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1 **SALT WELDING DURING CANOPY ADVANCE AND SHORTENING IN THE**
2 **GREEN CANYON AREA, NORTHERN GULF OF MEXICO**

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20 **Abstract**

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22 Welds form due to the tectonically-induced thinning and/or dissolution of salt, with their
23 composition and completeness thought to at least partly reflect their structural position within
24 the salt-tectonic system. Despite their importance as seals or migration pathways for
25 accumulations of hydrocarbons and CO₂, we have relatively few examples of drilled subsurface
26 welds; such examples would allow us to improve our understanding of the processes and
27 products of welding, and to test analytical models of the underlying mechanics. In this study
28 we integrate 3D seismic reflection and borehole data from the Green Canyon Area of the
29 northern Gulf of Mexico, USA to characterize the geophysical and geological expression of a
30 tertiary weld, as well as its broader salt-tectonic context. These data show although it appears
31 *complete* on seismic reflection data, the weld contains 124 ft (c. 38 m) of pure halite. This
32 thickness is consistent with the predictions of analytical models, and with observations from
33 other natural examples of subsurface welds. Our observations also support a model whereby
34 compositional fractionation of salt occurs as the salt-tectonic system evolves; in this model,

less mobile and/or denser units are typically stranded within the deeper, autochthonous level, trapped in primary welds, or stranded near the basal root of diapirs, whereas less viscous and/or less dense units form the cores of these diapirs and, potentially, genetically related allochthonous sheets and canopies. We also show that shearing of the weld during downslope translation of the overlying minibasin did *not* lead to complete welding.

Introduction

Salt welds form in response to the removal of salt by tectonically-induced thinning and/or dissolution (e.g., Jackson and Cramez, 1989; Rowan, 2004; Wagner & Jackson, 2011; Jackson et al., 2014; 2018; Jackson & Hudec, 2017). We can identify three main types of welds depending on the structural level (i.e., autochthonous or allochthonous) at which they occur in a salt-tectonic system; (i) *primary*; (ii) *secondary*; and (iii) *tertiary* (Fig. 1) (Jackson and Cramez, 1989). We can further classify these as *complete*, *incomplete* or *discontinuous* based on the continuity and degree of welding (see Wagner & Jackson, 2011; see also fig. 1b in Jackson et al., 2014). The type of rock left within an apparent weld (or the incomplete parts of a discontinuous weld) principally reflects the rheological variations between the mobile salt (herein defined as halite) and the less mobile, related lithologies (e.g., anhydrites, carbonates and/or clastics; Kupfer, 1968), and the position of the weld within the overall salt-tectonic system (i.e., primary, secondary, or tertiary; Fig. 1). For example, primary welds may be halite-poor because this high-viscosity, relatively mobile lithology is preferentially expelled (or dissolved) before lower-viscosity, less mobile lithologies. In contrast, tertiary welds formed at structurally shallower levels in the salt-tectonic system may contain only halite, with less mobile components left stranded at depth (Fig. 1).

Regardless of structural level and weld composition, analytical models show that viscous flow alone is rarely sufficient to produce a complete weld (Wagner and Jackson, 2011). In this case, up to 50 m of salt may remain within the weld, a prediction supported by the very few studies of natural subsurface salt welds (Jackson et al., 2014; 2018). Wagner and Jackson (2011) argue that the remaining salt must be removed by dissolution. However, they also propose that viscous flow with a shear component, perhaps due to the horizontal translation of a suprasalt minibasin onto and along base-salt relief, may promote the complete removal of salt from a weld (Fig. 2). To date, however, relatively simple models linking salt weld composition and

structural position, and analytical model-based predictions of weld thickness, have only rarely been directly tested by data from natural examples of exposed or subsurface salt welds (Jackson et al., 2014; 2018).

Understanding the composition and thickness of salt welds is critically important to the hydrocarbon industry (Rowan, 2004; Rowan et al., 2012) and those wishing to store CO₂ in subsalt reservoirs. Halite typically has very low permeability and can therefore act as a regional or local seal for accumulations of hydrocarbons or CO₂. However, welds may act as conduits for gas and fluid migration if they are relatively thin and/or composed of non-halite lithologies (e.g., sandstone or carbonate; Jackson et al., 2014). Understanding when a weld forms in relation to the timing of hydrocarbon migration is also important, given welding needs to occur before subsalt source rock expulsion to charge a suprasalt trap (Peel, 2014). In the case of the Gulf of Mexico, the focus of this study, hydrocarbons are found within both subsalt (i.e., primary) and suprasalt (i.e., secondary) minibasins (e.g., K2/K2-North; McBride et al., 1998; and Marco Polo field; Mount et al., 2006), meaning it is also important to understand the role of salt welds in controlling hydrocarbon migration within this particular region. At present, however, there is no clear way to predict if a weld is complete or incomplete due to the lack of well penetrations, limited seismic resolution, and the poor preservation of some evaporite rock-types (e.g., halite) in the field (e.g., La Popa Basin, Mexico; Rowan et al., 2012; Flinders Range, Australia; Dyson and Rowan, 2004; Hearon et al., 2014; onshore Texas, US; Willis et al., 2001).

In this study, we integrate 3D seismic reflection and borehole data from the Green Canyon area of the northern Gulf of Mexico, USA to characterize the geophysical and geological expression of an apparent tertiary salt weld (Fig. 3). The weld underlies an c. 8.5 km thick secondary minibasin that subsided into allochthonous salt forming part of the Sigsbee Canopy. Although the weld appears *complete* on seismic reflection data, our borehole-based analysis shows 124 ft (c. 38 m) of pure halite is preserved (i.e., the weld is *incomplete*, at least at the borehole location, and may be best-classified as *discontinuous*). This thickness is consistent with the analytical model-based predictions of Wagner & Jackson (2011), and observations from other natural examples of subsurface salt welds (Jackson et al., 2014; 2018). By studying the structural evolution of the overlying minibasin and flanking salt structures, we also place the weld within its broader salt-tectonic framework, showing that shearing of the weld during

downslope translation of the overlying minibasin (see Fig. 1) did *not* lead to complete welding, at least in the location penetrated by the borehole.

Geological Setting

The northern Gulf of Mexico initially formed in the Late Triassic-Early Jurassic in response to rifting between the North American and African-South American plates (e.g., Pindell and Dewey, 1982; Kneller and Johnson, 2011; Hudec et al., 2013a). Terrestrial clastic-dominated syn-rift sediments were overlain by a thick, extensive, evaporite-dominated succession known as the Louann Salt, which is approximately dated as Middle to Upper Jurassic (e.g., Hazzard et al., 1947; Humphris, 1978; Salvador, 1987; Kneller and Johnson, 2011; Hudec et al., 2013b). Subsequent gravity-driven flow of these evaporites during the Cenozoic played a primary role in the structural evolution of the Gulf of Mexico and the distribution of overlying sediments. After subsidence of primary minibasins into the autochthonous salt layer, salt flowed out of diapiric feeders and extruded onto and advanced across the seabed, coalescing to form an allochthonous salt layer known as the Sigsbee Canopy (e.g., Diegel et al., 1995; Peel et al., 1995; Rowan, 1995; Pilcher et al., 2011). As this canopy advanced basinward during the Oligocene to Miocene, numerous secondary minibasins subsided into and were transported broadly south/south-eastwards on top of the advancing allochthonous body (see Fig. 2a) (e.g., Jackson et al., 2010; Jackson and Hudec, 2017). Previous studies have suggested that the secondary minibasins were carried tens of kilometres basinward before welding (Fig. 2; see also fig. 20 in Jackson et al., 2010; Duffy et al., 2020).

The salt weld of interest in this study is a tertiary weld located below a secondary minibasin that has subsided into the Sigsbee Canopy and welded to the primary minibasin below. This minibasin is situated in the Green Canyon Area of the northern Gulf of Mexico, USA and close to the frontal edge of the advancing canopy (the Sigsbee Escarpment), whose expression can be clearly seen in the present bathymetry (Fig. 3). In a salt tectonic context the studied minibasin and underlying weld lie within the ‘amalgamated salt-stock-canopy province’ of Pilcher et al. (2011), the upper part of which is characterised by a network of minibasins surrounded by canopy-sourced diapirs and related welds (Fig. 1b).

Data and methods

Seismic reflection data and seismic-stratigraphic framework

We use a 3D pre-stack depth migrated (PSDM) seismic reflection volume that covers c. 150 km² (12.5 x 12 km), and which has an inline and crossline spacing of 20 m (Figs 3 and 4). The volume is cropped at a depth of 23,760 ft (7,200 m). Seismic data quality is very good within the interval of interest, with the weld and encasing strata being very well-imaged (Fig. 5). We estimate the vertical seismic resolution within the depth interval at which the weld is developed (c. 20,000 ft; c. 6.1 km) to be c. 62 ft (c. 20 m) (resolution is approximated by the assumption that it equals $\lambda/4$, where $\lambda=80$ m at 20,000 ft). We display the seismic data using US normal polarity (i.e., a downward increase in acoustic impedance is represented by a negative reflection coefficient, which is a white reflection event in our images; Brown, 2011) (Fig. 5).

We mapped eight key seismic horizons across our 3D seismic reflection dataset; this included top and base salt, and six suprasalt seismic horizons that bound six suprasalt seismic units (SU1-6; Figs 4a-c, 5 and 6). The six suprasalt horizons are defined based on seismic-stratigraphic terminations, such as onlaps and erosional truncations (Fig. 5). Thickness maps and stratigraphic relationships are used to determine the tectonic evolution of the minibasin (Figs 4, 5 and 7). The ages of the horizons, which span the Miocene to Recent, are directly constrained (i.e., top SU3 and SU6) or estimated (i.e., top SU1-2 and SU4-5) from biostratigraphic data obtained from a borehole penetrating the central, thickest part of the minibasin and its underlying weld (Figs 4b-d, 5e and 6). An age-constrained seismic-stratigraphic framework is important because it enables us to determine the timing and duration of the major salt-tectonic events, including the likely timing of welding.

