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Subsurface temperature from seismic reflection data: application to the post break up sequence offshore Namibia

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Abstract

Accurate estimations of present-day subsurface temperatures are of critical importance to the energy industry, in particular with regards to geothermal energy and petroleum exploration. This paper uses seismic reflection observations of bottom-simulating reflections and subsurface velocities coupled with an empirical velocity to thermal conductivity transform to estimate subsurface temperature in a process dubbed reflection seismic

thermometry. The case study is a frontier passive margin extending from the shelf edge to deep water in the central Lüderitz Basin, offshore Namibia. The bottom simulating reflector is used to derive surface heat flow. The thermal conductivity model was applied to seismic processing velocities to determine the subsurface thermal conductivity. Knowledge of surface heat flow and thermal conductivity structure allowed us to estimate subsurface temperatures across the study area. The results suggest the Lüderitz Basin has a working hydrocarbon system with the inferred Aptian Kudu source interval within the gas generation window.

Introduction

Subsurface temperature is a key parameter in subsurface energy extraction from petroleum- and geothermal systems (Harper, 1971; Thompson, 1979; Hunt, 1984; Bonté et al., 2012). Accurate estimations of present-day subsurface temperatures are thus of critical importance to the energy industry. In frontier areas, petroleum source rock maturity is a key uncertainty and without access to bottom hole temperature (BHT) readings from boreholes, source rock characterisation is reliant on estimation and extrapolation. A crucial component of understanding the subsurface temperature field is how heat is transferred (i.e. heat flow and thermal conductivity) (Sclater et al., 1980). Often there is limited understanding of the variation in thermal conductivity both vertically and laterally in the subsurface domain due to the difficulty collecting such data. Prior to entry into frontier basins, it is advantageous to determine the source rock deliverability in the area. This is primarily controlled by two factors namely source rock type and temperature history. Along many passive margins the source rocks are at maximum burial depth and thus maximum temperature at the present day. Present day subsurface temperatures are typically acquired from temperature probe measurements that have been acquired through borehole drilling (Fuchs and Balling, 2016). To estimate heat flow and temperature information in adjacent areas often involves the deployment of multiple seafloor probes prior to the drilling stage (Davis et al., 2003). This then requires the extrapolation of data from nearby boreholes using structural and stratigraphic models (Davies and Davies, 2010). This methodology underutilises the available seismic datasets that are often acquired during the early stages of exploration in frontier basins. This paper presents a reflection seismic thermometry workflow for using seismic reflection data to estimate subsurface temperature before drilling and applies this to a frontier exploration setting.

It has been shown that gas hydrate identification on seismic reflection data through detection of bottom simulating reflectors (BSRs) at the base of gas hydrate stability zone (GHSZ), can be used for geothermal gradient estimation (Yamano et al., 1982; Calvès et al., 2010; Hodgson et al., 2014; Serié et al., 2017).

The reflection seismic thermometry workflow predicts subsurface temperatures by first estimating surface heat flow from BSRs and then utilizing seismic processing velocities to derive thermal conductivity through an empirical transform. This empirical relationship relating acoustic velocity and thermal conductivity is a key component in allowing the estimation of subsurface temperatures throughout the seismic volume.

Figure 1

Geological setting

The study area (Fig. 1) is in the Lüderitz Basin offshore Namibia, bounded by the Orange Basin to the south, and the Walvis Basin to the north. It is part of the southern West African continental margin. Successive rifting events from the Carboniferous onwards preceded the Mesozoic opening of the South Atlantic, and the breakup of Gondwana (Bagguley and Prosser, 1999; Karner and Driscoll, 1999; Schmidt, 2004). The margin offshore Namibia is characterised as having characteristics of both a volcanic passive margin and a non-volcanic margin end members (Light et al., 1993; Gladczenko et al., 1998; Bauer et al., 2000). Asymmetric rifting has resulted in significant variability in the sedimentary and subsidence history between the conjugate margins with this reflected in the nature of hydrocarbons discovered in these areas (Mello et al., 2011). The formation of the Walvis Ridge is contemporaneous with the extrusion of the Etendeka continental flood basalts and acted as a long-lived barrier to marine flow, creating restricted marine conditions to the north. These conditions promoted the formation of salt basins north of the Ridge in the Albian-Aptian, and these are observed on both the West African and Brazilian margins (Berger et al., 1998; Davison et al., 2012). In the Lüderitz Basin multiple features such as seaward dipping reflectors (SDRs) and mass transport deposits (MTDs) can be observed (Torsvik et al., 2009). There are however no seamounts within 50 km (~31.1 mi) from the study area, the outer limit for hydrothermal systems to extend from such a system (Sclater et al., 1980; Hasterok et al., 2011).

The neighbouring Orange and Walvis Basins both possess working petroleum systems with gas condensate discovered in the Kudu wells and oil in the Wingat well respectively (Fig. 1) (Intawong et al., 2015). The key source interval relevant for the Lüderitz Basin is the Aptian age Kudu shale (Fig. 2d). The source maturity of this interval in the Lüderitz Basin is as yet uncertain.

Figure 2

Gas Hydrates & Bottom Simulating Reflectors

A BSR is traditionally considered as a continuous and coherent seismic event that cross-cuts the primary sedimentary features, whilst mimicking the morphology of the seabed (Calvès et al., 2008; Le et al., 2015; Ruppel and Kessler, 2017; Schicks, 2018). A BSR with reverse polarity and near-parallelism relative to the seabed originates from the negative acoustic impedance (AI) contrast between partially frozen, gas-hydrate bearing sediment at the base of the GHSZ and the underlying zone of dissociated free gas and water bearing sediment (Kvenvolden & Lorenson, 2001; Paganoni et al., 2016). This variant of a BSR has been commonly noted in studies globally and is usually considered a sign of hydrate presence (Shipley and Houston, 1979; Stoll and Bryan, 1979; Haacke et al., 2007).

Heat Flow

Understanding heat flow is crucial to building reliable geological models of both the shallow and deep subsurface and has important implications for the exploration and development of natural resources such as petroleum (Tissot et al., 1987). Heat flow has traditionally been associated with tectonism and the thickness of the radiogenic crust. However mantle processes in continental margins also impact heat flow (Goutorbe et al., 2011). Heat from the mantle or primordial heat is one contributing factor to the thermal structure in sedimentary basins and is the deepest source of heat production (Hokstad et al., 2017). Mantle heat flow is estimated from the base of the crust, equivalent to the Moho (thus the prevalence of the 1330 °C (2426 °F) isotherm as a reference point in traditional bottom-up basin modelling workflows). The other contribution to heat is in the form of radiogenic heat production.

Radiogenic elements are found in insignificant quantities in oceanic crust and lithospheric mantle, therefore the radiogenic heat input will be greatest in areas of continental crust and sediments (Hasterok, 2010; Allen and Allen, 2013). Basins located in the transitional zone between onshore and offshore regions tend to have considerable structural variability and thus as a consequence have been the least predictable for heat flow using global averages only (Jaupart et al., 2016; Hokstad et al., 2017). Though young ocean crust is particularly susceptible to hydrothermal fluid circulation impacting heat flow, in the Lüderitz Basin this is not an issue due to the relative age of the underlying crust and proximity to the coast parallel continent ocean boundary (COB) (Lister, 1972; Gladczenko et al., 1998).

Global coverage of heat flow data is not extensive, with surface heat flow data globally being limited relative to estimates of total heat output (Gosnold & Panda, 2002; Lucazeau, 2019; Macgregor, 2020). In the study area, the solitary heat flow data point is from Ocean Drilling Program (ODP) Site 1084 as shown in Fig. 1. Reported values of heat flow in published literature are made either through direct measurement or through estimations based on crustal thickness and age (Davies and Davies, 2010; Davies, 2013). Such heat flow estimates can have a threefold basis with primary data from measured data points; in oceanic crustal settings, heat flow is based on crustal thickness to mitigate for measurement perturbation due to fluid flow; and finally in the absence of measurements an estimate can be made on the basis of geology. The Bullard method is commonly used to calculate heat flow from borehole data from the relation between temperature and the thermal resistance of the sediments (Bullard, 1939; Pribnow et al., 2000). For there to be a linear relationship between acoustic velocity and thermal conductivity conditions downhole must be conductive, steady state and with no internal heat sources. The latter is difficult as heat is introduced into the system during drilling from friction with the drill bit and the circulation of drilling fluids, thus necessitating time-based corrections for the impact of drilling on local thermal regime.

