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Abstract

Matched Field Processing (MFP) is a technique to locate the source of a recorded wave field. It is the generalization of beamforming, allowing for curved wavefronts. In the standard approach to MFP, simple analytical Green's functions are used as synthetic wave fields that the recorded wave fields are matched against. We introduce an advancement of MFP by utilizing Green's functions computed numerically for real Earth structure as synthetic wave fields. This allows in principle to incorporate the full complexity of elastic wave propagation, and through that provide more precise estimates of the recorded wave field's origin. This approach also further emphasizes the deep connection between MFP and the recently introduced interferometry-based source localisation strategy for the ambient seismic field. We explore this connection further by demonstrating that both approaches are based on the same idea: both are measuring the (mis-)match of correlation wave fields. To demonstrate the applicability and potential of our approach, we present two real data examples, one for an earthquake in Southern California, and one for secondary microseism activity in the Northeastern Atlantic and Mediterranean Sea. Tutorial code is provided to make MFP more approachable for the broader seismological community.

Keywords

Seismic noise, Seismic Interferometry, Interferometry, Wave propagation

1 Introduction

The ambient seismic field has become an attractive target of seismological studies over the last two decades (Nakata et al., 2019). Interferometry of this complex wave field, combined with increased

25 station density, has enabled detailed studies of Earth's structure (e.g., Shapiro et al., 2005; Lu et al.,
26 2018; Schippkus et al., 2018) and its temporal changes (e.g., Brenguier et al., 2008; Hadziioannou
27 et al., 2011). Such studies rely most commonly on seismic wave fields generated by the interaction
28 between the oceans and the solid Earth, so-called microseisms. Understanding the exact mechanism
29 for this interaction has been a challenge for more than half a century (Longuet-Higgings, 1950;
30 Hasselmann, 1963; Ardhuin et al., 2015) and some open questions remain, e.g., about the emergence
31 of Love waves in the secondary microseism (Ziane & Hadziioannou, 2019; Gualtieri et al., 2020).
32 More recently, other sources such as trains (Fuchs et al., 2017; Brenguier et al., 2019; Liu et al.,
33 2021), wind turbines (Stammler & Ceranna, 2016; Hu et al., 2019), direct wind-land interaction
34 (Johnson et al., 2019), rain (Dean, 2019), and rivers (Burtin et al., 2008; Smith & Tape, 2019)
35 have become the focus of several studies investigating high-frequency seismic noise.

36 To study all of these sources in detail and understand their mechanisms, precise knowledge of
37 their locations is necessary. Dense installations of seismic stations near known sources can provide
38 intriguing insight into the sources' interactions with the solid Earth (Riahi & Gerstoft, 2015), and
39 can give evidence for previously unrecorded interactions (Schippkus et al., 2020). Installations like
40 these are not widely available, though. For other sources, it may not be technically feasible to install
41 stations close to all expected source locations, e.g., in the deep oceans to study ocean microseisms
42 or in the Earth's subsurface. Beyond the interest in the fundamental principles of seismic wave
43 generation by different sources, studies that rely on interferometry of the ambient seismic field to
44 gain knowledge about Earth's structure ideally incorporate a priori knowledge of source locations to
45 account for the potential bias introduced by their spatial distribution (Fichtner et al., 2017; Sergeant
46 et al., 2020). Strategies of earthquake seismology to locate seismic sources, such as travel-time
47 inversion, are not applicable to ambient seismic noise due to the complexity of the analysed wave
48 field. There is not one single dominant source (e.g., an earthquake or explosion) that results in
49 clearly identifiable and thus exploitable phase arrivals in seismograms across several stations.

50 Instead, strategies have emerged that aim to quantify the angle of arrival of seismic energy
51 in recorded seismograms, emitted by sources of unknown type (Fig. 1a,b). Polarization analysis
52 exploits the particle motion of the seismic wave field at one location \vec{x}_j , resolved by three-component
53 seismometers (Fig. 1a, e.g., Schimmel & Gallart, 2003). Depending on the analysed wave type, the
54 particle motion gives an indication of the angle of arrival. When combining results from multiple
55 stations, this analysis can be used to triangulate the source location \vec{x}_s (e.g., Schimmel et al., 2011).
56 However, a number of assumption have to be made, e.g., great-circle propagation, as well as proper

57 identification and clear separation of wave types. This approach can be a first step in understanding
58 the recorded wave field, but is often quite tricky in practice, especially on recordings of ambient
59 seismic noise (Gal & Reading, 2019).

60 Beamforming is a source localisation approach based on the assumption that seismic waves
61 propagating across seismic arrays can be treated as plane waves, if their wavelengths are much larger
62 than the aperture of the array (Fig. 1b). To test whether a candidate plane wave - characterised by
63 its horizontal slowness or equivalently arrival angle and apparent velocity - was recorded on the array,
64 expected relative time delays $\Delta t(\vec{x}_j, \vec{x}_k)$ between the stations are computed and corrected for. This is
65 called delay-and-sum beamforming, where each seismogram is shifted in time and summed together,
66 forming the beam (Rost & Thomas, 2002). The quality of the beam is evaluated, giving the so-called
67 beampower. Other formulations of this method exist, e.g., an equivalent cross-correlation approach
68 (Ruigrok et al., 2017). Beamforming has been widely adopted by the seismological community and is
69 currently the standard tool for identifying sources of the ambient seismic field (Gal & Reading, 2019,
70 and references therein). Recent advances focus on incorporating three-component seismograms
71 (Riahi et al., 2013; Juretzek & Hadziioannou, 2016, 2017), avoiding bias introduced by averaging
72 across broad frequency bands (Gal et al., 2014), or estimating surface wave anisotropy directly from
73 beamforming (Löer et al., 2018). Beamforming has its main advantages in computational speed,
74 little if any data processing, and high time resolution. Its main drawbacks all result from the plane-
75 wave assumption: sources have to be far from the array, the wave field has to be strictly coherent
76 across stations, and the array geometry limits the resolution capabilities (Rost & Thomas, 2002).
77 For a recent review of beamforming and polarization analysis see Gal & Reading (2019).

78 A new source localisation strategy based on seismic interferometry has been introduced in recent
79 years as an attractive alternative, sometimes referred to as kernel-based source inversion (Ermert
80 et al., 2016). The goal of this approach is not to determine the angle of arrival, but to directly
81 quantify the distribution of seismic sources in space. Interferometry of the ambient seismic field
82 recorded on multiple stations gives new wave fields, propagating to and from the respective reference
83 stations (Fig. 1c, Aki, 1957; Wapenaar et al., 2010; Campillo & Roux, 2015; Fichtner et al., 2017).
84 An inhomogeneous distribution of sources results in asymmetric cross-correlation functions, indicated
85 by the thickness of the wave fronts in Fig. 1c (Paul et al., 2005). In practise, this asymmetry is
86 usually quantified by comparing the causal and acausal part of each correlation function. In the
87 interferometry-based approach, synthetic cross-correlation functions are computed for a given source
88 distribution and compared against cross-correlation functions from real data. The mismatch between

89 the two is evaluated (e.g., by quantifying amplitude asymmetry), the source model perturbed, and a
90 best-fit source distribution is found via gradient descent in an iterative manner (Ermert et al., 2016).
91 Recent work has focused on improving efficiency (Igel et al., 2021b), the mismatch measure (Sager
92 et al., 2018), or expanding the method to multiple frequencies (Ermert et al., 2021). The advantages
93 of this approach are the stability of results, not as strict requirements on station geometry, and a
94 comprehensive theoretical foundation. Its disadvantages lie in computational cost, treatment of
95 recorded data, through that introduction of assumptions, and loss of temporal resolution.

96 Another approach that has gained some popularity in seismology in recent years is Matched
97 Field Processing (MFP). MFP is the generalisation of beamforming to allow arbitrary wavefronts
98 (Baggeroer et al., 1993). This approach has been developed in ocean acoustics, where coherency
99 of the wave field emitted by transient sources is high even for stations far away. Candidate sources
100 are defined in space and absolute travel times $t(\vec{x}_j, \vec{x}_s)$ are computed based on true distance to the
101 source (Fig. 1d). Synthetic wave fields are computed for these travel times and matched against
102 the recorded wave field. In the seismological context, MFP has been applied successfully on local
103 (Corciulo et al., 2012; Umlauf & Korn, 2019; Umlauf et al., 2021) and regional scale (Gal et al.,
104 2018). Recent developments in MFP include the development of different beamformers (e.g., Zhu
105 et al., 2020), improved estimation of travel times (Gal et al., 2018), or estimating synthetic wave
106 fields empirically (Gibbons et al., 2017). MFP is an attractive strategy for source localisation of the
107 ambient seismic field. It allows for curved wavefronts, is based on only few assumptions, requires no
108 intermediate step such as pre-processing of recordings, and retains computational efficiency. While
109 the plane-wave assumption is neglected in MFP, coherency of the wave field across stations is still
110 required for good results. This poses challenges when analysing recordings for stations that are not
111 close together, and especially so for ambient seismic noise.