Borehole data

We use data from a borehole that was drilled in a water depth of c. 4,200 ft (1,300 m) to a total depth of 30,803 ft (9,389 m). Borehole-related datasets include well-logs, and mudlogging, biostratigraphic, and operational reports. Well-logs cover the interval 4,235-21,422 ft (1,290-6,529 m), which includes the studied weld (Fig. 6). Well-logs include gamma ray (gAPI), sonic ($\mu\text{s}/\text{ft}$), density (g/cm^3), neutron (ft^3/ft^3), caliper (in) and deep resistivity (ohm-m) (Fig. 4). We used data from these well-logs to determine weld lithology and thickness, which helped

understand its sealing potential. These logs also helped constrain the lithology of material above and below the weld, which was critical when considering its seismic expression at and lateral to the borehole location. Biostratigraphic samples span 10,920-22,300 ft (3,328-6,797 m) and were examined by the borehole operator and partners at 30 ft (9.1 m) increments. Because these data are confidential, we report here only the key geological age boundaries (Fig. 6).

Salt-tectonic structure

Base-allochthonous salt and base-salt relief

Allochthonous salt overlies a reflective, clastic-dominated succession, the uppermost part of which is Tortonian-to-earliest Messinian (i.e., Late Miocene; Figs 5 and 6). The base of the allochthonous salt is rugose, consisting of a prominent, NW-trending, steeply SW-dipping ramp (c. 30°) that is at least 5000 ft km (1,524 m) long and defines relief of at least 2000 ft (609 m) (Figs 4a, 4d, 5a and 5d). North of this ramp, base-salt dips gently (c. 3°) to the WNW, although low-relief rugosity of a few hundred metres is also locally observed in this area (Figs 4a, and 5a-b). Where the base-salt reflection lies beneath the seismic reflection volume, such as in the west of the study area, we infer the presence of a diapiric feeder that provided salt to the Sigsbee Canopy (Pilcher et al., 2011; Jackson et al., 2018) (Figs 4a, 4d and 5e). As we will discuss below, base-salt relief, in particular the NW-trending ramp and the local structural high it delineates, are important controls on the structural development of the suprasalt minibasin.

Allochthonous salt

Diapiric allochthonous salt, which is up to 21724 ft (6,621 m) thick, almost fully encircles the studied minibasin (Figs 4b-d and 5). A discontinuous weld is present beneath the minibasin; this weld comprises areas of (apparently) complete welding and small, elongate, wall-like pockets of salt that are up to 3750 ft (1,143 m) thick and 2000 ft wide (Figs 4b and 5). Some of these pockets occur in the footwall of salt-detached, intra-minibasin thrusts (Figs 5a and 5b) or at the base of sub-vertical welds (Fig. 5d) (see below).

The suprasalt minibasin contains clastics that are Serravallian (Middle Miocene) to Holocene (Fig. 6). It is important to note that the strata directly above the weld are older (Serravallian) than the strata directly underlying it (Messinian) (c. 20300 ft; Fig. 6); we discuss the significance of this observation below. The geometry of the top salt surface (Fig. 4), and thickness changes in its lowermost part (Fig. 4c), indicate the studied minibasin is, at least in its lower part, composed of at least seven smaller, broadly bowl-shaped sub-basins (labelled A-G; Fig. 4d; see also Fig. 5). These sub-basins are separated by salt-detached thrusts that have pockets of salt preserved in their footwall (see above; Fig. 5a and b) or sub-vertical welds (Figs 3b, 3d and 5d). These thrusts show highly variable strikes (i.e., N-S to ENE-WSW) and dips (i.e. W to SSE), but we note that they restricted to the northern side of the base-salt ramp and its related structural high (Fig. 5d). All of the salt-detached thrusts are flanked by hangingwall anticlines and footwall synclines, and are overlain by unbreached monoclines, which we interpret as fault-propagation folds (Fig. 5a-c). Strata within the lower sub-basins *and* within the overlying, larger, singular minibasin, thin towards and onlap onto flanking diapirs (most clearly seen in Fig. 5d-e; see also 5a-b). We provide a more detailed description of the minibasins seismic-stratigraphic patterns below.

Supra-salt minibasin seismic stratigraphy and evolution

Vertical changes in seismic-stratigraphic patterns and stratal thickness (Figs 5 and 6) suggest the studied minibasin initially comprised at least seven sub-basins and underwent six main stages of structural development. We describe and interpret these sub-basins and related stages below (see Fig. 10), using the age-constrained seismic-stratigraphic framework (Fig. 6) to constrain their timing and duration.

Stage 1 (Serravallian-Messinian)

The thickness map of SU1 shows at least seven distinct sub-basins (A-F and H; Fig. 7a). The sub-basins contain broadly bowl- to locally wedge-shaped seismic packages (Fig. 5). Strata within these packages onlap the large, flanking diapirs and the pockets of salt locally preserved beneath the minibasin (Fig. 5).

Based on these observations we interpret that the minibasin was initially comprised of seven smaller minibasins that independently subsided symmetrically and sub-vertically (where containing bowl-shaped packages), or slightly asymmetrically (where containing wedge-shaped packages) into the allochthonous salt canopy during a phase of passive diapirism (Fig. 10A and B) (e.g., Rowan & Weimer, 1999; Jackson et al., 2019). Although hard to prove at this particular locality, we suggest that these minibasins were located updip (i.e., north) of their present location and were translating basinward (i.e., broadly southward) above the advancing salt canopy, consistent with other minibasins documented in this area (Fig. 10A and B) (see Jackson et al., 2010; see also Duffy et al., 2020 and Fernandez et al., 2020).

Stage 2 (Messinian)

In contrast to SU1, which defined seven sub-basins, depocentres within SU2 define only four sub-basins; a relatively large, bowl-shaped depocentre centred on the borehole (an amalgamation of sub-basins A, D and E) and two smaller sub-basins located to the north (sub-basin B, and sub-basins C and F, which are now linked; Fig. 7b). Strata within these sub-basins still onlap the large diapirs flanking the host minibasins although they do not onlap intra-minibasin diapirs, which were buried by strata within the upper part of SU1 (Fig. 5). Instead, SU2 thins across, and the larger minibasin is segmented by, fault-related folds above the upper tips of intra-minibasin thrusts forming the boundary between, for example, sub-basins B and A (Fig. 5a), B and C (Fig. 5b), C and D (Fig. 5b), and A and E (Fig. 5a).

These seismic-stratigraphic relationships indicate that the intra-minibasin thrusts became active, and thus that the causal shortening initiated, in the Messinian (see also Figs 7b and 10C). We suggest that the low-relief diapirs that previously separated sub-basins defined by SU1 were squeezed and the sub-basins collided to form steeply dipping thrust welds, with small pockets of the salt beneath these welds representing remnant diapir pedestals (Figs 5d-e and 10C). The origin of the intra-minibasin shortening is not clear, although we speculate this could reflect the onset of welding of the suprasalt minibasin as it translated onto, and was buttressed against, the broadly, gently NW-dipping base-salt ramp (Fig. 10C) (e.g., Duffy et al., 2020).

Stage 3 (Messinian-Piacenzian)

SU3 lies conformably above SU2 but is capped by a major angular unconformity that truncates underlying reflections (Fig. 5). Although influenced by the capping erosional surface (Fig. 5), thickness patterns within SU3 clearly differ to those observed in SU1 and SU2. First, only two main depocentres are defined; (i) a broadly NE-trending depocentre north of the borehole spanning sub-basins C, F, and the northern part of A; and (ii) a sub-circular depocentre spanning sub-basins B and G (Figs 5 and 7c). Second, these thickness patterns are less obviously controlled by intra-minibasin thrusts or diapirs, although stratigraphic thinning above and onlap onto thrust-related folds are locally observed (Fig. 5a-c).

These observations suggest that shortening-related thrusting continued into the Piacenzian, implying welding-related deformation was ongoing (Fig. 10C). Welding-related shortening and tilting, combined with an influx of sediment across the evolving canopy, may have led to the development of the erosional unconformity capping SU3 (not shown in Fig. 10).

Stage 4 (Gelasian-Pleistocene)

SU4 displays overall thickening towards the NW. However, in the northern part of the study area we observe two sub-circular depocentres (Fig. 7D), related to the filling of erosional relief developed along the top Pliocene erosional unconformity (see Fig. 5B). Most critically, however, SU4 shows no thickness changes with respect to the thrust-related folds, indicating the minibasin was less segmented, and was subsiding as a single, large depocentre by the Gelasian (Figs 5, 7D and 10D). This also suggests that welding-induced, intra-minibasin shortening has ceased by the Gelasian. SU4 also differs to SU2 and SU3 in that it is dominated by broadly layer- to weakly wedge-shaped seismic packages that overstep and cap the large, minibasin-flanking diapirs (Fig. 5).

The dominance of areal extensive, layer-shaped, diapir-capping packages indicates passive diapirism may also have ceased at this time, possibly due to weld-induced termination of salt supply to the flanking diapirs (see Rowan and Weimer, 1989; Jackson et al., 2019). However, the shift in depocentre toward the NW, combined with the weakly wedge-shaped seismic packages observed in similarly trending seismic profiles (Fig. 5a and 5b), suggests that the minibasin was tilting broadly north-westwards at this time (Fig. 10D). Given we infer that the minibasin had welded by this time, we suggest minibasin tilting was triggered by differential active rise of flanking diapirs during ongoing shortening (Fig. 10D) (Fernandez et al. 2020).

Stage 5 (Late Pleistocene-Holocene?)

SU5 comprises broadly tabular packages of sub-parallel reflections that locally thin towards flanking diapirs at the minibasin margins, but which invariably cap these structures (Figs 5 and 7e). At this shallow structural level, we observe salt-detached thrusts at the minibasin margins (Fig. 5c-d). These relatively low-displacement (<50 m) thrusts are best-developed in the NE of the minibasin, where they dip NE and strike NW-SE.

