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50 Displacement/length scaling relationships for normal faults; a review, critique, and

51 revised compilation

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- 53
- 54 Abstract

55 The relationship between normal fault displacement (D) and length (L) varies due to 56 numerous factors, including fault size, maturity, basin tectonic history, and host rock 57 lithology. Understanding how fault D and L relate is useful, given related scaling laws are 58 often used to help refine interpretations of often incomplete, subsurface datasets, which has 59 implications for hydrocarbon and low-carbon energy applications. Here we provide a review 60 of D/L scaling laws for normal faults, discuss factors that could influence these relationships, 61 including both geological factors and errors in measurement, and provide a critique of 62 previously published D/L databases. We then present our newly assembled database of 4059 normal faults from 66 sources that include explicit information on: (i) fault length and 63 displacement, (ii) host rock lithology, (iii) host basin tectonic history, and (iv) maturity, as 64 well as fault D and L through time when these data are available. We find an overall scaling 65 66 law of $D=0.3L^{0.92}$, which is similar to previously published scaling equations and that varies in response to the aforementioned geological factors. Our data show that small faults (<1 m 67 68 length) tend to be over-displaced compared to larger faults, active faults tend to be overdisplaced compared to inactive faults, and faults with stiffer host rock lithologies, like 69 70 igneous and carbonate rocks, tend to be under-displaced with respect to faults within softer, more compliant host rocks, like clastic sedimentary rocks. Our dynamic D/L through time 71 72 data show that faults follow the hybrid fault growth model, i.e., they initially lengthen, during 73 which time they will appear under-displaced, before accumulating displacement. To the best 74 of our knowledge, this is the first comprehensive, integrated, critical study of D/L scaling 75 laws for normal faults and the factors influencing their growth. These revised relationships 76 can now be utilized for predicting fault length or displacement when only one variable is 77 available and provide the basis for general understanding D/L scaling laws in the context of 78 normal fault growth. This underpinning database is open-access and is available for analysis 79 and manipulation by the broader structural geology community.

80

81 **1. Introduction**

The relationship between normal fault displacement (D) and length (L) has been widely researched over several decades (e.g., Walsh & Watterson 1988; Cowie & Scholz 1992a; Dawers et al., 1993; Clark and Cox, 1996; Schultz & Fossen, 2002; Kim & Sanderson, 2005;

Schultz et al., 2008; Torabi & Berg, 2011; Xu et al., 2006). The empirical relationship

86 between D and L is often described by:

87

88 $Dmax=cL^n$

89

90 The value *n* may range from 0.5 to 2.0 (n=0.5, Fossen & Hesthammer, 1997; n=1, Cowie &

91 Scholz, 1992a; Dawers et al., 1993; Scholz et al., 1993; Clark & Cox, 1996; Schlische et al.,

92 1996; Kim & Sanderson, 2005; Xu et al., 2006; *n*=1.5, Marrett & Allmendinger, 1991;

Gillespie et al., 1992; n=2, Watterson, 1986; Walsh & Watterson, 1988). N=1 indicates a

94 linear scaling law, which implies that faults of different sizes act similarly and $n \neq 1$ indicates a

scale-dependent geometry (Kim & Sanderson, 2005; Schultz et al., 2008).

96 The value c (sometimes written as P or γ) is an expression of fault displacement and is

97 hypothesized to be related to rock material properties such as shear strength and elasticity, as

98 well as the driving stress; for example, as rock shear strength increases from a mudstone to a

99 granite, *c* increases (Walsh & Watterson, 1988; Cowie & Scholz, 1992b; Gillespie et al.,

100 1992; Ackermann et al., 2001; Kim & Sanderson, 2005; Schultz et al., 2008; Torabi & Berg,

101 2011). Reported values of c range from 0.0001-1 (Schulz et al., 2008; Torabi & Berg, 2011),

although they typically fall between 0.001 and 0.1 (Schultz et al., 2008; Torabi & Berg,

103 2011). High values of c (i.e., c=1) have been documented from strike-slip faults (MacMillan,

104 1975; Torabi & Berg, 2011).

105 This scaling relationship defined above has typically been used to: i) assess the way in which

normal faults form, with applications to geohazard analysis (Cowie & Scholz, 1992b), and ii)

107 allow better prediction of fault dimensions, with applications to energy resource exploration

and extraction, nuclear waste, and CO₂ storage, which all rely on robust structural models

that are commonly constructed from incomplete datasets (Torabi & Berg, 2011; Kolyukhin &

110 Torabi, 2012). We may need to estimate L when only D (or vice versa) can be observed in an

isolated field exposure or in a single 2D seismic reflection profile. For example, fault

112 connectivity impacts fluid flow from source to reservoir, thus knowing how fault length

113 might impact that, and how displacement may influence fault seal, is key when assessing the

114 resource potential of a sedimentary basin.

115 When plotted in log-log space, the relationship between displacement and length appears

strongly positively correlated across several orders of magnitude (see D/L plots in Walsh &

117 Watterson, 1998; Cowie & Scholz, 1992a; Schlische et al., 1996; Kim & Sanderson, 2005;

118 Torabi & Berg, 2011). However, the relationship between normal fault length and

displacement is highly variable, and a one-size-fits all equation to describe D/L scaling is

120 likely imprecise. Understanding how factors such as tectonic history, fault maturity, host rock

121 lithology, and fault size effect D/L scaling, and using these observations to create bespoke

122 D/L equations, will improve our ability to estimate either parameter.

123 D/L scaling relationships may not only describe the finite geometry of a normal fault, but

they may also provide insights into how faults grow. For example, a linear relationship (i.e.,

125 n=1) between D and L was used to justify a model of normal fault growth where faults

accumulated displacement and length synchronously; this was originally referred to as the

127 *isolated fault model*, but is now commonly referred to as the *propagating fault model* (e.g.,

128 Walsh & Watterson, 1988; Morley et al., 1990; Dawers et al., 1993; Cartwright et al., 1995;

Manighetti et al., 2001; Walsh et al., 2003; Childs et al., 2017b; Rotevatn et al., 2019). It has

also been suggested that asymmetric D/L fault profiles are showing that one fault tip is

131 pinned and the other is propagating, which could justify a propagating fault model

132 (Manighetti et al., 2001; Perrin et al., 2016).

133 Numerous studies have since challenged the notion that fault growth follows a linear

trajectory in D-L scaling space and have instead argued that faults grow in accordance with

the *constant-length model*, i.e., faults reach their near-final length rapidly and then accrue

displacement without significant further tip propagation (e.g., Walsh et al., 2002, 2003; Nicol

et al., 2005, 2017; Jackson & Rotevatn, 2013; Henstra et al., 2015; Fossen & Rotevatn, 2016;

Hemelsdaël & Ford, 2016; Tvedt et al., 2016; Childs et al., 2017b; Rotevatn et al., 2019; Pan

et al., 2021). Faults have also been shown to grow in accordance with the *hybrid fault model*;

this combines the propagating and constant-length models, suggesting that faults grow in two

141 distinct phases: (i) an initial phase (20-30% of the faults life), when maximum fault length is

reached by segment tip propagation and linkage and 10-60% of displacement is accrued, (ii) a

second stage (the remaining 70-80% of the faults life) when 40-90% of displacement is

accrued (Rotevatn et al. 2019). Some faults may also experience a stage of lateral tip-line

retreat in the last $\sim 25\%$ of their lives, where slip is concentrated along their central portions

146 (Meyer et al., 2002; Morley 2002; Nicol et al., 2020; Lathrop et al., 2021).

147 It has been suggested that fault arrays grow in cyclical stages where faults alternate between

- quick lengthening stages and prolonged displacement stages (Pan et al., 2021). During the
- 149 lengthening stage, faults grow via the constant-length model, lengthening quickly by linking
- 150 with an adjacent fault, followed by a period of displacement without additional tip
- 151 propagation. As rifts continue to develop, smaller faults in stress shadows (i.e., faults that are
- not optimally positioned to accommodate strain) become inactive as strain is partitioned and
- localised onto larger faults (Cowie et al., 2000; Gawthorpe & Leeder, 2000; Meyer et al,

154 2002; Pan et al., 2021). This pattern likely continues until extension stops in the area.

155 Global compilations of D/L data result in a range of scaling relationships with different 156 values for both c and n. There are several possible reasons for this. First, these compilations 157 may contain faults with errors in measurement of D and/or L, resulting in scaling laws that 158 are not as reliable as we wish or need. Second, there has been little research into how D/L 159 scaling relationships change for faults: (i) of different size, (ii) forming in differing tectonic settings (i.e., if a fault forms due to the reactivation of an older structure, or whether it is 160 161 newly formed in previously undeformed or only weakly deformed host rock), (iii) forming in 162 different host rock lithologies, and (iv) that have been active for different lengths of time (i.e., 163 fault maturity, which may relate to whether a fault is in a tectonically active area or not). It 164 has been noted that these factors can cause high variability in global datasets (e.g., Cowie & 165 Scholz, 1992a; Nicol et al., 2010; Rotevatn et al., 2019), but this variability has not yet been 166 quantified (see section 2). Finally, if faults really do grow via a constant-length or hybrid 167 fault growth model, D/L ratios will vary greatly throughout the life of a fault, and thus D/L 168 ratios from faults of different stages in their development are less meaningful, and a 169 compilation of dynamic D/L data will more accurately show how faults grow than a single 170 measurement taken: (i) at the end of a fault's life, once it has become inactive, or (ii) as a 171 snapshot at a specific, possibly unknown time in the fault's development.

172 It is clear there are numerous factors that may cause variability in the important, widely used 173 relationship between normal fault displacement and length. In this paper we look closely at 174 these two parameters, isolating various factors that could affect the relationship between the 175 two, and proposing improved scaling laws for specific geological setting. We first summarise 176 and discuss inconsistencies in previous compilations of D and L, critically quality checking 177 the included data. We next provide a new open-source normal fault database that includes factors such as fault maturity, tectonic history, and host rock lithology, which previous work 178 179 suggests may be important to consider when establishing and ultimately applying D/L

- relationships. We also compile data on normal fault D and L through time (i.e., from
- 181 structures flanked by growth strata that permit displacement and length backstripping; Meyer
- 182 et al., 2002; Tvedt et al., 2016; Jackson et al, 2017; Lathrop et al., 2021; Pan et al., 2021,
- 183 physical analogue studies; Schlagenhauf et al., 2008; and numerical modelling studies; Finch
- 184 & Gawthorpe, 2017) to show how faults may grow and how D/L ratios may change through
- time. Finally, we interrogate our new database and discuss how fault size, host rock lithology,
- regional tectonic history, and fault maturity affect fault growth and D/L scaling. Our new
- 187 database of normal fault properties demonstrates that one-size-fits-all scaling relationships
- are overly simplistic and that D/L scaling relationships should not be used indiscriminately.

190 2. How might geological factors and measurement errors influence scaling191 laws?

192 There are a range of geologic phenomena that can cause normal faults to be over or under-

193 displaced, and that are known to influence D/L scaling laws. Several common errors in

194 measurement can also influence D/L scaling laws. We briefly outline these and illustrate how

the related data would theoretically plot in D/L scaling space (Figure 1), before highlightingmeasurement errors in published datasets.

197

198 2.1. Geological factors

199 Different geological phenomena could affect the relationship between fault length and

200 displacement. Tectonic setting is said to affect the relationship between D and L (Cowie &

201 Scholz, 1992a). Specifically, reactivated faults can establish their maximum length more

- 202 quickly than non-reactivated faults, which means reactivated normal faults may have a
- relatively low D/L ratio, at least in the early stages of their growth (Walsh et al., 2002, Vétel
- 204 et al., 2005, Baudon & Cartwright, 2008, Giba et al., 2012, Whipp et al., 2014).

205 The amount of time that a fault has been active can also affect D/L scaling. For example,

- 206 Mouslopoulou et al. (2009) note that fault displacement rates vary through time, especially
- for 'young' faults (<20 Kyr), which can result in ~an order-of-magnitude scatter in D/L
- scaling. Nicol et al. (2010) demonstrate that active faults are under-displaced in the early
- stages of their growth, with the D/L ratio increasing with time (i.e., the constant-length fault
- 210 model, e.g., Walsh et al., 2002, 2003; Nicol et al., 2005; 2010, 2017; Rotevetn et al., 2019).

211 Host rock lithology can change the D/L ratio of a fault, with host rock lithology linked to 212 shear modulus and Young's Modulus. Walsh & Watterson (1988, 1989), Cowie & Scholz 213 (1992b) and Wibberley et al. (1999) compare D/L scaling and host rock shear modulus, 214 showing that stiffer lithologies (i.e., high shear modulus) are under-displaced compared to 215 softer lithologies (i.e., low shear modulus). Agreeing with this, Gudmundsson et al. (2004) 216 notes that faults with a low Young's Modulus and D/L are inversely related, i.e., faults within 217 softer and/or more deformed host rocks have a lower Young's Modulus and higher D/L ratios 218 (over-displaced), whereas faults within stiffer host rocks have a higher Young's Modulus and 219 lower D/L ratios (under-displaced). Several studies have also shown that mechanical 220 stratigraphy can affect D/L scaling (Muraoka & Kamata, 1983; Nicol et al., 1996; Gross et al., 1997; Schulz & Fossen, 2002; Soliva et al., 2006; Roche et al., 2013, 2014). For example, 221 222 faults can be stratigraphically confined within stiffer layers, with bounding softer or more 223 compliant layers preventing faults from propagating vertically (but not laterally), and thus causing them to be under-displaced (Schulz & Fossen, 2002). 224 225 Fault size could also affect D/L scaling, although there is some disagreement as to precisely

how. For example, Schlische et al. (1996) did not find a relationship between D/L and fault

size, although in contrast, Cowie & Scholz (1992a) found that large faults (>1 km of

displacement) are over-displaced compared to smaller faults, whereas Torabi & Berg (2011)

noted that small faults (<1 m of displacement) and large faults (>1 km of displacement) have

higher D/L ratios than medium faults (those with displacement between 1 m and 1 km).