112 In this paper, we introduce an advancement of MFP to incorporate real Earth structure and
113 account for the complexity of seismic wave propagation. In the following, we introduce the standard
114 MFP approach, demonstrate its shortcomings, and present our solution by incorporating realistic
115 Green's functions. We discuss implications of our approach, strategies to cope with some of them,
116 how different disciplines and localisation approaches intersect, and finally demonstrate the applica-
117 bility of our approach on two real data examples.

118 2 Matched Field Processing

119 The MFP algorithm is straight-forward: For a given potential source location, a synthetic wave field
 120 is computed and matched against the recorded wave field, i.e., the seismograms, taking coherency
 121 of the wave fields across stations into account. This match is evaluated and compared against
 122 other potential source locations. The potential source location with the highest score or beampower
 123 (representing the best-matching synthetic wave field) is the resolved source location.

124 More precisely, spectra $d(\omega, \vec{x}_j)$ are computed from the recorded seismograms at each receiver
 125 position \vec{x}_j . The cross-spectral density matrix is computed as

$$K_{jk}(\omega) = d^*(\omega, \vec{x}_j)d(\omega, \vec{x}_k), \quad (1)$$

126 with $*$ denoting the complex conjugate. $K_{jk}(\omega)$ holds all information about the recorded wave
 127 field and encodes its coherency across stations; it contains the cross correlations of the seismograms
 128 from all station pairs. Following Bucker (1976), auto correlations are excluded, i.e., only components
 129 $k \neq j$ are computed and later utilized. This is particularly useful in the context of ambient seismic
 130 noise, because noise wave fields are likely to be only weakly coherent across stations.

131 The synthetic wave field, i.e., the seismograms expected at each station from the candidate
 132 source, is represented through synthetic spectra $s(\omega, \vec{x}_j, \vec{x}_s)$, with \vec{x}_s the source position and \vec{x}_j the
 133 receiver position. In principle, these could be estimated in the time domain, but MFP computations
 134 are done in frequency domain for simplicity and computational speed. More on how these are
 135 computed in practise in section 2.1 and onwards.

136 The match of the two wave fields represented through $K_{jk}(\omega)$ and $s(\omega, \vec{x}_j, \vec{x}_s)$ is then estimated
 137 through a so-called beamformer or processor. The most straight-forward beamformer is the con-
 138 ventional beamformer, which in its most compact form in vector notation is often written as (e.g.,
 139 equation 25 in Baggeroer et al., 1993)

$$B = \mathbf{s}^* \cdot \mathbf{K} \cdot \mathbf{s}, \quad (2)$$

140 with B the beampower score for a potential source location. In literature, this beamformer is
 141 sometimes called Bartlett processor, although the origin of this name is unclear (e.g., Gal & Reading,
 142 2019), linear beamformer (e.g., Baggeroer et al., 1993), or frequency-domain beamformer (DeMuth,
 143 1977). We express B more explicitly, excluding auto correlations, for clarity as

$$B = \sum_{\omega} \sum_j \sum_{k \neq j} s_j^*(\omega, \vec{x}_j, \vec{x}_s) K_{jk}(\omega) s_k(\omega, \vec{x}_k, \vec{x}_s). \quad (3)$$

144 Other estimators of beampower exist, and their development is an active field of research (e.g.,
 145 Capon, 1969; Schmidt, 1986; Cox et al., 1987; Cox, 2000; Gal et al., 2014; Zhu et al., 2020).
 146 Beamformers are often classified into conventional (eq. 3), adaptive (e.g., Capon, 1969; Cox et al.,
 147 1987; Cox, 2000) and sub-space beamformers (e.g., Schmidt, 1986). Adaptive beamformers aim to
 148 increase resolution of the beampower distribution by increasing sensitivity to signal, but inherently
 149 rely on high signal-to-noise ratio (SNR). The increased resolution is also accompanied by increased
 150 computational cost, e.g., the Capon beamformer involves computing the inverse of $K_{jk}(\omega)$ (Capon,
 151 1969). Sub-space detectors such as MUSIC (Schmidt, 1986) involve computation of the eigenvectors
 152 of $K_{jk}(\omega)$, and making a selection of those for further computations based on which eigenvectors
 153 contribute to the signal and which are "noise". Corciulo et al. (2012) used a similar approach and
 154 were able to resolve multiple sources this way. One of the expressed goals of the approach we
 155 introduce in this paper is to be able to locate sources of ambient seismic noise, and as such SNR
 156 is by definition low. Beamformers beyond the conventional beamformer may not be appropriate for
 157 this, because they either require high SNR or a choice of what part of the cross-spectral density
 158 matrix is signal and what is "noise". Krim & Viberg (1996) have addressed the question of which
 159 beamformer performs best under what circumstances for standard MFP before. A detailed analysis
 160 of this in the context of our approach we introduce here is beyond the scope of this paper.

161 2.1 Synthetic wave field in the standard approach

162 In practise, assumptions and simplifications about structure and wave propagation have to be made
 163 in order to compute the synthetic wave fields $s(\omega, \vec{x}_j, \vec{x}_s)$ that the recorded data are matched against.
 164 In most seismological and almost all ocean acoustics applications so far, simple analytical Green's
 165 functions of the form

$$s(\omega, \vec{x}_j, \vec{x}_s) = e^{-i\omega t(\vec{x}_j, \vec{x}_s)}, \quad (4)$$

166 are used, with $t(\vec{x}_j, \vec{x}_s)$ the travel time of the investigated wave between source and receiver (Fig.
 167 1d). In some seismological studies, the addition of an amplitude term $A(\vec{x}_j, \vec{x}_s)$ that accounts for
 168 geometrical spreading and/or inelastic attenuation has been discussed (Corciulo et al., 2012; Bowden
 169 et al., 2020). The goal of such a term would be to increase the accuracy of the synthetic wave field
 170 by incorporating some of the seismic waves' propagation behaviour. Neglecting the amplitude term
 171 entirely, as is usually done, makes standard MFP equivalent to delay-and-sum beamforming without
 172 the plane-wave assumption (Bucker, 1976). More on this in section 2.4.

173 In the simplest possible study target, i.e., a single stationary source in an isotropic, homogeneous

174 medium with constant velocity $v = \text{const}$ and only straight-ray propagation of a single phase, the
175 travel time is simply $t(\vec{x}_j, \vec{x}_s) = \Delta x/v$. This requires prior knowledge of v and the assumption that
176 $v = \text{const}$ is a good approximation of the medium. In seismology, this approach has been successfully
177 demonstrated on local scale (e.g., Corciulo et al., 2012; Umlauf & Korn, 2019; Umlauf et al., 2021),
178 where propagation effects due to heterogeneous Earth structure can be neglected. Without any prior
179 knowledge of the velocity structure, another approach is to treat v as an additional dimension in the
180 parameter space that needs to be explored, though this can become computationally quite expensive
181 and may require sampling strategies other than a standard grid search (Gradon et al., 2019).

182 On regional scale, Gal et al. (2018) estimated $t(\vec{x}_r, \vec{x}_s)$ from already available phase velocity
183 maps using Fast Marching Method (Sethian, 1999), which accounts for off-straight-ray propagation
184 of surface waves, and by that incorporating some complexity of wave propagation in real Earth
185 structure. This approach also inherently incorporates frequency-dependent effects, i.e., $t(\vec{x}_r, \vec{x}_s)$
186 becomes $t(\vec{x}_r, \vec{x}_s, \omega)$. Gal et al. (2018) used this to study the primary (~ 16 sec. period) and
187 secondary (~ 8 sec. period) microseism separately by estimating phase travel times from their
188 respective phase velocity maps. This approach requires knowledge of the analysed wave type. Gal
189 et al. (2018) solve this by rotating seismograms into the radial/transverse-system and assuming
190 that for the chosen frequencies (microseism), surface waves are dominant and only recorded on their
191 respective component (Love on transverse, Rayleigh on radial). This is a reasonable assumption,
192 commonly made when analysing ocean microseism (Nakata et al., 2019), but may not always be
193 appropriate depending on the study target. Incorporating multiple phases (e.g., a mix of body
194 and surface waves) at the same frequency is not straight-forward with the standard approach and
195 clearly requires further assumptions about the number of phases and their respective travel times,
196 increasing the parameter space considerably. Furthermore, when investigating frequencies at which
197 the identification of wave types may be challenging, this strategy potentially misses or misattributes
198 important information in the recorded wave field and may bias results. Approaching the complexity
199 of wave propagation in real Earth structure in this manner seems quite cumbersome and impractical,
200 as it ends up requiring manual consideration of all of these effects.