The dominance of layer-shaped seismic packages suggests minibasin subsidence had ceased and aggradation above the now-welded depocentres continued (Rowan and Weimer, 1998; Jackson et al., 2019). However, thinning of strata within SU5 towards flanking diapirs suggests these structures continued to actively rise, possibly in response to ongoing shortening within the canopy. This shortening may have also been accommodated by the development of shallow-level thrusts (Figs 5a, 5b and 10E).

Stage 6 (Late Pleistocene-Holocene?)

SU6 defines a NW-trending depocentre characterised by broadly layer-shaped seismic packages that cap and show only moderate thickness changes within respect to minibasin-flanking diapirs (Figs 5 and 7f). Based on this seismic-stratigraphic architecture, which is crudely like that observed in SU5, we suggest the latest Pleistocene to Holocene was characterised by only minor salt tectonics (e.g., minibasin subsidence and/or diapir rise), and dominated by deep-water sediment aggradation (Fig. 10E).

Salt weld thickness and composition

The salt-bearing interval penetrated by the borehole (i.e., the weld) is characterised by anomalously low gamma ray values (c. 24 gAPI), high density (2.4-2.95 g/cm³), low neutron porosity (-0.5-0.2 pu.), high resistivity (c. 10³), low sonic slowness (c. 68 s/ft) (i.e., it has a high p-wave velocity) (Figs 8 and 9). We note there is some scatter in these values, particularly in terms of density and sonic slowness (i.e., velocity), an observation we discuss further below. Based on these criteria, we confidently picked, stratigraphically rather than seismically, top salt at 20255 ft (6174 m) and base-salt at 20379 ft (6212 m), interpreting that the (apparent)

weld is 124 ft (38 m) thick and dominated by halite (Fig. 9) (Rider and Kennedy, 2011; Jackson et al., 2014, 2018). Mudlogging reports are consistent with our well-log-based interpretation, describing only halite from this approximate depth interval. We also, however, note that the halite is: (i) denser (by c. 0.4-1 g/cm³) than ideal values (Rider and Kennedy, 2011) and values documented from elsewhere in the northern Gulf of Mexico for this rock type (Jackson et al., 2018); and (ii) acoustically faster (by sonic slowness values of c. 20-40 us/ft) than values documented from elsewhere in the northern Gulf of Mexico for this rock type (Jackson et al., 2018). We explore the potential reasons for this further in the Discussion.

INTERPRETATION AND DISCUSSION

Age and salt-tectonic context of the salt weld

Previous regional studies suggest canopy emplacement in this area of the northern Gulf of Mexico occurred during the Middle–Late Miocene in response to regional shortening and the related extrusion of salt from diapiric feeders (Peel et al. 1995). Using 3D seismic reflection and borehole data, Jackson et al. (2018) interpret that canopy emplacement in the Atwater Valley area, c. 100 km to the ENE of our study area, was in fact considerably later, sometime in the Early Pleistocene. Our observation that the weld (and laterally equivalent salt structures forming the canopy) studied here is underlain and overlain by late Miocene (Messinian) and middle Miocene (Serravallian) strata, respectively, suggests canopy emplacement in the middle to late Miocene, consistent with the age originally proposed by Peel et al. (1995). Given that we use seismic reflection data of a broadly similar vintage and, we infer, quality to that of Jackson et al. (2018), we propose that the difference in *local* canopy emplacement reflects *regional* diachroneity in the timing of emplacement, rather than dataset quality (i.e., borehole data are of sufficient resolution to constrain the age of sub- and suprasalt rocks and, thus, the timing of canopy emplacement; see Jackson et al. 2018). More specifically, given that the canopy was fed by squeezed diapirs (i.e., feeders) during regional shortening, this diachroneity might reflect systematic changes in the timing of shortening and related squeezing. For example, feeders in the Atwater Valley area of Jackson et al. (2018) may have been shortened and expelled salt later than elsewhere, meaning the canopy advanced into this area only after a period of latest Miocene and Pliocene sediment aggradation. An alternative interpretation is that shortening was regionally synchronous, but that locally higher sediment accumulation

rates in the Atwater Valley area meant that salt expulsion from feeders and break-out into a canopy was delayed by aggrading sediment in flanking minibasins.

The age inversion observed in the borehole (i.e., Serravallian strata overlying *younger* Messinian across an incomplete salt weld) likely reflects the overall salt-tectonic setting and evolution of the study area, in particular the downslope translation of the minibasin within an evolving canopy and subsequent welding. We interpret that deep-water sedimentation within the developing minibasin commenced in the Serravallian when the structure was located some unconstrained distance upslope to the north. Ahead of the advancing canopy and secondary minibasin, younger sediment (i.e., Tortonian and the earliest Messinian) continued aggrading within primary minibasins. As a result, an age inversion occurred when the secondary minibasin translated onto, and eventually welded to, the underlying primary minibasin (e.g., Duffy et al., 2020; Fernandez et al., 2020).

Canopy dynamics and related welding also controlled minibasin structural style by driving early thrusting and folding (Fig. 10C). Contractional structures such as these are common on salt-detached slopes, forming when minibasins collide due to; (i) an unwelded, mobile minibasin colliding with a welded, immobile minibasin (i.e., it becomes “obstructed”; *sensu* Duffy et al., 2020); or (ii) two welded, yet still mobile minibasins colliding due to ongoing shortening (Jackson et al., 2008; Duffy et al., 2021). In the former case, the contractional structures most commonly develop during the latter stages of minibasin development, once minibasins become thick enough to touch down on the base-salt surface, thus welding and forming an obstruction. This is typically associated with the squeezing and eventual secondary welding of intervening diapirs, which readily explains the formation of the relatively young thrusts and related secondary welds at relatively shallow levels on the NE margin of the studied minibasin (Fig. 5C, D). However, the relatively old contractional structures observed at the base of the minibasin show that here the collision of sub-basins occurred during the very early stages of minibasin development, when the depocentre was relatively thin (i.e., c. 30% of its eventual total thickness; Fig. 10C) and presumably surrounded by thick salt (Figs 4C and 5). In this case, we might expect that shortening would have been absorbed by the relatively weak salt rather than the relatively strong minibasin (Rowan and Vendeville, 2006; Duffy et al., 2021). We tentatively suggest that early shortening was induced by obstruction of the southwards translating sub-basins by the NE-dipping base-salt ramp. As the most seaward sub-basin migrated southwards it became grounded against the ramp and welded to the shallowing base-salt surface (i.e., sub-basin E; Fig. 4D). Unable to translate

further, it was then collided into by still-translating, updip sub-basins (i.e., sub-basins A and D; Fig. 4D).

Geological, geophysical, and petrophysical expression of welds and implications for the process of welding

Although they are readily imaged in seismic reflection data from a range of salt-tectonic settings, there are relatively few published examples of salt welds penetrated by boreholes. Such data are required to determine the completeness, composition, and petrophysical expression of the weld and encasing wall rocks. Jackson et al. (2014) show that a primary weld in the Santos Basin, offshore Brazil is *incomplete* (*sensu* Wagner, 2010; Wagner and Jackson, 2011), containing 22 m of carbonate, anhydrite, sandstone, and marl, with halite absent. A tertiary weld in the Atwater Valley area of the northern Gulf of Mexico is also incomplete; however, rather than being halite-poor, this c. 24 m thick weld is halite-dominated and contains a 4 m-thick mudstone inclusion (Jackson et al., 2018). Although data remain sparse, current observations of salt composition and thickness are consistent with a model whereby compositional fractionation of salt occurs as the salt-tectonic system evolves, i.e. more viscous, less mobile and/or denser units are typically stranded within the deeper, autochthonous level, trapped in primary welds, or stranded near the basal root of diapirs, whereas less viscous and/or less dense units form the cores of these diapirs and, potentially, genetically related allochthonous sheets and canopies (Fig. 1) (cf. ‘differential purification by movement’: Kupfer 1968; see also Wagner & Jackson 2011; Jackson et al. 2014; 2018). Current data are also consistent with the predictions of analytical and numerical models presented by Wagner & Jackson (2011), which suggest natural salt welds formed by viscous flow alone may contain anywhere from $\ll 1$ m to up to c. 50 m of remnant salt. Viscous flow may therefore be a good analytical approximation of the physical processes occurring during salt thinning and welding; viscous flow alone is unlikely, however, to result in complete evacuation of salt.

Our borehole data from the northern Gulf of Mexico allow us to further test and refine these related models for salt welding during the development of multi-level salt-tectonic systems. Our data indicate that the seismically imaged tertiary weld is *incomplete* (i.e., it is an “apparent weld”; *sensu* Jackson et al., 2014), being defined by c. 124 ft (38 m) of remnant evaporitic rocks (i.e., halite). This thickness is slightly more than previously documented in the Santos Basin (Jackson et al., 2014) and elsewhere in the northern Gulf of Mexico (Jackson et al., 2018), but is consistent with the analytical model-based prediction of welding via viscous

flow (Wagner and Jackson, 2011). The halite has a very clear expression in well-log data, being characterised by relatively very low radioactivity (as expressed in gamma-ray log data), and high density, velocity (i.e., low acoustic slowness), and resistivity. However, as noted above; (i) our cross-plot of halite density and velocity displays some scatter (Fig. 9); and (ii) the halite is denser than ideal values for this rock type (Rider and Kennedy, 2011) and values documented from natural halite penetrated elsewhere in the northern Gulf of Mexico for this rock type (Jackson et al., 2018), and acoustically faster than values documented from elsewhere in the northern Gulf of Mexico (Jackson et al., 2018). The former observation might suggest the halite could be slightly impure due to the presence of disseminated grains or thin laminae of denser and acoustically faster (e.g., carbonate), or less dense and acoustically slower (e.g., siliciclastic) material; we infer that this effect, if present, is only very minor, given that the halite retains very different petrophysical properties to that of encasing clastic rocks (Fig. 9). Determining why the halite is denser and acoustically faster is more challenging, but it might reflect the fact that different logging tools and drilling approaches (e.g., drilling fluids) were used to acquire the data in the different boreholes.

