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Data from the drain: a sensor framework that captures multiple drivers of chronic coastal floods

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Key Points:

- We present a new low-cost, open-source sensor framework that measures coastal flooding from multiple sources
- For a five month deployment, 25% of floods were driven by land-based sources, contributions not present in tide gauge water levels
- Measures of flood frequency that rely only on tide gauges are likely underestimates where stormwater networks are routinely impaired

Abstract

Tide gauge water levels are commonly used as a proxy for flood incidence on land. These proxies are useful for projecting how sea-level rise (SLR) will increase the frequency of coastal flooding. However, tide gauges do not account for land-based sources of coastal flooding and therefore flood thresholds and the proxies derived from them likely underestimate the current and future frequency of coastal flooding. Here we present a new sensor framework for measuring the incidence of coastal floods that captures both subterranean and land-based contributions to flooding. The low-cost, open-source sensor framework consists of a storm drain water level sensor, roadway camera, and wireless gateway that transmit data in real-time. During five months of deployment in the Town of Beaufort, North Carolina, 24 flood events were recorded. 25% of those events were driven by land-based sources – rainfall, combined with moderate high tides and reduced capacity in storm drains. Consequently, we find that flood frequency is higher than that suggested by proxies that rely exclusively on tide gauge water levels for determining flood incidence. This finding likely extends to other locations where stormwater networks are at a reduced drainage capacity due to SLR. Our results highlight the benefits of instrumenting stormwater networks directly to capture multiple drivers of coastal flooding. More accurate estimates of the frequency and drivers of floods in low-lying coastal communities can enable the development of more effective long-term adaptation strategies.

1 Introduction

Coastal communities around the world are confronting the growing challenge of sea-level rise (SLR). In the United States, six feet of SLR by 2100 could affect 1.7 million homes and up to 3.6 million people (Bernstein et al., 2019; Hauer et al., 2016). Already, coastal communities from Florida to Alaska are actively investing in reducing their risk from SLR, whether through a full community relocation or large-scale infrastructure investments (Bronen & Chapin, 2013; Gornitz et al., 2020; Molinaroli et al., 2019). Long before communities are permanently inundated, they experience recurrent flooding (Dahl et al., 2017). As local SLR and heavy rainfall events increase, so does the frequency of flooding in low-lying coastal areas (Sweet et al., 2018). The tidal cycle now takes place on higher average sea levels, resulting in “sunny-day” flooding of roadways during high tides. Because sea water infiltrates drainage systems at even low tidal levels (Gold et al., 2022), ordinary rain storms can now cause flash floods. We refer to locations that experience flooding multiple times per year, from drivers other than extreme storms (e.g., tropical cyclones, nor’easters), as chronically flooded.

It is well-established that higher sea levels will lead to more frequent flooding, but it is not clear which areas will be affected, how quickly, and how intensely. Chronic coastal flooding is difficult to monitor because the floods are hyper-local, creating a patchwork of affected intersections, blocks, or homes, and because floods can be caused by multiple sources. While chronic flooding is often associated with tidally-driven sunny-day flooding, it can also be influenced by groundwater, wind, rainfall runoff, and riverine discharge (Loftis et al., 2018; Moftakhari et al., 2017). Analysis of tide gauge data has shown that non-tidal residuals are particularly important components of floods along the mid-Atlantic coast of the United States (Li et al., 2022). The role of stormwater drainage systems is also poorly understood. In Norfolk, VA, recent instrumentation efforts have shown that SLR has reduced the city’s stormwater system capacity by 50% (independent of the tide), and thus is hampering the ability of the system to handle heavy rainfalls (Coutu, 2021). The viability of stormwater systems is also affected by rising groundwater, which has led to corrosion and failure of underground infrastructure in Hawaii and Florida (Befus et al., 2020; Habel et al., 2020), a problem that is likely to occur elsewhere. The influence of subterranean infrastructure on flooding is not typically included in large-scale SLR driven flood risk assessments (e.g., “bathtub” inundation modeling approaches, Sweet et al., 2018) or smaller-scale assessments of compound coastal floods (Jane et al., 2020).

