

# **Matched Field Processing accounting for complex Earth structure: method and review**

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- Section 3.2 Secondary Microseism rewritten and corresponding changes to Figure 6

# Matched Field Processing accounting for complex Earth structure: method and review

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## Abstract

Matched Field Processing (MFP) is a technique to locate the source of a recorded wavefield. It is the generalization of plane-wave beamforming, allowing for curved wavefronts. In the standard approach to MFP, simple analytical Green's functions are used as synthetic wavefields that the recorded wavefields are matched against. We introduce an advancement of MFP by utilizing Green's functions computed numerically for Earth structure as synthetic wavefields. This allows in principle to incorporate the full complexity of elastic wave propagation without further manual considerations, and through that provide more precise estimates of the recorded wavefield's origin. We call this approach *numerical MFP* (nMFP). To demonstrate the applicability and potential of nMFP, we present two real data examples, one for an earthquake in Southern California, and one for secondary microseism activity in the Northeastern Atlantic and Mediterranean Sea. In addition, we explore and clarify connections between localisation approaches for the ambient seismic field, real world limitations, and identify key areas for future developments. To increase the adoption of MFP in the seismological community, tutorial code is provided.

## Keywords

Seismic noise, Seismic Interferometry, Interferometry, Wave propagation

## 1 Introduction

The ambient seismic field has become an attractive target of seismological studies over the last two decades (Nakata et al., 2019). Interferometry of this complex wavefield, combined with increased

25 station density, has enabled detailed studies of Earth's structure (e.g., Shapiro et al., 2005; Lu et al.,  
26 2018; Schippkus et al., 2018) and its temporal changes (e.g., Brenguier et al., 2008; Hadziioannou  
27 et al., 2011). Such studies rely most commonly on seismic wavefields generated by the interaction  
28 between the oceans and the solid Earth, so-called microseisms. Understanding the exact mechanism  
29 for this interaction has been a challenge for more than half a century (Longuet-Higgings, 1950;  
30 Hasselmann, 1963; Arduin et al., 2015) and some open questions remain, e.g., about the emergence  
31 of Love waves in the secondary microseism (Ziane & Hadziioannou, 2019; Gualtieri et al., 2020).  
32 More recently, other sources such as trains (Fuchs et al., 2017; Brenguier et al., 2019; Liu et al.,  
33 2021), wind turbines (Stammler & Ceranna, 2016; Hu et al., 2019), direct wind-land interaction  
34 (Johnson et al., 2019), rain (Dean, 2019), and rivers (Burtin et al., 2008; Smith & Tape, 2019)  
35 have become the focus of several studies investigating high-frequency seismic noise.

36 To study all of these sources in detail and understand their mechanisms, precise knowledge of  
37 their locations is necessary. Dense installations of seismic stations near known sources can provide  
38 intriguing insight into the sources' interactions with the solid Earth (Riahi & Gerstoft, 2015), and  
39 can give evidence for previously unrecorded interactions (Schippkus et al., 2020). Installations like  
40 these are not widely available, though. For other sources, it may not be technically feasible to install  
41 stations close to all expected source locations, e.g., in the deep oceans to study ocean microseisms  
42 or in the Earth's subsurface. Beyond the interest in the fundamental principles of seismic wave  
43 generation by different sources, studies that rely on interferometry of the ambient seismic field to  
44 gain knowledge about Earth's structure ideally incorporate a priori knowledge of source locations to  
45 account for the potential bias introduced by their spatial distribution (Fichtner et al., 2017; Sergeant  
46 et al., 2020).

47 Strategies of earthquake seismology to locate seismic sources, such as travel-time inversion, are  
48 not applicable to ambient seismic noise due to the complexity of the analysed wavefield. There is  
49 not one single dominant source (e.g., an earthquake or explosion) that results in clearly identifiable  
50 and thus exploitable phase arrivals in seismograms across several stations. In other words, methods  
51 that rely heavily on data abstraction may not be useful (Li et al., 2020). Instead, strategies have  
52 emerged that aim to quantify the angle of arrival of seismic energy in recorded seismograms emitted  
53 by sources of unknown type. In the following, we give a brief overview of the current methods for  
54 locating sources of the ambient seismic field.

55 Polarization analysis exploits the particle motion of the seismic wavefield at one location  $\vec{x}_j$ ,  
56 resolved by three-component seismometers (Fig. 1a, e.g., Schimmel & Gallart, 2003). Depending

57 on the analysed wave type, the particle motion gives an indication of the angle of arrival. When  
58 combining results from multiple stations, this analysis can be used to triangulate the source location  
59  $\vec{x}_s$  (e.g., Schimmel et al., 2011). However, a number of assumption have to be made, e.g., great-  
60 circle propagation, as well as proper identification and clear separation of wave types. This approach  
61 can be a first step in understanding the recorded wavefield, but is often quite tricky in practice,  
62 especially on recordings of ambient seismic noise (Gal & Reading, 2019).

63 Beamforming is a source localisation approach based on the assumption that seismic waves  
64 propagating across seismic arrays can be treated as plane waves, which is valid if wavelengths are  
65 much larger than the aperture of the array (Fig. 1b). To test whether a candidate plane wave  
66 - characterised by its horizontal slowness or equivalently arrival angle and apparent velocity - was  
67 recorded on the array, expected relative time delays  $\Delta t(\vec{x}_j, \vec{x}_k)$  between the stations are computed  
68 and corrected for. This is called delay-and-sum beamforming, where each seismogram is shifted in  
69 time and summed together, forming the beam (Rost & Thomas, 2002). The quality of the beam  
70 is evaluated, giving the so-called beampower. Other formulations of this method exist, e.g., an  
71 equivalent cross-correlation approach (Ruigrok et al., 2017). Beamforming has been widely adopted  
72 by the seismological community and is currently the standard tool for identifying sources of the  
73 ambient seismic field (Gal & Reading, 2019, and references therein). Recent advances focus on  
74 incorporating three-component seismograms (Riahi et al., 2013; Juretzek & Hadziioannou, 2016,  
75 2017), avoiding bias introduced by averaging across broad frequency bands (Gal et al., 2014), or  
76 estimating surface wave anisotropy directly from beamforming (Löer et al., 2018). Beamforming  
77 has its main advantages in computational speed, little if any data processing, and high resolution in  
78 time. Its main drawbacks all result from the plane-wave assumption: sources have to be far from  
79 the array, the wavefield has to be strictly coherent across stations, and the array geometry limits the  
80 resolution capabilities (Rost & Thomas, 2002). For a recent review of beamforming and polarization  
81 analysis see Gal & Reading (2019).

82 A new source localisation strategy based on seismic interferometry has been introduced in recent  
83 years as an attractive alternative, sometimes referred to as kernel-based source inversion (Ermert  
84 et al., 2016). The goal of this approach is not to determine the angle of arrival, but to directly  
85 quantify the distribution of seismic sources in space. Interferometry of the ambient seismic field  
86 recorded on multiple stations gives new wavefields, propagating to and from the respective reference  
87 stations (Fig. 1c, Aki, 1957; Wapenaar et al., 2010; Campillo & Roux, 2015; Fichtner et al., 2017).  
88 An inhomogeneous distribution of sources results in asymmetric cross-correlation functions, indicated

89 by the thickness of the wave fronts in Fig. 1c (Paul et al., 2005). In practise, this asymmetry is  
90 usually quantified by comparing the causal and acausal part of each correlation function. In the  
91 interferometry-based approach, synthetic cross-correlation functions are computed for a given source  
92 distribution and compared against cross-correlation functions from real data. The mismatch between  
93 the two is evaluated (e.g., by quantifying amplitude asymmetry), the source model perturbed, and a  
94 best-fit source distribution is found via gradient descent in an iterative manner (Ermert et al., 2016).  
95 Recent work has focused on improving efficiency (Igel et al., 2021b), the mismatch measure (Sager  
96 et al., 2018), or expanding the method to multiple frequencies (Ermert et al., 2021). The advantages  
97 of this approach are the stability of results, not as strict requirements on station geometry, and a  
98 comprehensive theoretical foundation. Its disadvantages lie in computational cost, treatment of  
99 recorded data and related introduction of assumptions, and loss of temporal resolution.

100 Another approach that has gained some popularity in seismology in recent years is Matched  
101 Field Processing (MFP). MFP is the generalisation of beamforming to allow arbitrary wavefronts  
102 (Baggeroer et al., 1993). This approach has been developed in ocean acoustics, where coherency  
103 of the wavefield emitted by transient sources is high even for stations far away. Candidate sources  
104 are defined in space and absolute travel times  $t(\vec{x}_j, \vec{x}_s)$  are computed based on true distance to the  
105 source (Fig. 1d). Synthetic wavefields are computed for these travel times and matched against the  
106 recorded wavefield. In the seismological context, MFP has been applied succesfully on local (Corciulo  
107 et al., 2012; Umlauf & Korn, 2019; Umlauf et al., 2021) and regional scale (Gal et al., 2018).  
108 Recent developments in MFP include the development of different beamformers (e.g., Zhu et al.,  
109 2020), improved estimation of travel times (Gal et al., 2018), or estimating synthetic wavefields  
110 empirically (Gibbons et al., 2017). MFP is an attractive strategy for source localisation of the  
111 ambient seismic field. It allows for curved wavefronts, is based on only few assumptions, requires no  
112 intermediate step such as pre-processing of recordings, and retains computational efficiency. While  
113 the plane-wave assumption is not required in MFP, coherency of the wavefield across stations is still  
114 necessary for good results. This poses challenges when analysing recordings for stations that are not  
115 close together, and especially so for ambient seismic noise.