231 When faults have along-fault changes in dip (i.e., fault dip changes in cross-section), strain,

typically in the form of folding, is partitioned onto bends; this may cause faults to appear

either over or under-displaced. According to estimates by Delokgos et al. (2020), fault bends

can cause throw to be under-estimated by approximately 10%, and up to 50% in extreme

cases. Related to this, fault drag can reduce the amount of displacement measured on a

normal fault, especially on large faults (Walsh & Watterson, 1987; Gross et al., 1997; Kim &

237 Sanderson, 2005; Childs et al., 2017a; Delogkos et al., 2017). Delogkos et al. (2017) noted

that fault drag accounted for up to $\sim 24\%$ of the total throw on faults with throws between 35-

239 550 m.

240 Igneous sill emplacement can also modify D/L scaling. For example, the inflation of an

igneous sill within the hanging wall of a pre-existing normal fault can cause reverse

reactivation of the fault, causing a decrease in fault displacement and in the ratio between D

- and L. As a result, the fault geometry and related scaling relationship may not reflect thefault's growth history (Norcliffe et al., 2021).
- 245 The growth of normal faults by linkage of segments can also cause faults to have multiple,
- smaller displacement maxima, instead of a single, large maximum displacement value. This
- can cause the faults to appear under-displaced (e.g., Peacock & Sanderson, 1991; Gillespie et
- al., 1992; Cartwright et al., 1995; Dawers et al., 1995; Acocella et al., 2000; Xu et al., 2006;
- Faure Walker et al., 2009).
- Low-angle normal faults and listric faults with a low angle (dips between 20-30 degrees) can
- have higher D values than standard normal faults due to their geometries (Morley, 2009;
- 252 Madarieta-Txurruka et al., 2021). This could skew D/L scaling laws. Typically, this
- information is not reported, and we encourage future researchers to provide this information
- 254 for future analysis.

255 2.2. Measurement errors

- In addition to the geological factors outlined above, the relationship between displacement
- and length could be affected by precisely where on a fault surface these values are measured,
- i.e., it is possible that the true maximum length and displacement have not been recorded
- 259 (Kim & Sanderson, 2005; Torabi et al., 2019). Maximum displacement is typically located
- 260 near the fault centre, however an arbitrary section of the fault exposed in outcrop may not
- pass through the centre, which is referred to as the 'cutting effect' (Kim & Sanderson, 2005).
- 262 If fault offset is measured as throw instead of displacement and is then included in a D/L
- 263 database without knowledge of fault dip, the D/L ratio would be inaccurate (Figure 1). This
- does not greatly alter the position of a data point on a D-L plot (Figure 1), but it could affect
- the derived scaling equations.
- 266 D/L ratios can be skewed if different types of faults are plotted together. For example, strike-
- slip faults tend to be over-displaced compared to normal faults, with D/L ratios being as high
- as 1:1, whereas normal faults have a maximum ratio of 1:2 (Kim & Sanderson, 2005; Torabi
- & Berg, 2011), so this could skew normal fault scaling laws towards being more over-
- displaced (Figure 1). The higher D/L ratios in this case are possibly due to fault length being
- 271 measured parallel to slip direction, whereas fault length should be measured perpendicular to
- dip for a pure dip-slip normal fault (Kim & Sanderson, 2005; Torabi & Berg, 2011). It is also
- 273 possible that oblique-slip faults could be included in a normal fault database, which could
- have a lower D than purely dip-slip normal faults.

- 275 Displacement and length relationships measured from individual earthquakes scale
- differently to those derived from faults, i.e., the average slip to rupture length scaling
- 277 relationship for individual earthquake events is $D=5x10^{-5}L$ (Wells & Coppersmith, 1994;

278 Iezzi et al., 2018; Figure 1), thus data from individual earthquakes should not be added to D-

279 L scaling databases. D-L data derived from individual earthquakes record only the length

- 280 dimension of the slip patch and the magnitude of slip.
- 281 Deformation bands are mechanically different than tectonic faults; deformation bands
- experience strain hardening after formation due to grain interlocking, with strain then tending
- to localize elsewhere and form new bands instead of increasing displacement on existing
- bands (Fossen & Rotevatn, 2012). This causes deformation bands to be under-displaced
- compared to tectonic faults, usually having a value of n=0.05. Inclusion of deformation bands
- in D/L scaling databases would thus skew D/L scaling relationships (Wibberly et al., 2000b;
- 287 Schulz et al., 2008; Fossen & Rotevatn, 2012; Figure 1).
- 288 There is also error associated with D/L measurements obtained from normal faults imaged in
- 3D seismic reflection data. For example, length could be underestimated by a few hundred
- 290 meters to a few kilometres, depending on fault size, due to the displacement near the fault tips
- being under seismic resolution (Yielding et al., 1996; Pickering et al., 1997; Rotevatn &
- Fossen, 2011). If fault displacement is measured in time- (rather than depth-) migrated
- seismic reflection data, a good knowledge of subsurface velocities is needed to accurately
- convert values of displacement in milliseconds two-way time (ms TWT) to metres. If these
- velocity data are poor, there will be uncertainty around D, and the D/L ratio may accordingly
- be inaccurate, i.e., if the applied velocity is too high, displacement, and the D-L ratio, will be
- under-estimated. Compaction could also decrease throw values (up to 20% compaction
- according to Taylor et al., 2008; Figure 1), which can be an issue for deeply buried faults in
- 299 compactable, mudstone-dominated host rock.
- 300 The measurement errors described above can visually skew plotted data and significantly
- 301 change calculated D/L scaling laws. D/L scaling laws are undoubtedly important for
- attempting to estimate D from L (or vice-versa), but D/L plots are also important as they are
- 303 often used to qualitatively check if a D/L relationship is strong or weak. These errors can
- skew D/L plots to different extents, depending on how the data are presented (Figure 1). The
- 305 effects of errors such as measuring throw instead of displacement, the cutting effect, the
- 306 impact of post-formation decompaction, and issues related to seismically imaging low-

307 displacement fault tips, result in changes that are apparent in a graph not presented in log-log 308 space (Figure 1A), but that make little difference in a log-log D/L graph (Figure 1B). Data in 309 log-log space tend to 'hide' fluctuations due to small measurement errors, as data will move 310 very little and will still lie within the range of values in the global database. These errors in 311 measurement could change D/L scaling laws, but unless the error is more than an order of 312 magnitude than the correct value, it likely will not be seen in log-log space. However, when 313 structures other than normal faults, such as strike-slip faults and deformation bands, or 314 measurements from singular earthquake events are included in a database, they fall 315 significantly outside the typical range of D/L values (Figure 1). While more error is visible in 316 a plot not in log-log space, there is a bias towards larger faults if the plot spans several orders 317 of magnitude, as only the largest faults are visible when faults of all sizes are included on one 318 plot (see Figure 1).

319

320 **3. Issues with previous D/L databases**

321 Several highly cited D/L and throw/L databases have been complied in the past 35 years 322 (Walsh & Watterson, 1988; Cowie & Scholz, 1992a; Schlische et al., 1996; Bailey et al., 323 2005; Torabi & Berg, 2011). Some of the data included in these contributions do not measure 324 true D or L, despite these data being reused in newer compilations. As a result, D/L scaling 325 laws could be affected. The way in which these data were presented, in non-digital format, 326 plotted tightly in log-log space, made the data unobtainable and non-replicable. We here 327 review these complications and suggest which data points could inaccurately skew D/L 328 scaling laws and should not be included in future databases.

Walsh & Watterson (1988) was, to the best of our knowledge, the first contribution that

compared the relationship between length (referred to as fault width) and displacement using

a global compilation of faults. 308 normal faults from the British Coalfields were compared

to a global dataset of 58 faults from 22 sources (Supplementary Table 1). In that paper, the

relationship between fault length and displacement was described as $D=L^2/P$, where P

(equivalent to c) is a variable and related to rock properties, such as host rock shear modulus,

- 335 (e.g., Cowie & Scholz, 1992b; Bailey et al., 2005; Kim & Sanderson, 2005; Nicol et al.,
- 336 2020). They use the assumption that n=2 because all their data was bounded by a slope of 2,
- despite their data having an overall regression line of n=1.58 (Walsh & Watterson, 1988). An
- average best-fit equation was not given, so the average value of c is not known. Of the 22
- sources included in their dataset, nine had included data where D or L was not explicitly

340 given, which could have skewed their final D/L scaling law. For example, neither D and/or L 341 were included in some of the original sources used by Walsh and Watterson (1988) (Teas, 342 1929; Babenroth & Strahler, 1945; Brunstrom, 1963; Mayuga, 1970; Huntoon, 1974; Van 343 den Bark & Thomas, 1980; Aitkenhead et al., 1985). We note that Teas (1929) lists the 344 measurement of the "closure around the fault", which was likely included as displacement, 345 and Huntoon (1974) does not explicitly state fault length and displacement. We therefore 346 assume that Walsh & Watterson (1988) may have established fault length and displacement 347 from a schematic map of the study area (see Figures 2, 3, 5, and 6 in Huntoon, 1974). In some 348 papers, D and/or L were given as a range rather than a single value (i.e., displacement ranges 349 from 100-500 m; Shepherd & Burns, 1978; Frost & Halliday, 1980), and Walsh & Watterson 350 (1988) may have picked a mid-point or maximum value of the range; this could possibly 351 change the derived scaling relationship, making the data appear over or under-displaced, 352 depending on what value was chosen. The data from Babenroth & Strahler (1945) and Huntoon (1974) were also originally given as throw and was included in the Walsh and 353 354 Watterson (1988) dataset as displacement, which could make the faults look slightly under-355 displaced; throw data could be converted to displacement if the fault dip is known or 356 assumed, however this is not discussed in their methodology. It is also entirely possible that 357 correct fault length and displacement values were given to Walsh & Watterson (1988), via 358 personal correspondence with the authors, however that was not included in the methodology 359 or indicated by an in-text citation.

- 360 Cowie & Scholz (1992a) subsequently compared D/L relationships of ~210 faults compiled
- from nine different sources, one of which overlaps with the sources used in Walsh &
- 362 Watterson (1988; Supplementary Table 1). Their data suggest a linear D/L scaling
- relationship (n=1) (Cowie & Scholz, 1992a), which would suggest an equation of D=cL.
- Average values of c are not given. They note that large faults (defined as faults longer than 1)
- km) have a higher D/L ratio, possibly since faults that cut through the brittle upper crust
- 366 (usually faults with L > 10 km) have a higher displacement (Cowie & Scholz, 1992a).
- 367 Cowie & Scholz (1992a) included normal faults, as well as thrust (Elliot, 1976), and strike-
- 368 slip faults ((MacMillan, 1975; Peacock, 1991) in their analysis. This was not an error as it
- 369 was the intention of the paper, however grouping different types of faults together could skew
- 370 D/L ratios.Additionally, neither D nor L data was presented in the data from Krantz (1988)
- 371 (which contributed ~ 12 of ~ 210 data points) so we cannot be sure where, geologically

372 speaking, these values were obtained from or how robust they are. Again, it is possible that 373 the correct fault length and displacement values were obtained via personal correspondence. 374 Schlische et al. (1996) compared 201 normal faults from the Dan River Basin, USA to a 375 global database of 346 faults from 11 sources, nine of which overlap with the earlier Walsh & 376 Watterson (1988) and Cowie & Scholz (1992a) compilations (Supplementary Table 1). One 377 of the key aims of this paper was to compare the D/L relationship of small (L ≤ 1.25 m) and 378 larger faults. They found that D/L did not vary as a function of fault size. Of the faults in their 379 global compilation, 174 were strike-slip faults from two different sources, and 172 were 380 normal faults from 11 different sources (Supplementary Table 1). They note a broadly linear

relationship between D and L (n=1), with c values between 0.001 and 1; some of the

variability in c could be due to the inclusion of strike-slip faults in the dataset, which

typically have a higher D/L ratio than normal faults (Kim & Sanderson, 2005). The best fit

curve through the compiled data is arithmetically defined by $D=0.03L^{1.06}$, with the authors noting that there is no significant change in the D/L scaling relation across many orders of

386 magnitude.