Conventional thermal data

Over large regions like continental margins, it is difficult to ensure high spatial resolution of thermal data from conventional techniques such as downhole temperature measurements and gravity driven thermal probes (Phrampus et al., 2017). This is both a result of scarcity of boreholes and prohibitive expense. Heat flow derived from the seismic imaging of gas hydrates can be useful in areas where significant bottom water temperature (BWT) fluctuation adversely affects the reliability of thermal probe data or where hard ground may prevent probe insertion (Hyndman et al., 2001). ODP thermal conductivity measurements on core samples from gas hydrate provinces are unreliable due to gas exsolution during recovery (Phrampus et al., 2017). This phenomenon depresses onboard thermal conductivity measurements. For the transient line source needle probe used in ODP studies to measure thermal conductivity it is important to note the orientation of the needle insertion relative to the sediment bedding direction as the thermal conductivity measurement is provided for a plane perpendicular to the needle axis (Pribnow et al., 2000). For shipboard temperature measurements temperature-time curves are subjectively fit to APC probe data (to restore to equilibrium temperatures and negate the effect of frictional heating upon insertion of the probe) (Grevemeyer and Villinger, 2001).

The Curie isotherm is a common subsurface thermal marker sometimes representing a petrophysical boundary (Langel and Hinze, 1998). It is commonly considered to be ~580 °C (~ 1076 °F) as this is the Curie Point temperature of magnetite, the most common magnetic mineral in the continental crust, especially in deeper regions (Frost and Shive, 1986). Thus, the depth corresponding to a lack of magnetism is likely at temperatures in excess of the Curie point of magnetite or a result of compositional changes leading to magnetite poor rocks at depth (Beardsmore and Cull, 2001). However, this method simply defines a solitary subsurface isotherm over a great depth interval from the seabed, thus making any linear geothermal gradient calculated greatly approximated. Furthermore, for high resolution estimation of the Curie isotherm depth, regional scale gravity data would be required.

Global thermal data coverage may also suffer from spatial bias, as there tends to be a greater interest for scientists in areas of higher heat flow resulting in a greater concentration of data, with another potential driving factor being interest in areas with geothermal energy application (Davies, 2013).

Data

Seismic data

This study uses a combination of 2D and 3D multichannel, post-stack, time-migrated seismic reflection data from offshore Namibia, covering both the shallow- and deep-water sectors of the Lüderitz basin (Fig. 1). The seismic database is correlated with a single exploration well located on the continental shelf, in addition to ODP Site 1084 in the deep-water area.

The 2D seismic data were provided by Spectrum ASA and consists of two surveys conducted in 2006 and 2012 respectively, with further reprocessing in 2012 (to improve image quality in legacy data and to tie 2006 vintage seismic to newly shot 2012 seismic data), and a combined total line length of 752 km (~ 467 mi). The lines have a 4 ms two-way travel time (TWT) sample rate. The frequency range is 3 - 206 Hz (dominant frequency ~ 90 Hz) with a common midpoint (CMP) spacing of 12.5 m (~7.77 ft) and a shot interval of 25 m (~15.5 ft). 2006 vintage 2D seismic data was collected with a streamer length of 8100 m (~5033 ft) while 2012 vintage 2D seismic data was collected with a streamer length of 10500 m (~6524 ft).

The 3D seismic survey covers an area of 4150 km^2 (~1602 mi^2) and was acquired for Serica and partners by Polarcus in 2012 using *M/V Polarcus Nadia*. Primary objective of the survey was to establish prospectivity by mapping pinch out structures and a large channel feature in the study area. Streamer length was 8100 m (~5033 ft) with 50 m (~164 ft) source separation of dual source (0.0695 m^3 [2.45 ft^3]) air guns. It is 80-fold with a 4 ms TWT sample rate and Inline spacing of 12.5 m (~7.77 ft) and Xline spacing of 25 m (~15.5 ft). 3D pre-stack time migration was conducted by ION GXT. The isotropic frequency range for Kirchhoff pre-stack time migration (PreSTM) ranged between 3-110 Hz. All data were processed through stack and time migration. Velocity model building was done using two iterations of dense residual move out (RMO) auto-picking to create a smooth velocity model constrained by the geological horizons. Velocity model parameters of 4 ms sample interval, 9000 ms trace length and a 6000 m (~19685 ft) aperture. By parameterising the final velocity model (Fig. 3) for steep dips and high frequency gathers, the amplitude preserving preSTM resulted in high resolution image gathers.

Figure 3

Well data

Well data included ODP Site 1084 and Norsk Hydro Exploration well 2513/8-1 (Fig. 1). The ODP borehole was drilled as part of ODP Leg 175 with the primary intention of documenting the migration of the Benguela Current along the South Atlantic West African Margin (Wefer et al., 1998). It is located in a water depth of 1992 m (~6535 ft) and targeted the downslope rim of the Lüderitz depositional basin. Useful subsurface borehole data included headspace gas analysis, gas chromatography results and core data.

The exploration well 2513/8-1 is situated on the shelf in a water depth of 243 m (~797 ft) and targeted a Lower Cretaceous lobe in a thrust ramp graben before terminating in Barremian-Aptian age volcanic rocks at a total depth of 2553 m (~8376 ft). Some sparse BHT data points from this well provide the only available calibration for the temperature estimation workflow.

Method

Figure 4

The temperature estimation workflow utilised in this study is outlined in Fig. 4 and described below. The entirety of the workflow has been developed and tested using commercial software developed for use in the petroleum industry (Schlumberger Petrel).

The gas hydrate stability field can be utilised to estimate the temperature at the base of the zone of stable gas hydrates, demarcated on seismic by a BSR (Dickens and Quinby-Hunt, 1994; Sloan et al., 1998; Lu and Sultan, 2008). This in turn allows a shallow geothermal gradient across the GHSZ to be estimated and surface heat flow to be estimated (Minshull, 2011; Priyanto, 2018). The stability conditions are controlled in part by the geochemical properties of the fluids available to form clathrate hydrates, which in frontier settings with limited ground truthing are generally assumed to be average salinity (33.5 ‰) seawater and pure methane (Sloan et al., 1998). Pore fluid pressure conditions are generally assumed to be hydrostatic, equivalent to 0.0101 MPa m^{-1} (~0.446 psi ft^{-1}). The following relationship (Eq. 1) as defined by (Dickens and Quinby-Hunt, 1994) describes methane hydrate stability:

Equation 1: $$\frac{1}{T_{BSR}} = 3.79 \times 10^{-3} - 2.83 \times 10^{-4} (\log P)$$

where T_{BSR} is temperature at the base of GHSZ (K); and P is the corresponding pressure (MPa). Assuming hydrostatic pressure at the BSR depth, temperature at the base of the hydrate stability zone has been established:

Equation 2: $$\mathrm{T}_{BSR} = ((3.79 \times 10^{-3} - 2.83 \times 10^{-4} (\log(\rho \times g \times Z_{BSR})))^{-1}) - 273$$

Where T_{BSR} is the temperature at GHSZ (°C); ρ is density (kg m^{-3}) (of seawater); g is acceleration due to gravity (m s^{-2}) and Z_{BSR} is the depth (m) of the BSR. It must be noted that this is a minimum temperature estimate based on assumed stability field conditions (Dickens, 2001).

The National Oceanic and Atmospheric Administration (NOAA) World Ocean Atlas (WOA) (Boyer et al., 2005) is an open source dataset containing data covering the world's oceans for temperature, salinity, density, etc. Seabed temperature (Eq. 3) was modelled in the study area using a synthetic hydrothermal gradient derived from the closest WOA data nodes, with the misfit from this approach amounting to ±0.4 °C (±0.18 °F) across the water column.