Notwithstanding its slightly unusual petrophysical expression, the occurrence of only halite within the tertiary weld is consistent with a model of rheologically-controlled compositional fractionation, i.e., the less mobile units (e.g., clastic, carbonate, or anhydrite rocks) remain at the deeper, autochthonous level, trapped in primary welds, whereas more mobile units (e.g., halite, potash salts) flow into diapiric salt structures and canopies, thus dominating salt composition at the allochthonous level (Fig. 1). As such, when allochthonous salt welds, we suggest these secondary and tertiary welds will be relatively enriched in halite and possibly potash salts, as opposed to halite-poor primary welds. This is the case in the example presented here, although we note that the compositional variability encountered in salt welds will also likely reflect several factors such as compositional variations in the autochthonous salt or preferential dissolution of more soluble salts (e.g., halite and bittern salts).

Why is there salt left in the weld?

Two main processes control the evacuation and removal of salt in a weld; dissolution and solid-state flow (Jackson and Hudec, 2017). We do not think dissolution played a role in salt thinning and/or was able to fully remove the remaining salt from the weld due to the weld being buried >1 km (around 3,300 ft); at such depths sluggish water flow are anticipated, limiting

dissolution, even if a large amount of NaCl-undersaturated water is present (Jackson and Hudec, 2017). Welding by solid-state flow is more plausible, although Wagner and Jackson (2011) use analytical solutions to show that viscous flow alone cannot fully remove salt from a weld due to boundary drag along the perfectly flat and parallel, upper and lower contacts. Because of this process, they suggest that 1-50 m (3–165 ft) of residual salt will remain in a weld, a range consistent with the thickness of salt observed here (38 m), and in welds in the Santos Basin, Brazil (22 m; Jackson et al., 2014) and elsewhere in the northern Gulf of Mexico (24 m; Jackson et al., 2018).

Borehole and field data demonstrate complete welding is at least locally possible along incomplete welds (Rowan et al., 2012; Jackson and Hudec, 2017). Based on analytical models, Wagner and Jackson (2011) hypothesize that shear-thinning could lead to the complete removal of salt from a weld. Our interpreted structural evolution based on seismic-stratigraphic analysis and borehole data suggests that the basal weld of the studied minibasin has been sheared. More specifically, the presence of squeezed diapirs, and thrusts and related secondary welds in the lower parts of the minibasin suggests horizontal shortening, which we infer occurred after the minibasin had welded onto an upslope-dipping, base-salt ramp. Despite this, the weld is incomplete, suggesting that more shearing is required to fully remove all the salt from a weld.

Implications for hydrocarbon exploration and the storage of CO₂

Salt has relatively low permeability and can therefore form a high-quality seal to underlying or laterally adjacent accumulations of hydrocarbons or CO₂ (e.g., Warren, 2016). The precise sealing properties of salt are at least partly dictated by its thickness and composition, i.e., all other things being equal, a relatively thin (<10 m), incomplete, halite-dominated tertiary weld may be a better seal than a substantially thicker primary weld dominated by carbonates and clastics. The differential purification by movement-model outlined above might, with further testing by borehole data, be refined and may ultimately be predictive.

Conclusions

We used 3D seismic reflection and borehole data from the Green Canyon Area of the northern Gulf of Mexico, USA to characterize the geophysical and geological expression, and the regional salt-tectonic structural context of a tertiary salt weld. The weld is developed at the base of a secondary minibasin that likely translated seaward in allochthonous salt of the Sigsbee

Canopy, before colliding with and welding to a base-salt ramp. Welding and the related collision of otherwise mobile minibasins led to at least two phases of shortening, both of which were associated with the development of salt-detached thrusts and folds, and secondary welds. The seaward translation and eventual welding of the minibasin also led to an across-weld stratigraphic repetition, with Serravallian strata overlying younger Messinian strata. Our petrophysical analysis of borehole data showed that although it appears *complete* on seismic reflection data, and although it may have undergone some shortening-related shearing, the basal weld is in fact *incomplete*, containing 124 ft (c. 38 m) of pure halite. This thickness is consistent with observations from other natural examples of subsurface welds, and with the predictions of analytical models of welding by viscous flow. Our observations support a model in which compositional fractionation of salt occurs as the salt-tectonic system evolves; in this model, less mobile and/or denser units are typically stranded within the deeper, autochthonous level, trapped in primary welds, or stranded near the basal root of diapirs, whereas less viscous and/or less dense units form the cores of these diapirs and, potentially, genetically related allochthonous sheets and canopies. More studies of drilled subsurface welds are required to assess the processes (i.e., mechanics) and products of salt welding, and the role they play in the trapping of hydrocarbons and the storage of CO₂.

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Figures captions

Fig. 1. Schematic cross section (not to scale) illustrating the three main types of salt weld that can develop in salt-tectonic basins. This classification is based on the structural level at which salt evacuation occurs (i.e. deep, intermediate, and shallow), the attitude of the weld (i.e. sub-horizontal or sub-vertical), and the origin of the weld (i.e. thinning of autochthonous or allochthonous salt, or squeezing and closure of a diapir) (modified from Jackson et al., 2014; see also Jackson and Cramez, 1989). The pie-charts schematically illustrate the inferred proportion of three main evaporite-related rock types that may be encountered in a primary, secondary, and tertiary welds. Note the upwards increase in halite and relative enrichment in other rock types due to “differential purification by movement” (*sensu* Kupfer, 1968). See text, and Jackson et al. (2014 and 2018) for full discussion.

Fig. 2. (a) Schematic cross section showing a minibasin translating along the top of an extruding salt sheet (Time 1). As the minibasin translates, its base impinges on a subsalt ramp, forming a fault weld (Time 2). This natural geometry minimizes the limitations of boundary drag and promotes nearly complete welding by viscous flow alone (modified from Wagner and Jackson, 2011). (b) Schematic diagram highlighting the formation of a complete fault weld, which forms if shear displacement occurs before, during or after salt evacuation. Concepts and terminology after Jackson and Cramez (1989), Hossack and McGuinness (1990), and Rowan et al. (1999), Wagner and Jackson (2011). Modified from Wagner and Jackson (2011).

Fig. 3. Seafloor bathymetry map of the northern Gulf of Mexico and the Sigsbee canopy. The study area is located on the mid-to-lower slope. Bathymetry map sourced from the Bureau of Ocean Energy Management (<https://marinecadastre.gov/nationalviewer>). Black lines show offshore protraction areas. Inset shows broader geographical location of bathymetry data.

Fig. 4. Maps illustrating the salt-tectonic structure of the study area. (a) base-salt seismic horizon depth-map; (b) base-salt seismic horizon depth-map; (c) salt isopach (thickness) map; and (d) interpretative sketch map showing the spatial relationship of the key salt-tectonic structures identified in (a), (b), and (c). The locations of the seismic profiles in Fig. 5 are shown. Note the thrust and related secondary weld in the NE of the study area are at a shallower structural level than those found elsewhere; see Fig. 5c and d.

Fig. 5. Interpreted seismic reflection profiles showing the salt-tectonic structure of the study area, and the structural context and seismic expression of the studied salt weld and its encasing

strata. The locations of the profiles are shown in Fig. 4, and the geological ages of the sub- and suprasalt seismic-stratigraphic units (SUs) are shown in Fig. 6. Uninterpreted seismic reflection profiles are available in Supplementary Material.

Fig. 6. Simplified stratigraphic column showing key well-log information and the petrophysical expression of the main, biostratigraphically age-constrained seismic-stratigraphic units (SUs) penetrated in the borehole. The location of Fig. 8 is shown. Circled numbers on the left of the column show the borehole diameter.

Fig. 7. Isochron (thickness) maps showing temporal changes in minibasin depocentre location because of canopy advance, salt welding, and minibasin shortening and tilting. (a) SU1 – Serravallian-Messinian; (b) SU2 – Messinian; (c) SU3 – Messinian-Piacenzian; (d) SU4 – Gelasian-Pleistocene; (e) SU5 – Late Pleistocene-Holocene(?); and (f) SU6 – Late Pleistocene-Holocene(?). The position of the base-salt ramp (e.g., Fig. 5a; see also text for description and interpretation) is indicated in (a)-(c). The key intra-minibasin, sub-basin-bounding structures inferred to be active during the deposition of the Serravallian-Messinian (SU1), Messinian (SU2), and Messinian-Piacenzian (SU3) are shown; the approximate positions of these structures are inferred from their present locations as shown in Fig. 4d. Key for structures is shown in Fig. 4d. (A-H) in (a) are sub-basins described in the text and shown in Figs 4d and 5.

Fig. 8. Details of the well-log data from the depth interval c. 20170-20350 ft in the borehole, illustrating the petrophysical expression and composition of the apparent salt weld and flanking strata (see also Fig. 9). The location of the borehole is shown in Figs 4, 5 and 7. The colour-code refers to colours shown in Fig. 6. Note that the density and neutron porosity log responses are slightly offset from the base salt due to the 13 7/8-inch casing point being set just below the weld.

Fig. 9. Density (RHOB)-sonic slowness (DT) (i.e., velocity) cross-plot of petrophysical data from the depth interval shown in Fig. 8. Note the distinct expression of intra-weld halite, which is characterised by significantly higher density (typically $>2.4 \text{ g/cm}^3$) and slow sonic slowness values (typically $<80 \text{ us/ft}$) (i.e., higher velocities) than underlying or overlying clastics. The range of ideal values for clean halite are shown (taken from Rider and Kennedy, 2011), as are those documented by Jackson et al. (2018) from the northern Gulf of Mexico. See text for discussion.