While local residents often know of problem areas to avoid, information on the drivers, frequency, and spatial extent of these floods is rarely gathered systematically. One commonly-used proxy for flood incidence (i.e., an indirect measure of flooding on land) is tide gauge water levels exceeding a locally-defined threshold. Some National Oceanic and Atmospheric Administration (NOAA) tide gauges have impact-based flooding thresholds created by local National Weather Service (NWS) Forecast Offices for issuing flood advisories. These thresholds can be revised periodically based on local infrastructure vulnerabilities and are therefore challenging to use for determining how flood frequency changes over time. For this purpose, the NOAA National Ocean Service (NOS) developed the “high-tide flooding” (HTF) thresholds using a nationally-consistent approach to define a threshold for each tide gauge (Sweet et al., 2018). These thresholds are not based on impacts on land but rather derived from a statistical (regression) relationship for water levels measured at NOAA tide gauges. Using the HTF thresholds, 12 NOAA tide gauges set records for flood frequency in 2018, and nationally, flood frequency is expected to double or triple by 2030 (Sweet et al., 2020).

These tide gauge-based proxies for coastal flooding clearly show the implications of rising sea levels, but as an indirect measure of flooding on land, they likely paint an incomplete picture. First, the U.S. tide gauge network is sparse, and water levels can vary substantially over small geographies due to different winds, bathymetry, proximity to rivers or inlets, and other characteristics. Tide gauges also only show contributions to flooding within large water bodies (tides, surge, river discharge), and they will miss events that occur due to a combination of land-based sources (rainfall runoff, groundwater, infrastructure). Moore & Obradovich (2020) found that local tweets about flooding increased well before tide gauge water levels surpassed the NWS minor flood thresholds in several major cities. This suggests flooding may be occurring more often than existing flood proxies indicate.

There have been several recent efforts to develop instrumentation for measuring chronic floods, the majority of which rely on ultrasonic depth sensors (i.e., air sonars). The FloodNet sensor (Silverman et al., 2022) is open-source and uses downward-looking ultrasonic sensors to detect street flooding by attaching the sensors to subaerial structures (e.g., street signs); the data are communicated in real-time using long-range radio (LoRa; FloodNet, 2022). Because the sensor is deployed subaerially, it cannot capture subterranean impairments to stormwater networks that may contribute to street floods. The StormSensor, which also relies on an ultrasonic depth sensor, is proprietary and is designed to be deployed within storm drains while still communicating data at regular intervals using LoRa. Notably, a nonprofit spent \$280,000 USD to collect data on stormwater capacity in Norfolk using 25 of the StormSensors in 2021 (Coutu, 2021). In addition to the high cost, upon submergence, the StormSensors (and all ultrasonic depth sensors) cannot provide information about street water levels or flood extent. Pressure transducers are commonly used to measure water depths in water bodies at low-cost (Lyman et al., 2020; Maisano et al., 2019; Temple et al., 2020; Ware & Fuentes, 2018), however, they similarly only provide information about water levels at a single point. If deployed within a storm drain, real-time communication can also be impeded by stormwater infrastructure (grates, pipes). While not necessary for measuring flood incidence, real-time communication ensures no loss of data (e.g., due to sensor damage) and allows data to be used for hazard identification by stakeholders, practitioners, and researchers alike.