116 In this paper, we introduce an advancement of MFP to incorporate Earth structure and account  
117 for the complexity of seismic wave propagation. In the following, we introduce the standard MFP  
118 approach, demonstrate its shortcomings, and present our solution by incorporating more realistic  
119 Green's functions. We discuss implications of our approach, strategies to cope with them, how  
120 different disciplines and localisation approaches intersect, and finally demonstrate the applicability

121 of our approach on two real data examples. In line with the informative nature of this paper,  
 122 we provide broader context and discuss ideas as they become relevant instead of deferring such  
 123 considerations to a separate discussion section.

## 124 2 Matched Field Processing

125 The MFP algorithm is straight-forward: For a given potential source location, a synthetic wavefield  
 126 is computed and matched against the recorded wavefield, i.e., the seismograms, taking coherency  
 127 of the wavefields across stations into account. This match is evaluated and compared against other  
 128 potential source locations. The potential source location with the highest score or beampower  
 129 (representing the best-matching synthetic wavefield) is the resolved source location.

130 More precisely, spectra  $d(\omega, \vec{x}_j)$  are computed from the recorded seismograms at each receiver  
 131 position  $\vec{x}_j$ . The cross-spectral density matrix is computed as

$$K_{jk}(\omega) = d^*(\omega, \vec{x}_j)d(\omega, \vec{x}_k), \quad (1)$$

132 with  $*$  denoting the complex conjugate.  $K_{jk}(\omega)$  holds all information about the recorded wavefield  
 133 and encodes its coherency across stations; it contains the cross-correlations of the seismograms from  
 134 all station pairs.

135 The synthetic wavefield, i.e., the seismograms expected at each station from the candidate  
 136 source, is represented through synthetic spectra  $s(\omega, \vec{x}_j, \vec{x}_s)$ , with  $\vec{x}_s$  the source position and  $\vec{x}_j$  the  
 137 receiver position. In principle, these could be estimated in the time domain, but MFP computations  
 138 are done in frequency domain for simplicity and computational speed. More on how these are  
 139 computed in practise in section 2.1 and onwards.

140 The match of the two wavefields represented through  $K_{jk}(\omega)$  and  $s(\omega, \vec{x}_j, \vec{x}_s)$  is then estimated  
 141 through a so-called beamformer or processor. The most straight-forward beamformer is the con-  
 142 ventional beamformer, which in its most compact form in vector notation is often written as (e.g.,  
 143 equation 25 in Baggeroer et al., 1993)

$$B = \mathbf{s}^* \cdot \mathbf{K} \cdot \mathbf{s}, \quad (2)$$

144 with  $B$  the beampower score for a potential source location. In literature, this beamformer is  
 145 sometimes called Bartlett processor, although the origin of this name is unclear (e.g., Gal & Reading,  
 146 2019), linear beamformer (e.g., Baggeroer et al., 1993), or frequency-domain beamformer (DeMuth,

147 1977). We express  $B$  more explicitly, for clarity as

$$B = \sum_{\omega} \sum_j \sum_{k \neq j} s_j^*(\omega, \vec{x}_j, \vec{x}_s) K_{jk}(\omega) s_k(\omega, \vec{x}_k, \vec{x}_s). \quad (3)$$

148 We exclude auto-correlations ( $k = j$ ), as in Bucker (1976), because they carry "noise", i.e., the  
 149 incoherent parts of the wavefield (Soares & Jesus, 2003) and provide no useful additional information.  
 150 Auto-correlations scale the retrieved beampowers by recorded energy, which is not necessarily caused  
 151 by a higher signal-to-noise ratio (SNR). Here, signal refers to those parts of the ambient seismic  
 152 field that are (often weakly) coherent across stations.

153 Other estimators of beampower exist, and their development is an active field of research (e.g.,  
 154 Capon, 1969; Schmidt, 1986; Cox et al., 1987; Cox, 2000; Gal et al., 2014; Zhu et al., 2020).  
 155 Beamformers are often classified into conventional (eq. 3), adaptive (e.g., Capon, 1969; Cox et al.,  
 156 1987; Cox, 2000) and sub-space beamformers (e.g., Schmidt, 1986). Adaptive beamformers aim to  
 157 increase resolution of the beampower distribution by increasing sensitivity to signal, but inherently  
 158 rely on high SNR. The increased resolution is also accompanied by increased computational cost,  
 159 e.g., the Capon beamformer involves computing the inverse of  $K_{jk}(\omega)$  (Capon, 1969). Sub-space  
 160 detectors such as MUSIC (Schmidt, 1986) involve computation of the eigenvectors of  $K_{jk}(\omega)$ , and  
 161 making a selection of those for further computations based on which eigenvectors contribute to  
 162 the signal and which are "noise". Corciulo et al. (2012) used a similar approach and were able to  
 163 resolve multiple sources this way. One of the expressed goals of the approach we introduce in this  
 164 paper is to be able to locate sources of ambient seismic noise, and as such SNR is by definition low.  
 165 Beamformers beyond the conventional beamformer may not be appropriate for this, because they  
 166 either require high SNR or a choice of what part of the cross-spectral density matrix is signal and  
 167 what is "noise". Krim & Viberg (1996) have addressed the question of which beamformer performs  
 168 best under what circumstances for standard MFP. A detailed analysis of beamformer performance  
 169 in the context of our approach we introduce here is beyond the scope of this paper.

## 170 2.1 Synthetic wavefield in the standard approach

171 In practice, assumptions and simplifications about structure and wave propagation have to be made  
 172 in order to compute the synthetic wavefields  $s(\omega, \vec{x}_j, \vec{x}_s)$  that the recorded data are matched against.  
 173 In most seismological and almost all ocean acoustics applications so far, simple analytical Green's  
 174 functions of the form

$$s(\omega, \vec{x}_j, \vec{x}_s) = e^{-i\omega t(\vec{x}_j, \vec{x}_s)}, \quad (4)$$

175 are used, with  $t(\vec{x}_j, \vec{x}_s)$  the travel time of the investigated wave between source and receiver (Fig.  
176 1d). In some seismological studies, the addition of an amplitude term  $A(\vec{x}_j, \vec{x}_s)$  that accounts for  
177 geometrical spreading and/or inelastic attenuation has been discussed (Corciulo et al., 2012; Bowden  
178 et al., 2021). The goal of such a term would be to increase the accuracy of the synthetic wavefield  
179 by incorporating some of the seismic waves' propagation behaviour. Neglecting the amplitude term  
180 entirely, as is usually done, makes standard MFP equivalent to delay-and-sum beamforming without  
181 the plane-wave assumption (Bucker, 1976). More on this in section 2.4.

182 For a single stationary source in an acoustic, isotropic, homogeneous medium, i.e., with constant  
183 velocity  $v = \text{const}$  and only straight-ray propagation of a single phase (the simplest possible study  
184 target), the travel time is simply  $t(\vec{x}_j, \vec{x}_s) = \Delta x/v$ . Estimating travel times requires prior knowledge  
185 of  $v$  and the assumption that  $v = \text{const}$  is a good approximation of the medium. In seismology, this  
186 approach has been successfully demonstrated on local scale (e.g., Corciulo et al., 2012; Umlauf &  
187 Korn, 2019; Umlauf et al., 2021), where propagation effects due to heterogeneous Earth structure  
188 can be neglected. Without any prior knowledge of the velocity structure, another approach is to  
189 treat  $v$  as an additional dimension in the parameter space that needs to be explored, though this can  
190 become computationally quite expensive and may require sampling strategies other than a standard  
191 grid search (Gradon et al., 2019).

192 On regional scale, Gal et al. (2018) estimated  $t(\vec{x}_r, \vec{x}_s)$  from already available phase velocity  
193 maps using Fast Marching Method (Sethian, 1999), which accounts for off-straight-ray propagation  
194 of surface waves, and by that incorporating some complexity of wave propagation in complex Earth  
195 structure. This approach also inherently incorporates frequency-dependent effects, i.e.,  $t(\vec{x}_r, \vec{x}_s)$  be-  
196 comes  $t(\vec{x}_r, \vec{x}_s, \omega)$ . Gal et al. (2018) used this to study the primary ( $\sim 16$  sec. period) and secondary  
197 ( $\sim 8$  sec. period) microseism separately by estimating phase travel times from their respective phase  
198 velocity maps. They assume that surface waves are dominant in the microseism frequency band  
199 and are only recorded on their respective component (Love on transverse, Rayleigh on radial). This  
200 assumption is reasonable and commonly made when analysing ocean microseism (Nakata et al.,  
201 2019), but may not always be appropriate depending on the study target. Incorporating multiple  
202 phases (e.g., a mix of body and surface waves) at the same frequency is not straight-forward with  
203 the standard approach and clearly requires further assumptions about the number of phases and  
204 their respective travel times, increasing the parameter space considerably. Furthermore, when in-  
205 vestigating frequencies at which the identification of wave types may be challenging, this strategy  
206 potentially misses or misattributes important information in the recorded wavefield and may bias



207 results. Approaching the complexity of wave propagation in real Earth structure in this manner  
208 requires numerous manual interventions, as outlined above, and could therefore become impractical  
209 in wider use.

## 210 **2.2 Numerical synthetic wavefields for complex Earth structure**

211 We propose to use Green's functions computed numerically for Earth structure directly as the syn-  
212 thetic wavefield  $s(\omega, \vec{x}_r, \vec{x}_s)$  ("numerical MFP" or nMFP) instead of the analytical form described  
213 above (eq. 4, "standard approach"). Effects such as dispersion and multiple wave types are then  
214 inherently accounted for, even for simple 1D media. If the Green's function are computed for a 3D  
215 Earth, further effects such as focusing and defocusing, wave-type conversion, and coupling can all  
216 be accounted for, increasing the precision of this approach further.

