig. 1). The Ruatoria seamount could deflect and bend the  
385 slab, causing the intraslab stress state to rotate from trench-normal compression to  
386 trench-parallel compression across the hypocentral area. Numerical models of slab  
387 stress in the presence of subducted buoyant features in the oceanic plate support such  
388 a stress rotation and lateral spreading mechanism (e.g., Mason et al., 2010). Trench-  
389 parallel compression has also been seen in other parts of the Hikurangi subduction  
390 zone, for example, Reyners and McGinty (1999) and McGinty et al. (2000) observed  
391 some strike-slip seismicity with a trench-parallel compression component, which are  
392 close to the trench axis offshore of the Raukumara Peninsula. Although these earth-  
393 quakes beneath the Raukumara Peninsula should reflect the stress state once the plate  
394 is already subducted, rather than at the trench region which is where the 2021 East  
395 Cape earthquake illuminates, it is possible they reflect stress heterogeneity due to per-  
396 vasive seamount subduction along the northern Hikurangi subduction zone (Barker  
397 et al., 2009).

398 An alternative explanation may arise from the location of the East Cape earth-  
399 quake with respect to the transition between the Kermadec trench and Hikurangi mar-  
400 gin, marked by the edge of the Hikurangi plateau, which is represented by a clear bathy-  
401 metric scarp running along its northern boundary (Davy & Collot, 2000). This tran-  
402 sition from the subduction of normal oceanic lithosphere to the north, to the subduc-  
403 tion of the thickened oceanic crust associated with the igneous Hikurangi plateau likely  
404 leads to a pronounced, short-wavelength flexural warping at the plateaus edge. The  
405 superposition of this N-S flexural stress field in conjunction with the down-dip bend-  
406 ing stress field could have produced a complex pattern that varies at short-length scales  
407 within the subducted slab. Such a heterogeneous stress field may have regulated the  
408 rupture process of the East Cape earthquake. The sporadic background seismicity north  
409 of the 2021 source region (Fig. S16) might also result from such a complex stress field.  
410 It is noteworthy that in 2001, ~80 km northeast of the 2021 event, there was a  $M_W$   
411 7.1 earthquake deep in the Pacific plate (~60 km depth) showing a reverse faulting  
412 mechanism with its P-axis oriented perpendicular to the Kermadec trench (Fig. S8),  
413 which was likely driven by conventional trench-normal down-dip compression. This





**Figure 4.** Cartoon interpretation of the inferred slab geometry and stress regimes based on our observations of the 2021 East Cape earthquake. The star shows the hypocenter. The arrow shows the compressional axis. The left panel shows the cross-section of our finite-fault solution (Fig. S7). The upper right panel is a cross-section with the arrows showing the relative force applied in the slab. The lower right panel shows the compressional axes in a top view.

414 earthquake suggests that flexural warping due to the subducting Hikurangi plateau  
 415 does not extend this far to the north.

416 Whilst there have been many studies on the impact of subducting buoyant fea-  
 417 tures on subduction megathrust coupling and interface seismogenesis (e.g., Wang &  
 418 Bilek, 2011; Nishikawa & Ide, 2014), there have been far fewer studies that have con-  
 419 sidered their impact on intraslab seismicity. The rarity of deep intraslab earthquakes  
 420 in the northern Hikurangi subduction zone makes it difficult to distinguish between  
 421 the seamount and plateau models of stress rotation. However, it is also possible that  
 422 both features play a concurrent role, with stress rotations superimposed from both.