Here we present the utility of a new sensor framework for measuring the incidence and drivers of chronic floods. The sensor framework – which we coin SuDS: the **Sunny Day** flood Sensors – consists of a pressure logger deployed within a storm drain and a subaerially-mounted communications gateway equipped with a camera. Data are streamed to a web-based (open-source) platform for real-time communication of chronic flood hazards. This framework overcomes limitations of existing instrumentation by 1) identifying street flooding from a combination of subterranean and subaerial sources, and 2) allowing for real-time communication of water depths and visual confirmation of flood extent. Further, the sensor framework is open-source and can be manufactured using online tutorials at low-cost. We confirm through a 5-month deployment of the SuDS in Beaufort, North Carolina (NC) that land-based sources contribute significantly to chronic coastal floods at this location and consequently, flood frequency is higher than that suggested by proxies that rely exclusively on tide gauge water levels for determining flood incidence (i.e., the NWS and NOAA HTF thresholds).

2 Materials and Methods

Detailed step-by-step instructions for manufacturing the SuDS framework are available online (Hayden-Lowe et al., 2022). Sensor hardware and software are all open-source. At the

time of publication, the SuDS framework costs approximately \$650 USD to manufacture (excluding handheld tools, 3D printers, and soldering irons), which is comparable to the cost of a single commercial (real-time) pressure transducer. Herein we summarize both sensor components – the in situ pressure logger and the subaerial camera and gateway – and the workflow for real-time communication. We then describe the initial SuDS deployment in Beaufort, NC.

2.1 Pressure logger in storm drain

We designed a pressure logger that can be deployed in storm drains to measure real-time water levels coming into storm drains from both below (e.g., tides) and above (e.g., rainfall) while transmitting these data to a subaerial communications gateway (Figure 1A). All electronics for the pressure logger are located within a watertight PVC housing attached to the bottom of the grate covering the storm drain. The electronics housing connects to the pressure transducer via a vertical PVC pipe that extends to near the bottom of the drain (Figure 1B). We use a low-cost BlueRobotics pressure transducer that can measure up to 10 m depths with a reported depth resolution of 0.16 mm. The transducer communicates with an open-source data logger (SparkFun OpenLog Artemis) that records absolute pressure and temperature, which is later converted to water depth in the cloud (Section 2.3). The real-time data collected by the data logger are transmitted via Bluetooth to a communication gateway (described below) using a low-energy Bluetooth board. The logger electronics are powered with three D-cell batteries and secured to the PVC electronics housing using custom 3D-printed mounts (Figure 1D). The D-cell batteries in the pressure logger are replaced approximately every 4-6 months.

Pressure is sampled every six minutes, but this rate can be modified to suit local conditions. The data logger and Bluetooth board are powered off between samples to reduce battery consumption. The logger is mounted at an elevation in the storm drain so that the pressure transducer is out of water and able to dry at least once every 24 hours; this is a requirement for proper functionality of the transducer (as prescribed by the manufacturer). When the pressure logger is entirely submerged, the Bluetooth connection with the gateway is lost, and data are stored locally on the data logger. Once the water recedes, the Bluetooth connection is reestablished and the previously logged data are downloaded by the gateway. The pressure transducer is sensitive to temperature. To account for this, we calibrate each transducer in the lab by recording pressure at known depths for a range of temperatures (Figure S1). The results are used to develop a transducer-specific equation that corrects the pressure readings for temperature. This calibration also serves as (pre-deployment) validation for the manufacturer-supplied accuracy of the pressure transducer: ± 2 mbar/yr in the 0 to 60 deg C operating range. Raw pressure readings are corrected for temperature at the communications gateway (Section 2.2) and drift is corrected in the cloud (Section 2.3).