387 Bailey et al. (2005) compared throw-length (rather than displacement-length) relationships of 388 their 7862 normal faults from the East Pennine Coalfield, UK to a global dataset of 1756 faults from 46 different sources, 22 of which overlap with Walsh & Watterson (1988), Cowie 389 390 & Scholz (1992a), or Schlische et al. (1996) (Supplementary Table 1). Of the 46 sources 391 used, 29 had potential errors in measurement, included data that was not from normal faults, 392 or were from a source that was not publicly available; together, these issues could have 393 affected the derived D/L scaling law. For example, length and/or displacement/throw are not 394 listed in the original sources of several datasets (Beck, 1929; Teas, 1929; Babenroth & 395 Strahler, 1945; Brunstrom, 1963; Woodland & Evans, 1964; Wood et al., 1969; Mayuga, 396 1970; Huntoon, 1974; Van den Bark & Thomas, 1980; Aitkenhead et al., 1985; Gillespie et 397 al., 1993). For example, Beck (1929) only had displacement shown in a schematic cross-398 section, Krantz (1988) only measured slip vector direction, Gillespie et al. (1993) measured 399 fault spacing, and Gross et al. (1997) measured maximum dip separation, yet all these values 400 were included as throw. Thrusts were included in the compilation (Fox, 1959; Elliott, 1976; 401 Rowan, 1997), as well as strike-slip faults (Freund, 1970; MacMillan, 1975; Peacock, 1991). 402 Data from unpublished (and still publicly inaccessible) theses were also included (MacMillan, 1975; Gillespie et al., 1991), as were data from individual earthquakes (Jackson 403 404 et al., 1996). Some faults had either displacement or length listed as a range of values instead

- 405 of a single measurement (see Figure 1) (Shepherd & Burns, 1978; Frost & Halliday, 1980).
- 406 There were also some duplicate data, where the same faults were studied in two separate
- 407 papers and both were included; note that this does not visually affect the data plot but can
- 408 influence scaling relationship calculations (Dawers et al., 1993; Dawers & Anders, 1995).
- 409 Deformation bands were also included as faults (Fossen & Hesthammer, 1998), with these
- 410 structures having displacements up to two orders-of-magnitude smaller than tectonic faults of
- 411 the same length. Several sources measured fault displacement in their original sources
- 412 (Muroaka & Kamata, 1983; Opheim & Gudmundsson, 1989; Walsh & Watterson, 1988;
- 413 Marrett & Allmendinger, 1991; Dawers et al., 1993; Nicol et al., 1996; Schliche et al., 1996),
- but were included in Bailey et al. (2005) as throw. Despite these issues, the data compiled by
- 415 Bailey et al. (2005) has been used in several subsequent papers (Nicol et al., 2010, 2017;
- 416 Reilly et al., 2017; Rotevatn et al., 2019; Bramham et al., 2021).

417 To the best of our knowledge, the most recent compilation of D and L is by Torabi & Berg 418 (2011), who studied faults in siliciclastic rocks from 27 sources, 16 of which have overlap 419 with Walsh & Watterson (1988), Cowie & Scholz (1992a), Schlishe et al. (1996), or Bailey et 420 al. (2005) (Supplementary Table 1). The total number of faults they include is unclear, as the data is very tightly spaced in the presented scatterplot and the raw data are not available for 421 422 analysis. However, in the text they state these data are for normal faults from 22 sources, 423 reverse faults from four sources, and strike-slip faults from three sources (some sources had 424 more than one type of fault; Supplementary Table 1). Torabi & Berg (2011) consider the 425 potential causes of scatter in the data, such as the underestimation of the frequency of small 426 faults (truncation effect), and the under-estimation of the frequency of long faults due to 427 sample line limitations (censoring effect). They found that small faults ($L \le 1$ m) and large 428 faults (L>1 km) have a similar D/L ratio, and that medium-sized faults (L=1-1000 m) tend to be comparatively under-displaced (Torabi & Berg, 2011). They suggest this difference arises 429 because medium-sized faults are still growing by segment linkage, and that their D/L ratio 430 431 will eventually match that of larger faults as they mature (Torabi & Berg, 2011). They also 432 found that strike-slip faults are over-displaced compared to normal and reverse faults, and 433 that cataclastic deformation bands are under-displaced compared to faults (Torabi & Berg 434 2011). Length and/or displacement was also not listed in the original sources of several 435 datapoints (Krantz, 1988; Gillespie et al., 1993. Vertical offset (i.e., throw) was measured in Villemin & Sunwoo (1987), which would vary slightly from displacement. 436

438 **4. Methodology**

- 439 Our D/L database includes 4059 normal faults from 66 sources (Supplementary Table 2), 440 ranging in length from 10 mm to 245 km, in age from the Carboniferous to presently active 441 faults, and in duration of activity from faults that were active for >100 Myr to those that have 442 been active for <1 Myr, and includes natural faults and those generated by physical and 443 numerical models (Supplementary Table 2). Maximum length and maximum displacement 444 are noted in our database, along with fault host rock lithology, fault maturity, and tectonic 445 history when the information is available. We focused on these parameters because they are known to affect fault growth (e.g., Cowie & Scholz, 1992a; Torabi & Berg, 2011), and they 446 447 provide a relatively easy and replicable way of characterizing and comparing faults. All the 448 data are provided in raw format and are publicly available, such that the wider geologic 449 community can easily access, analyze, and add to. We created what was to our knowledge at 450 the time of the submission of this manuscript, all of the normal fault data that could be found, 451 however it is likely that additional data exists that we did not include, and additional sources 452 will continue to become available in the future.
- When displacement and length were not explicitly stated in the original sources, we used dataacquisition software (Quintessa Graph Grabber;
- 455 <u>https://www.quintessa.org/software/downloads-and-demos/graph-grabber-2.0.2</u>) to pick the
- displacement and length from graphs. This yields a certain level of error, especially when
- 457 taking values from a graph in log-log space, because: (i) several overlapping data points may
- 458 only yield one datapoint; and (ii) there is some minor imprecision on where the extracted data
- lie on the X (length) and Y (displacement) axis, which in a log-log plot could be moderately
- 460 significant (see Figure 1).
- 461 To be included, faults had to be normal (i.e., extensional) faults dominated by dip-slip
- 462 kinematics; reverse and strike-slip faults were not included. All of the included faults were
- 463 reported to be purely dip-slip in their original sources; however the results could be skewed if
- the faults did have an oblique slip component. Fault length is defined as 'the longest
- 465 horizontal or sub-horizontal dimension along the fault plane, perpendicular to slip direction
- 466 (Watterson, 1988; Kim & Sanderson, 2005). Fault displacement describes the movement
- 467 between two fault blocks, calculated by measuring an offset marker bed separated by a fault
- 468 (Walsh & Watterson, 1988; Xu et al., 2006). Displacement should be measured at its
- 469 maximum point on the fault. If throw was listed in the original source, it was converted to
- 470 displacement using the listed fault dip, or an average 55 degrees when fault dip was not

471 explicitly stated. An average dip of 55 degrees is used because normal fault dip tends to range

472 between 40 and 70 degrees. All data are from geologic faults and not individual earthquakes.

- 473 Faults have been sorted and analyzed by size. We use length as a measure of fault size,
- defining three classes: *small* (<1 m), *medium* (1 m-1 km), and *large* (>1 km) (see also Torabi
- 475 & Berg, 2011).

476 Since host rock lithology might influence scaling laws, we sorted D/L data into the following 477 groupings: clastic (fine-grained sand and coarser), fine-grained clastic (siltstone and finer), 478 carbonate (specifically a carbonate 'coarser' than lime-mud), fine-grained carbonate (e.g., 479 lime mud), mixed carbonate-clastic, evaporite-bearing sedimentary rocks, igneous, igneous 480 with clastic, and unlithified sand. Faults with metamorphic host rocks have been included in 481 the database, however there were not enough to calculate meaningful statistics, so they were 482 not included in our analysis. Information on host rock lithology could not be found for every 483 fault, and it is only included in the database when explicitly listed by the author or found in 484 another source documenting the same basin. Faults often offset a variety of host rock 485 lithologies, especially for large faults, but they were categorized by the dominant lithology 486 (i.e., over c. 50%). 'Carbonate' host rocks are those with >50% carbonate material that is coarser than lime-mud. Faults with host rocks classified as 'clastic sedimentary' have host 487 488 rocks whose lithologies are >50% clastic sedimentary rock, with sand-sized or coarser grains. 489 Faults with host rocks classified as sedimentary with evaporites have host rocks whose 490 lithologies are sedimentary rocks in areas with evaporites; not every fault is necessarily 491 physically linked to an evaporite detachment. Faults with host rocks classified as 'fine-492 grained clastic' have host rocks whose lithologies are >50% clastic sedimentary rock with 493 silt-sized or smaller grain sizes. Faults in rocks classified as 'fine-grained carbonate' have 494 host rocks whose lithologies are >50% carbonate rock with fine-grained lithologies, such as 495 lime-muds. Faults in rocks classified as 'mixed carbonate and clastic' have host rocks whose lithologies are roughly 50:50 clastic and carbonate. Faults with host rocks classified as 496 497 'unlithified' were formed in unlithified sediment at the time of active faulting. Faults with 498 host rocks classified as 'igneous' have igneous host rocks. Faults in rocks classified as 499 'sedimentary with igneous' have both sedimentary and igneous host rocks. Faults in 500 metamorphic host rocks were included in the overall dataset, however, there were not enough 501 of them to be statistically significant, so they are not separated in their own sub-group. To 502 compare the relationship between D/L to lithology and Young's Modulus, we compiled a list 503 of known Young Modulus for different lithologies from published sources to find a range of

possible values and average value for each lithology; these data can be downloaded here
 https://figshare.com/articles/dataset/Young s Modulus/17087342.

506 Faults were also classified based on tectonic history to assess how end-member tectonic 507 histories might affect their length and displacement. More specifically, we categorized them 508 as *reactivated* and *no pre-existing structures*; the former are from areas where faults clearly 509 reactivated structures that after a period of quiescence, became active again. These faults may 510 have formed in response to the reactivation of structures that previously experienced 511 extensional, compressive, strike-slip deformation, or a combination of these, before being 512 reactivated as normal faults. Faults categorized as having no pre-existing structures are from 513 areas thought to have not experienced significant earlier deformation. Information on tectonic 514 history is not always available, so not every fault is categorized this way.

515 Faults were classified as *active* and *inactive*; this allowed us to assess whether active faults 516 show different length and displacement relationships compared to inactive (i.e., dead) faults. 517 Faults categorised as active are from study areas where faults are currently active in 518 tectonically deforming regions, although every fault might not necessarily be active. Faults 519 categorised as inactive are from areas that are not tectonically active, i.e., inactive rifts now 520 buried and imaged in seismic reflection data or exposed in the field in exhumed basins. This 521 information is not available for every fault in the database, so not every fault is included in 522 this categorization. Care must be taken with these data because it is possible for an active 523 fault to have been active for a long period of time and thus be over-displaced compared to an 524 inactive fault that became inactive prematurely due to the removal of the driving stress. Additionally, faults displacement measurements could be affected by climate and erosion, 525 526 especially faults that have been inactive for a long period of time.

We stress that care must be taken when evaluating how these factors affect D/L scaling relationships as it might be difficult or impossible to isolate the role of each. For example, if a large fault is newly active, has an igneous host rock, and formed due to reactivation of a preexisting structure, it may be difficult or impossible to determine which factors has the most influence on its D/L ratio.

For each subcategory, we present the data in four ways: (i) in log-log space – even though
data can visually 'hide' in log-log space (Rotevatn et al., 2019), they allowed us to view all
data in one plot where all orders of magnitude can be seen together (ii) in non-log-log space,
with data shown all together in one graph spanning all orders of magnitude – this allowed us

536 to show overall D/L average trendlines, even though smaller faults cannot be visualised, (iii) 537 non-log-log space, grouped by order-of-magnitude so that all of the data can be seen more 538 clearly, (iv) and in a probability density plot. Probability density plots calculated the 539 probability density of D/L values in the each of the different aforementioned categories. We 540 used a kernel density estimation (KDE), which is a non-parametric method of estimating the 541 probability density of a function of a random value, in this case D/L. The height of each plot 542 (y-axis) corresponds to the probability density of the data at a given value of D/L (x-axis). 543 The peaks of the density plot are at the D/L values with the highest probability. A log-log 544 linear model (linear regression) was conducted to calculate a scaling law relationship of the 545 entire dataset, as well as each sub-category (i.e., fault size, tectonic history, fault maturity, 546 host rock lithology). Power law relationships were used because that is the standard in the 547 literature when relating fault displacement and length, and because it tended to fit the data 548 best. When describing faults throughout the paper, we refer to faults as over-displaced if D/L>0.1 and under-displaced if D/L<0.01. 549

550

551 **5. Results**

552 In our database, faults are 0.011-344,800 m long (Figure 2) and have a power-law trendline of $Dmax=0.03L^{0.92\pm0.01}$ (i.e., $n=0.92\pm0.01$ and c=0.03; Table 1). Our value of n is thus 553 broadly consistent with the estimate of Cowie & Scholz (1992a) and others (n=1) for normal 554 555 faults. However, there is a large amount of scatter in our data, with displacements for a given 556 fault length ranging across 1.5-4 orders of magnitude (Figure 2). In this section we 557 investigate how D/L relationships are affected by fault size, maturity, tectonic history, and 558 host rock lithology. We also look at examples of how D and L (and their related scaling 559 relationship) change through time, assessing how this relates to the D/L global database, which is based on finite (i.e., present) fault geometry. 560

561

562 **5.1. Size**

A total of 395 small faults were included from 11 different sources, 3246 medium faults were included from 48 sources, and 394 large faults were included from 35 sources (seen in Figure

2). The dataset includes small faults from areas such as the High Atlas, Morocco and the Dan

566 River Rift, USA, medium faults from areas such as the Pyrenees and Utah, USA, and large

567 faults from areas such as the Levant Basin, offshore Lebanon, and the North Sea, offshore

568 Norway. Our data show that small faults have a higher D/L ratio, with a power-law trendline

569 indicating $Dmax=0.04L^{0.97\pm0.02}$, $n=0.97\pm0.02$ and c=0.04; Table 1, Figure 2). Medium and

570 large faults have similar power-law trendlines of $Dmax=0.03L^{0.94\pm0.01}$ and

571 $Dmax=0.001L^{1.3\pm0.01}$, respectively, $n=0.94\pm0.01$ and c=0.03 for medium faults and

572 $n=1.3\pm 0.11$ and c=0.001 for large faults (Table 1). However, the values of *n* of small and

573 medium faults are within the same confidence interval (Table 1).