217 We demonstrate our method with synthetic examples for a broadband and a narrowband explosion  
218 source (Fig. 2). The setup consists of two small arrays of three stations each that record the  
219 wavefield emitted by a seismic source located at the surface between them. The medium is a 3D  
220 axisymmetric Earth (Nissen-Meyer et al., 2014), based on PREM (Dziewonski & Anderson, 1981).  
221 The "recorded" seismograms are computed for the same model and incoherent noise is added. With  
222 the standard MFP approach (assuming  $t(\vec{x}_r, \vec{x}_s) = \Delta x/v$ ), locating the source precisely is quite  
223 challenging for both broad- and narrowband sources (Fig. 2a, c). The resolved location is clearly  
224 sensitive to the chosen velocity of the medium  $v$ . When the chosen velocity is too low, the resolved  
225 source lies further away than the real source. When it is too high, the resolved source lies closer.  
226 This applies to both broadband and narrowband sources (Fig. 2a, c). For the broadband source,  
227 the highest frequency available in the numerical Green's functions is 0.2 Hz. The error in location  
228 introduced for  $v = 3.0$  km/s is smaller for the broadband source than for the narrowband source.  
229 This occurs, because the broadband wavefield contains phases that are of different type and travel  
230 with different velocities, and  $v = 3.0$  km/s is a good estimate for at least some of them. For  
231 the narrowband wavefield, which contains mainly Rayleigh waves at 0.13-0.15Hz,  $v = 3.0$  km/s is  
232 already clearly too slow. For surface waves in particular, a different choice of velocity  $v$  for each  
233 analysed frequency band would seem appropriate due to their dispersive nature (Gal et al., 2018).

234 With Green's functions computed numerically for the same Earth structure, the location of the  
235 source is resolved precisely for both broad- and narrowband sources (Fig. 2b, d). This is unsurprising,  
236 given that we are essentially matching the synthetic wavefield against itself with some noise. But  
237 this is also exactly the intent behind the approach: matching the recorded wavefield with a more

238 realistic synthetic wavefield. Our simple synthetic tests show that the standard approach can be  
239 imprecise for locating realistic sources in slightly complex media, even under ideal conditions, and  
240 is highly dependent on choosing the correct velocity. With nMFP, we do not have to consider  
241 frequency-dependant effects explicitly as long as the numerical Green's functions applied are a good  
242 representation of elastic wave propagation.

243 MFP for narrowband sources results in prominent side lobes of beam power, regardless of ap-  
244 proach (Fig. 2c,d). These are interference patterns that emerge because of the near-monochromatic  
245 nature of the wavefield. The exact shape and position of sidelobes depends on the station distri-  
246 bution and wavelength of the investigated wave, while the correct location does not. Sidelobes will  
247 be suppressed, if a wide frequency band is used (Fig. 2a,b) or several runs of MFP for narrow  
248 neighbouring frequency bands are stacked (Umlauf et al., 2021). MFP originated as a narrowband  
249 localisation technique (Bucker, 1976) and has been adopted for broadband sources thereafter (e.g.,  
250 Baggeroer et al., 1993; Brienzo & Hodgkiss, 1993; Soares & Jesus, 2003), where the suppression  
251 of sidelobes plays a role. This has some implications for the resolution capability of MFP, which  
252 depends heavily on whether the analysed source emits a wide frequency band or not. These inter-  
253 ference patterns can also be thought of as a trade-off between spatial and frequency resolution of  
254 MFP. Using more precise Green's functions has in principle no impact on this.

255 The basic idea of incorporating more realistic Green's functions in MFP is not new. In ocean  
256 acoustics, waveforms are coherent across large distances due wave propagation being focused in the  
257 SOFAR channel, but MFP results can be highly sensitive to acoustic wave velocities (Tolstoy, 1989),  
258 similar to what we have shown in Figure 2. Bathymetry and multiple reflections may complicate the  
259 recorded wavefield even further and impact MFP performance significantly, and thus should ideally  
260 be incorporated (e.g., D'Spain et al., 1999). For elastic waves in solid Earth structure, further effects  
261 would need to be considered, as described above. One approach to this is empirical Matched Field  
262 Processing (Gibbons et al., 2017). Gibbons et al. (2017) estimate empirical Green's functions for each  
263 station from recordings of known sources by computing the principal eigenvector of the covariance  
264 matrix of the incoming wavefield for two nearly identical sources. They have demonstrated their  
265 approach in the context of mining blasts. The obvious limitation is that such template sources are  
266 required, which allows its application only for certain scenarios. This approach inspired the name  
267 for our approach (numerical MFP, nMFP), as we estimate Green's function numerically instead of  
268 empirically.

269 nMFP is not limited to recorded template sources. Using numerically computed synthetic wave-

270 fields, we can place candidate sources wherever we want. Our approach is then mainly limited by  
271 the accuracy of the numerical model and computation strategy. Improving MFP in this way has only  
272 become possible recently thanks to efforts by other authors to improve the computation of databases  
273 of Green's functions for modelled Earth structure and provide them to the community (e.g., Nissen-  
274 Meyer et al., 2014; van Driel et al., 2015; Krischer et al., 2017; Heimann et al., 2017). Computing  
275 Green's functions for complex Earth structure is expensive, which is why we rely in our analysis on  
276 pre-computed databases using *instaseis* (van Driel et al., 2015). Green's functions databases for  
277 realistic Earth structure up to frequencies of the secondary microseism are available for download at  
278 IRIS-DMC (Hutko et al., 2017) or Pyrocko Green's Mill (Heimann et al., 2017).

## 279 **2.3 On amplitudes in MFP**

280 The standard approach does not include an amplitude term. When it is incorporated, it ideally  
281 describes the two dominant contributions to amplitudes for geometrical spreading and inelastic  
282 attenuation (e.g., Bowden et al., 2021). Computing both requires assumptions about wave type and  
283 the attenuation properties of the Earth, again increasing the parameter space. Bowden et al. (2021)  
284 show in a synthetic example that first applying and later correcting for this amplitude term does not  
285 improve source locations compared to neglecting it from the beginning. It merely tests whether the  
286 assumed wave type and quality factor are correct, which poses the danger that wrong assumptions  
287 may bias results in real data studies, but also opens the opportunity to constrain anelastic properties  
288 of the Earth, if the source locations are already well-known. More importantly though, Bowden  
289 et al. (2021) also showed that computing MFP results including the amplitude term in the synthetic  
290 Green's function without correcting for it is equivalent to mapping out the sensitivity kernel for  
291 the given station-source distribution. As the authors have pointed out, MFP and interferometry-  
292 based localisation are closely connected (more on this in section 2.4). MFP without correcting for  
293 amplitudes is not useful for directly locating sources (as the highest score is no longer necessarily at  
294 the source location), but can be an appropriate starting model for the interferometry-based strategy  
295 (Igel et al., 2021a).

296 A strategy similar to the interferometry-based scheme, where the source strength at a position  
297 is perturbed and the fit between model and data is evaluated, is not viable for MFP itself. The  
298 beampower at a potential source location scales linearly with the absolute amplitudes of the recorded  
299 seismograms. This is the case, even if the match in amplitude decreases, because MFP is ultimately  
300 summing over correlations of waveforms. For this reason, other measures of waveform-similarity

301 that account for a mismatch in amplitude are commonly applied in other approaches, e.g., in full  
302 waveform inversion (Yong et al., 2019, and references therein). Accounting for this behaviour directly  
303 in MFP would require significant changes to how beamformers are designed.

304 Therefore, a strategy is required to correct for amplitude terms. Numerically computed Green's  
305 functions for complex Earth structure inevitably contain amplitude terms. Several approaches may  
306 appear reasonable to correct for them: correcting for amplitude decay (Fig. 3b), time-domain  
307 normalisation (Fig. 3c), and spectral whitening (Fig. 3d). Without any treatment of amplitudes,  
308 the beampower distribution is heavily biased by distance to stations (Fig. 3a). This effect is more  
309 pronounced compared to Bowden et al. (2021), because our Green's functions also contain body  
310 waves. Only a zoomed-in view allows to see the distribution of beampowers with a linear colorscale.  
311 The retrieved source location without amplitude treatment is close to one of the stations nearest to  
312 the actual source at the center.

313 Applying a correction factor for geometrical spreading of surface waves as has been demonstrated  
314 by Corciulo et al. (2012) corrects for some but not all of the amplitude bias (Fig. 3b). The  
315 beampower peak is still found near a station, because body waves are not corrected for. It is not  
316 clear how a single correction term could be designed to correct for both body and surface waves  
317 simultaneously. When we neglect the near-station beampowers, we find a local maximum (small red  
318 circle) near the correct source location. We are not able to resolve the source location correctly.  
319 For now, we advise against application of a correction term for amplitude decay, because it requires  
320 assumptions about wave type and the medium's inelastic properties, opening up room for error  
321 and bias as demonstrated here. When synthetic Green's function contain only a single wave type,  
322 applying a correction term is a viable strategy as shown by Bowden et al. (2021). In real applications  
323 and without prior knowledge of the source location (which defeats the purpose of MFP), such bias is  
324 not trivial to resolve. More drastic approaches to dealing with amplitude-induced bias are necessary.

325 Time-domain normalisation aims to completely remove the impact of amplitudes by converting  
326 the synthetic wavefields to time domain  $s(t, \vec{x}_j, \vec{x}_s)$  and dividing those by their maximum amplitude.  
327 With this approach, we resolve the beampower peak close to the true source (Fig. 3c), but introduce  
328 ripple-shaped artefacts in the entire beampower distribution. Time-domain normalisation is only then  
329 equivalent to properly removing the effect of amplitude decay, if waveforms did not change their  
330 shape across stations. Elastic wave propagation in realistic Earth structure results in the emergence of  
331 different phases depending on source-receiver distance, changes to the waveforms due to dispersion,  
332 as well as their amplitudes being affected differently by decay. These effects introduce the observed

333 pattern, which is undesirable.