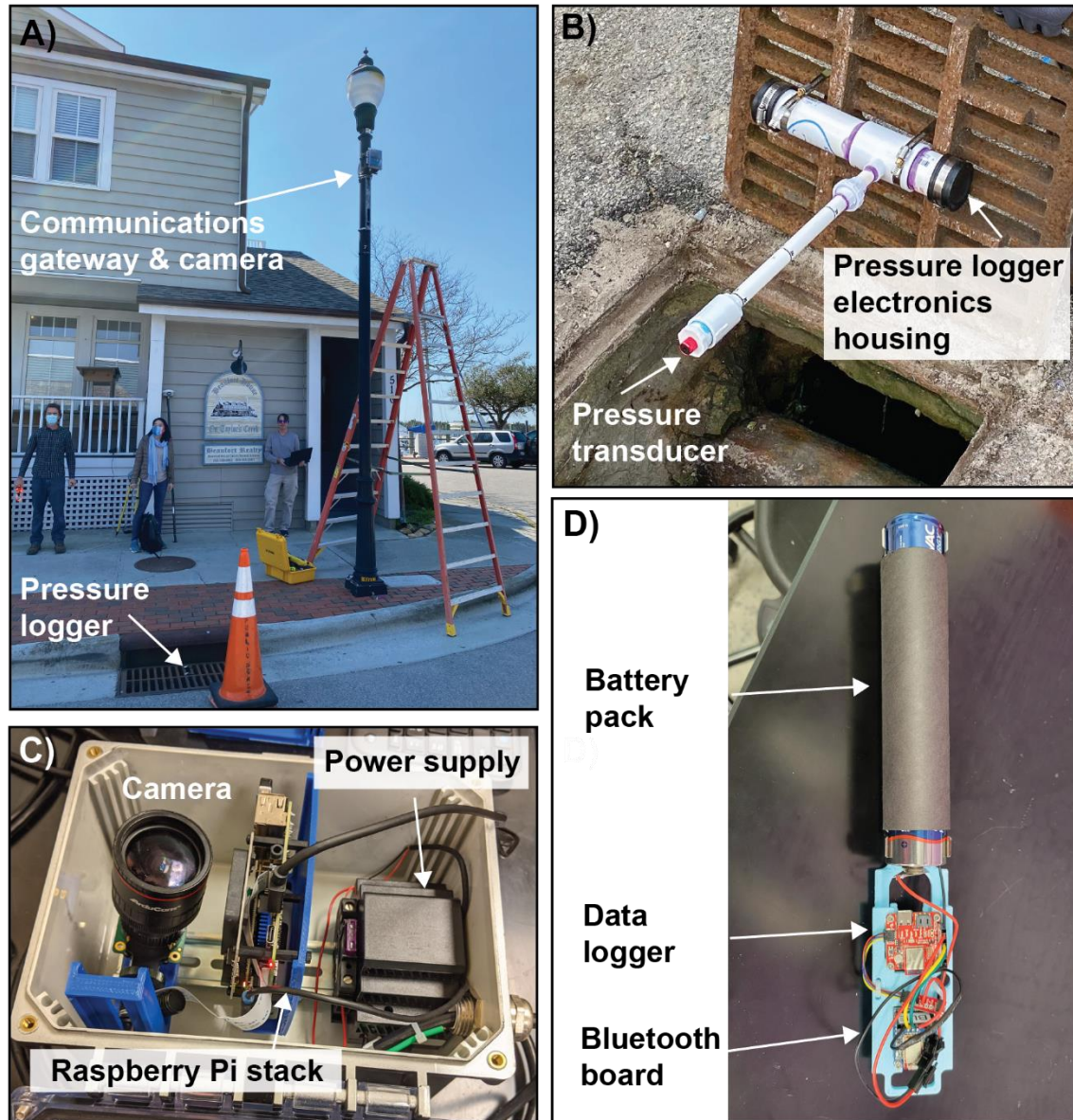


Figure 1. (A) Installation of the Sunny Day Flood Sensors (SuDS) in Beaufort, North Carolina. The SuDS consist of (B) a pressure logger deployed within a storm drain and (C) a subaerially-mounted communications gateway equipped with a camera. The gateway is powered by an outlet on the light post. (D) Internal view of the pressure logger. The SuDS are open-source and can be manufactured using online tutorials at low cost.