574 There is a significant amount of scatter in the relationship between D and L, especially for

575 larger faults (i.e., 3-4 orders of magnitude; Figure 2). For example, faults that are 10,000 m (\pm

576 200 m) long have displacements ranging from 4 m to 999 m, with a standard deviation of 303

577 m. In contrast, medium faults only vary by 1-2 orders of magnitude (Figure 2). For example,

faults that are 50 m (\pm 1 m) long have displacements ranging between 0.3 m and 7 m, with a

579 standard deviation of 1.6 m. Small faults have the least amount of scatter, with displacements

that vary by only 1-1.5 orders of magnitude (Figure 2). For example, faults that are 0.1 ± 0.05

581 m long have displacements between 0.002 m and 0.01 m, with a standard deviation of 0.003

582 m.

583 Medium and large faults plot similarly in a probability density plots (Figure 3); there is a

 $\sim 24\%$ probability and $\sim 23\%$ probability, respectively, of a D/L value of ~ 0.02 , i.e., medium

to large faults in the dataset are most likely to have a displacement that is $\sim 2\%$ of fault length.

586 More small faults in the dataset were over-displaced compared to medium and large faults;

small faults have a $\sim 15\%$ probability of a D/L value of ~ 0.035 , i.e., small faults in this dataset

are most likely to have a displacement that is $\sim 3.5\%$ of fault length (Figure 3). The shape of

the distribution of small faults is relatively long-tailed, meaning that there are more small

590 faults with a higher D/L value than medium or large faults.

591

592 **5.2. Maturity**

1959 active faults from 27 sources were included, ranging in size from 0.3 m to 345 km in
length, with data from areas such as Crete, the Apennines, Italy, and the Turkana Rift, Kenya
(Figures 4-5). A total of 2059 inactive faults were included from 38 sources, ranging in size
from 0.01 m to 123.4 km in length, with data from areas such as the Exmouth Plateau,

offshore NW Australia, Horda Platform, offshore Norway, and the Levant Basin, offshore

598 Lebanon (Figures 4 and 5).

599 The active faults have a power-law trendline of $Dmax=0.03L^{0.90\pm0.01}$, which requires

600 $n=0.90\pm0.02$ and c=0.03, whereas inactive faults have a trendline of $Dmax=0.05L^{0.93\pm0.01}$,

- 601 which requires $n=0.93\pm0.01$ and c=0.05 (Table 1). The confidence values of *n* for inactive 602 and active faults overlap (Table 1). Inactive faults have a higher displacement/length ratio
- than active faults (Figure 4B and 6).

According to the probability density plot (Figure 6), there is a ~37% probability of active

- faults having a D/L value of ~ 0.025 , i.e., active faults are most likely to have a displacement
- that is 2.5% of length. Inactive faults have two probability peaks; there is $\sim 12\%$ probability
- of a D/L value of 0.025 and $\sim 11\%$ probability of a D/L value of 0.05, i.e., inactive faults are
- most like to have a displacement that is $\sim 2.5\%$ or $\sim 5\%$ of length. The density plot of inactive
- faults has a longer tail, which means that higher D/L values are more probable in inactive
- 610 faults than active faults.
- 611

612 5.3. Tectonic history

613 1620 reactivated faults from eight sources were included, ranging in size from 17 m to 123

- 614 km in length, with data from areas such as the Porcupine Basin, offshore Ireland and the
- North Malay Basin, Thailand (Figures 7 and 8). 265 faults with no pre-existing structures
- 616 were taken from 15 sources from areas such as Canyonlands, Utah, USA and the East Pacific
- 617 Rise (Figures 7 and 8). Faults range in size from 0.2 m to 54 km. The reactivated faults have
- 618 a power-law trendline of $Dmax=0.03L^{0.92\pm0.01}$, $n=0.96\pm0.1$ and c=0.03, and the non-
- for reactivated faults have a power-law trendline of $Dmax=0.04L^{0.87\pm0.05}$, $n=0.87\pm0.05$ and
- 620 c=0.04 (Table 1). Reactivated faults have a higher D/L ratio on average than faults not
- 621 forming in the presence of a pre-existing structure or structures (Figure 7B). This is unusual,
- 622 given several authors have suggested that reactivated faults tend to be under-displaced
- 623 (Walsh et al., 2002; Vétel et al., 2005). We discuss the possible reasons for this in sub-section624 6.3.
- 625 In probability density plots (Figure 9), reactivated faults and faults with no pre-existing
- 626 structures plot similarly; for reactivated faults and faults with no pre-existing structures, there
- 627 is a \sim 27% and \sim 24% probability, respectively, of a D/L value of \sim 0.025, i.e., both reactivated
- faults and faults with no pre-existing structures in this dataset are most likely to have a
- displacement that is $\sim 2.5\%$ of length. The distribution of reactivated faults has a slightly
- 630 longer tail, which means that there is a slightly higher probability of reactivated faults having
- 631 a higher D/L value.

633 **5.4.** Lithology

- A power-law trendline was calculated for each lithology sub-category, with *n* values ranging
- from 0.007 to 1.1 and c values from 0.79 to 1 (Table 1). The confidence intervals for n of
- faults in fine-grained carbonate, fine-grained clastic, mixed carbonate/clastic, and
- 637 sedimentary with igneous rocks overlap and other host rocks do not (Table 1). Faults with
- 638 clastic sedimentary and fine-grained clastic sedimentary host rocks tend to have a higher D/L
- ratio (i.e., they are over-displaced) compared to the other lithologies (Figures 10 and 11).
- 640 Faults with igneous host rocks tend to have a lower D/L ratio compared to the other
- 641 lithologies (Figures 10 and 11).
- 642 According to density plots (Figure 12), clastic sedimentary rocks have the highest probability
- 643 of high D/L values compared to the other lithologies, i.e., there is a $\sim 13\%$ probability of a
- fault in a clastic host rock having a D/L value of ~ 0.09 , i.e., faults with clastic sedimentary
- host rocks in this dataset are most likely to have a displacement that is $\sim 9\%$ of the fault
- length. Faults with igneous and clastic with igneous host rocks have a higher probability of
- 647 low D/L values than other lithologies; for igneous and clastic with igneouds host rocks, there
- is a \sim 32% and \sim 35% probability respectively of a D/L value of \sim 0.01, i.e., faults with igneous
- or igneous/clastic host rocks are most likely to have a displacement that is $\sim 1\%$ of length.

650 5.5. D/L through time

- 651 37 faults from six different sources were included in a dynamic D-L through time dataset
- (Figure 13). 24 natural faults imaged in 3D seismic reflection data were included, with these
- faults being 1.9-42 km long. Six faults generated in physical analogue models and three from
- numerical models were also included. The D/L trajectories of these faults are shown against
- the global D/L database (Figure 13A) and in normalised D vs. time and L vs. time plots
- 656 (Figure 13B).
- 657 There is a wide range of displacement trajectories in the studied faults. For example, in the
- 658 first 25% of the faults' lives, some faults had only accumulated only 6% of their (eventual)
- total displacement, whereas others had reached up to 75% of their final maximum
- displacement (Figure 13B). On average, faults accumulate displacement at a constant rate,
- although on a fault-to-fault basis there is more variability (Figure 13B). 26 of the 37 (70%)
- faults attain >75% of their maximum length within the first 25% of their lives, and 35 of 37
- 663 (95%) faults reach their lengths within the first half of their lives (Figure 13B). Faults then
- either maintain their maximum length or decrease in active trace length until they become

665 inactive. On average, faults reach their maximum length within the first 30% of their lives

- and then decrease in length by 5-10%. 23 of the 37 (62%) faults experience late-stage lateral
- tip retreat, where their tips become inactive in the later stages of the faults' lives.
- 668

669 6. Discussion

670 We here summarise some key observations regarding the relationship between normal fault D

and L, and fault size, activity, tectonic history, and lithology, and then use specific, well-

672 constrained case studies to indicate how the various parameters control fault growth and

associated scaling relationships. We then discuss D/L changes through time, fault growth

models, and the processes that control the upper limits of the D/L scaling relationship.

675

676 **6.1. Size**

677 There is little consensus in the literature on how fault size affects the relationship between D

and L. Schlische et al. (1996) found no relationship between fault size and D/L ratio. In

679 contrast, Cowie & Scholz (1992a) found that very large faults (>1 km) were over-displaced

680 compared to smaller faults. Torabi & Berg (2011) showed that small faults (<1 m

displacement) and large faults (>1 km displacement) have a higher displacement/length ratio

than medium faults (between 1 m and 1 km), suggesting both small and large faults are over-

displaced. They explained that the low D/L ratio of medium-sized faults is likely due to faults

of this size being in the process of overlapping, interacting, and linking, i.e., they will

eventually become larger and accrue more displacement (Torabi & Berg, 2011). However,

the low D/L ratio of these faults could be due to sampling biases, i.e., there is a scarcity of

687 published medium-sized faults included in their database.

688 Our results show that large and medium-sized faults have similar displacement/length ratios,

but that small faults (<1 m) tend to be relatively over-displaced (Figure 3). Assuming a

690 constant-length growth model (e.g., Walsh et al., 2002; Jackson et al, 2017; Rotevatn et al.,

691 2019), faults reach their maximum length quickly and then accumulate displacement.

692 Medium and large faults are active for a longer period, and under a constant-length model

they are likely to have reached their maximum length and to be in some stage of displacement

694 accrual and thus be under-displaced. Under-displaced medium-to-large faults could either be

still active and in the displacement accrual stage or they could have become inactive before

they reached their maximum displacement potential (e.g., due to kinematic interactions

between faults, strain partitioning onto more optimally positioned faults). Small faults are

- 698 active for a shorter period, so faults can lengthen and accumulate a relatively high amount of
- displacement and are less likely to become inactive before reaching their maximum possible
- 700 displacement.

701 Duration of faulting may also explain scatter in the global D/L plot, i.e., the displacement on

⁷⁰² large faults, which presumably have been active for longer than small faults, span up to four

orders of magnitude, whereas small faults only span 1-1.5 orders of magnitude (Figure 2).

Scatter for large faults represents faults that have become inactive prematurely, and the lack

of scatter for small faults may represent fault growth stages not detectable using, for example,

- seismic reflection data (e.g., Jackson et al., 2017; Rotevatn et al., 2019).
- 707

708 **6.2. Maturity**

Fault length and displacement accumulation tend to be strongly partitioned in time (Figure
13B) (e.g., Walsh et al., 2002; Tvedt et al., 2016; Rotevatn et al., 2019). Thus, if the

711 maximum displacement had (in the case of an inactive fault) or has (in the case of a still-

active fault) been measured part-way through a fault's life rather than at the end, it would plot

as under-displaced, assuming a constant-length growth model. When estimating fault scaling,

it is important to keep in mind if the faults are active, and if so, how mature they are.

However, there is still a huge amount of scatter among both active and inactive faults;

inactive faults trend over-displaced compared to active faults (Figures 4 and 6), however the

scaling laws between inactive and active faults have *n* values with overlapping confidence

intervals (Table 1). Faults can become inactive at any point in their maturity, for example

719 dying pre-maturely with relatively low displacement, which could also add additional scatter.

720 We would expect that active faults tend to be younger and have been active for less time

compared to inactive faults; they therefore could be comparatively under-displaced. This

aligns with our understanding of fault growth under a "constant length" or "hybrid growth"

723 model (Walsh et al., 2002, 2003; Nicol et al., 2005, 2017; Jackson & Rotevatn, 2013; Henstra

724 et al., 2015; Fossen & Rotevatn, 2016; Hemelsdaël & Ford, 2016; Tvedt et al., 2016; Childs

et al., 2017b). Under a constant-length or hybrid growth model, faults reach their maximum

length in the first 20-30% (or less) of their life. Active faults could be generally under-

727 displaced because they have reached their maximum length but are still accruing

displacement, however the relationship is not clear (Table 1).