334 Spectral whitening or frequency-domain normalisation is the process of dividing the frequency  
335 spectrum by its amplitude spectrum, a technique commonly applied in processing of ambient seismic  
336 noise records for interferometry (Bensen et al., 2007; Fichtner et al., 2020). Neglecting amplitudes  
337 as done in the standard approach is equivalent to whitening of synthetic Green's functions. In fact,  
338 whitening of the synthetic wavefield is applied in early formulations of standard MFP (equation 24  
339 in Baggeroer et al., 1993). In the context of interferometry of the ambient seismic field, whitening  
340 is often performed with a water-level or smoothed amplitude spectrum to stabilise the procedure  
341 numerically and not over-emphasize frequencies that carry no useful information (Bensen et al.,  
342 2007). Because we treat the synthetic spectra only, we are not concerned with smoothing of the  
343 amplitude spectrum before division and artefacts that whitening may introduce in real data and  
344 directly perform whitening as

$$s_{\text{white}}(\omega, \vec{x}_j, \vec{x}_s) = \frac{s(\omega, \vec{x}_j, \vec{x}_s)}{|s(\omega, \vec{x}_j, \vec{x}_s)|}. \quad (5)$$

345 This approach successfully retrieves the correct source location and does not appear to introduce  
346 any unwanted biases (Fig. 3d).

347 From our tests, whitening the spectra of the synthetic wavefields (Fig. 3d) appears to be the most  
348 advantageous approach, and follows the original formulation of MFP (Baggeroer et al., 1993). It  
349 introduces no alteration of the recorded data, eliminates attenuation and spreading effects, removes  
350 potential issues caused by source strength, and successfully retrieves the true source location. With  
351 this approach, individually acting sources are weighted equally likely, regardless of distance to the  
352 receivers, as long as their wavefields are well-recorded on all stations. This may not always be  
353 an advantage, e.g., in global-scale studies, where the convergence of the wavefield at the source's  
354 antipode can introduce bias. By whitening we also lose the ability to, in principle, constrain anelastic  
355 parameters of the Earth, but it is not clear to us how that could be approached for numerically  
356 computed Green's functions that contain all wave propagation effects.

## 357 2.4 Naming conventions and conceptual approaches to MFP

358 To illustrate how literature from multiple disciplines intersects, we want to take a moment to clarify  
359 different naming conventions and how MFP can be understood conceptually in different ways.

360 In this paper, we use language that describes the results of MFP as the distribution of beam-  
361 power retrieved from matching recorded wavefields with synthetic wavefields or Green's functions

362  $s(\omega, \vec{x}_j, \vec{x}_s)$  for candidate source locations. This language, particularly *Green's functions*, is natu-  
 363 ral for seismologists (e.g., Gibbons et al., 2017; Umlauf & Korn, 2019), though rarely also used in  
 364 ocean acoustics studies (e.g., Li et al., 2021). In ocean acoustics, other terminology is more common  
 365 for some of these concepts.  $s(\omega, \vec{x}_j, \vec{x}_s)$  is instead sometimes called *steering vector*, expressing the  
 366 idea that the array is "steered" towards the source during beamforming or MFP, or *replica vector*,  
 367 communicating that the vector represents a replica of the expected wavefield (Baggeroer et al.,  
 368 1993). The distribution of beampowers may be called *ambiguity surface* (Bucker, 1976), intended  
 369 to express the emergence of sidelobes for narrowband sources (Fig. 2c,d).

370 Both the seismological and ocean acoustics communities understand MFP as matching of wave-  
 371 fields; this idea is the original concept introduced by Bucker (1976), and gives an intuitive understand-  
 372 ing of the physics involved. Above, we mentioned that array beamforming for plane waves is a special  
 373 case of MFP. For plane-wave beamforming, Green's functions of the form  $s(\omega, \vec{x}_j, \vec{x}_s) = e^{-i\omega t(\vec{x}_j, \vec{x}_s)}$   
 374 are used, and only the manner in which  $t(\vec{x}_j, \vec{x}_s)$  is estimated is adapted to use relative distances  
 375 perpendicular to the plane wavefront (Fig. 1b) instead of distances to potential source locations  
 376 (Fig. 1d). Standard MFP is delay-and-sum beamforming, and the difference lies in whether plane  
 377 waves or curved wavefronts are used (Bucker, 1976). The simple analytical Green's function used in  
 378 standard MFP can be understood in two ways: They are the wavefields emitted by point sources  
 379 (the impulse responses), if the medium is an acoustic, isotropic, homogeneous half-space. They also  
 380 represent a phase shift (or time-delay), if convolved with a waveform.

381 Understanding beamforming as convolution leads to another way of conceptualising MFP. We  
 382 rewrite the beampower score (eq. 3), omitting the variables  $(\omega, \vec{x}_j, \vec{x}_s)$  for readability, as

$$B = \sum_{\omega} \sum_j \sum_{k \neq j} s_j^* d_k^* d_j s_k = \sum_{\omega} \sum_j \sum_{k \neq j} (s_j^* s_k) (d_k^* d_j). \quad (6)$$

383 Here,  $d_k^* d_j$  is the correlation of the recorded wavefields and  $s_j^* s_k$  the correlation of the synthetic  
 384 wavefields for each station pair  $k, j$ . The cross-correlations  $s_j^* s_k$  constitute the relative phase shifts  
 385 to be applied in standard MFP and the "matching" of wavefields in MFP is exactly this: convolution  
 386 of their correlation wavefields, where the sum of the convolution is the mismatch measure.

387 This is particularly relevant, because it also makes the close connection between MFP and the  
 388 interferometry-based localisation strategy apparent, and gives a different perspective to the insights  
 389 provided by Bowden et al. (2021). In both approaches, cross-correlation functions of recorded data  
 390 and of synthetic data are computed and compared against each other. The main difference between  
 391 them lies in how exactly cross-correlation functions are computed and how the (mis-)fit between

392 the two is evaluated. It is then not surprising that MFP results are a good starting model for  
393 interferometry-based localisation (Igel et al., 2021a); in a very real sense MFP *is* interferometry-  
394 based localisation, without data processing, e.g., waveform-normalisation or stacking, and a different  
395 mismatch measure. Bowden et al. (2021) have described this connection more mathematically:  
396 starting from cross-correlation beamforming (Ruigrok et al., 2017), a simple change in the order of  
397 operations - from shifting waveforms first and then computing the cross-correlation coefficient to  
398 first computing the correlation function and then measuring at the corresponding time lag - creates  
399 an equivalency (under certain conditions) between MFP and interferometry-based source inversion.  
400 This description and the one we introduce above result in the same realisation. Fundamentally,  
401 only two approaches for locating sources of the ambient seismic field exist: polarisation analysis  
402 (Fig. 1a) and approaches that exploit exactly wavefield-coherency across stations (Fig. 1b-d).  
403 That beamforming, MFP, and interferometry-based localisation are essentially the same may not  
404 be intuitive at first, especially considering the strikingly different sketches to illustrate them (Fig.  
405 1b-d), and the different language both communities use.

406 To retrieve "reliable" cross-correlation functions of the recorded data in ambient noise seismol-  
407 ogy, processing and stacking over time is common (Bensen et al., 2007). MFP foregoes processing of  
408 seismograms for stability entirely, allowing for high time-resolution and avoiding artefacts potentially  
409 introduced by the processing (Fichtner et al., 2020). Importantly though, the mismatch measure  
410 employed in MFP does not allow iterative inversion by source-strength perturbation, because convo-  
411 lution (or correlation) does not account for amplitude mismatch. If signals are in phase, increasing  
412 amplitudes of one results in linearly-scaling beampowers regardless of how well the waveforms fit. It  
413 is clear that both communities may benefit from each other, as is one of the fundamental arguments  
414 by Bowden et al. (2021). It is fairly straight-forward to employ strategies of the ambient seismic  
415 noise community to "improve" the correlation functions  $d_k^* d_j$ . A detailed analysis of the advantages  
416 and disadvantages this would bring, and what exactly "improving" would mean in the context of  
417 MFP is beyond the scope of this paper. Similarly, increasing the accuracy of MFP in a seismological  
418 context and discussing its fundamental ideas and limitations, as is the intent of this paper, will  
419 benefit developments in the larger field of ambient seismic noise localisation.

## 420 **2.5 Limitations of MFP**

421 Above, we have already explored the advantages and limitations of using numerically computed  
422 synthetic wavefields (Fig. 2) and amplitudes (Fig. 3) in MFP, as well as the emergence of striped



423 interference patterns for narrowband sources (Fig. 2). MFP shows further undesired behaviour  
424 under certain conditions that we encounter in real-world applications. Some of these are more  
425 straight-forward to understand in the conceptual framework of convolution introduced above.

### 426 **2.5.1 Source-Station Geometry**

427 Standard MFP becomes plane-wave beamforming for very large distances between source and array,  
428 because accounting for curved wavefronts has negligible impact on travel times. In that case,  
429 the lessons learned in beamforming, e.g., what wavelengths are resolvable without aliasing, apply  
430 one-to-one (Rost & Thomas, 2002). When MFP is considered as an approach, the source-station  
431 geometry should be such that accounting for curved wavefronts actually has useful impact on the  
432 results, i.e., the difference in expected travel times compared to plane waves is much larger than the  
433 expected measurement error. Because MFP is not bound to the plane-wave assumption, there is no  
434 meaningful difference between treating a collection of stations as an array or a network. Still, the  
435 inter-station distance should not be much smaller than the investigated wavelength or incoherent  
436 noise may prevent being able to reliably resolve the source location.

437 Closely related to these considerations is that high waveform coherency is required across stations,  
438 regardless of approach. In standard MFP or beamforming, i.e.,  $s(\omega, \vec{x}_j, \vec{x}_s) = e^{-i\omega t(\vec{x}_j, \vec{x}_s)}$ , coherency  
439 means retaining the exact shape of the waveforms across stations, because waveforms are simply  
440 shifted in time. In nMFP, waveform coherency takes a slightly different meaning, because elastic  
441 wave propagation can change the shape of recorded waveforms significantly. So instead, waveforms  
442 need to be coherent after elastic wave propagation effects have been accounted for, in nMFP via  
443 synthetic Green's functions for Earth structure.