Equation 3:
$$T_{SEABED} = (-1.919 \ln Z + 21.899) \qquad \text{if } Z \leq 200$$
$$T_{SEABED} = 525.65 Z^{-0.714} \qquad \text{if } 200 < Z < 1000$$
$$T_{SEABED} = -0.0007 Z + 4.4905 \qquad \text{if } Z \geq 1000$$

where T_{SEABED} is the modelled hydrothermal gradient temperature (°C) and Z is seabed depth (m).

Given both T_{SEABED}, Z_{SEABED} and T_{BSR}, Z_{BSR} at any geographical locality, then the geothermal gradient (dT/dZ) across the GHSZ at that locality is given by the following relationship.

Equation 4: $$\frac{dT}{dZ}GHSZ = \frac{T_{BSR}-T_{SEABED}}{Z_{BSR}-Z_{SEABED}}$$

Where dT/dZ is geothermal gradient (°C km^{-1}); T_{BSR} is temperature at BSR (°C); T_{SEABED} is seabed temperature (°C); Z_{BSR} is depth of BSR (km); Z_{SEABED} is seafloor depth (km).

Alongside thermal gradient, two key thermal properties are the heat flow and thermal conductivity.

Equation 5: $$Q = k \times \frac{dT}{dZ}$$

Where Q is heat flow (mWm^{-2}); k is thermal conductivity (W m^{-1} K^{-1}) (see Section 3.1) and dT/dZ is geothermal gradient (°C km^{-1}).

Fourier's Law of heat conduction (Eq. 5) is crucial to understanding the interplay between heat flow, thermal conductivity, and geothermal gradient. Establishing a shallow linear geothermal gradient using BSRs is well established (Calvès et al., 2010; Serié et al., 2017) and studies have extrapolated this shallow geotherm for traditional basin modelling workflows. This however does not consider the thermal conductivity structure of the subsurface and how it might be possible to utilise seismic reflection velocity data to do so.

Thermal conductivity estimation

Thermal conductivity is a measure of how well heat is conducted through a material (Gu et al., 2017). Difficulty associated with measuring thermal conductivity in boreholes arise from poor contact between the measuring tool and the borehole wall (Horai, 1982). Thus, considerable attention has been devoted to determining methods for estimating thermal conductivity through more easily acquired secondary data such as seismic velocity measurements. Experimental studies have shown that primary controls on thermal conductivity include mineral composition, porosity and fractures (Gegenhuber and Schoen, 2012). Seismic wave velocity is also largely controlled by the same factors. Early work by (Horai, 1982) sought to correlate thermal conductivity with other physical properties such as water content, bulk density, porosity and compressional sound wave velocity. The direct approach involves deriving thermal conductivity from physical properties via empirical relationships (Zamora et al., 1993). Estimates of thermal conductivity computed directly from conventional wireline data can be accurate within 0.2 – 0.3 W m^{-1} K^{-1} (~0.116 – 0.173 BTU h^{-1} ft^{-1} $°F^{-1}$)when derived using empirical relationships from sonic velocity data (Hartmann et al., 2005). Such a direct approach has been utilised in this work using experimental data from existing correlation studies (Brigaud et al., 1990; Brigaud & Vasseur, 1989; Esteban et al., 2015; Griffiths et al., 1992; Gunn et al., 2005; Kukkonen & Peltoniemi, 1998; Francis Lucazeau et al., 2004; Mielke et al., 2017; Popov et al., 2003; Popov et al., 1999). Such a direct empirical approach derived from experimental data has also been tested by the authors in other basins (Sarkar, 2020; Sarkar and Huuse, 2021).

Experimental data can vary in terms of the conditions under which it was collected. Most measurements have been taken at ambient pressure and temperature conditions. Binary parameterisation of the experimental datasets allows characterisation of data points collected under similar parameters. Most studies measured thermal conductivity using the optical scanning method (Popov et al., 1999). There are fewer instances in the source datasets of the use of the divided bar method of measuring thermal conductivity (Hyndman and Jolivet, 1976; Evans, 1977). Only wet samples from these studies were used as our case study is in deep water and thus fully saturated with water, gas and/or gas hydrate. In dry samples, the contribution to thermal conductivity arising from lithological heterogeneities (matrix properties) can be masked by the stronger influence of porosity (Hartmann et al., 2005). In contrast wet samples reflect the impact of porosity and lithological variations.

The range of samples included in our fits cover a wide range of lithologies, including sandstones, limestones, granites, basalts, marble to name a few (Grevemeyer and Villinger, 2001; Hartmann et al., 2005; Boulanouar et al., 2013; Esteban et al., 2015; Jorand et al., 2015; Gu et al., 2017; Mielke et al., 2017). In so doing it is hoped that the resulting empirical relationship will best apply to the broadest possible range of rock types that can be expected subsurface across the study area. It must be noted though that variables within the sample set (Fig. 5) include and are not limited to the porosity (arising from cracks for example). Fractures are known to reduce both P wave velocities and thermal conductivity (Zamora et al., 1993).

A regression through the filtered experimental data points taken from the aforementioned studies gives the following empirical relationship for thermal conductivity:

Equation 6: $k_V = (0.001 \times V_P) - 0.5071$

Where k_V is thermal conductivity from velocity (W m^{-1} K^{-1}) and V_P is P wave velocity (m s^{-1}).

Figure 5

Certain trends are evident in the cross plot of sample data in Fig. 5. Due to the lack of salt encountered in the study area, there is a lack of sample points in the expected high conductivities associated with salt (Esteban et al., 2015). The regression is anchored by the large cluster of points associated with the Grevemeyer & Villinger (2001) data. The Hartmann et al. (2005) and Gu et al. (2017) samples are parallel to the best fit regression.

Seismic P wave velocity within the area is converted to thermal conductivity (k_V) using the thermal conductivity relationship (Eq. 6), with velocity averaged down to the depth of the BSR, Z_{BSR}. The variation in thermal conductivity with depth can be overlain on a 3D seismic reflection dataset in this manner. Using Z_{BSR}, determined on reflection seismic data, the hydrate stability field can be utilised to compute the temperature at this phase boundary for the base of the GHSZ (using Eq. 2). Temperature at the seabed is known from the hydrothermal gradient (given by Eq. 3). A shallow geothermal gradient may thus be computed between seabed and BSR (Eq. 4). As thermal conductivity has been derived from acoustic velocity data, and with shallow geothermal gradient also available, it becomes possible to reapply Fourier's Law (Eq. 5) to derive heat flow for this area through inverse modelling. Estimating the shallow geotherm and heat flow along the full extent of a BSR helps eliminate the bias in heat flow distribution from direct measurements taken at discrete locations (Shankar and Riedel, 2013). This BSR derived heat flow proxy is used in conjunction with the bulk thermal conductivity volume to generate a volume of average geothermal gradient for the bulk volume (rearranging Eq. 5).

Temperature below the seafloor can be summarised as being a function of the depth below the seafloor and the average geothermal gradient. It follows that an estimate of temperature may be arrived at through this simple relationship where the temperature at any given depth point is given by multiplying the average geothermal gradient against the depth to that point:

Equation 7: $T = T_{SEABED} + (\frac{dT}{dZ} \times Z_{SUBSURFACE})$

where *T* is predicted temperature (°C); T_{SEABED} is the temperature at seabed (°C); *dT/dZ* is the average geothermal gradient (°C km^{-1}); and $Z_{SUBSURFACE}$ is the subsurface depth (km). Seabed temperature is added to account for the effect of the hydrothermal gradient on the subsurface temperatures.

As the average geothermal gradient is only valid for the subsurface and due to the seismic input volume containing the water column it becomes necessary to negate the latter. Without flattening the volume to the seabed, it is instead possible to use the seabed depth map to derive a depth volume relative to seabed depth.

Equation 8: $Z_{SUBSURFACE} = Z - Z_{SEABED}$

where $Z_{SUBSURFACE}$ is the subsurface depth (km); *Z* is the absolute depth (km); and Z_{SEABED} is the seabed depth (km).

The steps outlined above are all possible using basic functions available within the Petrel seismic interpretation suite. A pillar grid corresponding to the extent of the seismic survey is built with voxel sizes of 50 m * 50 m * 10 m (~164 ft * 164 ft * 32.8 ft). The original seismic reflection and velocity data can be resampled into the pillar grid. It must be noted that resampling the original data can result in a loss of fidelity from the algorithm used and the size of the voxels comprising the model. The advantage of using such a pillar grid is that computation of the various properties such as velocity derived thermal conductivity (k_V) become easier. It is also easier to model pseudo boreholes in this manner.