201 **2.2 Numerical synthetic wave fields for complex Earth structure**

202 We propose to use Green's functions computed numerically for Earth structure directly as the syn-
203 thetic wave field $s(\omega, \vec{x}_r, \vec{x}_s)$ ("our approach") instead of the analytical form described above (eq.
204 4, "standard approach"). Effects such as dispersion and multiple wave types are then inherently ac-

205 counted for, even for simple 1D media. If the Green's function are computed for a 3D Earth, further
206 effects such as focusing and defocusing, wave-type conversion, and coupling can all be accounted
207 for, increasing the precision of this approach further.

208 We demonstrate our method with synthetic examples for a broadband and a narrowband explosion
209 source (Fig. 2). The setup consists of two small arrays of three stations each that record the wave
210 field emitted by a seismic source located at the surface between them. The medium is a 3D
211 axisymmetric Earth (Nissen-Meyer et al., 2014), based on PREM (Dziewonski & Anderson, 1981).
212 The "recorded" seismograms are computed for the same model and incoherent noise is added. With
213 the standard MFP approach (assuming $t(\vec{x}_r, \vec{x}_s) = \Delta x/v$), locating the source precisely is quite
214 challenging for both broad- and narrowband sources (Fig. 2a, c). The resolved location is clearly
215 sensitive to the chosen velocity of the medium v . When the chosen velocity is too low, the resolved
216 source lies further away than the real source. When it is too high, the resolved source lies closer.
217 This applies to both broadband and narrowband sources (Fig. 2a, c). For the broadband source,
218 the highest frequency available in the numerical Green's functions is 0.2 Hz. The error in location
219 introduced for $v = 3.0$ km/s is smaller for the broadband source than for the narrowband source.
220 This occurs, because the broadband wave field contains phases that are of different type and travel
221 with different velocities, and $v = 3.0$ km/s is a good estimate for at least some of them. For
222 the narrowband wave field, which contains mainly Rayleigh waves at 0.13-0.15Hz, $v = 3.0$ km/s is
223 already clearly too slow. For surface waves in particular, a different choice of velocity v for each
224 analysed frequency band would seem appropriate due to their dispersive nature (Gal et al., 2018).

225 With Green's functions computed numerically for the same Earth structure, the location of the
226 source is resolved precisely for both broad- and narrowband sources (Fig. 2b, d). This is unsurprising,
227 given that we are essentially matching the synthetic wave field against itself with some noise. But
228 this is also exactly the intent behind the approach: matching the recorded wave field with a more
229 realistic synthetic wave field. Our simple synthetic tests show that the standard approach can be
230 imprecise for locating realistic sources in slightly complex media, even under ideal conditions, and is
231 highly dependent on choosing the correct velocity. With our approach, we do not have to consider
232 frequency-dependant effects explicitly as long as the numerical Green's functions applied are a good
233 representation of elastic wave propagation.

234 MFP for narrowband sources results in prominent side lobes of beampower, regardless of approach
235 (Fig. 2c,d). These are interference patterns that emerge because MFP is ultimately a correlation-
236 based measure of waveform fit (more on that in section 2.4). The exact shape and position of

237 sidelobes depends on the station distribution and wavelength of the investigated wave, while the
238 correct location does not. Sidelobes will be suppressed, if a wide frequency band is used (Fig. 2a,b)
239 or several runs of MFP for narrow neighbouring frequency bands are stacked (Umlauf et al., 2021).
240 MFP originated as a narrowband localisation technique (Bucker, 1976) and has been adopted for
241 broadband sources thereafter (e.g., Baggeroer et al., 1993; Brienzo & Hodgkiss, 1993; Soares &
242 Jesus, 2003), where the suppression of sidelobes plays a role. This has some implications for the
243 resolution capability of MFP, which depends heavily on whether the analysed source emits a wide
244 frequency band or not. These interference patterns can also be thought of as a trade-off between
245 spatial and frequency resolution of MFP. Using more precise Green's functions has in principle no
246 impact on this.

247 The basic idea of incorporating more realistic Green's functions in MFP is not new. In ocean
248 acoustics, waveforms are coherent across large distances due wave propagation being focused in the
249 SOFAR channel, but MFP results can be highly sensitive to acoustic wave velocities (Tolstoy, 1989),
250 similar to what we have shown in Figure 2. Bathymetry and multiple reflections may complicate
251 the recorded wave field even further and impact MFP performance significantly, and thus should
252 ideally be incorporated (e.g., D'Spain et al., 1999). For elastic waves in solid Earth structure,
253 further effects would need to be considered, as described above. One approach to this is empirical
254 Matched Field Processing (Gibbons et al., 2017). Gibbons et al. (2017) estimate empirical Green's
255 functions for each station from recordings of known sources by computing the principal eigenvector
256 of the covariance matrix of the incoming wave field for two nearly identical sources. They have
257 demonstrated their approach in the context of mining blasts. The obvious limitation is that such
258 template sources are required, which allows its application only for certain scenarios.

259 Our approach does not have this limitation. Using numerically computed synthetic wave fields,
260 we can place candidate sources wherever we want. Our approach is then mainly limited by the
261 accuracy of the numerical model and computation strategy. Improving MFP in this way has only
262 become possible recently thanks to efforts by other authors to improve the computation of databases
263 of Green's functions for real Earth structure and provide them to the community (e.g., Nissen-Meyer
264 et al., 2014; van Driel et al., 2015; Krischer et al., 2017; Heimann et al., 2017). Computing
265 Green's functions for complex Earth structure is expensive, which is why we rely in our analysis on
266 pre-computed databases using *instaseis* (van Driel et al., 2015). Green's functions databases for
267 realistic Earth structure up to frequencies of the secondary microseism are available for download at
268 IRIS-DMC (Hutko et al., 2017) or Pyrocko Green's Mill (Heimann et al., 2017).

2.3 On amplitudes in MFP

The standard approach does not include an amplitude term. When it is incorporated, it ideally describes the two contributions for geometrical spreading and inelastic attenuation on the amplitudes (e.g., Bowden et al., 2020). Computing both requires assumptions about wave type and the attenuation properties of the Earth, again increasing the parameter space. Bowden et al. (2020) show in a synthetic example that first applying and later correcting for this amplitude term does not improve source locations compared to neglecting it from the beginning. It merely tests whether the assumed wave type and quality factor are correct, which poses the danger that wrong assumptions may bias results in real data studies, but also opens the opportunity to constrain anelastic properties of the Earth, if the source locations are already well-known. More importantly though, Bowden et al. (2020) also showed that computing MFP results including the amplitude term in the synthetic Green's function without correcting for it is equivalent to mapping out the sensitivity kernel for the given station-source distribution. As the authors have pointed out, MFP and interferometry-based localisation are closely connected (more on this in section 2.4). MFP without correcting for amplitudes is not useful for directly locating sources (as the highest score is no longer necessarily at the source location), but can be an appropriate starting model for the interferometry-based strategy (Igel et al., 2021a).

A strategy similar to the interferometry-based scheme, where the source strength at a position is perturbed and the fit between model and data is evaluated, is not viable for MFP itself. The beampower at a potential source location scales linearly with the absolute amplitudes of the recorded seismograms. This is the case, even if the match in amplitude decreases, because MFP is ultimately summing over correlations of waveforms. For this reason, other measures of waveform-similarity that account for a mismatch in amplitude are commonly applied in other approaches, e.g., in full waveform inversion (Yong et al., 2019, and references therein). Accounting for this behaviour directly in MFP is currently not possible, because it is inherent to how beamformers are designed.

Therefore, a strategy is required to correct for amplitude terms. Numerically computed Green's functions for real Earth structure inevitably contain amplitude terms. Several approaches may appear reasonable to correct for them: correcting for amplitude decay (Fig. 3b), time-domain normalisation (Fig. 3c), and spectral whitening (Fig. 3d). Without any treatment of amplitudes, the beampower distribution is heavily biased by distance to stations (Fig. 3a). This effect is more pronounced compared to Bowden et al. (2020), because our Green's functions also contain body waves. Only a zoomed-in view allows to see the distribution of beampowers with a linear colorscale. The retrieved

301 source location without amplitude treatment is close to one of the stations nearest to the actual
302 source at the center.