- 729 One example from the database of under-displaced, immature normal faults come from the
- 730 Taupo Rift on the central North Island of New Zealand (Nicol et al., 2010; Figure 14). Rifting
- began 1-2 Ma, with the studied faults having been active for 60 kyr and 300 kyr. The area is
- tectonically active, and the faults accommodate 15 mm/yr of extension. The older faults,
- which have been active for 300 kyr, are 2.3 km to 70.7 km long and have displacements
- ranging between 20.7 m and 2198 m. D_{max}/L is between 0.002- 0.06 (average 0.017) (Nicol et
- al., 2010; Figure 14). In contrast, the younger faults, which have been active for only 60 kyr,
- are 487 m to 28.7 km long, have displacements ranging between 1 m and 97.9 m, and a
- 737 D_{max}/L between 0.0009-0.01 (average 0.004) (Nicol et al., 2010; Figure 14). It is often
- difficult to deduce whether a fault is under-displaced due to fault maturity or lithology (see
- section 3); however, in the Taupo Rift case, given that these faults formed in the same host
- rock, it is likely these still-active faults are under-displaced solely due to fault maturity.
- 741 The Taupo Rift faults are under-displaced compared to a set of inactive faults of similar
- r42 length from the Exmouth Plateau, offshore NW Australia (Pan et al., 2021). Faults on the
- Exmouth Plateau were active from the Early Jurassic-Early Cretaceous (85.5 kyr), are 307 m
- to 181.2 km long, and have displacements ranging between 18.2 m and 857.6 m (Pan et al.,
- 2021). Dmax/L is between 0.006-0.5 (average of 0.06). These faults grew in accordance with
- and support the constant-length model, reaching their final length in less than 7.2 myr (8% of
- their total lifespan) before accruing significant displacement (Pan et al., 2021).
- 748

749 **6.3.** Tectonic history

- Faults that formed in response to the reactivation of a pre-existing structure tend to be slightly over-displaced compared to faults in areas that have no reported pre-existing faulting (Figure 7B and 9). Previous studies indicate reactivated faults tend to have a higher displacement to length ratio because the maximum length of the fault is generally established in the first phase of faulting (Vétel et al., 2005; Baudon & Cartwright, 2008). However, we believe that role the reactivation of older structures and thus pre-extensional tectonic history plays in controlling D/L ratios is strongly dependent on how long the fault has been active during its
- most recent deformation, since newly formed faults will tend to be under-displaced,
- according to both the constant-length and hybrid fault growth models (Rotevatn et al., 2019).
- 759 One example of reactivated normal faults is from the tectonically active Turkana Rift,
- 760 Northern Kenya (Vétel et al., 2005; Figure 15 in pink). Faults here range from 208 m-29.5
- km long, have displacements ranging from 82.5 m to 101 m, and have been active for <3 Myr

762 (Vétel et al., 2005). Faults are thought to have reactivated Proterozoic basement faults, or 763 possibly utilised basement metamorphic foliation, and the area currently extends with a strain 764 rate of $\sim 0.1 \text{ mm/yr}$ (Vétel et al., 2005). Fault arrays were able to reach relatively long lengths 765 $(\sim 40 \text{ km})$ in a relatively short period of time, despite these relatively low strain rates, likely 766 due to them exploiting and activating pre-existing weaknesses (Vétel et al., 2005). The 767 average D/L ratio is 0.007, (displacement is 0.7% of length). These faults are thus under-768 displaced, which is likely due to them having lengthened rapidly by exploiting intra-basement 769 weaknesses; these faults are thus likely still at the beginning of their displacement 770 accumulation stage.

771 An example of more mature, but still-active reactivated faults come from the Mergui Basin, 772 Thailand (Morley, 2017; Figure 15, in green), which unlike the Turkana Rift faults (Vétel et 773 al., 2005) are relatively over-displaced. The area has a complicated tectonic history: the 774 Mergui basin experienced Triassic-Early Jurassic and Early Cenozoic transtension, with the 775 related strike-slip faults later reactivated as normal faults (Morley, 2017). These faults have 776 been active since the Early Eocene to Late Miocene, are 20.9-123 km long, and have 458 m-21.8 km displacement (Morley, 2017). They are over-displaced, with a D/L average of 0.14 777 778 (displacement is 14% of length), with D/L ratios as high as 0.26. These faults are over-779 displaced because they were able to establish their maximum length quickly by exploiting 780 and reactivating pre-existing weaknesses inherited from previous faulting, and then 781 accommodate strain by accruing displacement. These faults are still-active, but are very 782 mature (i.e., they have been active since the Early Eocene); as a result, they have been able to 783 attain high D/L ratios.

In summary, reactivated faults are, on average, over-displaced (Figures 7 and 9), and this

should be considered when using D/L scaling laws to estimate faults length or displacement.

786 However, we hypothesise that relatively young reactivated, still-active faults, such as the

ones in the Turkana Rift (Vétel et al., 2005), could be under-displaced as they have reached

maximum length quickly but are still accruing displacement. When assessing reactivated

faults, it is important to consider how long the faults have been active.

790

791 **6.4.** Lithology

Host rock lithology can influence the relationship between fault length and displacement dueto the stiffness of different lithologies, often described by host rock shear modulus (Walsh et

al., 1988, 1989; Cowie & Scholz, 1992a; Wibberley et al., 1999). In previous studies an

inverse relationship between host rock shear modulus and D/L has been reported; faults in

host rocks with a high shear modulus (stiffer rocks, for example, a granite) are under-

displaced compared faults with a high shear modulus (softer rocks, for example, a mudstone)

798 (Walsh et al., 1988, 1989; Cowie & Scholz, 1992a; Wibberley et al., 1999; Gudmundsson,

799 2004; Childs et al., 2017a).

800 The stiffness of rocks relates to their elastic properties, also expressed by the Young's

Modulus and the Poisson ratio (Roche et al., 2013). Fault length and displacement have been

related to rock stiffness in the following equation from crack models:

803

 $\frac{L}{Dmax} = \frac{E}{2\Delta\tau(1+v)}$

804 805

806 Where E is Young's Modulus, v is Poisson's ratio, and $\Delta \tau$ is the shear stress driving the fault 807 (Roche et al., 2014). Poisson ratio can fall between 0.05 and 0.4, although values usually 808 range between 0.3 and 0.4 (Gereck, 2007). There is generally little variation in Poisson's ratio between different lithologies, compared to Young's Modulus (Gudmundsson, 2004). Young's 809 810 Modulus has a high amount of variation, ranging between 0.05 GPa and 100 GPa (Roche et 811 al., 2013). Fault displacement is inversely proportional to the Young's modulus of the rock 812 (Wibberly et al., 1999, 2000a; Gudmundsson, 2004) which suggests that stiffer rocks, such as 813 igneous and metamorphic rocks, are more likely to be under-displaced than pyroclastic or 814 sedimentary rocks. Factors such as increasing temperature, increasing porosity, and water 815 content can decrease Young's Modulus. Highly fractured rocks have a low Young's 816 Modulus; the breccia of a faults core has a low Young's Modulus, like that of a weak clay or 817 pyroclastic tuff (Gudmundsson, 2004). 818 The data compilation presented in this paper appears to reveal a relationship between the D/L

The data complication presented in this paper appears to revear a relationship between the D/1

ratio of normal faults and host rock lithology, with faults with a low Young's Modulus

tending to have a higher D/L ratio (i.e., they are over-displaced) (Figure 16). Evaporite-

- bearing sedimentary host rocks tend to be over-displaced compared to other lithologies,
- which could be due to the softness of the rocks making tip propagation difficult. Both
- 823 evaporites and sedimentary rocks have a relatively low Young's Modulus, with sedimentary
- rocks ranging between 0.04-67 GPa (24 GPa average; Figure 16) and evaporites ranging

between 4-64 GPa (23 GPa average; Figure 16). Faults within either fine- and coarse-grained

826 clastic host rocks, are also relatively over-displaced, with Young's Modulus estimated

between 0.04-36 GPa (14 GPa average; Figure 16) for fine-grained clastic sedimentary rocks,

and 6-67 (25 GPa average) for sandstones and conglomerates (Figure 16). Faults in

829 carbonates and mixed clastic/carbonates tend to lie in the middle of the various D/L

trendlines, with carbonates having an estimated Young's Modulus between 24-66 GPa (45

GPa average; Figure 16). Faults within igneous host rocks are significantly under-displaced

(Figure 10B), which is possibly in part due to the stiffness of igneous rocks; igneous rocks

have the highest estimated Young's Modulus, between 5-99 GPa (49 GPa average; Figure

834 16).

835 One example of under-displaced faults in host rocks with a high Young's Modulus are in the 836 East African Rift (Figure 17; Williams et al., 2021). Here, normal faults are forming in a 837 metamorphic host rock. Fault ages are not well constrained, but they are estimated to be 838 roughly Pliocene in age and they are demonstrably still active (Scholz et al., 2020). Faults are 839 13 km to 130 km long and have displacements ranging from 122 m to 2.5 km. Dmax/L is very low, between 0.003-0.03 (average of 0.01), indicating the faults are relatively under-840 841 displaced (Williams et al., 2021). It should be noted that these faults are active, which as 842 discussed in section 2 could result in them being under-displaced. Additionally, some of the 843 faults in the East African Rift have reacted foliation, making it ambiguous as to whether these 844 faults being under-displaced are related to Young's Modulus, fault maturity, reactivation, or a 845 combination.

846 Another example of under-displaced normal faults within stiff host rocks come from an

847 active rift zone in Iceland (Figure 17; Gudmundsson, 2004). The faults here are Holocene

848 (<10,000 years old) and cut through basaltic pahoehoe lava flows with an estimated Young's

Modulus of 30-60 GPa, and possibly as high as 100 GPa. Faults range from 345 m to 9 km

long and have displacements ranging from 1.3 m to 33 m. Dmax/L is between 0.0009-0.01

851 (average of 0.004), meaning the faults are under-displaced (Gudmundsson, 2004). We expect

the stiff host rock lithology has contributed to these faults being under-displaced; however,

these are active faults, so according to a constant-length fault growth model, they have

854 possibly reached their maximum length, but not yet their maximum displacement.

Differences in mechanical stratigraphy between lithological units can create vertical barriers
that inhibit fault growth, which can cause faults to be under-displaced (Peacock & Sanderson,

857 1992; Wilkins & Gross, 2002; Welch et al., 2009; Roche et al., 2014). There is a relationship 858 between rock stiffness and fault displacement gradient (i.e., the displacement variation per 859 unit length across a fault), with these gradients tending to be higher in rock units with lower 860 Young's Modulus (Roche et al., 2014). Mechanical stratigraphy can restrict faults from 861 propagating vertically, causing faults to have a high aspect ratio (fault height/length; height is 862 the fault dimension along dip) (Nicol et al., 1996; Schultz & Fossen, 2002; Soliva et al., 863 2006; Roche et al., 2013; Alghuraybi et al., 2021). In a numerical modelling analogue study 864 by Roche et al. (2013), aspect ratios for faults in homogeneous rock properties not bounded 865 by mechanical stratigraphy are typically >2, whereas aspect ratios of faults in limestone-clay 866 sequences are, on average, 13, and even as high as 50 (Roche et al., 2013). However, no 867 aspect ratios >20 have been reported in natural studies (Torabi et al., 2019). If faults have a 868 high aspect (height-length) ratio, it stands that they would likely also have a high 869 displacement-length ratio. However, this is likely only applicable to relatively small faults, or possibly large faults cutting through thick layers (e.g., a fault with 1 m of displacement 870 offsetting a 20 cm-thick mudstone package, vs. a 1 km displacement fault offsetting a 100 m-871 thick mudstone package). 872

873 One example of under-displaced faults with high aspect ratios included in our database are

layer-bound, thin-skinned normal faults from the NW Barents Sea (Figure 17; Alghuraybi et

al., 2021). The faults in this study were only active in the Late Jurassic and they occur in a

fine-grained clastic host rock. Faults are 4.7 km to 42.7 km long, have displacements ranging

from 21 m to 103 m, and their D_{max}/L is between 0.001-0.009 (average of 0.003). They have

aspect ratios as high as 19, compatible with aspect ratios found in the numerical models of

879 Roche et al. (2013). The faults from the NW Barents Sea are interpreted to have reached their

final length quickly (i.e., they grew in accordance with the constant-length model) and were

not able to reach their likely maximum displacement, likely due to the mechanical layering.

882 In summary, host rock lithology influences D/L ratios; softer rocks (such as sedimentary

rocks) tend to be over-displaced, and stiffer rocks (such as igneous rocks) tend to be under-

displaced, which agrees with the initial hypothesis from previous literature (Wibberly et al.,

885 1999, 2000a; Gudmundsson, 2004). Mechanical stratigraphy also causes rocks to be

vertically restricted and causes them to be under-displaced.

887

888 6.5. How useful are D/L scaling laws?

- 889 Our overall scaling relationship between normal fault length and maximum displacement for
- all data in our revised database is $D=0.03L^{0.92\pm0.01}$. This agrees with previous literature that
- estimated *n*=1 (Cowie & Scholz, 1992a; Dawers et al., 1993; Scholz et al., 1993; Clark &
- 892 Cox, 1996; Schlische et al., 1996; Kim & Sanderson, 2005; Xu et al., 2006). Our database has
- thousands of faults that span eight orders of magnitude in terms of fault length, thus we
- believe that we can confidently say that, overall, n=1, and that our equation could be used to
- reliably estimate D or L within 1-2 orders of magnitude in most cases.
- 896 There is so much variability in our plots ($r^2=0.85$) when all D/L data is considered that it
- could be questioned whether a single global scaling law should be used at all. Even after
- conducting a detailed quality check of the data and removing data for which we believe there
- are errors/inconsistencies, there is still significant variation in the D/L scaling relationship for
- normal faults. As we discuss above, we suggest that some of these differences may be related
- to properties such as lithology, fault maturity and reactivation. The scaling relationships for
- data within each of these categories are different, however in some cases overlap within the
- confidence intervals. This may be related to the fact that feedbacks between the properties
- 904 considered in this study likely exist and more analysis is needed to establish which are the
- 805 key properties which most control D/L. Despite this, we believe that there *is* value in being
- able to estimate D from L, and that more specialised scaling relationships like those provided
- 907 here considering fault size, lithology, tectonic history, and fault maturity are thus warranted.
- 908 For example, using our global scaling law $(Dmax=0.03L^{0.92})$, we would estimate that a 3 km
- 909 long normal fault within a sandstone host rock in a tectonically active area would have a
- 910 displacement of c. 47 m. In contrast, if we use the 'clastic sedimentary' D/L equation
- 911 ($Dmax=0.11L^{0.84}$), we would estimate a displacement of c. 277 m; by using the 'inactive' D/L
- equation $(Dmax=0.05L^{0.93})$ we would estimate a displacement of c. 126 m. Both values are
- 913 likely more accurate than the global estimate, which may have implications for situations
- 914 which requite estimating fault displacement or length, such as understanding fault sealing,
- $possible CO_2$ leakage in a potential CCS locality, how large an earthquake might be. For the
- 916 most accurate estimates, we would suggest either 1) calculating an average of the applicable
- equations, in this example, an average between the value for a 'clastic sedimentary' and
- 918 'inactive', or to have an even more accurate estimation, 2) use our database to combine faults
- 919 with similar factors to make a bespoke equation for that area.