Uncertainty modelling

An attempt to model uncertainty was made following the use of 95% confidence interval method as used by Phrampus et al. (2017) to derive bounds for both the heat flow proxy from BSR and the overall temperature prediction. The approach to calculating these bounds can be considered modular for the two aforementioned predicted thermal properties, with the same workflow (Fig. 4) also used here but with an upper bound and lower bound approach for each step as shown in Table 1. For example, to model the lower bound of the shallow heat flow proxy, firstly the lower bound of the root mean square (RMS) of interval velocity across the GHSZ is used to domain convert the TWT BSR pick. This has the effect of varying the BSR in depth, to a shallower depth because of the lower interval velocity selected which in turn would result in a lower temperature for the BSR using the phase relationship described previously. It must be noted that the hydrate phase composition is not varied and that the pressure field is unaltered from previous modelling. Similarly, the seabed depth and temperature are considered unchanged. This gives the lower bound for geothermal gradient. Using the 1D approximation of Fourier's law (Eq. 5) this lower bound geothermal gradient is convolved with the lower bound regression for thermal conductivity from velocity separate from that discussed in Section 3.1 but based on the same 95% confidence interval. This results in the lower bound of the heat flow estimate from the BSR. Using the opposite bound of the various component steps helps arrive at the upper bound for heat flow. The bounds for the temperature prediction can be simplified to varying the bulk thermal conductivity volume and conditioning the model with the upper and lower bound heat flow from BSR. This gives an envelope of temperatures representing the spread of values possible using 95% confidence for all input parameters.

Table 1

Results

The BSR observed in the area has been mapped across the NW and SW quadrants of the 3D reflection seismic coverage (Fig. 6). Though the full extent of the visible BSR was mapped, only the extent corresponding to the highest confidence seismic picks are displayed as the clarity of the BSR degrades towards the edges. This should preclude any resulting anomalous artefacts and edge effects. It is this high confidence extent of the BSR that is referred to in the following sections unless otherwise specified. The BSRs are found to have opposite seismic reflection polarity to the seabed reflection indicating the likelihood of gas hydrate above free gas (Kretschmer et al., 2015). Though there is no record of hydrates from ODP Site 1084, high amplitude reflections are observed to occur in close proximity below the BSR (Fig. 2a), characteristic of the presence of trapped gas. Temperature at BSR depth and the phase relationship used to determine this is shown in Fig. 6.

Figure 6

Neither the exploration well nor ODP Site 1084 fall within the bounds of the thermal model. As a result, direct calibration is not possible. However well 2513/8-1 contains BHT information that may provide some calibration for the predicted results. Pseudo-wells provide a means of simulating 2513/8-1 at a comparable location along strike (Fig. 1a). P1 is projected into the study area following bathymetric contours as close as possible along strike from 2513/8-1, to maintain structural parity. BHT recordings typically are lower than actual formation temperature due to cooling effect of circulating fluids in a borehole and thus they must be corrected (Deming, 1989). There are insufficient points for a Horner correction (Horner, 1951;

Bonté et al., 2012) to be applied and hence a rudimentary correction is made for time since circulation (see https://www.zetaware.com/utilities/bht/timesince.html first accessed August 2018). The predicted temperatures are between 17 and 26% higher than the corrected BHT (Fig. 7a).

Figure 7

On seismic data it was evident that there is a deeply incised canyon like structure trending NE – SW that can be seen in the north-eastern most extent of the seismic volume (Wanke and Toirac-proenza, 2018). This corresponds to the location of P1, which is seen to intersect the channel fill structures of this canyon. It becomes evident then that though P1 was projected into the seismic volume maintaining bathymetric parity, in the subsurface, due to the occurrence of this channel like geometry, it is not possible to maintain stratigraphic parity to 2513/8-1. This is surmised to be the primary factor for the misfit with BHT seen.

Further pseudo-wells (T1 – 3) were modelled to examine the change in thermal profile moving from the proximal section to the distal part of the study area. The results (Fig. 7) display what the thermal profile in these boreholes would be like should a typical geothermal gradient of 30 °C km^{-1} or 40 °C km^{-1} was applied linearly from seabed. The temperature window considered prospective for reservoirs in present day has been referred to as the Golden Zone (60 – 120 °C [140 – 248 °F]) (Nadeau, 2011). It becomes apparent then that the varying geothermal gradient with depth of the proposed model would significantly alter the subsurface depth at which the Golden Zone would begin and end in comparison to the typical linear geothermal gradients that are often considered in a traditional basin modelling workflow. Analysing the geothermal gradient between these pseudo-wells it is seen that in the proximal section (T1) there is a much steeper drop off (~57.1 °C km^{-1} in the uppermost 800 m [~2625 ft] to 15 °C km^{-1} in the deepest 1000 m [~3281 ft]) compared to the intermediate (T2) and deeper sections (T3). The spread of isotherms in a dip section (Fig. 8) reflects this. Isotherm spacing is regular in the Mesozoic section moving into deeper water. However, in the proximal end corresponding to minimal Tertiary cover, there is observed the greatest divergence between isotherms in Mesozoic sediment. Temperature for the Aptian 'Kudu shale' source rock in the region has also been mapped (Fig. 8).

Figure 8

Below both BSRs, but particularly the northern BSR (Fig. 6), the effects of gas blanking were observed in the seismic reflection data. An average interval velocity extraction reveals anomalously low values within this area (Fig. 8). Pseudo-well T4 was modelled to capture this area. The results of this borehole are consistent with the deep-water pseudo-well T3 with similar geothermal gradient at each 1000 m (~3281 ft) interval between the two boreholes.

Discussion

Uncertainty

In a quantitative workflow such as the one discussed in the paper, there are multiple avenues for uncertainty in the constituent steps. Previous literature includes attempts to quantify the uncertainty in predictions using a BSR derived geothermal gradient (5 – 35%) and heat flow (10 – 50%) (Grevemeyer and Villinger, 2001). Such attempts have usually quantified uncertainty for the component steps rather than the compound uncertainty for the entire process. For this work, with a lack of well data for ground truthing, the temperature estimation bounds for 95% confidence were used to give an idea of the range within which the estimates can vary. It is important to note the impact of variability in input factors for the component steps. For example, results from the Blake Ridge show that actual temperatures at the BSR depth could be between 0.5 – 2.9 °C (32.9 – 37.22 °F) lower than the temperature predicted by the hydrate phase relationship for that particular depth and pressure (Wood and Ruppel, 2000). This implies that a significant source of uncertainty in the thermal modelling could result from the assumptions made about the conditions at the base of the GHSZ. As stated earlier, an assumption has been made on the lattice fluid and trapped gas mix for the hydrate zone in the absence of direct piston core sampling. Varying gas compositions can vary the hydrate stability and thus alter the temperature at the bottom simulating reflector (Chand et al., 2008). The prevalence of methane hydrates globally leads us to assume it is the most likely composition of the hydrates in the study area.

BWT fluctuations, both the magnitude and time scale for which they occur provide another element of uncertainty. It must be noted that the strong Benguela Current flows along the Namibian margin in this area and it is difficult to directly factor in the impact that this may have on the modelling. However, the data used to generate a model of the hydrothermal gradient in the area utilised NOAA data that have been averaged annually over an eight-year period. It thus hoped that any temporal perturbations of BWT are accounted for by this dataset.

The quality of the initial velocity model is another source of uncertainty. As thermal conductivity is derived from it using a direct empirical relationship, any anomalies in the existing velocity model or velocity data will be translated into the derived properties. From the low spread of RMS interval velocities for the GHSZ it is apparent the application of a default 1500 m s^{-1} (~4921 ft s^{-1}) velocity above seabed during the velocity model building stage results in a heavily smoothed velocity model. This is expected to be reflected in the nature of the temperature profile generated using velocities as input.

In the absence of a reliable heat flow recording for this area, a BSR derived heat flow proxy has been used. This is a shallow heat flow as it uses an average velocity derived thermal conductivity and geothermal gradient valid within the GHSZ (Eq. 5). Unlike in traditional basin modelling the radiogenic heat production of the rock column has not been integrated.