303 Applying a correction factor for geometrical spreading of surface waves as has been demonstrated
304 by Corciulo et al. (2012) corrects for some but not all of the amplitude bias (Fig. 3b). The
305 beampower peak is still found near a station, because body waves are not corrected for. It is not
306 clear how a single correction term could be designed to correct for both body and surface waves
307 simultaneously. When we neglect the near-station beampowers, we find a local maximum (small red
308 circle) near the correct source location. We are not able to resolve the source location correctly.
309 For now, we advise against application of a correction term for amplitude decay, because it requires
310 assumptions about wave type and the medium's inelastic properties, opening up room for error
311 and bias as demonstrated here. When synthetic Green's function contain only a single wave type,
312 applying a correction term is a viable strategy as shown by Bowden et al. (2020). In real applications
313 and without prior knowledge of the source location (which defeats the purpose of MFP), such bias
314 seems not trivial to resolve. More drastic approaches to dealing with amplitude-induced bias are
315 necessary.

316 Time-domain normalisation aims to completely remove the impact of amplitudes by converting
317 the synthetic wave fields to time domain $s(t, \vec{x}_j, \vec{x}_s)$ and dividing those by their maximum amplitude.
318 With this approach, we resolve the beampower peak close to the true source (Fig. 3c), but introduce
319 ripple-shaped artefacts in the entire beampower distribution. Time-domain normalisation is only then
320 equivalent to properly removing the effect of amplitude decay, if waveforms did not change their
321 shape across stations. Elastic wave propagation in realistic Earth structure results in the emergence of
322 different phases depending on source-receiver distance, changes to the waveforms due to dispersion,
323 as well as their amplitudes being affected differently by decay. These effects introduce the observed
324 pattern, which is undesirable.

325 Spectral whitening or frequency-domain normalisation is the process of dividing the frequency
326 spectrum by its amplitude spectrum, a technique commonly applied in processing of ambient seismic
327 noise records for interferometry (Bensen et al., 2007; Fichtner et al., 2020). Neglecting amplitudes
328 as done in the standard approach is equivalent to whitening of synthetic Green's functions. In fact,
329 whitening of the synthetic wave field is applied in early formulations of standard MFP (equation 24
330 in Baggeroer et al., 1993). In the context of interferometry of the ambient seismic field, whitening
331 is often performed with a water-level or smoothed amplitude spectrum to stabilise the procedure
332 numerically and not over-emphasize frequencies that carry no useful information (Bensen et al.,

333 2007). Because we treat the synthetic spectra only, we are not concerned with smoothing of the
 334 amplitude spectrum before division and artefacts that whitening may introduce in real data and
 335 directly perform whitening as

$$s_{\text{white}}(t, \vec{x}_j, \vec{x}_s) = \frac{s(t, \vec{x}_j, \vec{x}_s)}{|s(t, \vec{x}_j, \vec{x}_s)|}. \quad (5)$$

336 This approach successfully retrieves the correct source location and does not appear to introduce
 337 any unwanted biases (Fig. 3d).

338 From our tests, whitening the spectra of the synthetic wave fields (Fig. 3d) appears to be the
 339 most advantageous approach, and follows the original formulation of MFP (Baggeroer et al., 1993).
 340 It introduces no alteration of the recorded data, eliminates attenuation and spreading effects, removes
 341 potential issues caused by source strength, and successfully retrieves the true source location. With
 342 this approach, all sources are weighted equally likely, regardless of distance to the receivers, as long
 343 as their wave fields are well-recorded on all stations. This may not always be an advantage, e.g., in
 344 global-scale studies, where the convergence of the wave field at the source's antipode may introduce
 345 bias. By whitening we also lose the ability to, in principle, constrain anelastic parameters of the
 346 Earth, but it is not clear to us how that could be approached for numerically computed Green's
 347 functions that contain all wave propagation effects.

348 2.4 Naming conventions and conceptual approaches to MFP

349 To illustrate how literature from multiple disciplines intersects, we want to take a moment to clarify
 350 different naming conventions and how MFP can be understood conceptually in different ways.

351 In this paper, we have used language that describes the results of MFP as the distribution
 352 of beampower retrieved from matching recorded wave fields with synthetic wave fields or Green's
 353 functions $s(\omega, \vec{x}_j, \vec{x}_s)$ for candidate source locations. This language, particularly Green's functions,
 354 is natural for seismologists (e.g., Gibbons et al., 2017; Umlauf & Korn, 2019), though rarely also
 355 used in ocean acoustics studies (e.g., Li et al., 2021).

356 In ocean acoustics, other terminology is more common for some of these concepts. The dis-
 357 tribution of beampowers may be called ambiguity surface (Bucker, 1976), intended to express the
 358 emergence of sidelobes for narrowband sources (Fig. 2c,d). $s(\omega, \vec{x}_j, \vec{x}_s)$ is sometimes called steering
 359 vector, expressing the idea that the array is "steered" towards the source during beamforming or
 360 MFP, or replica vector, communicating that the vector represents a replica of the expected wave
 361 field (Baggeroer et al., 1993).

362 Still, both the seismological and ocean acoustics communities understand MFP as matching of
 363 wave fields; this idea is the original concept introduced by Bucker (1976), and gives an intuitive
 364 understanding of the physics involved. Above, we mentioned that array beamforming for plane waves
 365 is a special case of MFP. For plane-wave beamforming, Green's functions of the form $s(\omega, \vec{x}_j, \vec{x}_s) =$
 366 $e^{-i\omega t(\vec{x}_j, \vec{x}_s)}$ are used, and only the manner in which $t(\vec{x}_j, \vec{x}_s)$ is estimated is adapted to use relative
 367 distances perpendicular to the plane wavefront (Fig. 1b) instead of distances to potential source
 368 locations (Fig. 1d). In that case, MFP is exactly delay-and-sum beamforming, regardless of whether
 369 plane waves or curved wavefronts are used (Bucker, 1976). In this formulation (what we called the
 370 "standard approach" to MFP) the Green's function can be understood in two ways: It is the wave
 371 field emitted by a point source (the impulse response), if the medium is an isotropic, homogeneous
 372 half-space. It also represents a phase shift (or time-delay), if it is convolved with a waveform.

373 Understanding beamforming as convolution leads to another way of conceptualising MFP. We
 374 rewrite equation 3, omitting the variables $(\omega, \vec{x}_j, \vec{x}_s)$ for readability, as

$$B = \sum_{\omega} \sum_j \sum_{k \neq j} s_j^* d_k^* d_j s_k = \sum_{\omega} \sum_j \sum_{k \neq j} (s_j^* s_k) (d_k^* d_j). \quad (6)$$

375 Here, $d_k^* d_j$ is the correlation of the recorded wave fields and $s_j^* s_k$ correlation of the synthetic wave
 376 fields for each station pair k, j . The "matching" of wave fields in MFP is exactly this: convolution
 377 of their correlation wave fields.

378 This is particularly relevant, because it further demonstrates the close connection between MFP
 379 and the interferometry-based localisation strategy, and gives a different perspective to the insights
 380 provided by Bowden et al. (2020). In both approaches, cross-correlation functions of recorded data
 381 and of synthetic data are computed and compared against each other. The main difference between
 382 them lies in how exactly cross-correlation functions are computed and how the (mis-)fit between
 383 the two is evaluated. It is then not surprising that MFP results are a good starting model for
 384 interferometry-based localisation (Igel et al., 2021a); in a very real sense MFP is interferometry-
 385 based localisation, just with less processing and a different mismatch measure. Bowden et al. (2020)
 386 have described this connection more mathematically: starting from cross-correlation beamforming
 387 (Ruigrok et al., 2017), a simple change in the order of operations - from shifting waveforms first and
 388 then computing the cross-correlation coefficient to first computing the correlation function and then
 389 measuring at the corresponding time lag - creates an equivalency (under certain conditions) between
 390 MFP and interferometry-based source inversion. This description and the one we introduce above
 391 result in the same realisation: fundamentally, there currently exists only one approach for locating

392 sources of ambient seismic noise in the sense that the coherency of the recorded wave field across
393 stations is the most important aspect that enables source localisation. That both approaches are
394 fundamentally the same may not be intuitive at first, especially considering the strikingly different
395 sketches to illustrate them (Fig. 1c,d), and the different language both communities use.

396 To retrieve "reliable" cross-correlation functions of the recorded data in ambient noise seismology,
397 processing and stacking over time is common (Fichtner et al., 2020). Such cross-correlation functions
398 are often called estimated or empirical Green's functions, relying on assumptions of homogeneous
399 noise source distribution or wave field equipartition (e.g., Nakata et al., 2019). These are not to
400 be confused with what Gibbons et al. (2017) called empirical Green's functions. Note that Fichtner
401 et al. (2017); Ermert et al. (2016) and others purposefully avoid naming and understanding cross-
402 correlation functions as empirical Green's functions and do not rely on the above assumptions. The
403 fact that these assumptions are incorrect is in fact what enables the interferometry-based strategy.