2.2 Subaerial camera and communications gateway

The camera and communications gateway (collectively referred to as “the gateway” herein) is mounted to a light post within Bluetooth range of the pressure logger (Figure 1A). Although not limited to deployment on light posts, the gateway requires an electrical outlet for power and must be within range of an accessible WiFi signal. The gateway contains a Raspberry Pi 4 Model B Quad Core computer (with Bluetooth and WiFi) running the Linux-based Raspberry Pi OS, an uninterruptible power supply (UPS) module, and an adjustable focal length

camera, all housed in a waterproof, polycarbonate enclosure retrofitted with an optical dome. Heatsinks and a CPU fan prevent gateway components from overheating. All components are secured within the waterproof enclosure using a DIN rail and custom 3D-printed mounts (Figure 1C).

The gateway manages communication between both the pressure logger and cloud data storage. Communication errors from events such as logger submergence and weak signal strength along either link are handled in the following manner. A continuously running Python program manages data flowing both from the pressure logger and to the cloud-based database. Data flow is shown in Figure 2. Upon collecting a sample, data collected on the pressure logger are stored to an internal file and transmitted over Bluetooth to the gateway. Bluetooth is then powered off and the logger enters a deep sleep mode to conserve power until the next sample. The gateway is always watching for the Bluetooth signal to appear. When it does, a connection is established and the gateway waits a predetermined amount of time for data to appear from the pressure logger. If data are not received within the expected time an attempt is made to recover from an error condition. Otherwise, if valid data are received, it is checked to see if it is sequential with previously received data. If so, the record is logged to files on the gateway. If it is not sequential, then the gateway downloads the relevant file(s) from the pressure logger filesystem to catch up. The gateway then attempts to transmit data through a data application programming interface (API) to the cloud (Section 2.3). If the gateway is in “catch-up” mode, the database is polled to find the most recent observation, and data are transmitted using the data cache stored in the gateway filesystem. Since pressure data are stored both on the logger and the gateway, gaps in the data can be recovered automatically despite any communication lapses.

Image acquisition is scheduled by time (every six minutes) using a built-in Linux-based Cron facility. This enables visual confirmation of roadway flooding and provides an indication of flood extents. Images are written to the gateway’s local storage and kept for four weeks. Images are transmitted to cloud storage through a photo API by first polling the database to find the most recent image and continuing from that point.

2.3 Data processing and storage in the cloud

The general workflow of data transmission to the cloud is shown in Figure 2. Two application programming interfaces (APIs) are used to route raw data from the gateway to cloud storage. The “photo” API receives images from the Raspberry Pi and saves them to Google Drive. The data API receives raw temperature and pressure data from the Raspberry Pi and stores it in a cloud-hosted PostgreSQL database table. Both APIs were created using the FastAPI framework in Python (<https://fastapi.tiangolo.com>), containerized using Docker (Merkel, 2014), and deployed on RedHat’s OpenShift platform. The APIs offer functions that respond to “POST” and “GET” requests to communicate with the Raspberry Pi and prevent duplicate data transmission (double sided arrows in Figure 2).

Raw pressure and temperature data are post-processed in the cloud. A scheduled processing function runs every six minutes and converts the raw absolute pressure data into water depth (above the pressure transducer) using atmospheric pressure data from the closest NOAA tide gauge. Water depth is then assessed for quality control issues (e.g., erroneous jumps in pressure) and converted to drift-corrected water levels relative to the road and NAVD88. Drift is common in low-cost pressure transducers (Lyman et al., 2020). Here, we identify and correct for drift by setting the running minimum water depth equal to zero (i.e., when no water is in the storm drain and the pressure transducer is recording atmospheric pressure). The methodology for

drift correction is shown in Figure S2. Notably, although the pressure transducer used in the pressure logger has a manufacturer-reported long-term stability of ± 2 mbar/yr, during our five-month deployment, the observed drift was significantly large: the equivalent of 0.5 feet of water depth. We illustrate the robustness of our drift correction through comparison of the SuDS pressure logger with a co-located commercial pressure logger in the Supplementary Information (Figure S3).