Instead, this solitary heat flow proxy has been used to condition the model for an average geothermal gradient. Though hydrothermal fluid circulation in the subsurface can also greatly alter heat flow, both vertically and laterally, the study area is likely to be minimally impacted in this regard. As the study area is sufficiently distant from a neighbouring seamount to negate the convective and advective heat flow impact of hydrothermal fluid circulation, heat transport in this area is predominantly conductive. Therefore, the assumption is of limited lateral heat flow variability, which is backed by the BSR-derived thermal gradients and derivative heat flow estimates. In a separate case study covering the data rich North Sea, it has been shown that the reflection seismic thermometric process can be conducted successfully using laterally varying shallow heat flow as an input (Sarkar, 2020). An idea of the uncertainty of the heat flow derived in this manner has been computed using the method shown in Phrampus et al. (2017). Heat flow is found to range between 46.2 – 76.2 mWm^{-2} (~0.01465 – 0.02416 BTU h^{-1} ft^{-2}), with the weighted mean for the heat flow used for computation of the temperature model equal to 63.8 mWm^{-2} (~0.02022 BTU h^{-1} ft^{-2}). The lower bound of the derived ranged is consistent with results from Macgregor (2020) while the upper bound would be in line with the preferred prediction from the global map in Lucazeau (2019). The weighted mean is interestingly consistent with the continental margin heat flow mean reported by Davies (2013). The heat flow range given by the bounds is consistent with observational data and estimations of heat flow from age relationships corresponding to this area (Hamza and Vieira, 2012).

Implications

As stated previously, the source maturity of the Aptian Kudu shale interval in the Lüderitz Basin is a key unknown in terms of the petroleum systems elements. With the thermal modelling workflow indicating an average temperature of 133.5 °C (272.3 °F) across the top of this Barremian structure (Fig. 8a), the base of the overlying Kudu shale source rock immediately above would therefore lie in the gas generation window (Bjørlykke et al., 1989). This is consistent with the nearby Kudu fields which produce gas condensate from the same Aptian source interval. The results would suggest then that the Lüderitz Basin has an improved prospectivity outlook with the potential for a working hydrocarbon system with gas charged reservoirs.

It was possible in this study to estimate present day temperature at key subsurface target depths in a frontier setting in the absence of any substantive well control. The workflow presented would enable seismic operators to utilise the data libraries of seismic reflection and velocity data available to them to generate present day estimations of subsurface temperature in a non-invasive manner, prior to an expensive drilling campaign. It is hoped that this would help streamline petroleum systems analysis and provide an additional dataset for basin modellers to use with the aim of decreasing the uncertainty with which frontier regions are explored.

Conclusions

The model proposed in this study is a simple and robust methodology for estimation of present-day subsurface temperature in frontier areas lacking borehole control for temperatures. It makes use of readily available seismic reflection and velocity data in a workflow developed on an industry standard software suite. It highlights how existing workflows for BSR derived heat flow may be combined with existing experimental thermal conductivity and velocity data for various lithologies to develop an empirical transform that may be applied to seismic velocity models. Given thermal conductivity and P wave velocity have sensitivity to similar parameters, this methodology would allow the user to examine the vertical and lateral variability in thermal properties in a frontier basin especially when high-quality pre-SDM and FWI velocity models are available. The results of the case study documented here suggest that the main prospect lies just below the golden zone and that sources rocks are in the generative window.

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Figures

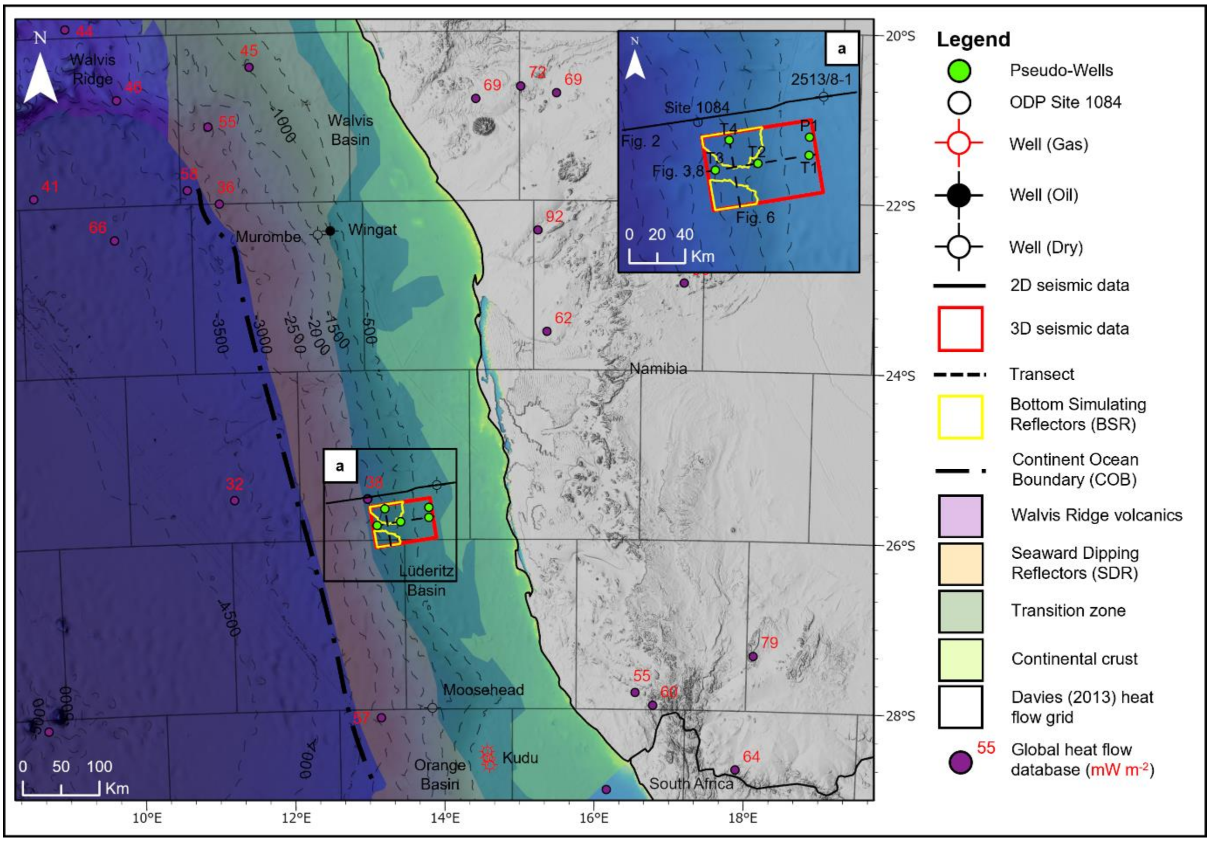

Figure 1: Location map displaying Lüderitz Basin area of interest with available seismic data, using a UTM projection. Key geological, structural and bathymetric features offshore Namibia are highlighted (contour intervals of 500 m [~1640 ft]), adapted from (Bray et al., 1998; Gladczenko et al., 1998; Becker et al., 2009)*. (a) Inset map displaying extent of seismic data available, mapped BSRs, modelled pseudo wells and transects along which modelling has been conducted. Example open source global heat flow databases are shown in the form of borehole data* (Gosnold and Panda, 2002) *and Davies (2013) heat flow grid. Regional exploration wells in neighbouring Walvis & Orange Basins are shown for context.*