404 MFP is similarly not concerned with such assumptions about the equipartition or source distribution
405 of the recorded wave field. Furthermore, it foregoes processing of seismograms for stability entirely,
406 allowing for high time-resolution and avoiding artefacts potentially introduced by the processing
407 (Fichtner et al., 2020). Importantly though, the mismatch measure employed in MFP does not
408 allow iterative inversion by source-strength perturbation, because convolution (or correlation) does
409 not account for amplitude mismatch. If signals are in phase, increasing amplitudes of one results
410 in linearly-scaling beampowers regardless of how well the waveforms fit. At this point, it is clear
411 that both communities may benefit from each other, as has already rightfully been pointed out by
412 Bowden et al. (2020). It is in principle possible to employ strategies of the ambient seismic noise
413 community to "improve" the correlation functions $d_k^* d_j$. A detailed analysis of the advantages and
414 disadvantages this would bring, and what exactly "improving" would mean in the context of MFP is
415 beyond the scope of this paper. Similarly, increasing the accuracy of MFP in a seismological context
416 and discussing its fundamental ideas and limitations, as is the intent of this paper, may benefit
417 developments in the larger field of ambient seismic noise localisation.

418 **2.5 Limitations of MFP**

419 Above, we have already explored the advantages and limitations of using numerically computed
420 synthetic wave fields (Fig. 2) and amplitudes (Fig. 3) in MFP, as well as the emergence of striped
421 interference patterns for narrowband sources (Fig. 2). MFP shows further undesired behaviour
422 under certain conditions that we encounter in real-world applications. Some of these are more

423 straight-forward to understand in the conceptual framework of convolution introduced above.

424 **2.5.1 Source-Station Geometry**

425 For beamforming, the impact of an array's geometry on its resolution capability is well studied, and
426 quantified by the array-response function (Rost & Thomas, 2002). Standard MFP becomes plane-
427 wave beamforming for very large distances between source and array, because accounting for curved
428 wavefronts has negligible impact on travel times. In that case, the lessons learned in beamforming,
429 e.g., what wavelengths are resolvable without aliasing, apply one-to-one. When MFP is considered
430 as an approach, the source-station geometry should be such that accounting for curved wavefronts
431 actually has useful impact on the results, i.e., the difference in expected travel times compared to
432 plane waves is much larger than the expected measurement error. Because MFP is not bound to the
433 plane-wave assumption, there is no meaningful difference between treating a collection of stations
434 as an array or a network. Still, the inter-station distance should not be much smaller than the
435 investigated wavelength or incoherent noise may prevent being able to reliably resolve the source
436 location. In MFP, quantifying resolution in a similar manner to the array-response function for
437 beamforming is an unsolved problem, because the parameter space is much larger.

438 Closely related to these considerations is that high waveform coherency is required across stations,
439 regardless of approach. In standard MFP or beamforming, i.e., $s(\omega, \vec{x}_j, \vec{x}_s) = e^{-i\omega t(\vec{x}_j, \vec{x}_s)}$, coherency
440 means retaining the exact shape of the waveforms across stations, because waveforms are simply
441 shifted in time. In our approach, waveform coherency takes a slightly different meaning, because
442 elastic wave propagation can change the shape of recorded waveforms significantly. So instead,
443 waveforms need to be coherent after elastic wave propagation effects have been accounted for, in
444 our approach via synthetic Green's functions for real Earth structure. This is an important distinction,
445 as our approach loosens the requirements on station geometry for MFP quite drastically. In principle,
446 stations on opposite sides of the Earth can be used simultaneously for MFP, as long as the wave
447 propagation effects are properly incorporated and the signal is recorded above the noise-level on
448 both stations. Therefore, our approach improves upon this limitation of MFP, and we make use of
449 this in the real data examples below.

450 **2.5.2 Station Density**

451 Station density has direct impact on the retrieved beampower distribution that is worth pointing out
452 explicitly (Fig. 4a). In a synthetic test, we place four times the stations, with the same coordinates,

453 on the right side than we do on the left (Fig. 4b). The beampower distribution shows a visual bias
454 towards the top-left, caused simply by the presence of more stations that recorded the signal in the
455 bottom-right. While in the ideal scenario here, the exact source location is still resolved correctly,
456 interpreting this distribution without prior knowledge of the sources in a real-world application seems
457 challenging. This bias in MFP results follows directly from understanding MFP as the sum over
458 convolutions of correlated wave fields, as described above. Regions with higher station density are
459 then inherently weighted higher and cause the observed effect.

460 This goes beyond increased resolution due to better suppression of incoherent noises, and is an
461 effect that essentially all real-world applications of MFP will have to take into consideration. We have
462 tested two possible approaches to correct for this without success. Introducing a coherency-weight
463 where stations that recorded similar waveforms are down-weighted to counter-act the described
464 behaviour, does not improve the retrieved beampower distribution. This approach further loses the
465 advantages that multiple measurements at similar positions can reduce impact of incoherent noise.
466 A different approach may be to homogenise the station distribution, but this often excludes high-
467 quality stations from the analysis, especially for permanent arrays. The loss in quality recordings
468 does not seem to be desirable here.

469 **2.5.3 Multiple Sources**

470 Single sources can cause prominent interference patterns for narrowband sources (Fig. 2c,d), which
471 depend on station geometry and frequency band. This leads to even more complex, secondary
472 interference when multiple sources are active at the same time. In a synthetic test, we place two
473 narrowband sources that excite identical wave fields simultaneously (Fig. 4b). The second source
474 is placed such that it lies at the edge of a sidelobe of the first source (Fig. 2d). From the retrieved
475 distribution of beampowers it is not at all obvious that two and only two sources are active here,
476 and instead this may be misidentified as a single source close to the left array (Fig. 4b). The
477 new beampower peak is entirely an interference artefact. This smearing of resolved source locations
478 clearly relates to the wavelength of the investigated waves, and similar issues are well-known in the
479 beamforming community, as described above. When the two sources placed are broadband instead
480 (Fig. 4c), one may interpret the beampower distribution as two sources. The true locations are not
481 recovered, with a smaller error for the closer source. Similar problems, such as smeared beampower
482 distributions can occur for single sources that move during the investigated time frame (Li et al.,
483 2021).

484 These effects briefly demonstrate the, in our view, most important limitation of MFP: the
485 concrete interpretation of individual MFP results. Interpretation seems quite challenging when either
486 stations are distributed heterogeneously or multiple sources are nearby and may have interfering
487 sidelobe patterns. Both conditions are true for most real-world applications. This is one of the main
488 reasons other beamformers are being developed (e.g., Capon, 1969; Schmidt, 1986; Cox et al., 1987;
489 Cox, 2000; Gal et al., 2014; Zhu et al., 2020). In future work, exploring their applicability to and
490 further developing them in the context of elastic waves propagating in real Earth structure, seems
491 like a clear way forward. A convenient way of quantifying MFP's resolution would be exceptionally
492 useful, but is not known to us. Here the interferometry-based localisation strategy shows its strength,
493 with a clear strategy for iteratively getting better estimates of source location.

494 **2.5.4 Time window length**

495 In MFP, a choice has to be made on how long of a time window is analysed. The basic requirement
496 is that the time needs to be long enough to record the correlated wave field propagating across all
497 stations, which can be estimated roughly from expected wave velocities. Because MFP is based
498 on correlation wavefields, by default the entirety of the chosen time window influences the result.
499 This is easier to understand with the delay-and-sum concept, where waveforms are shifted in time
500 and summed. Because the entire waveforms are used to compute the sum, all of the waveform
501 plays a role. This limits the time resolution of MFP and has implications depending on the type
502 of source one aims to investigate. If a source is exciting energy repeatedly, the wave field contains
503 more and more of that source's energy the longer the time window is and thus gets weighted higher
504 and higher. This is very useful for stationary "noise" sources. For impulsive sources that act rarely,
505 this can be a disadvantage and time windows should be chosen as small as possible for them. To
506 address this issue, the concept of a windowing function as developed for the interferometry-based
507 localisation strategy (Bowden et al., 2020), may be an opportunity to increase MFP's time resolution
508 even further in the future.