736

737 **Fig. 10.** Schematic diagram showing the general, simplified salt-tectonic evolution of the
738 studied minibasin, salt weld, and associated structures. The stages in the diagram are very
739 broadly tied to the six key stages described in the text: (a) and (b) Stage 1 (Serravallian-
740 Messinian) – minibasin nucleation and translation; (c) Stage 2 (Messinian) – minibasin
741 translation, welding, collision, and contraction, and depocentre coalescence; (d) Stages 3
742 (Messinian-Piacenzian) and 4 (Gelasian-Pleistocene) – contraction, diapir inflation, and
743 minibasin tilting; (e) Stage 5 and 6 (Late Pleistocene-Holocene?) – minibasin translation,
744 collision, contraction, and decay. Minibasin A-C do *not* correspond to those described in the
745 text; they are simply labelled here in so that their relative positions can be tracked during Stages
746 1-3. Note also that sheet/canopy inflation is inferred to result from the squeezing of diapiric
747 feeders (Peel et al., 1995), which may lie outside of the displayed profile, and that intra-
748 minibasin accommodation (in Stages 4 and 5) was principally generated by the passive rise of
749 flanking diapirs rather than the subsidence of the minibasins.

Fig. 1

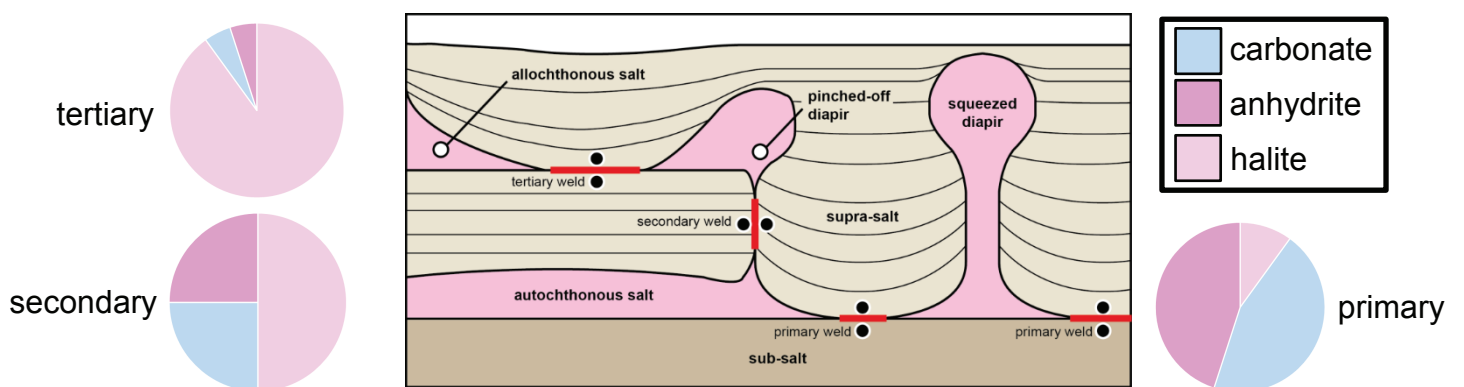


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Fig. 2

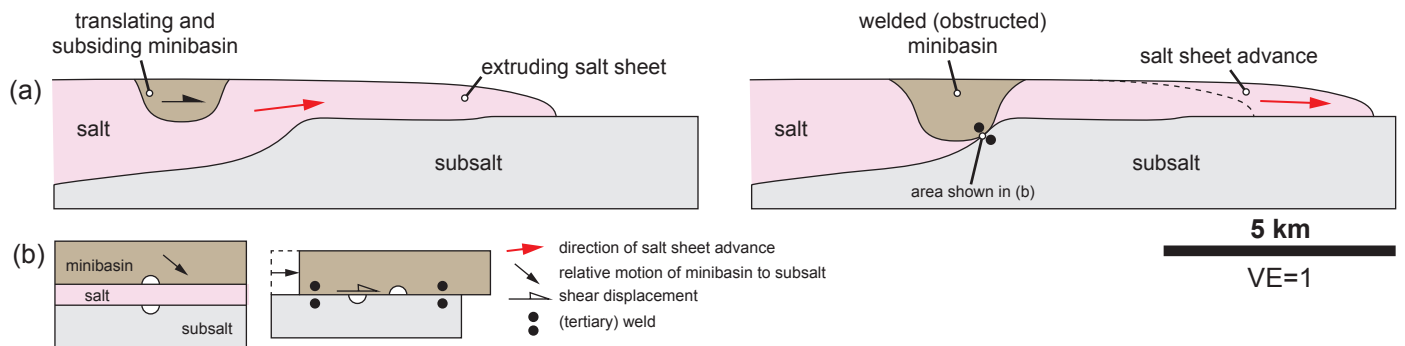


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Fig. 3

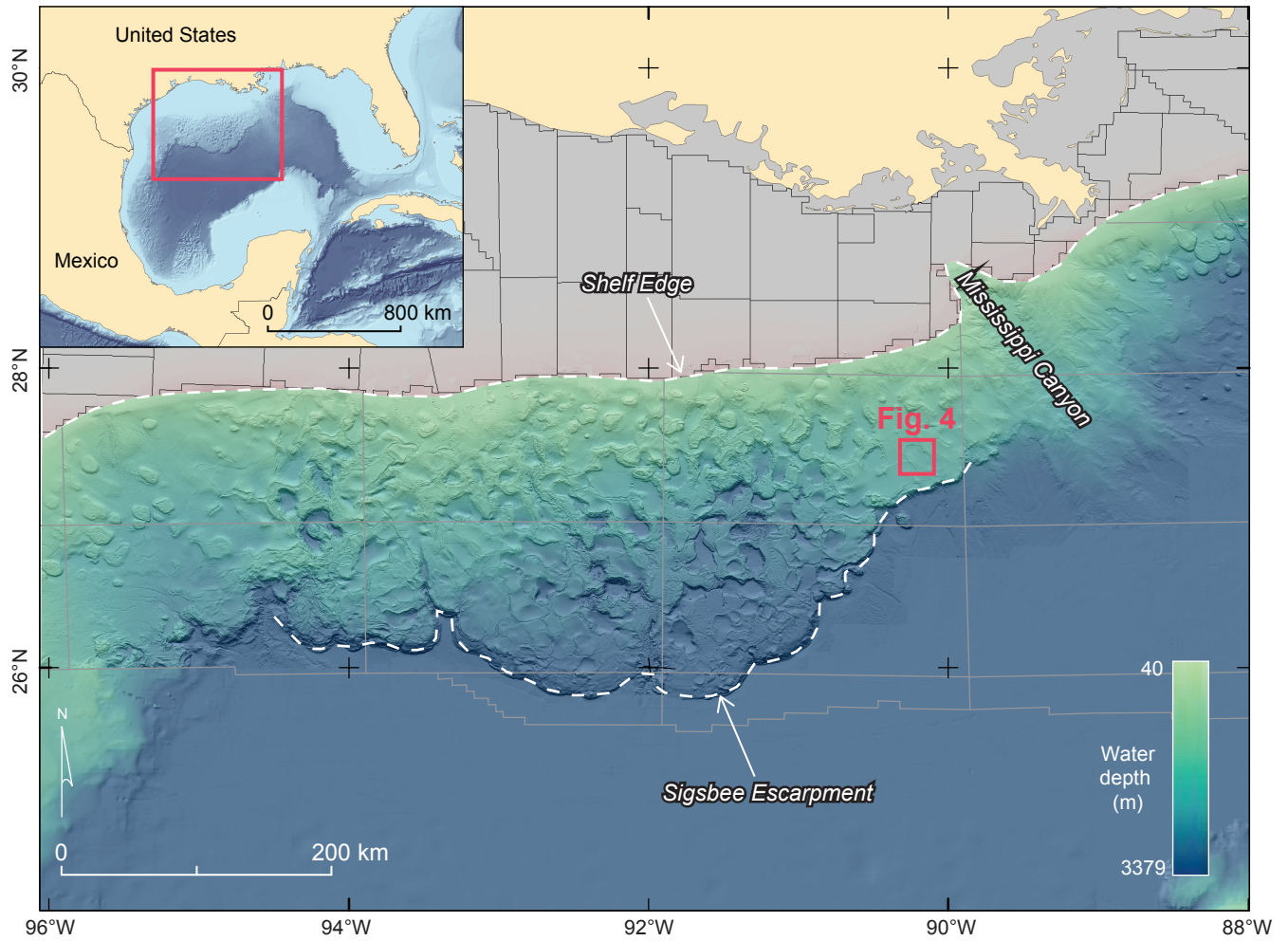


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Fig. 4

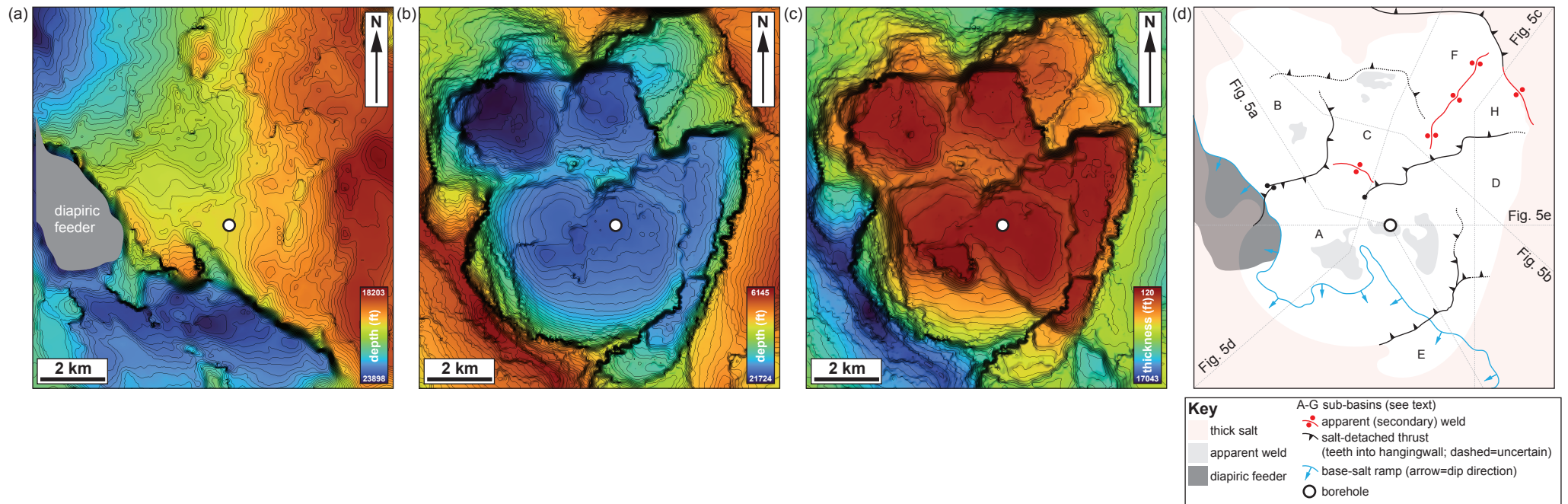


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Fig. 5

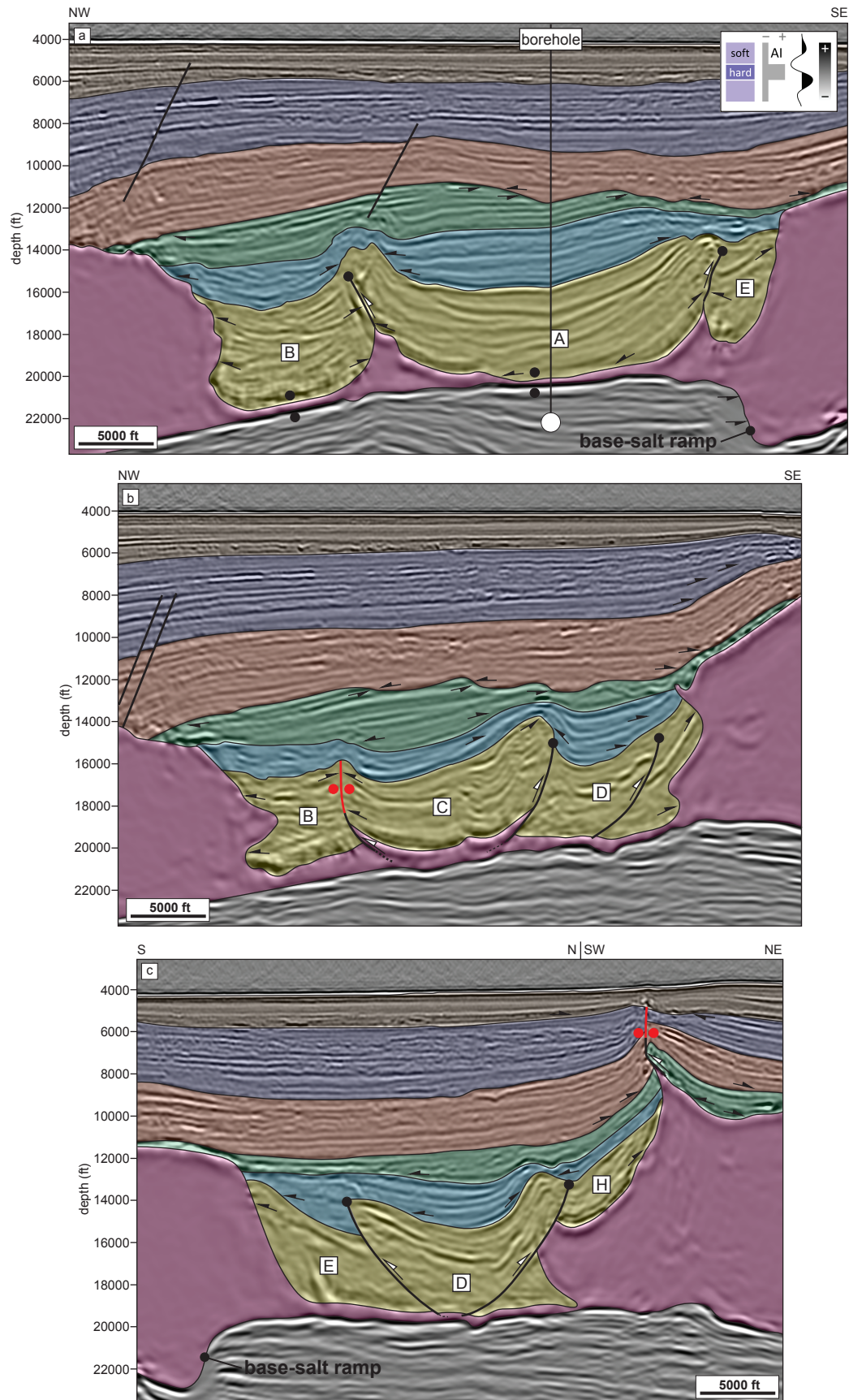


Fig. 5

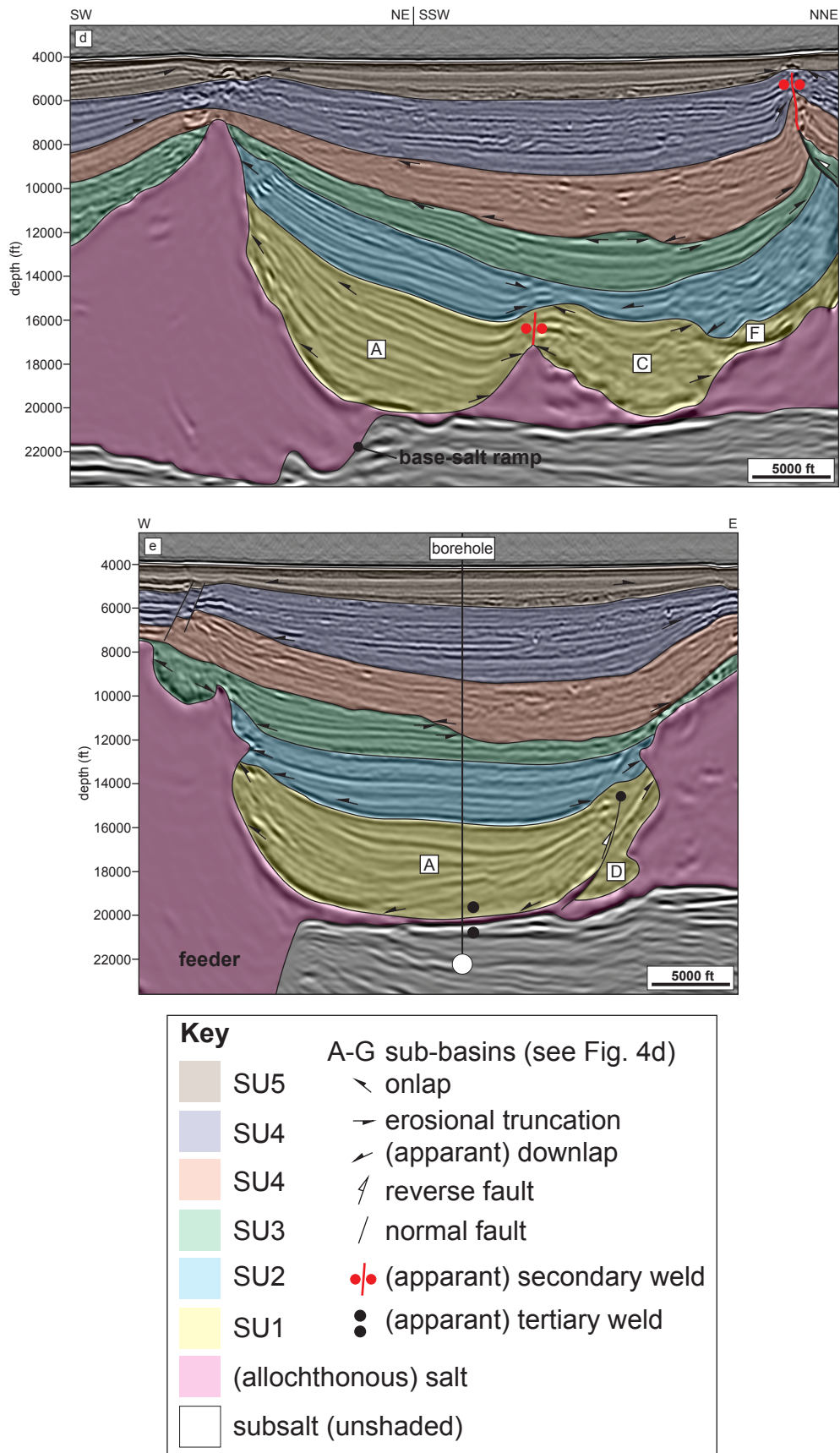


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Fig. 6

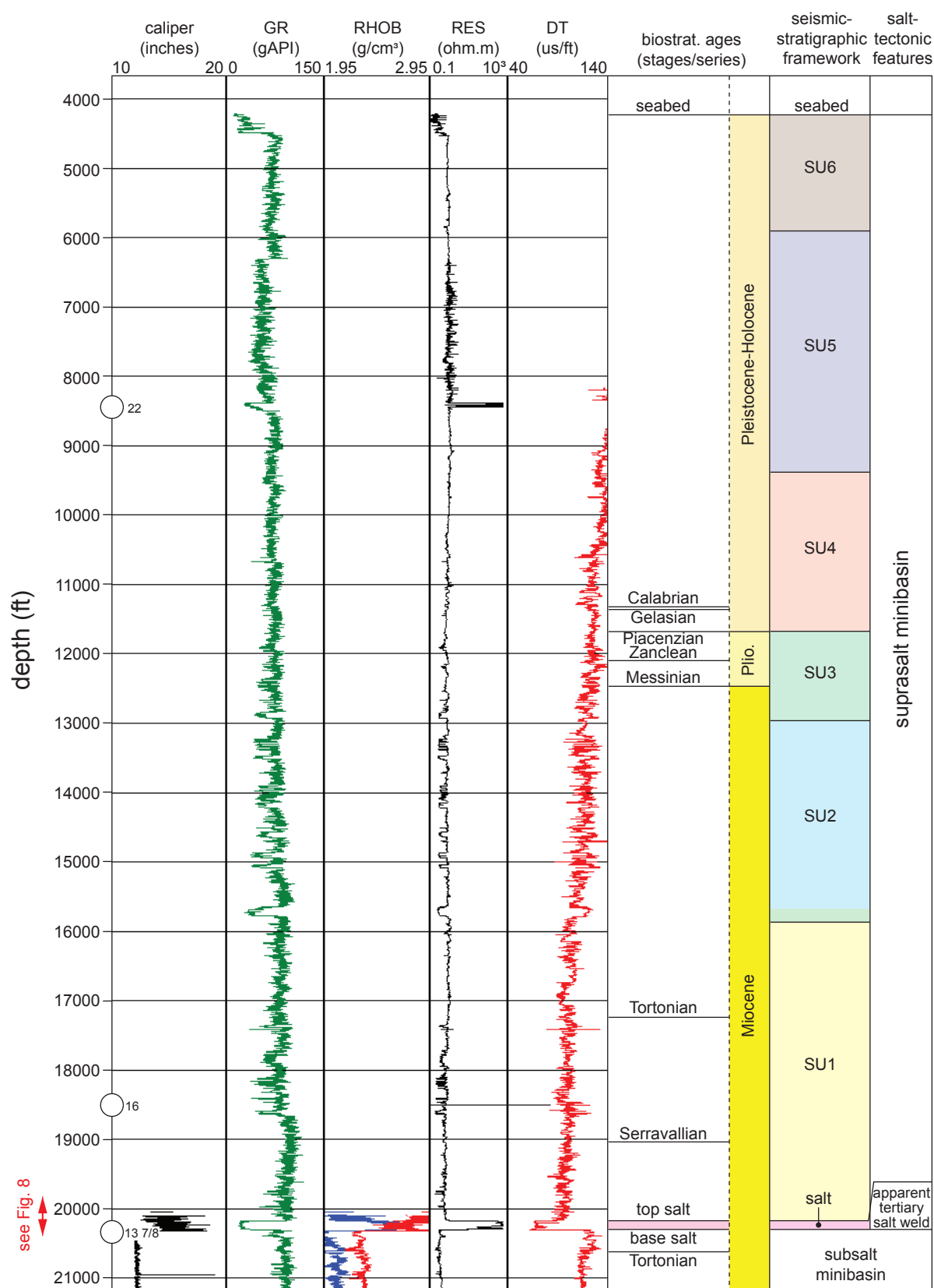


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Fig. 7