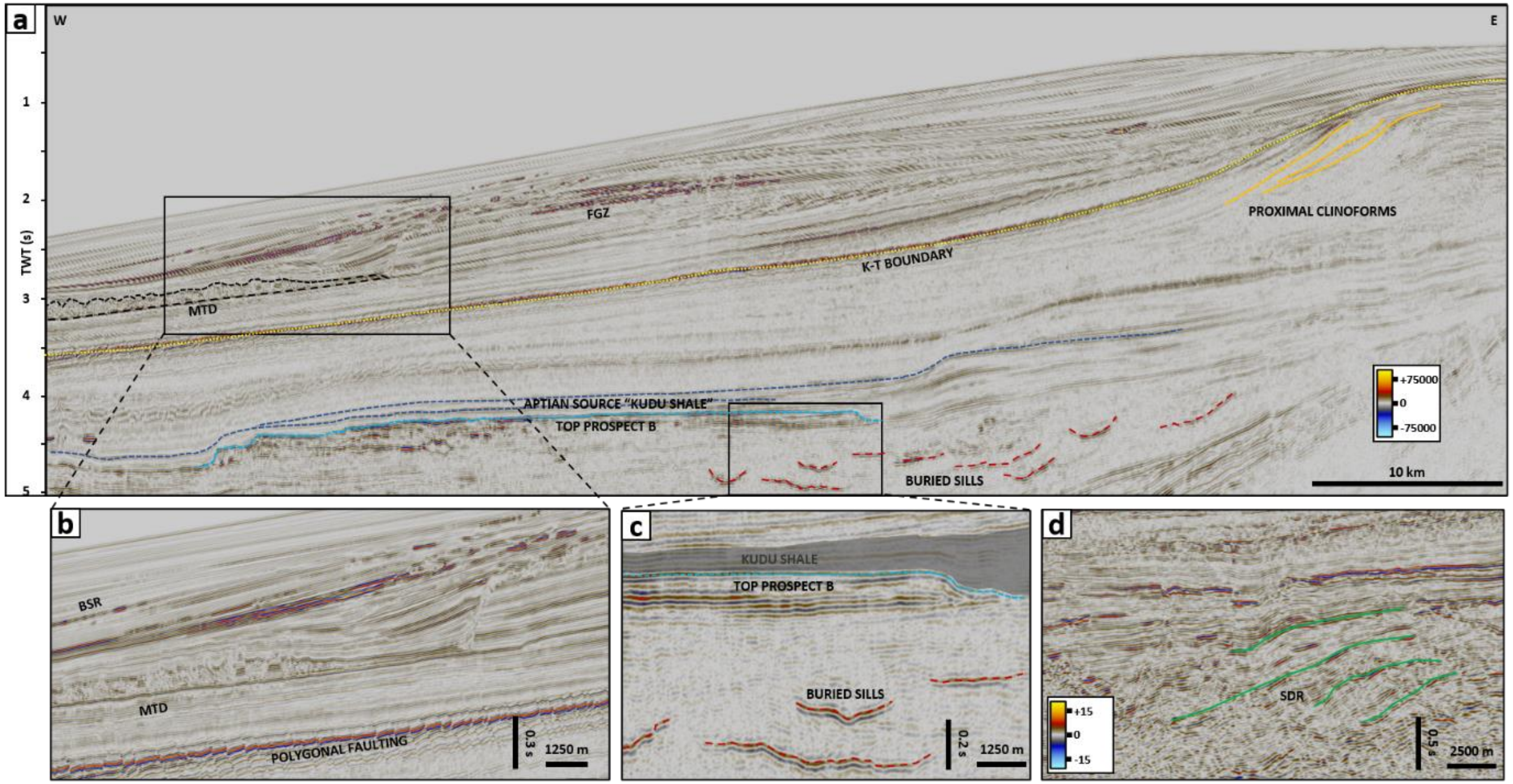

Figure 2: (a) West-East transect displaying two-way travel time (TWT) seismic reflection structure in the Lüderitz Basin. Features visible include clinoforms in near shore section, with BSR, free gas zone (FGZ) below it highlighted by bright reflectors (associated with gas) and mass transport features in Tertiary section; (b) Close up of shallow Cenozoic sediments displaying MTD complexes. Cretaceous – Tertiary (K-T) boundary marked by intense polygonal faulting; (c) Close up of deeper Mesozoic section highlighting intrusive sills beneath a mounded platform like structure (believed to be a Barremian carbonate reef) overlain by Aptian age "Kudu shale" source rock interval; (d) Close up of SDRs at depth in the distal section 2D seismic line (Fig. 1a). TWT = Two-way travel time; BSR = Bottom simulating reflector; FGZ = Free gas zone; MTD = Mass transport deposit; K-T = Cretaceous-Tertiary; SDR = Seaward dipping reflectors.

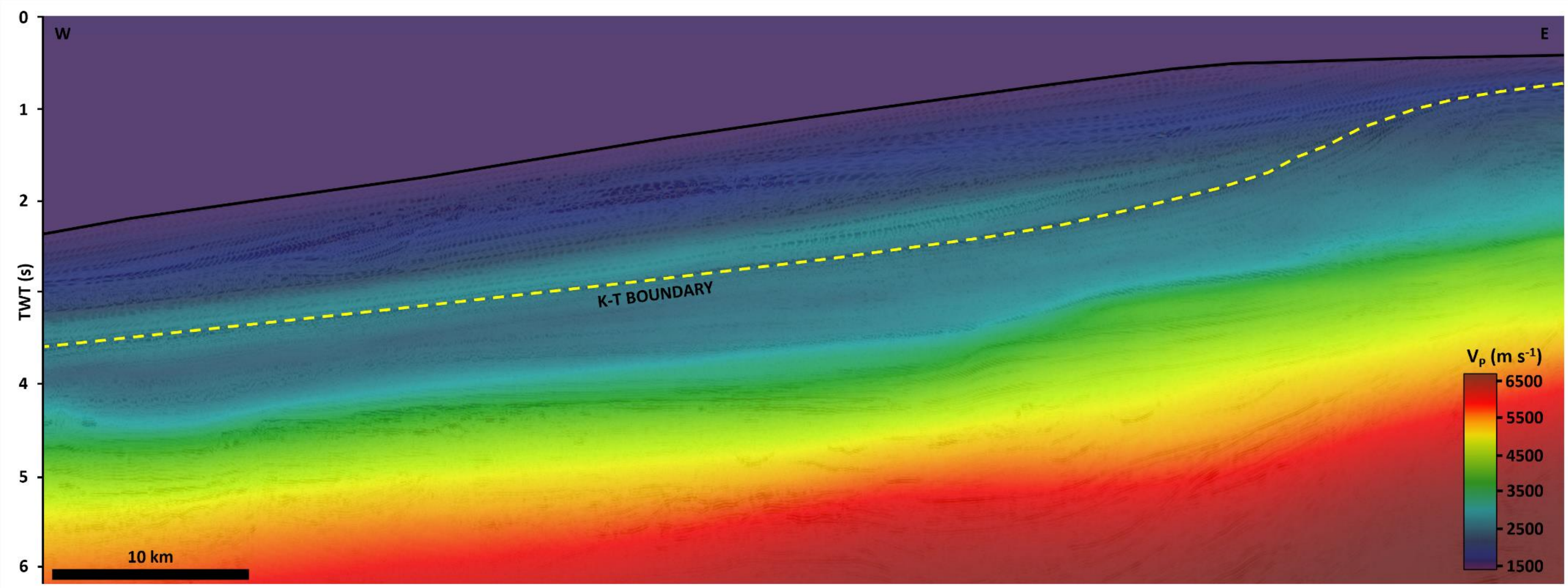

Figure 3: West-East transect (Fig. 1) of seismic reflection volume in time domain overlain with interval velocities and K-T boundary highlighted. Velocities near seabed (indicated by the black line) are low (close to water velocity). Overall Tertiary section is characterised by low velocities. Velocity inversion seen near K-T boundary (yellow dashed line). K-T = Cretaceous-Tertiary.