509 **3 Demonstration on real data**

510 We demonstrate our approach on two real data examples.

511 **3.1 2008 Chino Hills Earthquake**

512 First, we benchmark our approach with an earthquake in Southern California, the $M_W = 5.4$ Chino
513 Hills earthquake of 2008-07-29 (Fig. 5). When applying the standard MFP approach, with an
514 assumed velocity $v = 3.2$ km/s (the best fit in the synthetic test in Fig. 2), we find a relatively good
515 location of the earthquake with 7.7 km distance to the location in the CI catalog (Fig. 5a, SCEDC,
516 2013). The good fit here confirms what other authors have found before: standard MFP can
517 already perform quite well in seismological studies (Gal et al., 2018; Umlauf & Korn, 2019; Umlauf
518 et al., 2021). When we replace $s(\omega, \vec{x}_j, \vec{x}_s)$ with numerical Green's functions (our approach) for an
519 explosive source mechanism, we at first find a decrease in location accuracy (Fig. 5b). The retrieved
520 location is 18.3 km away from the CI location. When we incorporate the moment tensor solution
521 from the CI catalog (SCEDC, 2013), trivial to do with our approach, we find an improvement in
522 location accuracy with a distance of only 1.9 km to the CI location (Fig. 5c). This demonstrates one
523 of the potential use cases for MFP with numerical Green's functions: Searching for the best-fitting
524 moment tensor may help constrain the source mechanism of unknown weak sources. A related
525 strategy has been employed by Umlauf et al. (2021). The authors flipped the sign of waveforms,
526 based on visual inspection and expert judgement, before applying MFP. The spatial distribution of
527 whether a waveform had to be flipped or not to increase waveform-coherency across stations, gives
528 hints on the radiation pattern and thus source mechanism of the seismic sources, in their case stick-
529 slip tremor at the base of a glacier. In such a scenario, where clear identification of phase arrivals is
530 difficult, our approach may be a more systematic approach and help give improved estimates of the
531 source mechanism.

532 **3.2 Secondary Microseism**

533 In a second example, we locate seismic sources in the secondary microseism frequency band (0.13
534 to 0.15 Hz) in the Northeastern Atlantic and Mediterranean Sea using 342 stations distributed over
535 Europe during the first week of February 2019 (Fig. 6). Three snapshots of beampower distributions
536 are compared against hindcasts of significant wave height (WaveWatch III, Ardhuin et al., 2011).
537 On first order, we find a good match between the standard approach ($v = 3.2$ km/s, left), our
538 approach (middle), and the distribution of significant wave height (right). A good match between
539 seismic wave excitation and ocean wave activity is expected for the secondary microseism. The com-
540 mon explanation is that ocean gravity waves at the water surface, propagating in roughly opposite
541 direction, interact and cause a standing wave that generates a vertically-propagating pressure wave

542 field in the water column. This pressure wave field then interacts with the ocean bottom, generating
543 seismic waves in the solid Earth (Hasselmann, 1963; Ardhuin et al., 2015).

544 The similarity between the standard approach and our approach is high (Fig. 6 left and middle).
545 This is not surprising for a number of reasons. The sources we image here are generally far away
546 from most stations and towards one direction, West. The difference in waveforms recorded across
547 all stations then becomes relatively small. If sources were closer to all stations, as e.g., for the Chino
548 Hills earthquake (Fig. 5), improving the accuracy of the synthetic wave field has larger impact.
549 Furthermore, the Green's function we rely on are based on an axisymmetric 1D Earth. Therefore we
550 do not yet incorporate the full complexity of elastic wave propagation in this demonstration. Partic-
551 ularly relevant are likely the European shelf areas and the structure and velocity contrast between
552 oceanic and continental crust. Finally, because we investigate the secondary microseism, we are
553 limited to a narrow frequency band and cannot benefit from utilising broadband seismic waveforms,
554 for which we believe our approach should perform a lot better than the standard approach. Still,
555 we do find that beampower distributions retrieved with our approach are more focused on specific
556 regions compared to the standard approach. We do not yet feel comfortable in judging whether
557 these differences are certain to be an improvement in source estimation.

558 Our synthetic tests (Fig. 2) and the Chino Hills earthquake example (Fig. 5) suggests that
559 our approach can be more precise in locating the sources. However, we have to be careful with
560 interpreting these patterns, as we have also demonstrated in synthetic tests (Fig. 4). If our approach
561 will prove to be more precise also for microseisms, we may find that seismic waves are excited in
562 specific regions in the oceans and not distributed homogeneously beneath storm systems. It is
563 important to note here that for now we use an explosion source mechanism for the synthetic wave
564 fields to locate the microseism, which we have already shown to be inadequate for an earthquake
565 (Fig. 5). In the future, we require a strategy to describe and incorporate a source mechanisms
566 appropriate for microseisms. Some insight in how that could be approached has been given by
567 Gualtieri et al. (2020) and this is certainly an attractive prospect and may help better understand
568 the exact excitation mechanism.

569 **4 Conclusions**

570 Matched Field Processing (MFP) is generalized Beamforming for arbitrary wave fields, removing
571 the need for the plane-wave assumption. It is one of the current approaches to locating sources of

572 ambient seismic noise (Fig. 1). In this study, we advance MFP to better incorporate elastic wave
573 propagation in the Earth by using Green's functions numerically computed for real Earth structure
574 directly as the synthetic wave field that the data is matched against.

575 When amplitudes are considered in MFP, results are biased by amplitude effects such as geo-
576 metrical spreading and anelastic attenuation. In the standard approach, this is usually neglected
577 through spectral whitening of the synthetic wave field. We find that this strategy performs best for
578 us as well, and that trying to correct for spreading and attenuation via an amplitude term, as has
579 been suggested before, may not be advisable (Fig. 3). This is especially the case for our approach,
580 where multiple wave types can be considered simultaneously.

581 Two examples on real data showcase the potential of our approach (Figs. 5, 6). In principle, we
582 can use it to search for the source mechanism of a seismic source, as suggested by the improved source
583 location after incorporating the earthquake's moment tensor (Fig. 5). This could be particularly
584 useful in the context of tremor activity, where source mechanism determination is challenging with
585 classical approaches. In a second example, we locate sources of the secondary microseism in the
586 Northern Atlantic and Mediterranean Sea (Fig. 6). Results from our approach match the standard
587 approach's results closely, likely due to source geometry, narrow frequency band, and our reliance on
588 Green's functions computed for an axisymmetric Earth. Our approach retains the advantage that is
589 not biased by author choice of a constant velocity, and potentially provides higher resolution.

590 We clarify conceptual approaches to MFP and its close connection to the interferometry-based
591 localisation. The striking similarity between them suggests that it may be a worthwhile endeavour to
592 unify them in the future, or at least provide a framework to let the different communities benefit from
593 each others' work. MFP in particular would benefit tremendously from an approach for quantifying
594 its resolution. The lack of such a measure is currently its major disadvantage.

595 Future advances focused on MFP for real Earth structure could be on more precise Green's
596 functions databases, or investigating the performance of beamformers particularly for elastic wave
597 propagation. With current tools, there is the potential for reasonably sized databases that incorporate
598 true 3D Earth structure when limiting source locations to be only at the surface. More precise
599 Green's functions should also incorporate a better description of the microseism source mechanism,
600 different for the primary and secondary microseism. Our approach could improve MFP with few and
601 sparsely distributed stations, because it is less reliant on waveform-coherency across seismic stations
602 in its strict sense. While seismometer density is improving worldwide consistently, regions with sparse
603 deployments and without purposefully built arrays are still the norm. Furthermore, tremor activity

604 such as volcanic tremor is often challenging to locate with classical approaches. Particularly in such
605 regions and study targets, MFP is a powerful strategy for localising the origin of seismic energy.

606 **Data and Materials**

607 We provide all data and code used to generate the figures in this paper to make it entirely reproducible
608 (https://github.com/seismology-hamburg/schippkus_hadziioannou_2022). There, we also
609 provide a minimal working MFP example based on synthetic data and the standard approach to make
610 the method more accessible for students and researchers interested in MFP. The MFP computations
611 in this study rely on Python code developed for this work, which we make available under MIT
612 license at https://github.com/seismology-hamburg/matched_field_processing.

613 Seismic data used in this study was provided by network operators of international, national, and
614 regional seismic networks in Europe and America (California Institute of Technology and United
615 States Geological Survey Pasadena, 1926; ZAMG - Zentralanstalt für Meteorologie und Geody-
616 namik, 1987; Institut fuer Geowissenschaften, Friedrich-Schiller-Universitaet Jena, 2009; University
617 of Leipzig, 2001; Ruhr Universitaet Bochum (RUB Germany), 2007; RESIF, 2018; Instituto Português
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619 OGS, 2016; Norsar, 1971; KNMI, 1993; MedNet Project Partner Institutions, 1988; Instituto Dom
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621 Observatory (ROA) et al., 1996; INGV Seismological Data Centre, 1997; Albuquerque Seismological
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623 1967; Institut De Physique Du Globe De Paris (IPGP) & Ecole Et Observatoire Des Sciences De La
624 Terre De Strasbourg (EOST), 1982; GEOFON Data Centre, 1993; Dublin Institute for Advanced
625 Studies, 1993; Charles University in Prague (Czech) et al., 1973; University of Zagreb, 2001; Swiss
626 Seismological Service (SED) At ETH Zurich, 1983; Department of Earth and Environmental Sci-
627 ences, Geophysical Observatory, University of Munchen, 2001; Royal Observatory of Belgium, 1985;
628 Slovenian Environment Agency, 1990; RESIF, 1995; Federal Institute for Geosciences and Natural
629 Resources, 1976) and accessed through ORFEUS, EIDA, and IRIS via obspy (Krischer et al., 2015).