920 The relationship between fault D and L is also dynamic, changing throughout a fault's life. 921 Additionally, faults are typically not isolated structures. Some faults in a network become 922 inactive early due to being sub-optimally located (i.e., pinned tips, interacting with an 923 adjacent fault with opposing dips, fault rotation) and strain is partitioned onto larger and 924 longer lasting faults. It is important to practice caution when working with D/L ratios. As 925 shown in Figure 13, the relationship between D and L evolves through time, thus using static 926 data to infer a dynamic relationship can be problematic. Plotting data only in log-log space 927 can hide variability and statistical spread, as shown by Rotevatn et al. (2019). For example, 928 different stages of fault growth will likely be masked in a large log-log plot, as the fault lies 929 within the global scatter at every stage of fault growth. This shows that fault growth cannot 930 be inferred from global D/L plots, and that plotting D and L through time (Figure 13) is 931 important to understanding fault growth.

932

933 6.6. Upper bounds of displacement

934 In contrast to the lower limits of the D/L scaling dataset, which shows significant scatter 935 likely reflecting the process of fault growth, there appears to be an upper limit of maximum 936 displacement (Figure 18). The absolute upper bound is the upper limit of Dmax/L=0.5 (i.e., at 937 max, faults displacement can be $\frac{1}{2}$ of length), however very few faults have a D/L value that 938 high, i.e., 99.7% of the data falls below D/L = 0.3, and 94% of the data falls below D/L = 0.1. 939 We argue that the D/L upper-limit seen in our global dataset may be related to an overarching 940 rule of fault mechanics in which faults cannot accommodate a certain amount of 941 displacement without additional propagation or linkage with another fault. The wall-rock that 942 borders the fault tips can accommodate a finite amount of shear stress, and beyond that the 943 rock will fail, resulting in additional fault tip propagation (Freeman et al., 2010). Upper D/L 944 limits could also be due to isostatic restoring forces due to the topography generated in the 945 hanging wall and footwall blocks of the fault (Cowie & Scholz, 1992a).

946

947 **7. Conclusions**

948 We here present a new normal fault database that presents fault length and displacement

along with host rock lithology, fault maturity, and tectonic history that will now be available

950 to the public. In our interrogation of the new global normal fault database of 4046 faults, we

found that 1) for the complete dataset n=0.92 in terms of the standard equation $Dmax=cL^n$,

but there is a lot of scatter in D/L in the global dataset when faults of all lithologies,

maturities, and tectonic histories are grouped together, 2) small faults (> 1m) tend to be over-

displaced, 3) stiffer rocks tend to be under-displaced, and softer rocks tend to be over-

displaced, 4) active faults tend to be over-displaced compared to inactive faults, and 5)

956 reactivated faults are over-displaced compared to faults in previously undeformed settings,

unless the reactivated faults are still active. We also collected normal fault D/L through time

958 data and found that faults grow via a constant length-to-hybrid fault growth model. Since D/L

ratios are changing throughout a fault's life, it is important to express caution when looking atstatic D/L data.

961

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968 for their feedback provided during Bailey Lathrop's PhD viva. We also thank the Imperial

969 College Basins Research Group (BRG) for their feedback and help throughout this research.

970

971 Data availability statement

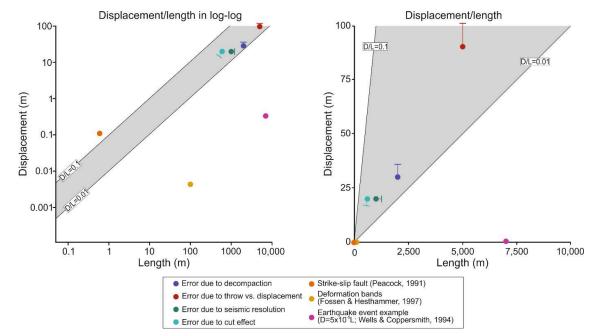
972 The databases compiled for this paper are available open-access via Figshare

973 (https://doi.org/10.6084/m9.figshare.17087273). All sources used in these databases are cited

974 within. Young's Modulus values for the different lithologies analysed were also compiled

- 975 and can be accessed via Figshare (<u>https://doi.org/10.6084/m9.figshare.17087342.v1</u>).
- 976
- 977
- 978
- 979
- 980





984 Figure 1. Schematic showing how errors in measurement and data from structures other than

985 normal faults that can affect D/L scaling in log-log and linear space. Dots signify observed

values and one-sided error bars delineate where the observed value should be.

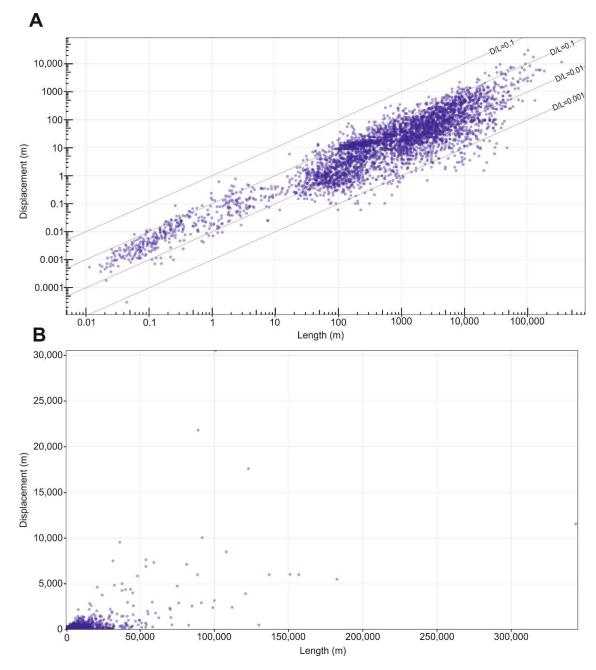


Figure 2. Plots showing fault length vs displacement for all data in our database. A) Data in
log-log space. B) Data in linear space.

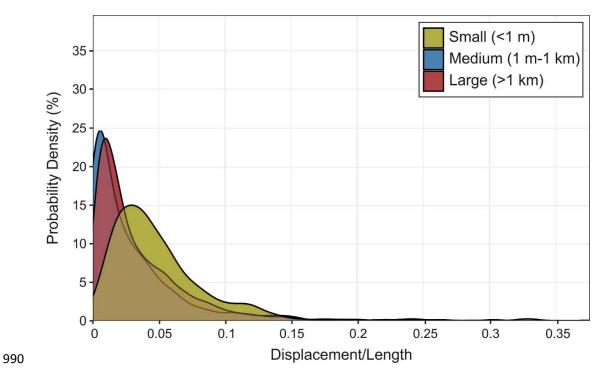


Figure 3. Density estimates of the D/L value of small, medium, and large faults in our
dataset. Peaks in the density plot are at the D/L values with the highest probability.

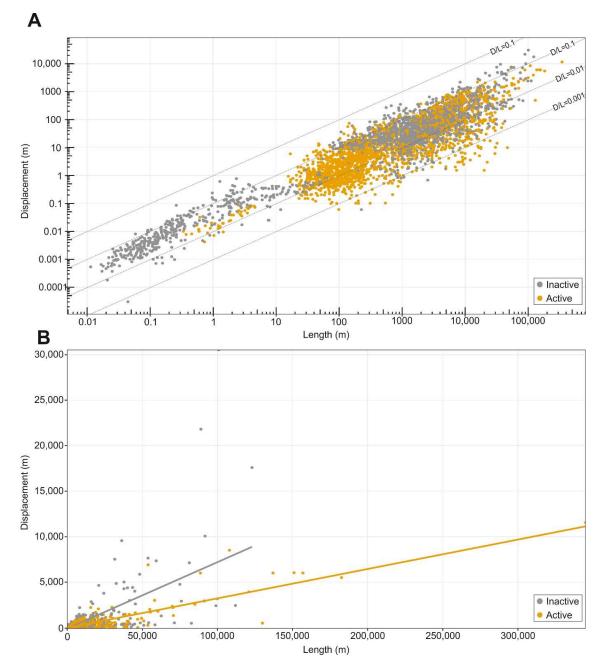


Figure 4. Plots showing fault length vs displacement for active and inactive normal faults inour database. A) Data in log-log space. B) Data in linear space.

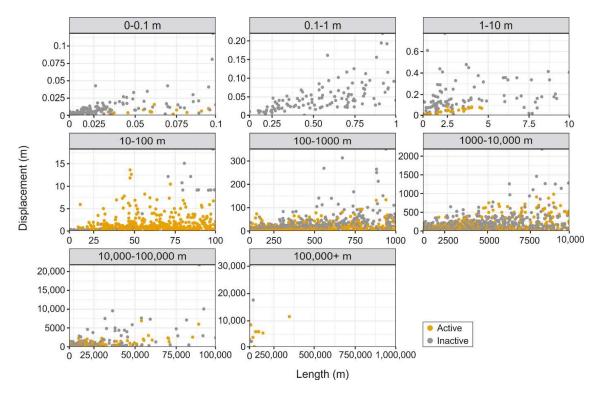


Figure 5. Plots showing active and inactive normal fault D/L data, separated by order ofmagnitude.

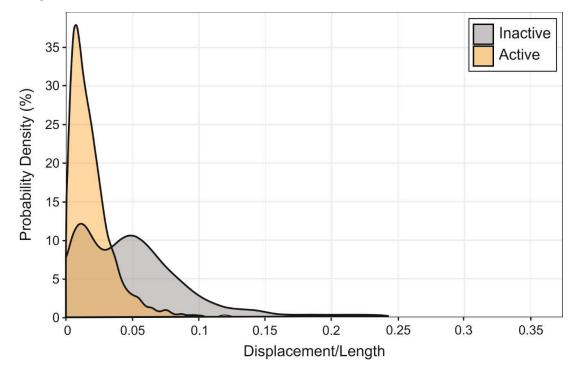


Figure 6. Density estimates of the D/L value of active and inactive faults in our dataset.
Peaks in the density plot are at the D/L values with the highest probability.

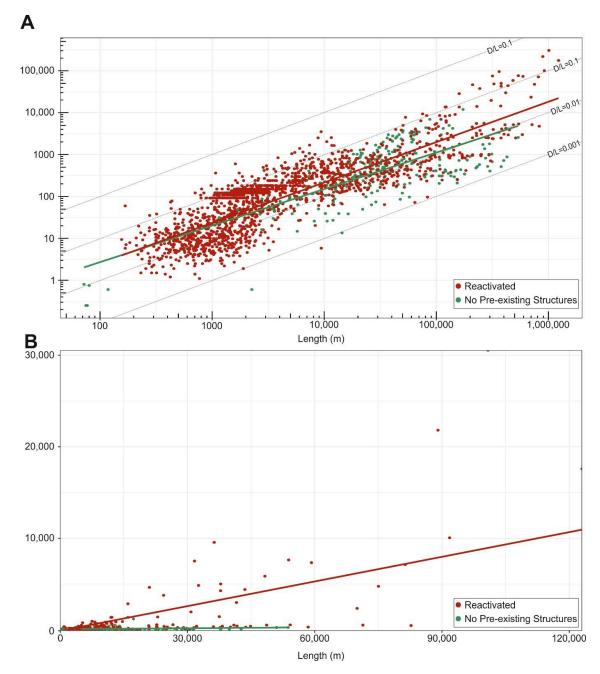


Figure 7. Plots showing fault length vs displacement for reactivated and non-reactivatednormal faults in our database. A) Data in log-log space. B) Data in linear space.

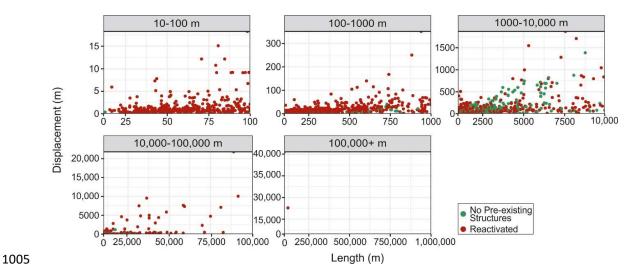


Figure 8. Plots showing normal fault D/L data from reactivated faults and faults with no pre-existing structures, separated by order of magnitude

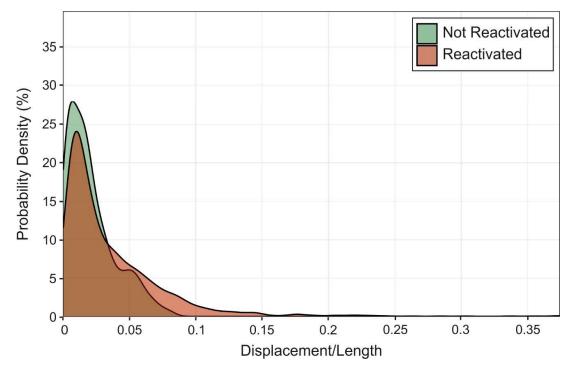


Figure 9. Density estimates of the D/L value of faults that have and have not been reactivatedin our dataset. Peaks in the density plot are at the D/L values with the highest probability.