444 Station density has direct impact on the retrieved beampower distribution that is worth pointing  
445 out explicitly. In a synthetic test, we place additional stations on the right side (Fig. 4a). The  
446 beampower distribution shows a bias towards the top-left, caused simply by the presence of more  
447 stations that recorded the signal in the bottom-right. While in the ideal scenario here, the exact  
448 source location is still resolved correctly, interpreting this distribution without prior knowledge of  
449 the sources in a real-world application is challenging. This bias in MFP results follows directly  
450 from understanding MFP as the sum over convolutions of correlated wavefields, as described above.  
451 Regions with higher station density are then inherently weighted higher and cause the observed  
452 effect.

453 This goes beyond increased resolution due to better suppression of incoherent noise, and is an



454 effect that essentially all real-world applications of MFP will have to take into consideration. We have  
455 tested two possible approaches to correct for this without success. Introducing a coherency-weight  
456 where stations that recorded similar waveforms are down-weighted to counter-act the described  
457 behaviour, does not improve the retrieved beampower distribution. This approach further lessens  
458 the advantage that multiple measurements at similar positions can reduce impact of incoherent  
459 noise. A different approach may be to homogenise the station distribution, but this often excludes  
460 high-quality stations from the analysis, especially for permanent arrays.

### 461 **2.5.2 Multiple Sources**

462 Single sources can cause prominent interference patterns, if they are narrowband (Fig. 2c,d), which  
463 depend on station geometry and frequency band. This leads to even more complex, secondary  
464 interference when multiple sources are active at the same time. In a synthetic test, we place two  
465 narrowband sources that excite identical wavefields simultaneously (Fig. 4b). The second source is  
466 placed such that it lies at the edge of a sidelobe of the first source (Fig. 2d). From the retrieved  
467 distribution of beampowers it is not at all obvious that two and only two sources are active here,  
468 and instead this may be misidentified as a single source close to the left array (Fig. 4b). The  
469 new beampower peak is entirely an interference artefact. This smearing of resolved source locations  
470 clearly relates to the wavelength of the investigated waves, and similar issues are well-known in  
471 the beamforming community (more on that in section 2.5.4). When the two sources placed are  
472 broadband instead (Fig. 4c), one may interpret the beampower distribution as two sources. The true  
473 locations are however not recovered, with a smaller error for the closer source. Similar problems, such  
474 as smeared beampower distributions can occur for single sources that move during the investigated  
475 time frame (Li et al., 2021).

### 476 **2.5.3 Time window length**

477 In MFP, a choice has to be made on how long of a time window is analysed. The basic requirement  
478 is that the time needs to be long enough to record the correlated wavefield propagating across all  
479 stations, which can be estimated roughly from expected wave velocities. Because MFP is based  
480 on correlation wavefields, by default the entirety of the chosen time window influences the result.  
481 This is easier to understand with the delay-and-sum concept, where waveforms are shifted in time  
482 and summed. Because the entire waveforms are used to compute the sum, all of the waveform  
483 plays a role. This limits the time resolution of MFP and has implications depending on the type

484 of source one aims to investigate. If a source is exciting energy repeatedly, the wavefield contains  
485 more and more of that source's energy the longer the time window is and thus gets weighted higher  
486 and higher. This is very useful for stationary "noise" sources. For impulsive sources that act rarely,  
487 this can be a disadvantage and time windows should be chosen as small as possible for them. To  
488 address this issue, the concept of a windowing function as developed for the interferometry-based  
489 localisation strategy (Bowden et al., 2021), may be an opportunity to increase MFP's time resolution  
490 even further in the future.

#### 491 **2.5.4 Quantifying resolution**

492 For plane-wave beamforming, the impact of an array's geometry on its resolution capability is well  
493 studied, and expressed by the array-response function (Rost & Thomas, 2002). The array response is  
494 calculated by computing the beampower distribution for a single synthetic incident wave. Assuming  
495 no interference between simultaneously acting sources, this is a four-dimensional problem: two  
496 dimensions for the horizontal slowness of the synthetic wave, and two for the horizontal slownesses  
497 sampled during beamforming. By choosing the slowness of the synthetic wave to be 0 km/s, as is  
498 commonly done, the resolution problem is reduced to two dimensions. With these simplifications  
499 the bias on beampower distributions can be visualised and understood, but does importantly not  
500 contain information about all possible plane waves and their interference behaviour. Subsequently,  
501 the array response is usually considered only qualitatively as a guide to which relative slownesses  
502 show sidelobes or have poor resolution (e.g., Rost & Thomas, 2002; Ruigrok et al., 2017; L er et al.,  
503 2018).

504 In MFP, the resolution problem gains four additional dimensions (eight total), because the  
505 location in three dimensions (and not just backazimuths) for both the synthetic source and the  
506 sampled source location can be resolved. If one considers sources at the surface, as done in the  
507 analysis above (Figs. 2 – 4), the problem reduces to six dimensions. To further reduce dimensions,  
508 similar to the array response in plane-wave beamforming, a choice of synthetic source location has  
509 to be made. However, in MFP there is no equivalent to slowness 0 s/km, i.e., there is no possible  
510 source location that results in all stations receiving the signal at the same time, if topography or  
511 heterogeneous structure are taken into account. Because of that, no source location exists that is  
512 a clear and widely accepted choice for synthetic tests independent of station geometry.

513 In our analysis, we have made choices of synthetic source locations for demonstration purposes  
514 (Figs. 2 – 4), which gives an impression of beampower bias similar to array-response functions in

515 plane-wave beamforming. This is possible, because we only investigate sources at the surface and our  
516 approach avoids sampling velocity by incorporating an Earth velocity model in the computation of  
517  $s(\omega, \vec{x}_j, \vec{x}_s)$ , which combined reduces the problem down to two dimensions. In particular, the choice  
518 of the synthetic source location can have significant impact on the beampower distribution. Multiple  
519 sources complicate this further and may cause dominant sidelobe artefacts that are impossible to  
520 identify and address in practice, especially if only a limited frequency band is available (Fig. 4b).  
521 This aspect is also not considered in the array response for plane-wave beamforming. It is important  
522 to keep the above assumptions and simplifications in mind when interpreting the array response or  
523 our synthetic tests. They do not provide comprehensive insight into the highly complex interactions  
524 across all dimensions of the problem. To address this, ideally a single metric would exist that  
525 expresses the entirety of beampower distribution bias for every possible source location, including  
526 multiple simultaneously acting sources. We do not see how such a measure could be designed in a  
527 universally applicable way.

528 A different approach to the resolution problem is deconvolution of the array response from the  
529 beampower distribution. Originally developed in radio astronomy, the CLEAN algorithm (Högbon,  
530 1974) has been applied to plane-wave beamforming of ambient seismic noise, enabling identification  
531 of previously undetected phases (Gal & Reading, 2016). Even though our approach reaches the  
532 resolution problem dimensionality of plane-wave beamforming (under the assumptions and simplifi-  
533 cations described above), the CLEAN algorithm relies on the same key assumption that the array  
534 response relies on: that a single synthetic source of a given horizontal slowness sufficiently describes  
535 the bias on the beampower distribution. For MFP, we have shown this to be potentially incorrect  
536 (Fig. 4b), which should be considered if designing an adaptation of the CLEAN algorithm to MFP.

537 The considerations above briefly demonstrate the, in our view, most important limitation of  
538 MFP: the concrete interpretation of individual MFP results. Interpretation seems quite challenging  
539 when either stations are distributed heterogeneously or multiple sources are acting and may have  
540 interfering sidelobe patterns. Both conditions are true for most real-world applications, especially  
541 in the context of ambient seismic noise. This is one of the main reasons other beamformers and  
542 processing techniques are being developed across disciplines (e.g., Capon, 1969; Schmidt, 1986;  
543 Cox et al., 1987; Cox, 2000; Gal et al., 2014; Gal & Reading, 2016; Zhu et al., 2020). In future  
544 work, exploring their applicability to and further developing them in the context of elastic waves  
545 propagating in complex Earth structure seems like a clear way forward. Significant advances on the  
546 resolution problem would have impact way beyond the seismological community.

## 547 **3 Demonstration on real data**

548 We demonstrate nMFP on two real data examples.

### 549 **3.1 2008 Chino Hills Earthquake**

550 First, we benchmark nMFP with an earthquake in Southern California, the  $M_W = 5.4$  Chino Hills  
551 earthquake of 2008-07-29 (Fig. 5). When applying the standard MFP approach, with an assumed  
552 velocity  $v = 3.2$  km/s (the best fit in the synthetic test in Fig. 2), we find a relatively good  
553 location of the earthquake with 7.7 km distance to the location in the CI catalog (Fig. 5a, SCEDC,  
554 2013). The good fit here confirms what other authors have found before: standard MFP can  
555 already perform quite well in seismological studies (Gal et al., 2018; Umlauf & Korn, 2019; Umlauf  
556 et al., 2021). When we replace  $s(\omega, \vec{x}_j, \vec{x}_s)$  with numerical Green’s functions for an explosive source  
557 mechanism, we at first find a decrease in location accuracy (Fig. 5b). The retrieved location is  
558 18.3 km away from the CI location. When we incorporate the moment tensor solution from the  
559 CI catalog (SCEDC, 2013), straight-forward to do with nMFP, we find an improvement in location  
560 accuracy with a distance of only 1.9 km to the CI location (Fig. 5c). This demonstrates one of the  
561 potential use cases for MFP with numerical Green’s functions: Searching for the best-fitting moment  
562 tensor may help constrain the source mechanism of unknown weak sources. A related strategy has  
563 been employed by Umlauf et al. (2021). The authors flipped the sign of waveforms, based on  
564 visual inspection and expert judgement, before applying MFP. The spatial distribution of whether a  
565 waveform had to be flipped or not to increase waveform-coherency across stations, gives hints on the  
566 radiation pattern and thus source mechanism of the seismic sources, in their case stick-slip tremor  
567 at the base of a glacier. In such a scenario, where clear identification of phase arrivals is difficult,  
568 our approach may be more systematic and help give improved estimates of the source mechanism.