630 Colormaps used in this study are perceptually uniform (Crameri et al., 2020).

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866 **Figures**

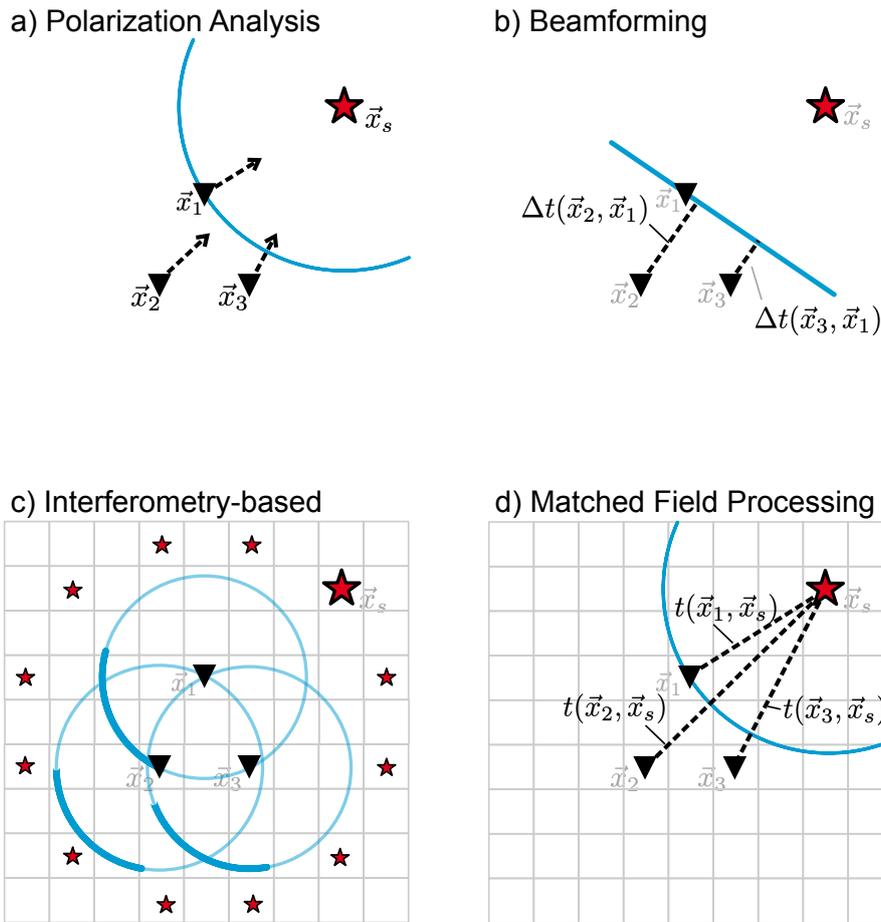


Figure 1: Current approaches to locating sources of the ambient seismic field. Wavefronts are marked blue. a) Polarization Analysis: The polarization of the wave field on individual three-component seismometers gives an indication of direction of propagation. Triangulation allows source localisation. b) Beamforming: Seismograms on multiple stations are shifted in time corresponding to candidate plane-waves, and summed over. c) Interferometry-based strategy: Compare cross-correlation functions computed from seismograms of multiple stations with synthetically computed cross-correlation functions for a given source distribution. Cross-correlation functions are sensitive to the source distribution and are asymmetric (indicated by thickness of wavefront), if sources are distributed heterogeneously. d) Matched Field Processing is generalized Beamforming, sampling candidate source locations. Allows for curved wavefronts.

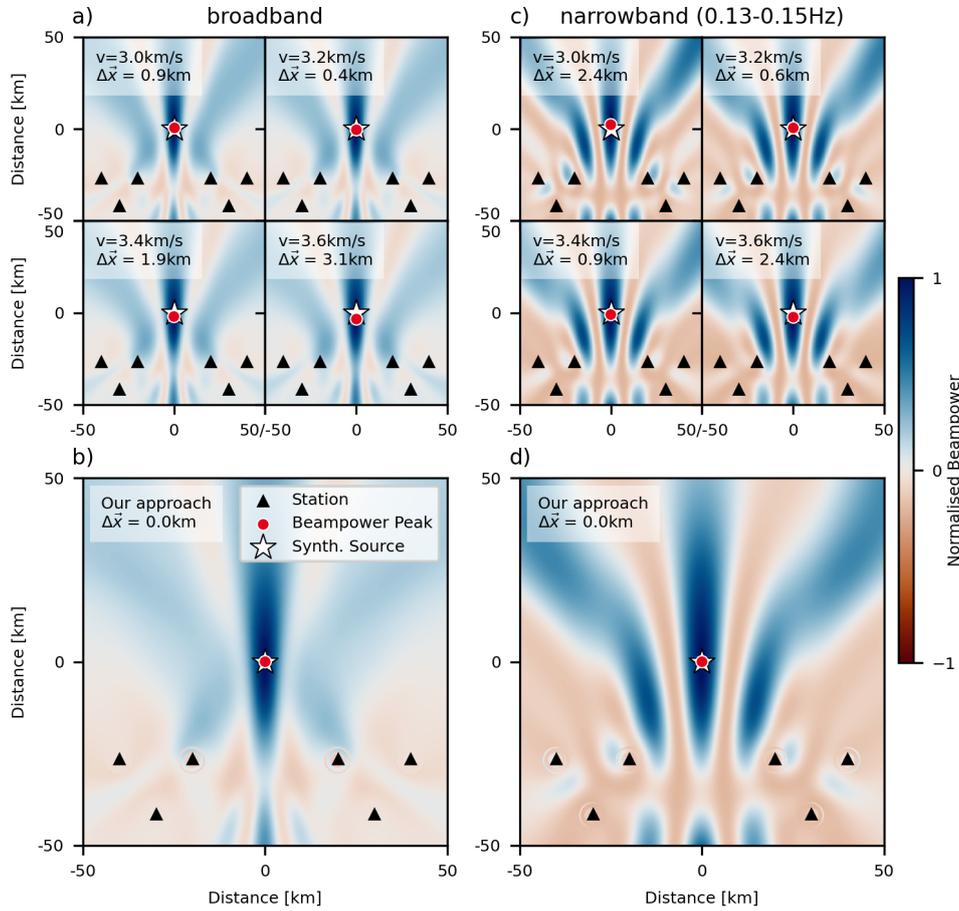


Figure 2: Synthetic demonstration for two three-station arrays locating an explosion source. The grid point with the highest beampower is the estimated source location (red circle). Left: broadband source. a) Standard approach, with travel times estimated for constant velocity. The retrieved source location is sensitive to the chosen velocity. b) Our approach, with numerical Green's functions as synthetic wave fields. Source is precisely located. Right: narrowband source (0.13-0.15Hz). c) Standard approach. Emergence of sidelobes due to interference. d) Our approach in the same narrow frequency band. Source is precisely located.

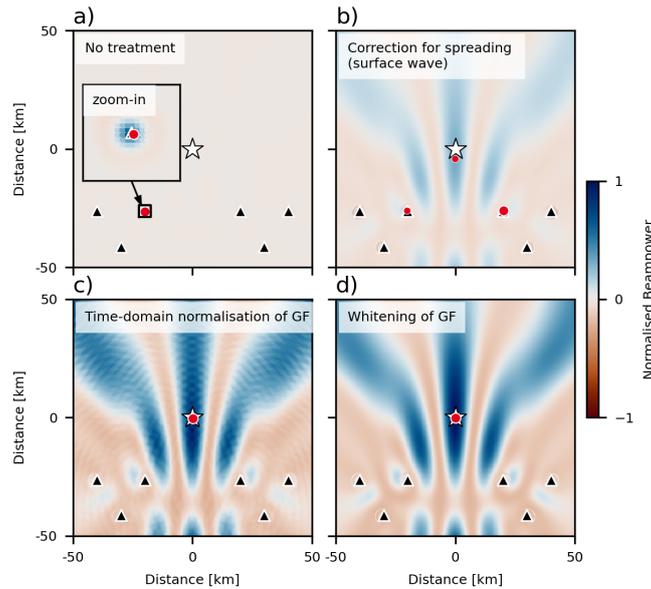


Figure 3: Strategies for treating amplitude information. a) No amplitude treatment. b) Correction for geometrical spreading of surface waves. Smaller red circles mark local beampower maxima. c) Time-domain normalisation of numerical Green's function (GF). d) Spectral whitening (frequency-domain normalisation) of numerical Green's function (GF).