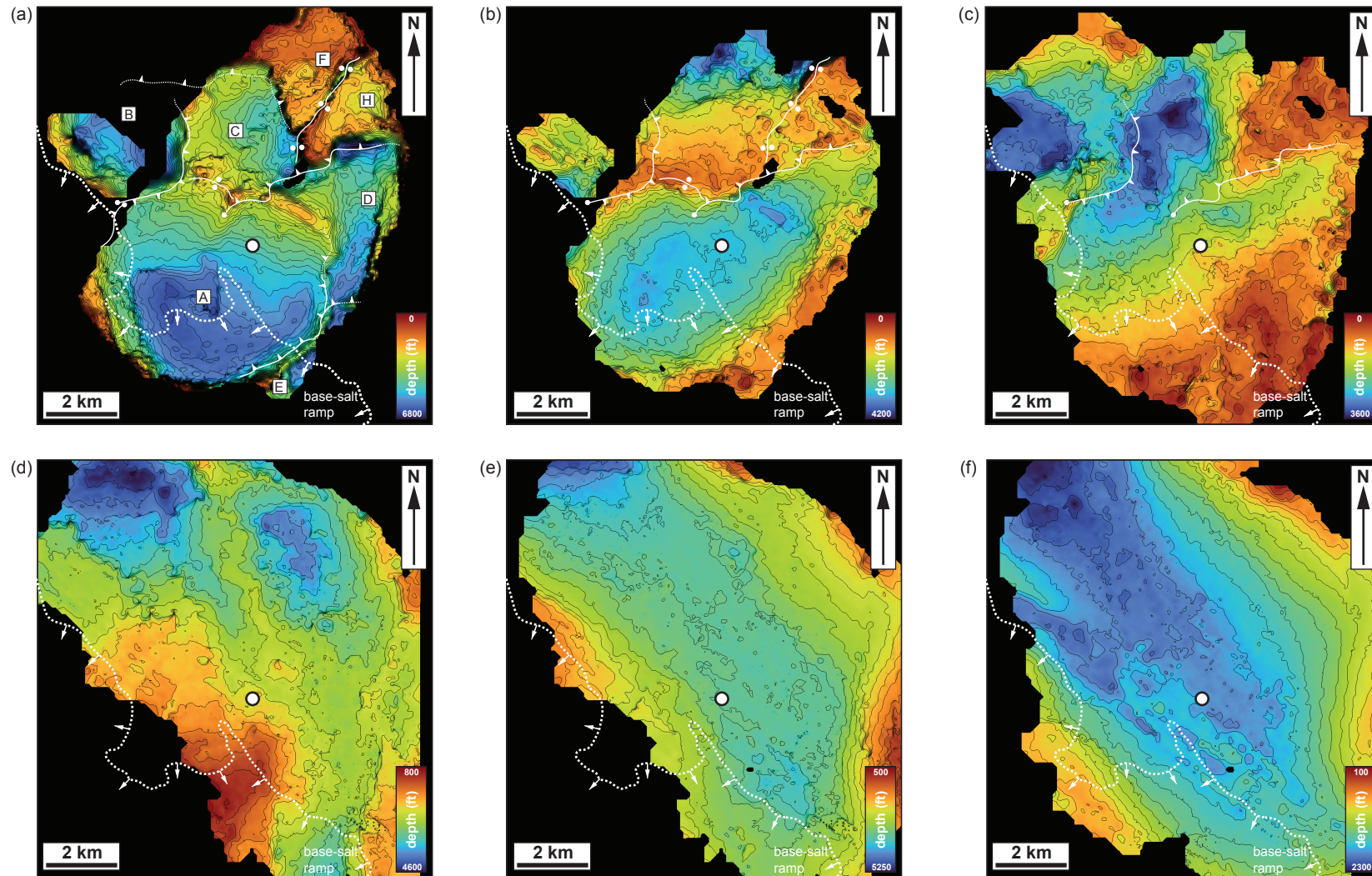


Fig. 7. Isochron (thickness) maps showing temporal changes in minibasin depocentre location because of canopy advance, salt welding, and minibasin shortening and tilting. (a) SU1 – Serravallian-Messinian; (b) SU2 – Messinian; (c) SU3 – Messinian-Piacenzian; (d) SU4 – Gelasian-Pleistocene; (e) SU5 – Late Pleistocene-Holocene(?); and (f) SU6 – Late Pleistocene-Holocene(?). The position of the base-salt ramp (e.g., Fig. 5a; see also text for description and interpretation) is indicated in (a)-(c). The key intra-minibasin, sub-basin-bounding structures inferred to be active during the deposition of the Serravallian-Messinian (SU1), Messinian (SU2), and Messinian-Piacenzian (SU3) are shown; the approximate positions of these structures are inferred from their present locations as shown in Fig. 4d. Key for structures is shown in Fig. 4d. (A-H) in (a) are sub-basins described in the text and shown in Figs 4d and 5.