569 In the case of strong earthquakes, such as this example, the usefulness of MFP is limited. Other  
570 approaches that rely on data abstraction are routinely applied and provide more precise results that  
571 allow uncertainty quantification (Li et al., 2020). We chose this example, exactly because we can  
572 compare with results from such trusted methods, i.e., the catalog location, which allows us to  
573 confirm the validity of nMFP.

## 574 3.2 Secondary Microseism

575 In a second example, we further showcase the usefulness of nMFP. We locate seismic sources  
576 in the secondary microseism frequency band (0.13 to 0.15 Hz) in the Northeastern Atlantic and  
577 Mediterranean Sea using 342 stations distributed over Europe during the first week of February  
578 2019 (Fig. 6). Three snapshots of beampower distributions are compared against hindcasts of  
579 significant wave height (WaveWatch III, Ardhuin et al., 2011). On first order, we find a good match  
580 between the standard approach (left), nMFP (middle), and the distribution of significant wave height  
581 (right) for all snapshots, at least with  $v = 3.2$  km/s in the standard approach. First, we focus on  
582 the results for the standard approach.

583 For the first snapshot (Fig. 6a,c), the results using the standard approach correlate well with  
584 significant wave heights regardless of chosen velocity, and seismic sources are located West of the  
585 British Isles. In the second example, however, we find considerable differences in the beampower  
586 distribution depending on chosen velocity (Fig. 6d). The increased ocean activity to the North and  
587 West of the Iberian Peninsula matches best with significant wave heights for velocities  $v = 3.0$  or  
588  $v = 3.2$  km/s (Fig. 6d,f). With  $v = 2.8$  km/s an entirely different region, to the West of France  
589 and South of the British Isles, is located as the dominant source (Fig. 6d). Similarly for the third  
590 snapshot, we find a clear region of high beampowers in the Mediterranean Sea, West of Corsica,  
591 that corresponds to significant wave heights only for  $v = 3.2$  km/s (Fig. 6g,i).

592 This suggests that  $v = 3.2$  km/s is a reasonable choice of seismic wave velocity for the analysed  
593 frequency band, reaffirming our synthetic analysis (Fig. 2) and our choice in the earthquake example  
594 above (Fig. 5). We claim that seismic sources of the secondary microseism should roughly co-locate  
595 with significant wave heights as an argument for the validity of this choice. This is reasonable, because  
596 the common explanation for the secondary microseism mechanism is that ocean gravity waves at the  
597 water surface, propagating in roughly opposite direction, interact and cause a standing wave that  
598 generates a vertically-propagating pressure wavefield in the water column. This pressure wavefield  
599 then interacts with the ocean bottom, generating seismic waves in the solid Earth (Hasselmann,  
600 1963; Ardhuin et al., 2015).

601 The choice of the "best" velocity for standard MFP relies heavily on exactly such prior knowl-  
602 edge and assumptions. Without prior knowledge about the study target, velocity would instead be  
603 searched as a parameter and the velocity corresponding to the highest beampower would be picked  
604 for the analysis (e.g., Gradon et al., 2019). Still, even then assumptions on the nature of possi-  
605 ble sources are made to simplify the problem, e.g., no distributed simultaneously acting sources.

606 Deviation from such assumptions can have significant impact on the retrieved beampowers and  
607 complicate the decision (Fig. 4b). Our example for the secondary microseism demonstrates the  
608 complexity of beampower distributions one encounters in a real world application that would need  
609 to be interpreted when making a choice of  $v$  (Fig. 6, left). Without relying on the assumption of  
610 seismic wave generation by the secondary microseism mechanism and other prior knowledge, it is  
611 impossible to judge whether any of the tested velocities is a better choice for standard MFP and may  
612 lead to significantly different interpretation of the results. All of the tested velocities are reasonable  
613 Rayleigh wave velocities, and deciding on one of them beforehand would include prior knowledge  
614 about what kind of shallow crustal structure is expected or dominant, e.g., sedimentary basins or  
615 crystalline basement.

616 nMFP makes a similar assumption by choosing a velocity model to compute synthetic wavefields  
617 for (Fig. 6 middle). We do, however, not base our selection of velocity model on how well MFP  
618 results match our expectations, which is fundamentally what testing of velocities in standard MFP  
619 achieves. Instead, we rely on the validity of the velocity model and computational strategy for  
620 computing wavefields, which have been developed by the seismological community over decades.  
621 This is an important assumption in its own right, but a profoundly different one. nMFP removes  
622 the need to search velocity as a parameter and reduces the solution space of MFP by one dimension  
623 (velocity) while incorporating complex Earth structure and elastic wave propagating at the same time  
624 through the use of an Earth model. These considerations give a different perspective to the main  
625 idea and biggest strength of nMFP: when we incorporate the complexity of elastic wave propagation  
626 through Green's functions computed numerically for a realistic model of Earth structure, we free  
627 ourselves from assumptions about the study target. Similar considerations apply to the earthquake  
628 example above. Importantly, this also means that nMFP likely performs worse when the real velocity  
629 structure in the study area deviates significantly from the Earth model used, an effect that is more  
630 pronounced for higher frequencies. Currently, we rely on an axisymmetric PREM model, which  
631 is a severe limitation. In future works, heterogeneous 3D models of Earth structure should be  
632 incorporated in the computation of Green's function databases utilised in nMFP.

633 The similarity between the standard approach (with  $v = 3.2$  km/s) and nMFP is generally high  
634 (Fig. 6 left and middle). This result is not surprising for a number of reasons and should be  
635 understood as an argument in favour of our approach, as discussed above. The sources we image  
636 here are generally far away from most stations and towards one direction, West. The difference  
637 in waveforms recorded across all stations then becomes relatively small. If sources were closer

638 to all stations, as e.g., for the Chino Hills earthquake (Fig. 5), improving the accuracy of the  
639 synthetic wavefield has larger impact. As mentioned above, the Green's function we rely on are  
640 based on an axisymmetric PREM Earth. Therefore we do not yet incorporate the full complexity  
641 of elastic wave propagation in this demonstration, which increases the similarity to the standard  
642 approach. Particularly relevant are the European shelf areas and the structural contrast between  
643 oceanic and continental crust (Le Pape et al., 2021). Finally, because we investigate the secondary  
644 microseism, we are limited to a narrow frequency band and cannot benefit from utilising broadband  
645 seismic waveforms. We find only slight differences between standard MFP with  $v = 3.2$  km/s and  
646 nMFP, e.g., that beampower distributions retrieved with nMFP are more focused on specific regions  
647 compared to the standard approach.

648 We do not yet feel comfortable in judging whether these differences are certain to be an improve-  
649 ment in source estimation due to the resolution problem discussed in section 2.5.4. Our synthetic  
650 tests (Fig. 2) and the Chino Hills earthquake example (Fig. 5) suggest that our approach can be  
651 more precise in locating sources. For the secondary microseism, however, we have to be careful with  
652 interpreting the observed patterns, as we have also demonstrated in synthetic tests (Fig. 4b). If  
653 nMFP will prove to be more precise also for microseisms, we may find that seismic waves are excited  
654 in specific regions in the oceans and not distributed homogeneously beneath storm systems. It is  
655 important to note here that for now we use an explosion source mechanism for the synthetic wave-  
656 fields to locate the microseism, which we have already shown to be inadequate for an earthquake  
657 (Fig. 5). In the future, we require a strategy to describe and incorporate a source mechanisms ap-  
658 propriate for microseisms. Such a mechanism should, in addition to the vertical forcing, incorporate  
659 the periodic nature of the source in a physical manner, and how excitation strength depends on local  
660 sea bed structure, such as topography and sediment thickness. Some insight in how that could be  
661 approached has been given by Gualtieri et al. (2020) and this is certainly an attractive prospect and  
662 may help better understand the exact excitation mechanism.

## 663 4 Conclusions

664 Matched Field Processing (MFP) is generalized beamforming for arbitrary wavefields, removing the  
665 need for the plane-wave assumption. It is one of the current approaches to locating sources of  
666 ambient seismic noise (Fig. 1). In this study, we advance MFP to better incorporate elastic wave  
667 propagation in the Earth by using Green's functions numerically computed for a model of Earth

668 structure directly as the synthetic wavefield that the data is matched against. We call this approach  
669 *numerical MFP* (nMFP).

670 When amplitudes are considered in MFP, results are biased by amplitude effects such as geo-  
671 metrical spreading and anelastic attenuation. In the standard approach, this is usually neglected  
672 through spectral whitening of the synthetic wavefield. We find that this strategy performs best for  
673 us as well, and that trying to correct for spreading and attenuation via an amplitude term, as has  
674 been suggested before, may not be advisable (Fig. 3). This is especially the case for nMFP, where  
675 multiple wave types can be considered simultaneously.

676 Two examples on real data showcase the potential of nMFP (Figs. 5, 6). In principle, we can  
677 use it to search for the source mechanism of a seismic source, as suggested by the improved source  
678 location after incorporating the earthquake's moment tensor (Fig. 5). This could be particularly useful  
679 in the context of tremor activity, where source mechanism determination is challenging with classical  
680 approaches. In a second example, we locate sources of the secondary microseism in the Northern  
681 Atlantic and Mediterranean Sea (Fig. 6). Results from nMFP match the standard approach's results  
682 closely, likely due to source geometry, narrow frequency band, and our reliance on Green's functions  
683 computed for an axisymmetric Earth. nMFP retains the advantage that is not biased by author  
684 choice of a medium velocity, and potentially provides higher resolution.