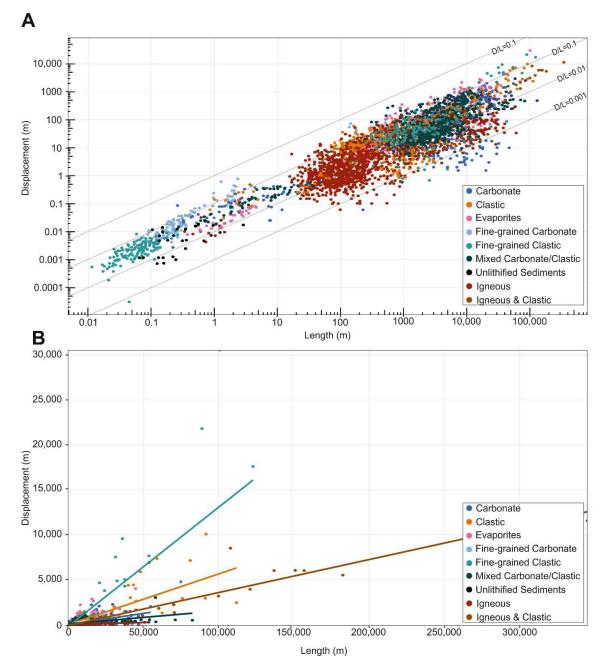


Figure 10. Plots showing fault length vs displacement for normal faults with host rocks of
different lithologies included in our dataset, including carbonate, clastic, evaporites, finegrained carbonate, fine-grained clastic, mixed carbonate/clastic, unlithified sediments,

1015 igneous, and igneous/clastic. A) Data in log-log space. B) Data not in linear space.

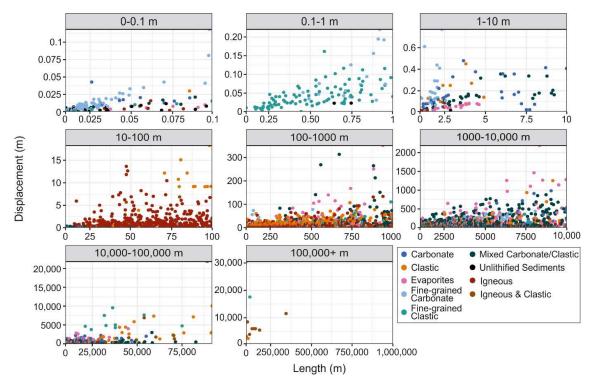


Figure 11. Plots showing normal fault D/L data for normal faults with host rocks of different
lithologies included in our dataset, including carbonate, clastic, evaporites, fine-grained
carbonate, fine-grained clastic, mixed carbonate/clastic, unlithified sediments, igneous, and
igneous/clastic, separated by order of magnitude.

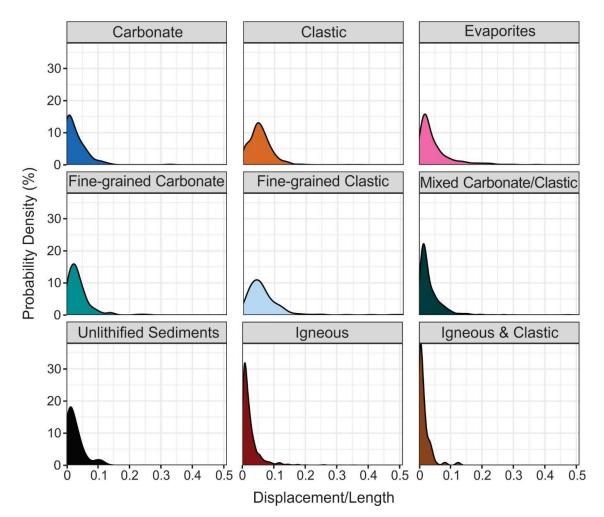


Figure 12. Density estimates of the D/L value of faults with host rocks of different

1023 lithologies included in our dataset, including carbonate, clastic, evaporites, fine-grained

1024 carbonate, fine-grained clastic, mixed carbonate/clastic, unlithified sediments, igneous, and

1025 igneous/clastic. Peaks in the density plot are at the D/L values with the highest probability.

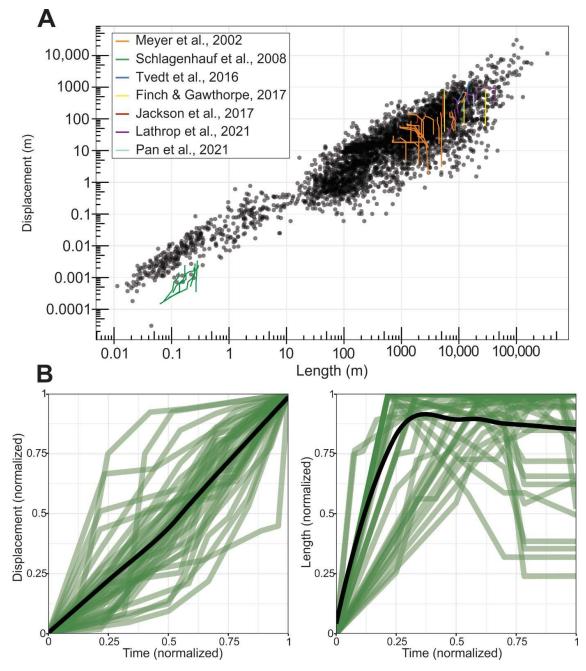


Figure 13. Figures showing fault growth through time (with data extracted from Meyer et al., 2002; Schlagenhauf et al., 2008; Tvedt et al., 2016; Finch & Gawthorpe, 2017; Jackson et al., 2017; Lathrop et al., 2021; Pan et al., 2021). A) Global D/L dataset (black) for normal faults in log-log space with D/L through time data in colour above it. B) Displacement and length through time, normalised in green, average values in black.

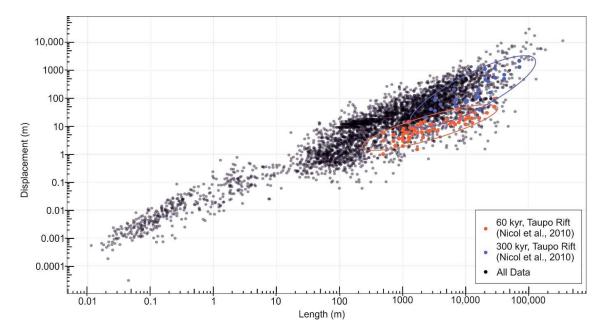




Figure 14. Global D/L dataset (black) for normal faults in log-log space with faults of
different maturities highlighted: 60 kyr faults from the Taupo Rift in orange and 300 kyr
faults from the Taupo Rift in purple (from Nicol et al., 2010).

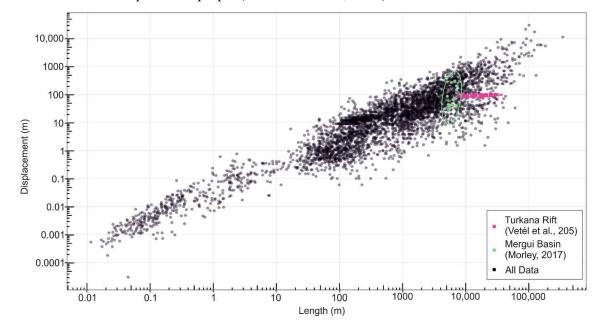
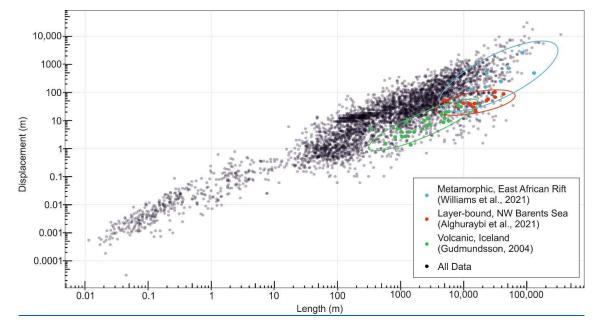


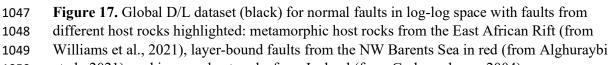
Figure 15. Global D/L dataset (black) for normal faults in log-log space with reactivated
faults highlighted: faults from the Turkana Rift in pink (from Vétel et al., 2005) and the
Mergui Basin in green (from Morley, 2017).

	Lithology	Young's Modulus (average)	Young's Modulus (range)	Average D/L ratio
ine	Sedimentary w/ Evaporites	4-64 GPa (Evaporites)	23 GPa (Evaporites)	0.05
trendline		0.04-67 GPa (Sedimentary)	24 GPa (Sedimentary)	
	Fine-grained Clastic Sedimentary	0.04-36 GPa	14 GPa	0.04
ratio	Clastic Sedimentary	6-67 GPa	25 GPa	0.06
	Igneous w/ Clastic Sedimentary	5-99 GPa (Igneous)	49 GPa (Igneous)	0.15
D/L		6-67 GPa (Clastic Sedimentary)	25 GPa (Clastic Sedimenta	ry)
bu	Carbonate	24-66 GPa	45 GPa	0.03
asi	Mixed Clastic & Carbonate	24-66 GPa (Carbonate)	45 GPa (Carbonate)	0.04
Decreasing		6-67 GPa (Clastic Sedimentary)	25 GPa (Clastic Sedimenta	ry)
De	Metamorphic	15.9-109 GPa	42 GPa	0.03
★	Igneous	5-99 GPa	49 GPa	0.02

- 1041 Figure 16. Figure showing how the Young's Modulus of different lithologies relates to D/L.
- 1042 The range of Young's Modulus, average Young's modulus, and average D/L for fault with
- 1043 host rocks of each lithology is shown. Generally, as Young's Modulus increases, D/L
- 1044 decreases. Our Young's Modulus data and sources can be accessed here:
- 1045 <u>https://figshare.com/articles/dataset/Young_s_Modulus/17087342</u>



1046



et al., 2021), and igneous host rocks from Iceland (from Gudmundsson, 2004).

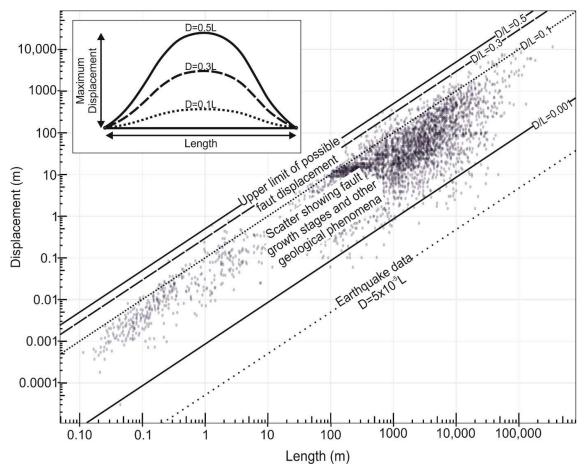


Figure 18. Global D/L dataset for normal faults with our suggested upper limit of D/L

1053 (D/L=0.1). The average D/L value of a single earthquake is also shown (Wells &

1054 Coppersmith, 1994).

1055

1051

1056 Table

Category	Sub-category	Number	Number of Sources	Power-law Equation	R-squared
All faults		4035	65	D _{max} =0.03L ^{0.92_0.01}	0.85
Size	Small (0-10 m)	395		D _{max} =0.04L ^{0.97_0.02}	0.81
Size	Medium (10-10,000 m)	3246	48	D _{max} =0.03L ^{0.94±0.01}	0.63
Size	Large (10,000+ m)	394	35	D _{max} =0.007L ^{1.3±0.01}	0.24
Maturity	Active	1959	27	D _{max} =0.02L ^{0.92_0.01}	0.74
Maturity	Inactive	2059	38	D _{max} =0.05L ^{0.93±0.01}	0.92
Tectonic Setting	Reactivated	1620	8	D _{max} =0.03L ^{0.96±0.01}	0.74
Tectonic Setting	Not Reactivated	265	15	D _{max} =0.04L ^{0.87±0.05}	0.56
Lithology	Clastic Sedimentary	644	13	D _{max} =0.11L ^{0.84±0.02}	0.71
Lithology	Clastic w/ Evaporites	344	12	D _{max} =0.02L ^{1.04±0.02}	0.85
Lithology	Carbonates	181	7	D _{max} =0.04L ^{0.79±0.03}	0.97
Lithology	FG Carbonates	220	2	D _{max} =0.06L ^{0.93±0.01}	0.20
Lithology	FG Clastic	324	6	D _{max} =0.03L ^{0.94±0.01}	0.95
Lithology	Mixed Carbonate & Clastic	124	14	D _{max} =0.04L ^{0.92±0.02}	0.78
Lithology	Unlithified Sand	28	1	D _{max} =0.01L ^{0.72_0.02}	0.31
Lithology	Sedimentary w/ Volcanics	130	7	D _{max} =0.007L ^{1.0±0.05}	0.77
Lithology	Volcanics	1317	8	D _{max} =0.04L ^{0.82+0.02}	0.63

Table 1. Table listing of all the results for each of the studied categories, including number of

faults, number of sources, power-law equation that can be used to estimate fault length ordisplacement, and the R-squared for that equation.