Fig. 8

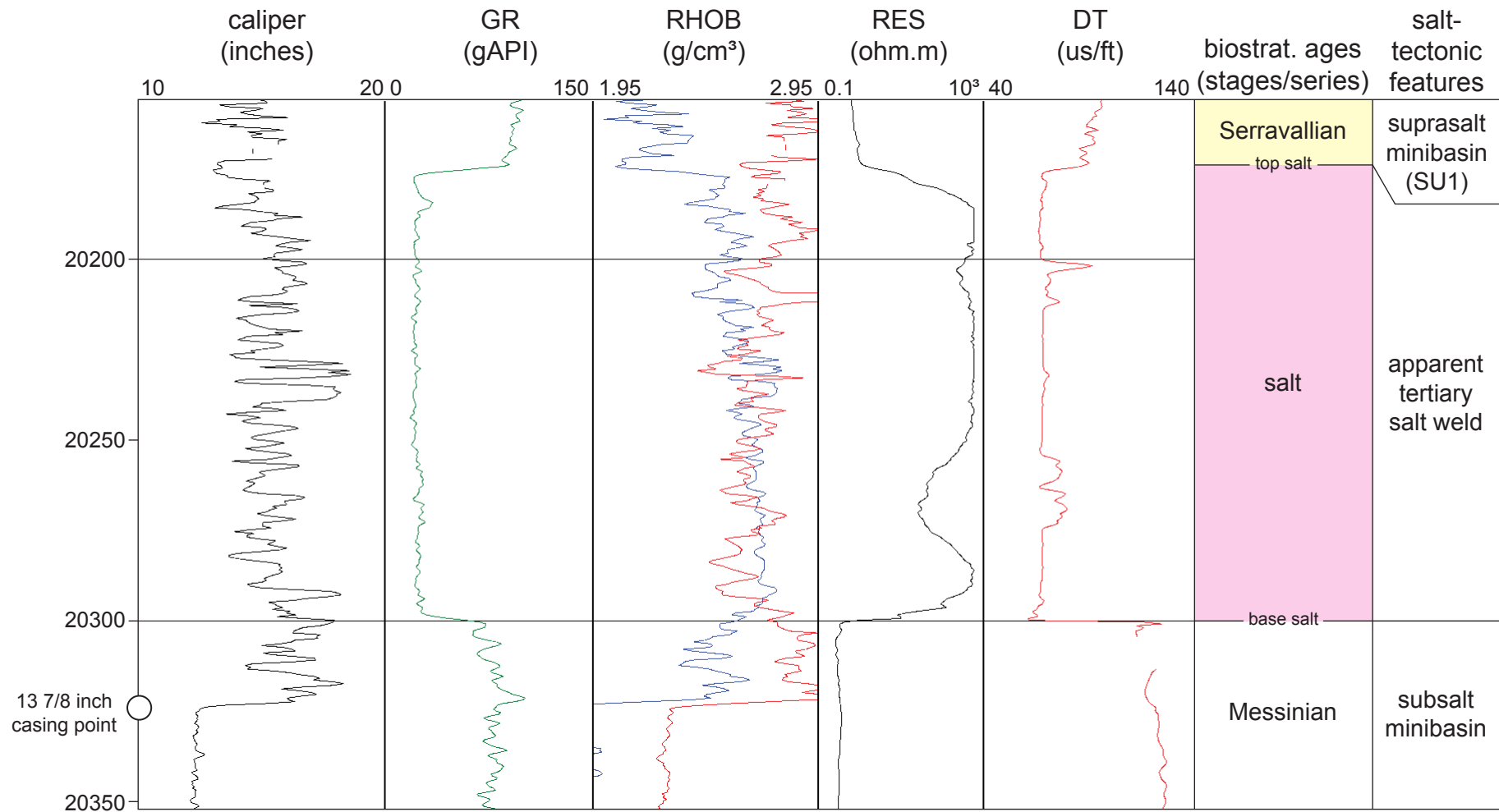


Fig. 8. Details of the well-log data from the depth interval c. 20170-20350 ft in the borehole, illustrating the petrophysical expression and composition of the apparent salt weld and flanking strata (see also Fig. 9). The location of the borehole is shown in Figs 4, 5 and 7. The colour-code refers to colours shown in Fig. 6. Note that the density and neutron porosity log responses are slightly offset from the base salt due to the 13 7/8-inch casing point being set just below the weld.

Fig. 9

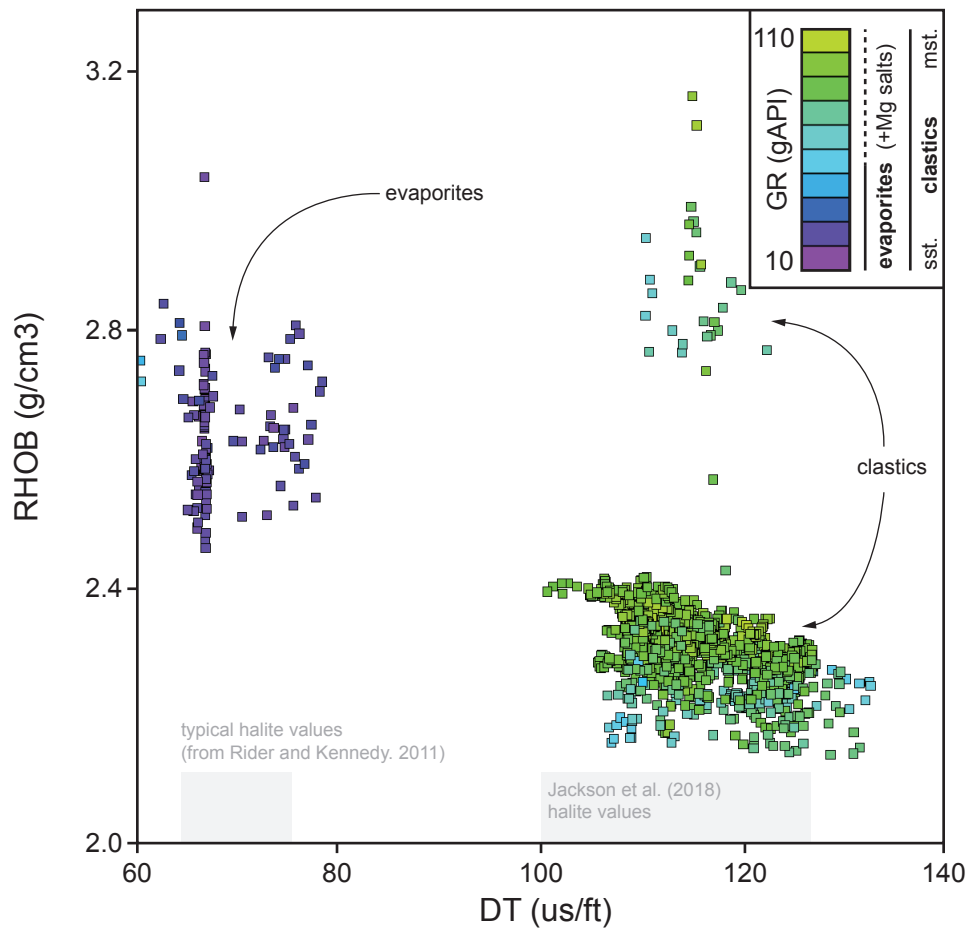


Fig. 9. Density (RHOB)-sonic slowness (DT) (i.e., velocity) cross-plot of petrophysical data from the depth interval shown in Fig. 8. Note the distinct expression of intra-weld halite, which is characterised by significantly higher density (typically >2.4 g/cm³) and slow sonic slowness values (typically <80 us/ft) (i.e., higher velocities) than underlying or overlying clastics. The range of ideal values for clean halite are shown (taken from Rider and Kennedy, 2011), as are those documented by Jackson et al. (2018) from the northern Gulf of Mexico. See text for discussion.

Fig. 10

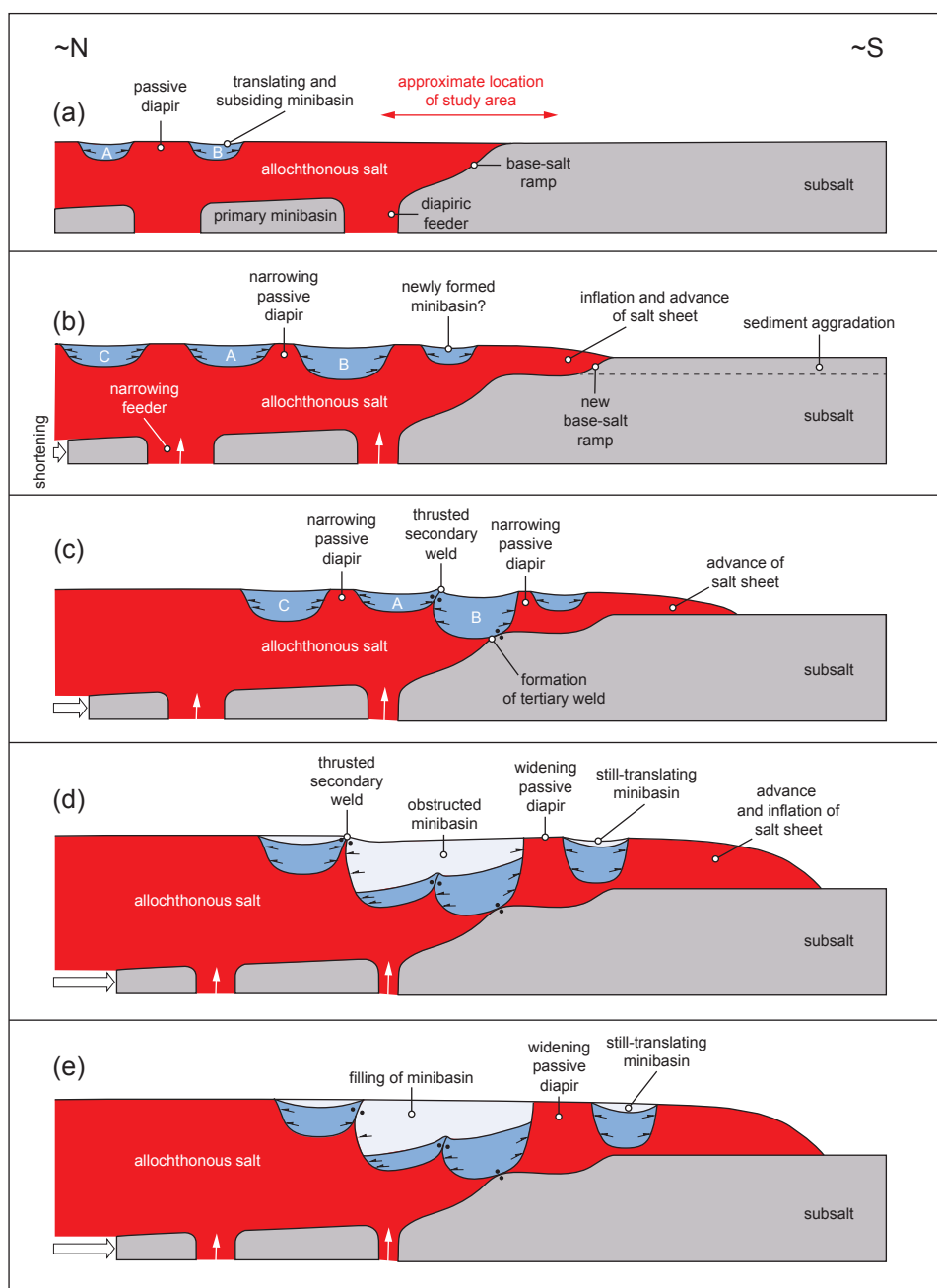


Fig. 10. Schematic diagram showing the general, simplified salt-tectonic evolution of the studied minibasin, salt weld, and associated structures. The stages in the diagram are very broadly tied to the six key stages described in the text: (a) and (b) Stage 1 (Serravallian-Messinian) – minibasin nucleation and translation; (c) Stage 2 (Messinian) – minibasin translation, welding, collision, and contraction, and depocentre coalescence; (d) Stages 3 (Messinian-Piacenzian) and 4 (Gelasian-Pleistocene) – contraction, diapir inflation, and minibasin tilting; (e) Stage 5 and 6 (Late Pleistocene-Holocene?) – minibasin translation, collision, contraction, and decay. Minibasin A-C do not correspond to those described in the text; they are simply labelled here in so that their relative positions can be tracked during Stages 1-3. Note also that sheet/canopy inflation is inferred to result from the squeezing of diapiric feeders (Peel et al., 1995), which may lie outside of the displayed profile, and that intra-minibasin accommodation (in Stages 4 and 5) was principally generated by the passive rise of flanking diapirs rather than the subsidence of the minibasins.