423

## 424 **6 Conclusions**

425 We determined the rupture geometry of the 2021  $M_W$  7.3 East Cape, New Zealand  
426 earthquake using a novel finite-fault inversion technique. Our method does not re-  
427 quire a-priori knowledge of the fault geometry and can flexibly resolve complex fault-  
428 ing styles in large earthquakes. Therefore, it can uniquely illuminate the heterogeneous  
429 stress state near the earthquake. We show that the East Cape earthquake has at least  
430 four rupture episodes and likely ruptured multiple faults with various faulting styles.  
431 We find distinct rupture episodes within the shallow ( $\sim 30$  km) and deep ( $\sim 70$  km)  
432 parts of the subducted oceanic plate, with distinct mechanisms of normal and a mix-  
433 ture of strike-slip and reverse faulting, respectively. The deep and shallow episodes  
434 likely reflect components of a flexural stress field, separated by a low-stress barrier  
435 in the middle of the plate. The rotation of P-axes suggests that the intraplate stress  
436 state is locally rotated from trench-normal compression to trench-parallel compres-  
437 sion. Such a stress rotation in depth requires the slab geometry to change sharply, which  
438 may have been induced by a subducted seamount or the additional buoyancy of the  
439 Hikurangi plateau. Our study suggests that understanding the generation of interme-  
440 diate and deep intraslab seismicity requires a detailed treatment of localized varia-  
441 tions in slab geometry caused by the subduction of heterogeneous features, such as  
442 ocean plateaus and seamounts.

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## 461 **Open Research**

462 All the materials presented in this paper are archived and available at [https://doi.org/](https://doi.org/10.5281/zenodo.5593739)  
463 [10.5281/zenodo.5593739](https://doi.org/10.5281/zenodo.5593739). All seismic data were downloaded through the IRIS Wilber  
464 3 system ([https://ds.iris.edu/wilber3/find\\_event](https://ds.iris.edu/wilber3/find_event)) or IRIS Web Services ([https://service](https://service.iris.edu)  
465 [.iris.edu](https://service.iris.edu)), including the following seismic networks: the GT (Global Telemetered Seis-  
466 mograph Network (USAF/USGS); Albuquerque Seismological Laboratory (ASL)/USGS,  
467 1993); the IC (New China Digital Seismograph Network; Albuquerque Seismological  
468 Laboratory (ASL)/USGS, 1992); the IU (Global Seismograph Network (GSN - IRIS/USGS);  
469 Albuquerque Seismological Laboratory (ASL)/USGS, 1988); the GE (GEOFON Seis-  
470 mic Network; GEOFON Data Centre, 1993); the AU (Australian National Seismograph  
471 Network (ANSN); Geoscience Australia (GA), 1994); the HK (Hong Kong Seismograph  
472 Network; Hong Kong Observatory, 2009); the G (GEOSCOPE; Institut De Physique  
473 Du Globe De Paris (IPGP) & Ecole Et Observatoire Des Sciences De La Terre De Stras-  
474 bourg (EOST), 1982); the NZ (New Zealand National Seismograph Network; Institute  
475 of Geological & Nuclear Sciences Ltd (GNS New Zealand), 1988; Petersen et al., 2011);  
476 the AI (Antarctic Seismographic Argentinean Italian Network - OGS; Istituto Nazionale  
477 Di Oceanografia E Di Geofisica Sperimentale, 1992); the II (IRIS/IDA Seismic Network;

478 Scripps Institution Of Oceanography, 1986); the C (Chilean National Seismic Network;  
 479 Universidad de Chile Dept de Geofisica (DGF UChile Chile), 1991); the PS (Pacific21  
 480 (ERI/STA); University of Tokyo Earthquake Research Institute (Todai ERI Japan), 1989).  
 481 We used ObsPy (Beyreuther et al., 2010, <https://doi.org/10.5281/zenodo.165135>), Py-  
 482 rocko (The Pyrocko Developers, 2017, <https://pyrocko.org/>), matplotlib (Hunter, 2007,  
 483 <https://doi.org/10.5281/zenodo.592536>), Generic Mapping Tools (Wessel & Luis, 2017,  
 484 <https://doi.org/10.5281/zenodo.3407865>); and Scientific colour maps (Cramer, 2018;  
 485 Cramer et al., 2020, <https://doi.org/10.5281/zenodo.1243862>) for data processing and  
 486 visualisation. The NonLinLoc software used for hypocenter relocation is available at  
 487 <http://alomax.free.fr/nlloc/>. The Grond software (Heimann et al., 2018) used for W-  
 488 phase CMT inversion is available at <https://pyrocko.org/grond/docs/current/>. The  
 489 ISOLA software used for R-CMT inversion is available at [http://seismo.geology.upatras](http://seismo.geology.upatras.gr/isola/)  
 490 [.gr/isola/](http://seismo.geology.upatras.gr/isola/).

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