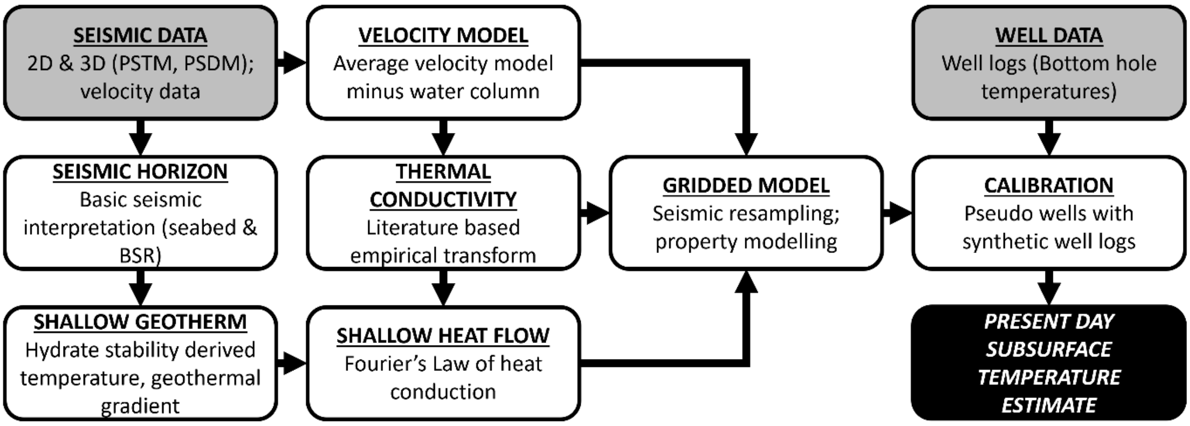

Figure 4: Schematic summary of the steps involved as part of the seismic led temperature estimation methodology explored in this paper. It utilises an adaptation of the reflection seismic thermometry workflow first presented in (Sarkar, 2020). *PSTM = Post Stack Time Migrated; PSDM = Post Stack Depth Migrated; BSR = Bottom Simulating Reflector.*

Figure 5: Empirical velocity to thermal conductivity transform utilising experimental datasets from published literature. These measurements are made on samples in laboratory conditions and represent a wide range of lithologies. Furthermore, only results from wet sample measurements are displayed, as the transform will be applied in the shallow subsurface where there is very likely to be fluid fill (for example the GHSZ). Measurements were made using transient method (using optical scanning equipment). GHSZ = Gas hydrate stability zone.

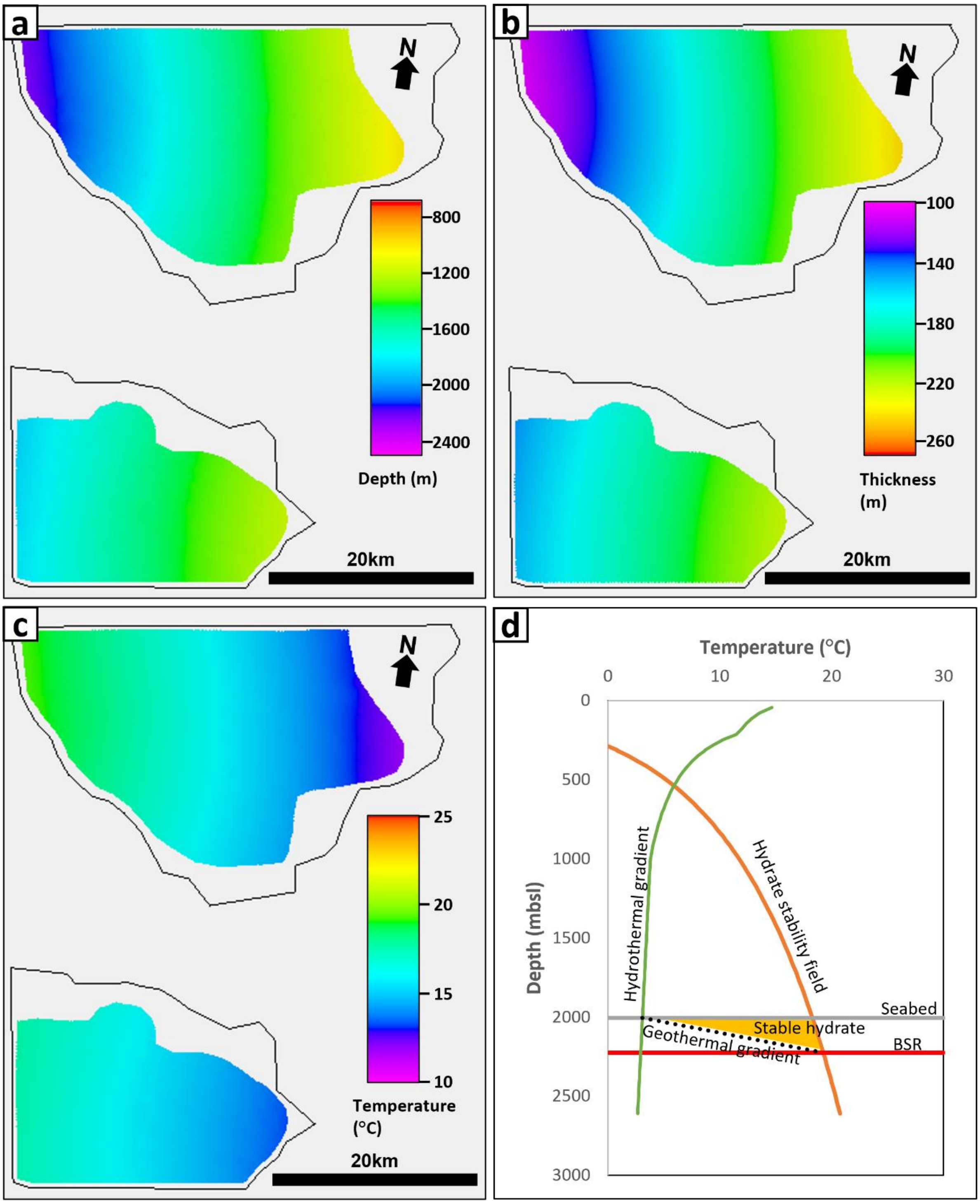

Figure 6: BSR attributes (a – depth; b – GHSZ thickness; & c – temperature at base of GHSZ) are displayed for high confidence area only, with black polygon representing whole BSR interpretation on seismic. (d) Hydrate stability diagram for a pure methane-seawater system, used to compute temperature at the phase boundary (Fig. 6c). A synthetic hydrothermal gradient is shown, computed using the annualised mean temperature data points from the 1 degree resolution dataset of the WOA (Locarnini et al., 2013)*. The hydrate*

*stability zone has an average thickness of 184 m (~604 ft) as observed within the study area (Fig. 6b). The cumulative area of both the mapped BSRs is 0.941*10^{9} m^{2} (~1.01*10^{10} ft^{2}). Assuming all the sediment above the BSRs contain gas hydrate, a typical hydrate saturation of 10 % (Waite et al., 2009) would yield a potential methane hydrate volume of 1.73*10^{10} m^{3} (~6.11*10^{11} ft^{3}). BSR = Bottom Simulating Reflector; GHSZ = Gas Hydrate Stability Zone; WOA = World Ocean Atlas.*