685 We clarify conceptual approaches to MFP and its close connection to the interferometry-based  
686 localisation. The striking similarity between them suggests that it may be a worthwhile endeavour  
687 to unify them in the future, or at least provide a framework to let the different communities benefit  
688 from each others' work. On a conceptual level, Beamforming, MFP, and the interferometry-based  
689 localisation strategy all rely on quantifying the mismatch of correlation wavefields. MFP in particular  
690 would benefit tremendously from a universally applicable approach for quantifying its resolution. The  
691 lack of such a measure is currently its major disadvantage.

692 Future advances specifically for nMFP could be on more precise Green's functions databases,  
693 or investigating the performance of beamformers particularly for elastic wave propagation. With  
694 current tools, there is the potential for reasonably sized databases that incorporate full 3D Earth  
695 structure when limiting source locations to be only at the surface. More precise Green's functions  
696 should also incorporate a better description of the microseism source mechanism, different for the  
697 primary and secondary microseism. nMFP could improve MFP with few and sparsely distributed  
698 stations, because it is less reliant on waveform-coherency across seismic stations in its strict sense.  
699 While seismometer density is improving worldwide consistently, regions with sparse deployments and



700 without purposefully built arrays are still the norm. Furthermore, tremor activity such as volcanic  
701 tremor is often challenging to locate with classical approaches. Particularly in such regions and  
702 study targets, nMFP is a powerful strategy for localising the origin of seismic energy.

## 703 **Data and Materials**

704 We provide all data and code used to generate the figures in this paper to make it entirely reproducible  
705 ([https://github.com/seismology-hamburg/schippkus\\_hadziioannou\\_2022](https://github.com/seismology-hamburg/schippkus_hadziioannou_2022)). There, we also  
706 provide a minimal working MFP example based on synthetic data and the standard approach to make  
707 the method more accessible for students and researchers interested in MFP. The MFP computations  
708 in this study rely on Python code developed for this work, which we make available under MIT  
709 license at [https://github.com/seismology-hamburg/matched\\_field\\_processing](https://github.com/seismology-hamburg/matched_field_processing).

710 Seismic data used in this study was provided by network operators of international, national, and  
711 regional seismic networks in Europe and America (Royal Observatory of Belgium, 1985; Department  
712 of Earth and Environmental Sciences, Geophysical Observatory, University of Munchen, 2001; Swiss  
713 Seismological Service (SED) At ETH Zurich, 1983; California Institute of Technology and United  
714 States Geological Survey Pasadena, 1926; Charles University in Prague (Czech) et al., 1973; GEUS  
715 Geological Survey of Denmark and Greenland, 1976; Dublin Institute for Advanced Studies, 1993;  
716 RESIF, 1995; Institut De Physique Du Globe De Paris (IPGP) & Ecole Et Observatoire Des Sci-  
717 ences De La Terre De Strasbourg (EOST), 1982; British Geological Survey, 1970; GEOFON Data  
718 Centre, 1993; Federal Institute for Geosciences and Natural Resources, 1976; Scripps Institution of  
719 Oceanography, 1986; None, 1965; Albuquerque Seismological Laboratory (ASL)/USGS, 1988; INGV  
720 Seismological Data Centre, 1997; Instituto Dom Luiz (IDL) - Faculdade de Ciências da Universidade  
721 de Lisboa, 2003; MedNet Project Partner Institutions, 1988; ZAMG - Zentralanstalt für Meteorologie  
722 und Geodynamik, 1987; Istituto Nazionale di Oceanografia e di Geofisica Sperimentale - OGS, 2016;  
723 KNMI, 1993; Norsar, 1971; Polish Academy of Sciences (PAN) Polskiej Akademii Nauk, 1990; Insti-  
724 tuto Português do Mar e da Atmosfera, I.P., 2006; RESIF, 2018; University of Leipzig, 2001; Institut  
725 fuer Geowissenschaften, Friedrich-Schiller-Universitaet Jena, 2009; San Fernando Royal Naval Ob-  
726 servatory (ROA) et al., 1996) and accessed through ORFEUS, EIDA, and IRIS via obspy (Krischer  
727 et al., 2015).

728 Colormaps used in this study are perceptually uniform (Crameri et al., 2020).

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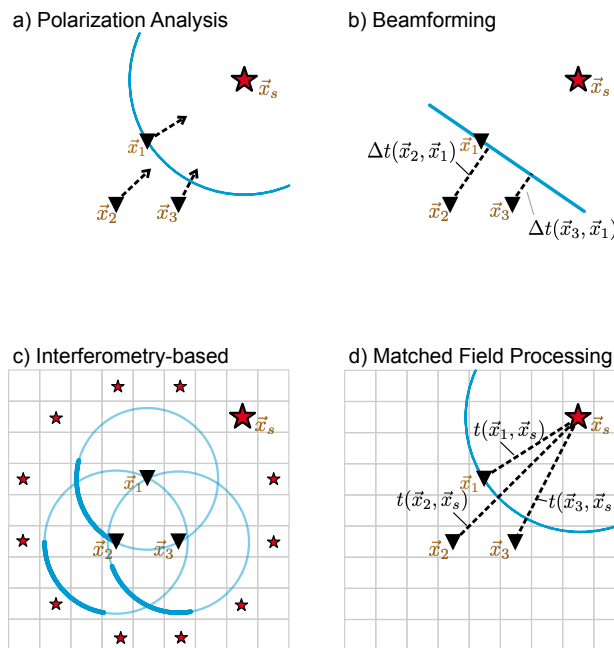


Figure 1: Current approaches to locating sources of the ambient seismic field. Wavefronts are marked blue. a) Polarization Analysis: the polarization of the wavefield on individual three-component seismometers gives an indication of direction of propagation. Triangulation allows source localisation. b) Beamforming: seismograms on multiple stations are shifted in time corresponding to candidate plane-waves, and summed over. c) Interferometry-based strategy: compare cross-correlation functions computed from seismograms of multiple stations with synthetically computed cross-correlation functions for a given source distribution. Cross-correlation functions are sensitive to the source distribution and are asymmetric (indicated by thickness of wavefront), if sources are distributed heterogeneously. d) Matched Field Processing is generalized beamforming, sampling candidate source locations instead of assuming plane waves, which allows for curved wavefronts.

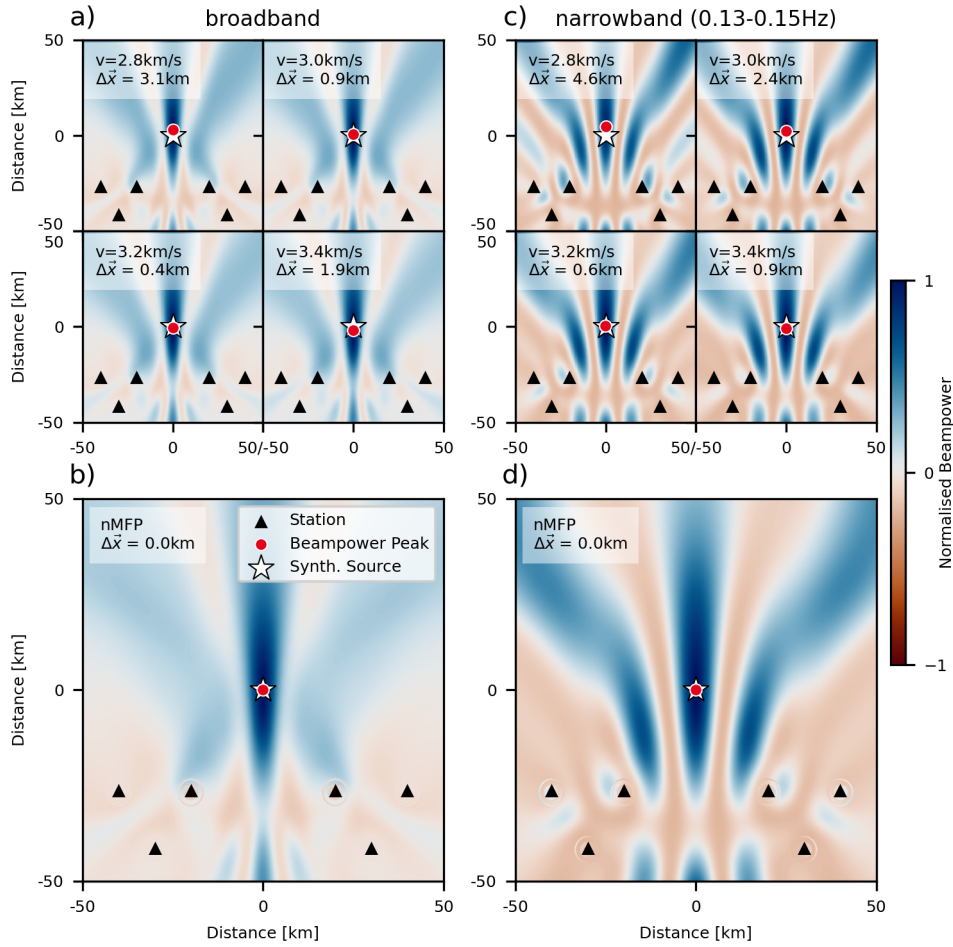


Figure 2: Synthetic demonstration for two three-station arrays locating an explosion source. The grid point with the highest beampower is the estimated source location (red circle), the white star marks the synthetic source. Note the difference between the two  $\Delta\vec{x}$  with standard MFP (top row). Left: broadband source. a) Standard approach, with travel times estimated for constant velocity. The retrieved source location is sensitive to the chosen velocity. b) Our approach, with numerical Green's functions as synthetic wavefields (nMFP). Source is precisely located. Right: narrowband source (0.13-0.15Hz). c) Standard approach. Emergence of sidelobes due to interference. d) nMFP in the same narrow frequency band and the source is precisely located.