1062 Supplementary table

Database # of faults Source		Sources Used	n	С	
Walsh & Watterson, 1988	308	Beck, 1929; Reeves, 1929; Teas, 1929; Babenroth & Strahler, 1945; Brunstrom, 1963; Tschopp, 1967; Janoschek & Gotzinger, 1969; Mayuga, 1970; Bond et al., 1971; Huntoon, 1974; Cave, 1977; Shepherd & Burns, 1978; Shoemaker et al., 1978; Frost & Smart, 1979; Drozdzewski, 1980; Frost & Halliday, 1980; Nelson, 1980; Van den Bark & Thomas, 1980; Verdier et al., 1980; Muroaka & Kamata, 1983; Aitkenhead et al., 1985	2	not given	
Cowie & Scholz, 1992	210	MacMillan, 1975; Elliott, 1976; Muraoka & Kamata, 1983; Walsh & Watterson, 1987; Krantz, 1988; Opheim & Gudmusson, 1989; Peacock, 1991; Peacock & Sanderson, 1991; Villemin et al., 1995		0.006-0.17 (range)	
Schlische et al., 1996	547	MacMillan, 1975; Elliott, 1976; Muroaka & Kamata, 1983; Walsh & Watterson, 1987; Krantz, 1988; Opheim & Gudmusson, 1989; Peacock, 1991; Peacock & Sanderson, 1991; McGrath, 1992; Dawers et al., 1993; Villemin et al., 1995		0.03 (average)	
Brunstrom, 1963; Woodland & Evans, 196 1969; Wood et al., 1969; Freund, 1970; Mi Huntoon, 1974; MacMillan, 1975; Elliott, 13 Burns, 1978; Frost & Smart, 1979; Drozdz al., 1980; Van den Bark & Thomas, 1981; 1985; Villemin & Sunwoo, 1987; Opheim & 1988, Gillespie, 1991; Marret & Allmending 1992; Gillespie et al., 1993; Dawers et al., 1995; Cartwright et al., 1996; Jackson et a		Beck, 1929; Reeves, 1929; Teas, 1929; Babenroth & Strahler, 1945; Fox, 1959; Brunstrom, 1963; Woodland & Evans, 1964; Tschopp, 1967; Janoschek & Gotzinger, 1969; Wood et al., 1969; Freund, 1970; Mayuga, 1970; Bond et al., 1971; MRRG, 1973; Huntoon, 1974; MacMillan, 1975; Elliott, 1976; Cave, 1977; Ruzhich, 1977; Shepherd & Burms, 1978; Frost & Smart, 1979; Drozdzewski et al., 1980; Nelson, 1980; Verdier et al., 1980; Van den Bark & Thomas, 1981; Muroaka & Kamata, 1983; Aitkenhead et al., 1985; Villemin & Sunwoo, 1987; Opheim & Gundmundsson, 1989; Walsh & Watterson, 1988; Gillespie et al., 1993; Dawers et al., 1993; Davison, 1994; Dawers & Anders, 1995; Cartwright et al., 1996; Jackson et al., 1996; Nicol et al., 1996; Schlische et al., 1996; Rowan, 1997; Fossen & Hesthammer, 1998	1.19	not given	
Torabi et al., 2011 not given		MacMillan, 1975; Elliot, 1976; Muroaka & Kamata, 1983; Watterson, 1986; Villemin & Sunwoo, 1987; Walsh & Watterson, 1987; Krantz, 1988; Opheim & Gudmundsson, 1989; Peacock, 1991; Peacock & Sanderson, 1991; Gillespie et al., 1992; McGrath, 1992; Scholz & Cowie, 1992; Dawers et al., 1993; Gillespie et al., 1992; McGrath, 1995; Villemin et al., 1995; Nicol et al., 1996; Schilsche et al., 1996; Yielding et al., 1996; Gross et al., 1997; Wibberly et al., 1999; Kim et al., 2000; Walsh et al., 2002; Wilkins & Gross, 2002; Davis et al., 2005; Schultz et al., 2008		0.0001-1	

Supplementary Table 1. Table showing previously published global databases with the
 number of faults used and their sources, along with their values of n and C if given.

Source	Number of Faul	ts Data Type	Dominant Lithology	Reactivated	Size Range (length in m)	Active/inactive
Alghuraybi et al., 2021	18	3D seismic	Fine-grained clastic	No	4714-42,673 m	Inactive
Balsamo et al., 2016	23	Outcrop	Mixed carbonate & clastic		412-9290 m	Inactive
Blaekkan, 2016	43	Physical analogue			0.1-2 m	N/a
Bramham et al., 2021	768 Sa	atellite imagery & topo	data Igneous	Yes	16-2009 m	Active
Cartwright et al., 1995	91	Outcrop	Sedimentary & evaporites	No	280 m	Active
Corti et al., 2019	23	Outcrop	Igneous	Yes	7050-60,540 m	Active
Crider & Pollard, 1998	2	Outcrop	Igneous		1800-2200 m	Active
Dawers et al., 1993	15	Outcrop	Igneous & clastic		20-2200 m	Active
Delokgos et al., 2017	16	Outcrop	Fine-grained carbonate		79-772 m	Active
Densmore et al., 2004	9	Outcrop	Igneous & clastic		32,421-344,800 m	Active
Duffy et al., 2017	3	3D seismic	Mixed carbonate & clastic	Yes	4250-6738 m	Inactive
Ellis & Barnes, 2015	4	Outcrop	Carbonate		15,700-55,000 m	Varies
Ellis & Barnes, 2015	6	Outcrop	Igneous & clastic		23,200-182,600 m	Active
Ellis & Barnes, 2015	1	Outcrop	Mixed carbonate & clastic		58,200 m	Active
Ellis & Barnes, 2015	3	Outcrop	Metamorphic, igneous & see	dimentary	55,400-99,000 m	Varies
Finch & Gawthorpe, 2017	7 10	Numerical model			55,400-99,000 m	N/a
Gauthier & Lake, 1993	380	3D seismic	Clastic	Yes	71-1904 m	Active
Ghalayini et al., 2017	82	3D seismic	Fine-grained carbonate	No	5580-63,530 m	Inactive
Gillepsie et al., 1992	54	2D seismic	Fine-grained clastic		327-2959 m	Inactive
Gross et al., 1997	121	Outcrop	Fine-grained clastic		0.05-2.6 m	Inactive
Gudmundsson, 2004	24	Outcrop	Igneous	No	629-8982 m	Active
Hollinsworth et al., 2019	1	Outcrop & seismic	Metamorphic	Yes	15,440 m	Active
Hus et al., 2005	25	Physical analogue			0.14-0.4 m	N/a
Jackson & Rotevatn, 201	3 4	3D seismic	Sedimentary & evaporites	Yes	5000-12,300 m	Active
Jackson et al., 2017	1	3D seismic	Sedimentary & evaporites		1950 m	Inactive
Karp et al., 2012	2	2D seismic	Metamorphic & clastic	Yes	23,873-27,140 m	Active
Khalil & McClay, 2017	3	3D seismic	Sedimentary & evaporites	Yes	12,000-23,000 m	Inactive
Kicono, 2005	1	2D Seismic	Metamorphic		6199 m	Active
Lamarche et al., 2005	3	2D Seismic	Clastic		225-436 m	Active

Source Nun	nber of Fault	s Data Type	Dominant Lithology	Reactivated	Size Range (length in m)	Active/inactive
Marrett & Allmendinger, 1991	133	GPS & 2D seismic	Sedimentary & evaporites		1957-34,464 m	Inactive
McClymont et al., 2009	2	2D & 3D Seismic	Volcanic & clastic		30-47 m	Active
McGlue et al., 2006	2	2D Seismic	Metamorphic	Yes	17,014-51,000 m	Active
McLeod et al., 2000	32	3D seismic	Clastic		368-111,570 m	Inactive
Meyer et al., 2002	84	3D seismic	Mixed carbonate & clastic		690-8592 m	Varies
Morley et al., 2007	4	2D seismic	Clastic	Yes	6075-37,529 m	Inactive
Morley 2017	78	3D seismic	Mixed carbonate & clastic	Yes	3028-82,704 m	Inactive
Morley 2017	14	3D seismic	Fine-grained clastic	Yes	20,900-123,400 m	Inactive
Morley 2017	33	Outcrop	Sedimentary & evaporites	Yes	231-100,838 m	Inactive
Morley 2017	7	3D seismic	Clastic	Yes	30,845-91,792 m	Inactive
Muraoka & Kamata, 1983	14	Outcrop	Volcanic		0.6-2.5 m	Active
Nicol et al., 1996	112	3D seismic	Mixed carbonate & clastic	No	174-8926 m	Inactive
Nicol et al., 2005	1	2D seismic	Clastic	Yes	70,000 m	Active
Nicol et al., 2010	29	Aerial photography	Clastic w/ volcanic		2271-70,742 m	Active
Nicol et al., 2020	122	Outcrop & DEM	Carbonate		32-46,993 m	Active
Opheim & Gudmundsson, 198	89 8	Outcrop	Volcanic	No	351-3383 m	Active
Pan et al., 2021	147	3D seismic	Mixed carbonate & clastic		307-18,182 m	Inactive
Peacock & Sanderson, 1991	6	Outcrop	Carbonate	No	7.2-226 m	Inactive
Poulimenos, 2000	45	Outcrop	Mixed carbonate & clastic		1383-17,633 m	Active
Reeve et al., 2015	3	3D seismic	Clastic		1874-17,299 m	Inactive
Reilly et al., 2017	75	2D & 3D seismic	Clastic		1207-91,281 m	Inactive
Rippon, 1985	36	Outcrop	Clastic		200-4600 m	Inactive
Robert & Michetti, 2004	6	Outcrop	Carbonate		17,720-29,800 m	Active
Roche et al., 2017	5	Outcrop	Carbonate		0.26-3.7 m	Inactive
Schlishe et al., 1996	116	Outcrop	Fine-grained clastic		0.02-1.0 m	Inactive
Sieburg et al., 2020	432	Lidar	Volcanic		25-9707 m	Active
Solvia et al., 2005	36	Outcrop	Carbonate		0.3-50 m	Inactive
Solvia et al., 2006	50	Outcrop	Mixed carbonate & clastic		19-51 m	
Solvia et al., 2008	2	Outcrop	Carbonate		0.2-0.5 m	Inactive?

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Source	Number of Faults	s Data Type	Dominant Lithology	Reactivated	Size Range (length in m)	Active/inactive
Soliva et al., 2008	2	Outcrop	Carbonate		0.2-0.5 m	
Solvia et al., 2008	2	Outcrop	Mixed carbonate & clastic		0.8-1 m	Inactive
Solvia & Schultz, 2008	25	Outcrop	Sedimentary & evaporites		0.4-5 m	Active
Solvia & Schultz, 2008	34	2D seismic	Igneous	No	66-53,700 m	Active
Shunshan et al., 2011	17	3D seismic	Sedimentary & evaporites	Yes	477-3298 m	Inactive
Torabi et al., 2019	21	3D seismic	Sedimentary & evaporites		238-23,255 m	Inactive
Tschopp 1967	1	2D seismic	Sedimentary & evaporites		45,000 m	Inactive
Tvedt et al., 2016	3	3D seismic	Sedimentary & evaporites	Yes	12,208-16,000 m	Inactive
Vétel et al., 2016	28 Sate	llite imagery & topo o	data Igneous	Yes	8772-29,467 m	Active
Villemin et al., 1995	26	Outcrop	Clastic		350-27,586 m	Inactive
Walsh & Watterson, 1988	3 32	Outcrop	Clastic		451-4985 m	Inactive
Walsh et al., 2002	22	Outcrop	Mixed carbonate & clastic	Yes	1200-18,900 m	Active
Watterson, 1986	7				4799-53,645 m	
Wedmore et al., 2020	6	Outcrop	Metamorphic	Yes	13,000-85,000 m	Active
Whipp et al., 2014	176	3D seismic	Mixed carbonate & clastic		892-54,227 m	Inactive
Wibberly et al., 1999	28	Outcrop	Unlithified sand		0.17-10 m	Inactive
Wilkins & Gross, 2002	41	Outcrop	Clastic		0.9-490 m	Inactive
Willemse, 1997	7	Outcrop	Igneous & clastic		47-151 m	Active
Williams et al., 2021	1	Outcrop	Metamorphic	Yes	130,000 m	Active
Worthington & Walsh, 20	17 11	3D seismic	Fine-grained clastic	Yes	554-10,000 m	Inactive
Yielding et al., 1996	114	3D seismic	Fine-grained clastic		253-24,574 m	Inactive
Young et al., 2001	2	2D seismic	Clastic	Yes	11,00-12,000 m	Inactive
Zygouri et al., 2008	93 2	2D seismic & outcrop	Mixed carbonate & clastic		1764-15,147 m	Active

1070 Supplementary Table 2. Table showing all of the sources used in our global database, along

1071 with the number of faults from each source, type of data, host rock lithology, if the fault was

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- are left blank because not all information was available for every source.
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