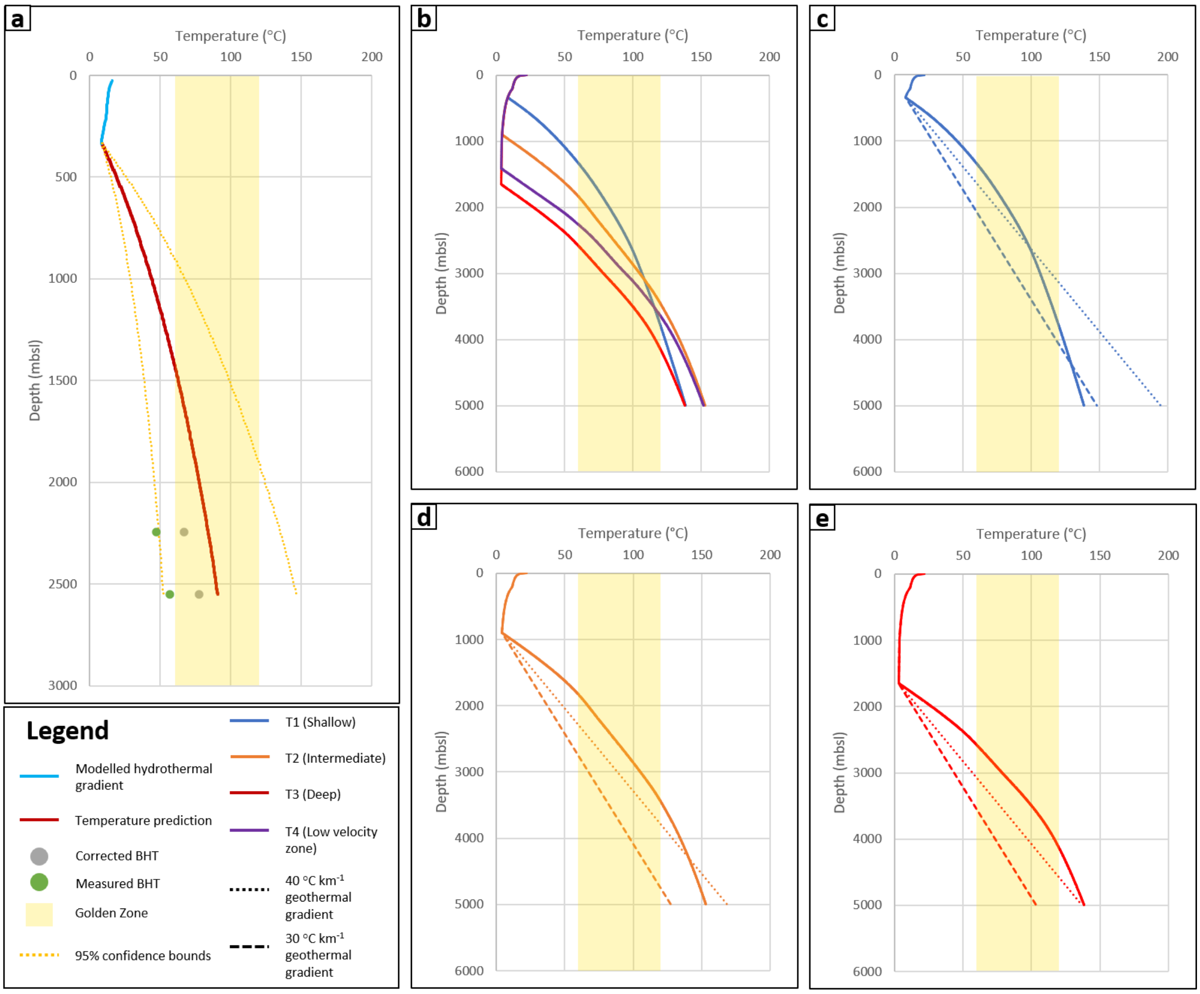

Figure 7: Modelled borehole results for subsurface temperature with Golden Zone interval overlain for reference. (a) Thermal profile for pseudo borehole P1 simulating 2513/8-1 with corrected and uncorrected BHT readings. 95% confidence upper and lower bounds are also displayed. (b) Thermal profile for boreholes T1-T4. (c) T1 shallow water thermal profile with modelled linear geothermal gradients. (d) T2 intermediate water depth thermal profile with modelled linear geothermal gradients. (e) T3 deep water thermal profile with modelled linear geothermal gradients. (c-e) Modelling subsurface temperature with typical linear geothermal gradients highlights the variability in depth expected for the Golden Zone. BHT = Bottom hole temperature.

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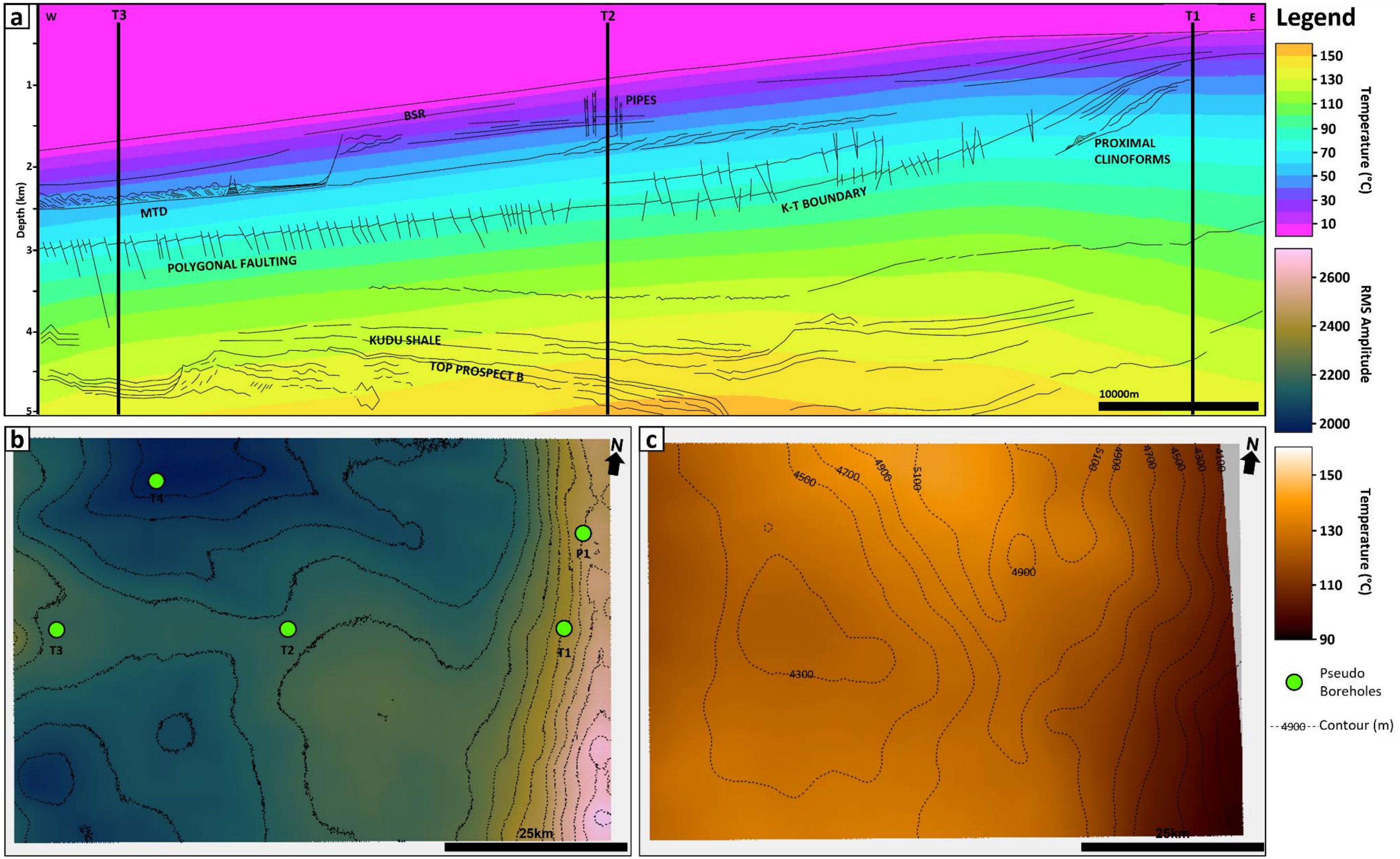

a
W
T3
T2
T1
E
Depth (km)
1
2
3
4
5
PIPES
BSR
PROXIMAL
CLINOFORMS
MTD
K-T BOUNDARY
POLYGONAL FAULTING
KUDU SHALE
TOP PROSPECT B
10000m
Legend
Temperature (°C)
150
130
110
90
70
50
30
10
RMS Amplitude
2600
2400
2200
2000
b
N
T4
P1
T3
T2
T1
25km
c
4500
4700
4900
5100
4900
4700
4500
4300
4100
4900
4300
25km
Temperature (°C)
150
130
110
90
Pseudo Boreholes
4900 Contour (m)

Figure 8: (a) Depth profile with temperature predicted from seismic model overlain. Boreholes corresponding to shallow, intermediate, and deep water are marked. (b) RMS velocity extraction of interval velocities (for interval up to 2 s below seabed) highlighting the zone of low velocities encountered below the Northern BSR. Borehole T4 specifically targets this. (c) Temperature prediction from the model mapped across the base of the Aptian source rock above the mounded structure referred to as Prospect B (Fig. 2c). The thermal model produced was used to interrogate the predicted present-day temperature for the base of the source rock interval as shown in Fig. 2c. The temperature ranged between 93.2 – 157.2 °C [200 – 315 °F] for a depth range of 3400 – 5400 mbsl [~11155 – 17717 ftbsl]. Scientific colour bar templates based on (Crameri et al., 2020)*. RMS = Root Mean Squared; BSR = Bottom Simulating Reflector; mbsl = metres below sea level; ftbsl = feet below sea level.*