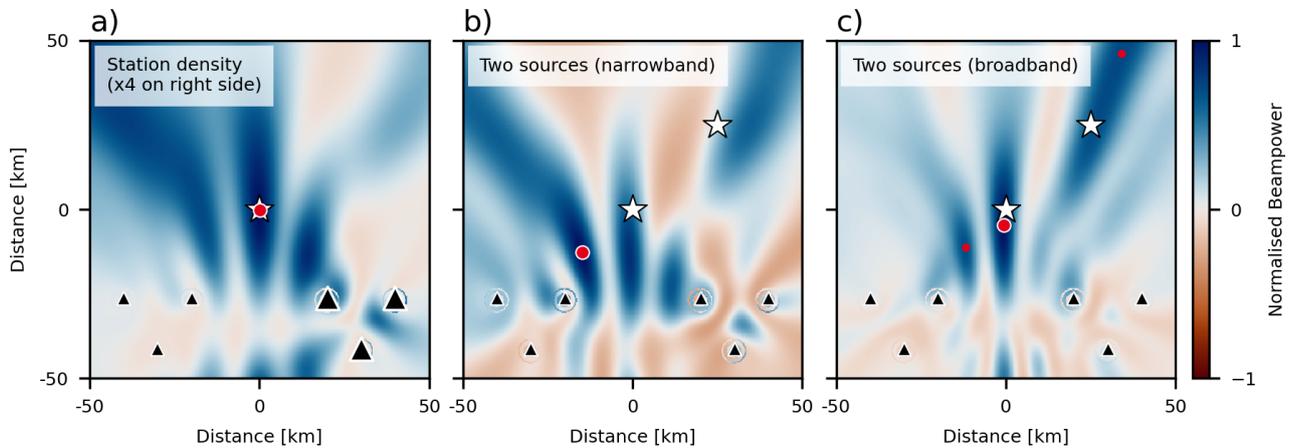


Figure 4: Some limitations of MFP, regardless of Green's function formulation. a) Impact of station density. Placing four times as many stations on the right side (indicated by larger triangles) results in visual bias of potential source locations. True source location is still resolved. b) Two narrowband (0.13 to 0.15 Hz) sources active at the same time. Beampower distribution does not represent source locations well. Global beampower maximum is an interference artefact. c) Same as b), but for a broadband source. Smaller red circles mark local beampower maxima. Closer to real source locations, but still not well-resolved.

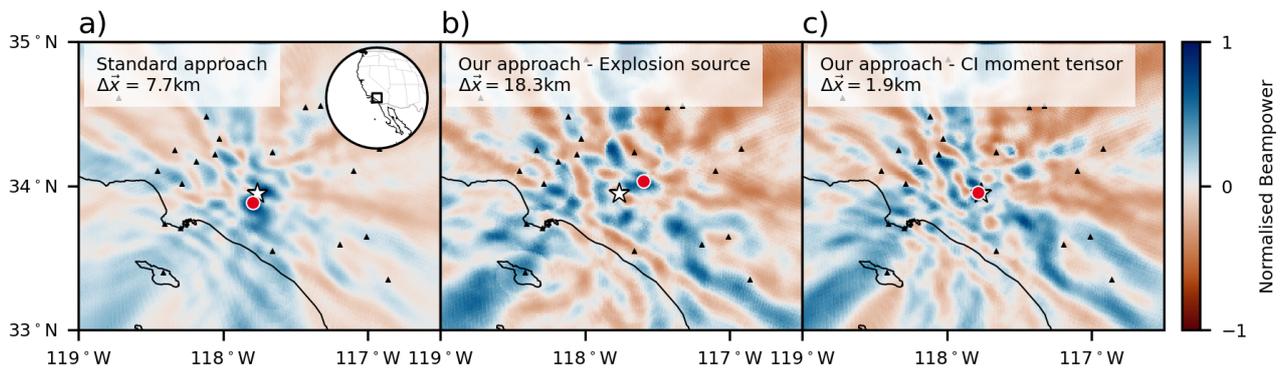


Figure 5: Location of the 2008-07-29 Chino Hills earthquake from the CI catalog (white star, SCEDC, 2013) and MFP (red circle) at 15.5km depth. MFP results were obtained using stations of the Southern California Seismic Network (black triangles) and frequencies from 0.1 to 0.2 Hz. a) Beampower distribution with simple analytical Green's functions, assuming $v = 3.2$ km/s. 7.7 km distance to the CI location. b) Beampower distribution using numerical Green's functions for an explosive source mechanism. 18.3 km distance to the CI location. c) Beampower distribution using numerical Green's functions for the moment tensor solution in the CI catalog (SCEDC, 2013). 1.9 km distance to the CI location.

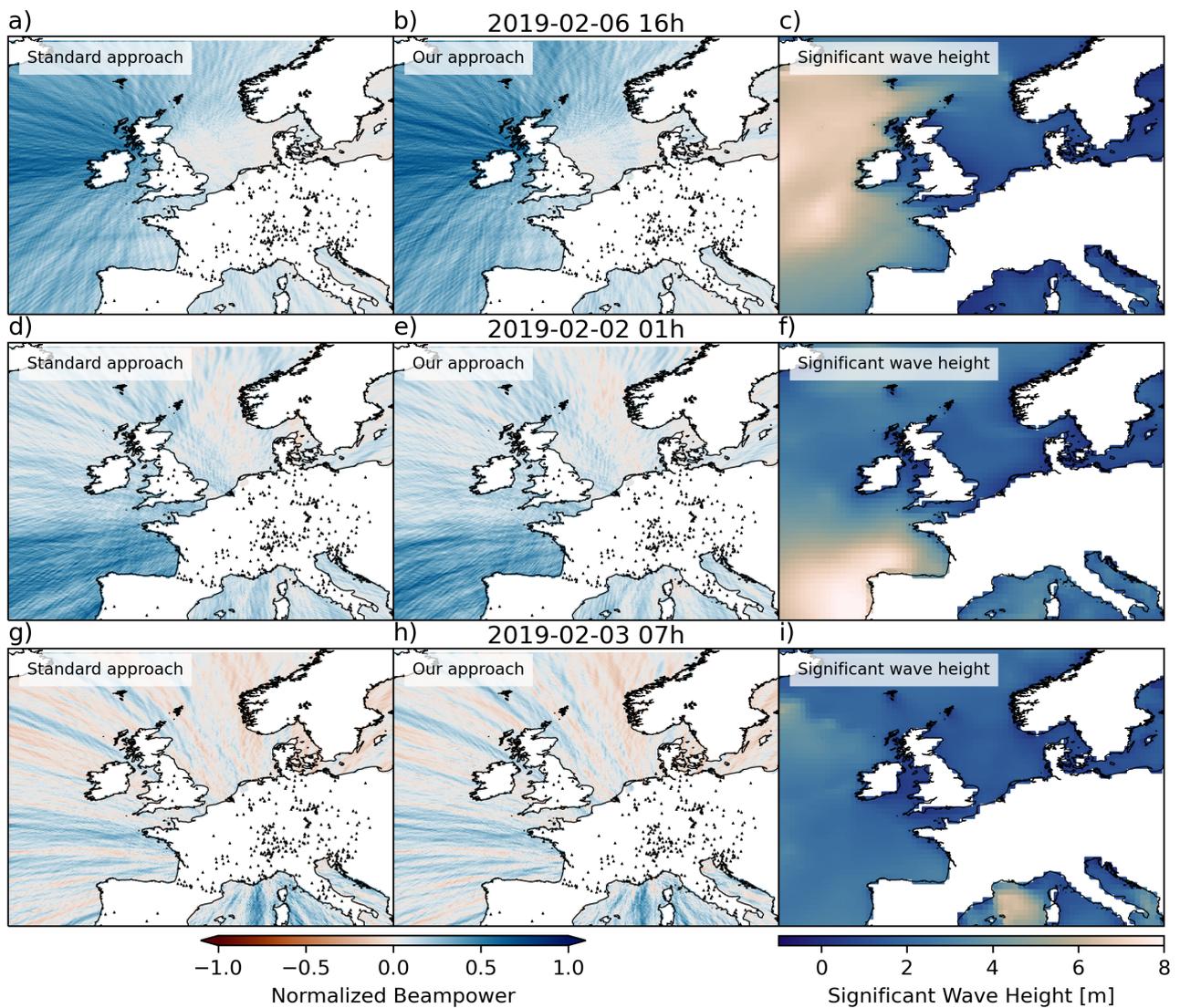


Figure 6: MFP results for the secondary microseism (0.13 to 0.15 Hz) during the first week of February 2019 for three time windows (rows). 342 stations distributed over Europe were used (black triangles). Left: MFP using analytical Green's functions, assuming $v = 3.2$ km/s. Middle: MFP using numerically computed Green's functions (our approach). Right: Maps of significant wave height hindcasts, provided by WaveWatch III (Ardhuin et al., 2011).