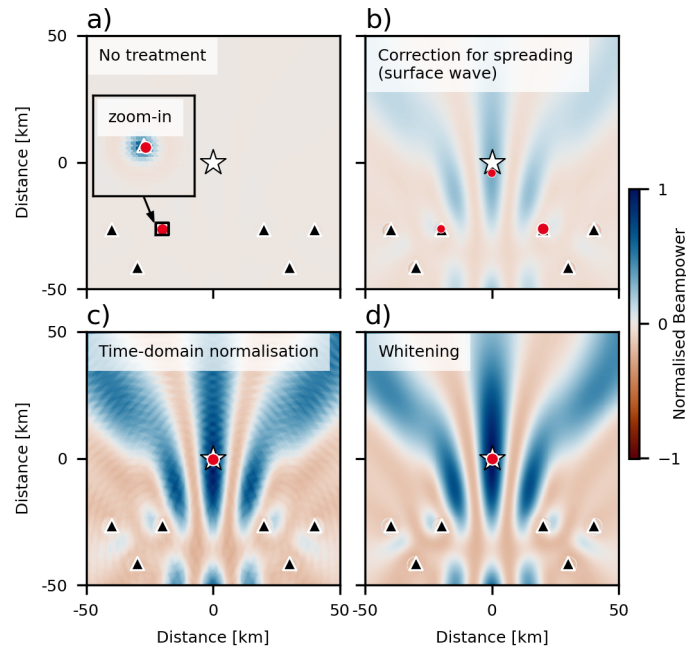


Figure 3: Strategies for treating amplitude information. a) No amplitude treatment. b) Correction for geometrical spreading of surface waves. Smaller red circles mark local beampower maxima. c) Time-domain normalisation of numerical Green's function (GF). d) Spectral whitening (frequency-domain normalisation) of numerical Green's function (GF).

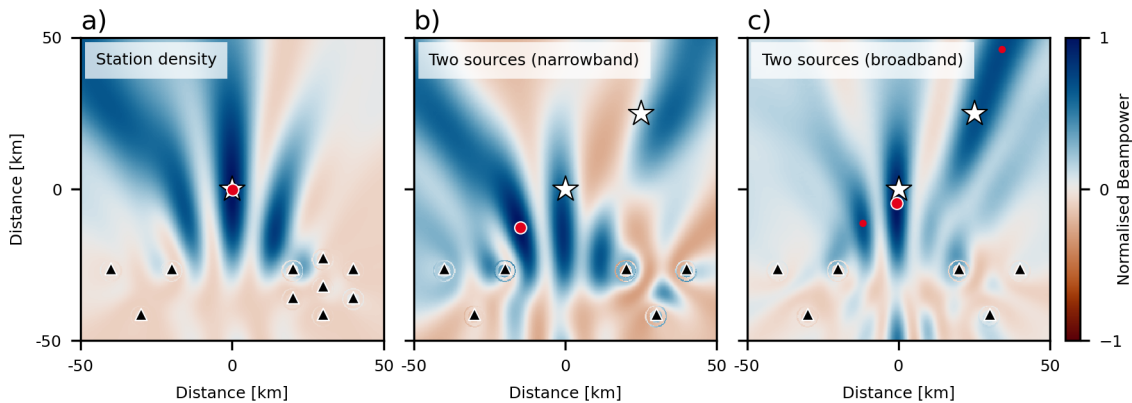


Figure 4: Some limitations of MFP, regardless of Green's function formulation. a) Impact of station density. Increased number of stations on one side results in bias of potential source locations. True source location is still resolved. b) Two narrowband (0.13 to 0.15 Hz) sources active at the same time (white stars). Beampower distribution does not represent source locations well. Global beampower maximum (red circle) is an interference artefact. c) Same as b), but for broadband sources. Beampower maxima lie closer to the synthetic source locations, but still not well-resolved. Smaller red circles mark local beampower maxima.

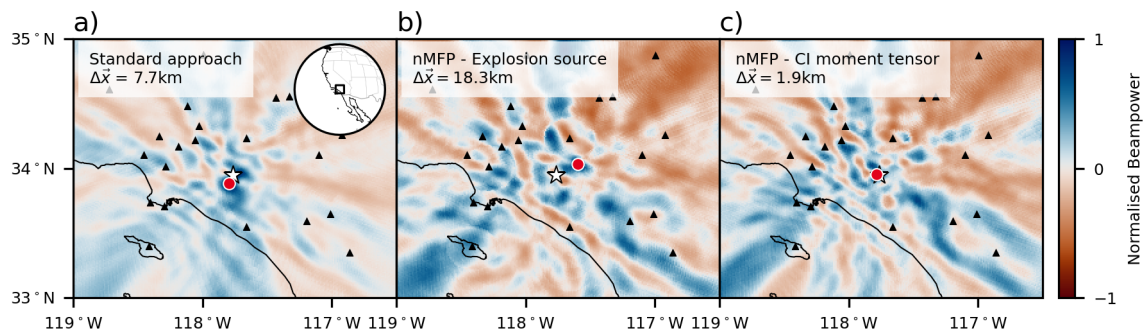


Figure 5: Location of the 2008-07-29 Chino Hills earthquake from the CI catalog (white star, SCEDC, 2013) and MFP (red circle) at 15.5km depth. MFP results were obtained using stations of the Southern California Seismic Network (black triangles) and frequencies from 0.1 to 0.2 Hz. a) Beampower distribution with simple analytical Green's functions, assuming  $v = 3.2$  km/s. 7.7 km distance to the CI location. b) Beampower distribution using numerical Green's functions for an explosive source mechanism. 18.3 km distance to the CI location. c) Beampower distribution using numerical Green's functions for the moment tensor solution in the CI catalog (SCEDC, 2013). Accounting for the source mechanism of the earthquake improves the resolved location, performing better than standard MFP (1.9 km distance to the CI location).



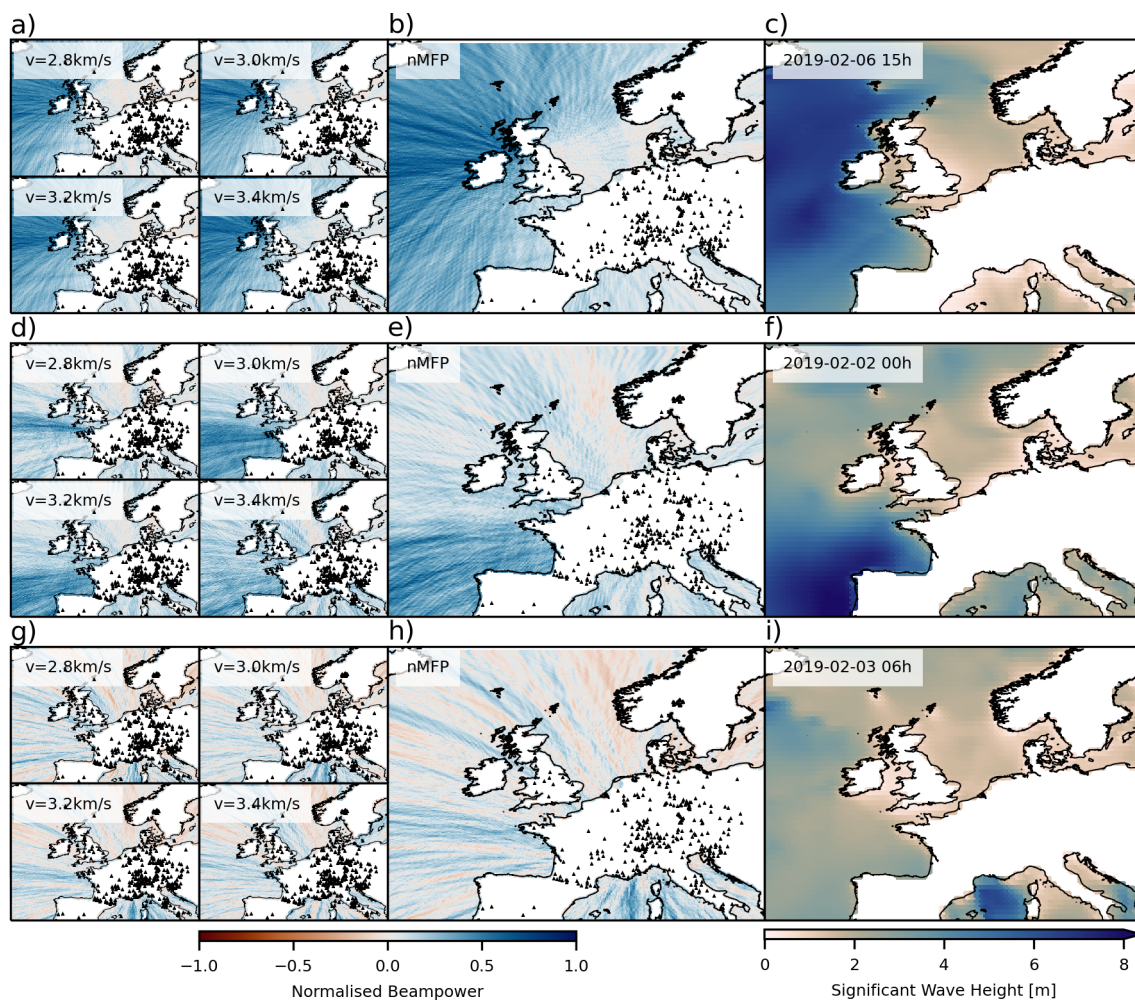


Figure 6: MFP results for the secondary microseism (0.13 to 0.15 Hz) during the first week of February 2019 for three time windows (rows). 342 stations distributed over Europe were used (black triangles). Left: MFP using analytical Green's functions for different chosen velocities  $v$ . Significant impact of choice on beampower distribution. Middle: MFP using numerically computed Green's functions (nMFP). Right: Maps of significant wave height hindcasts, provided by WaveWatch III (Ardhuin et al., 2011).