Once in the cloud, data and images can be loaded to other web interfaces for real-time communication of flood hazards.

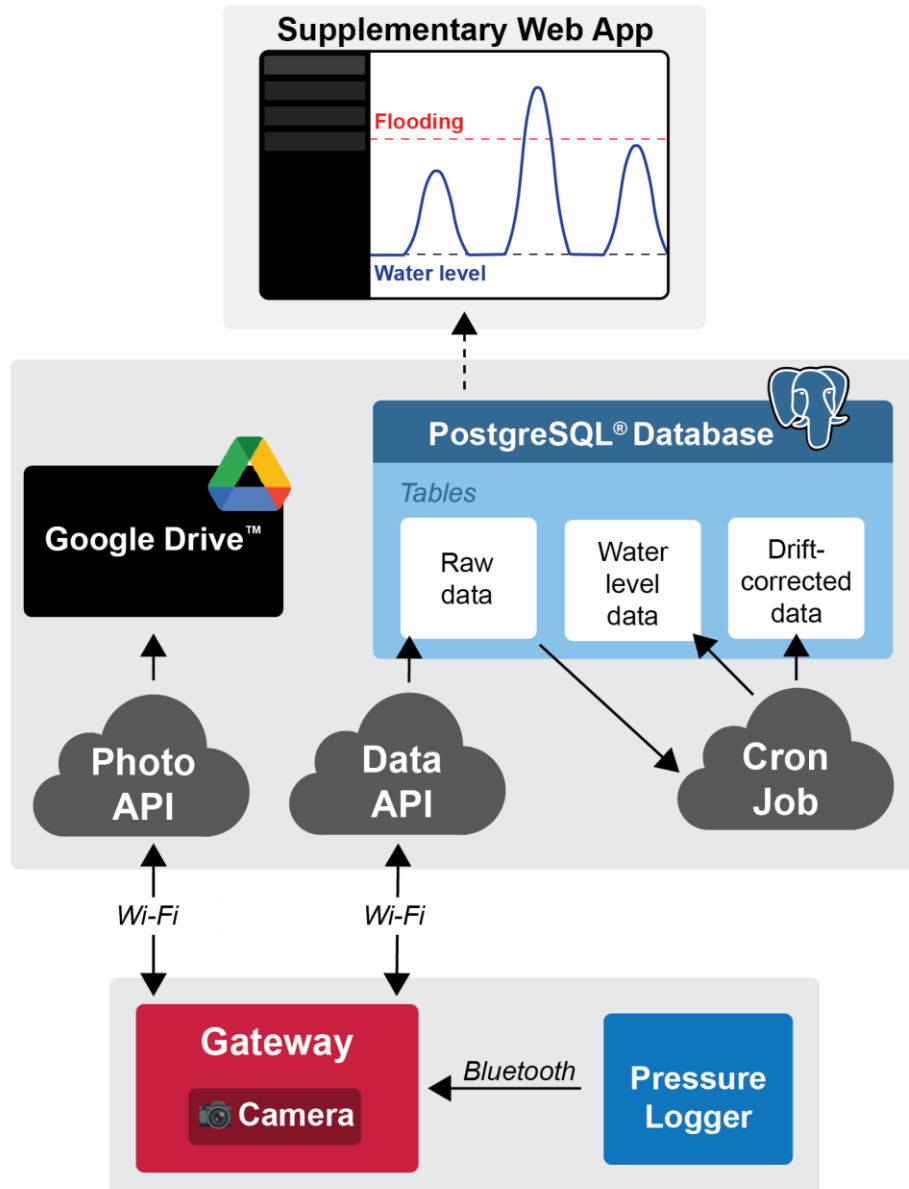


Figure 2. Schematic of data transmission to the cloud and post-processing workflow. After data is collected in the field (bottom), application programming interfaces (APIs) are used to transmit data to cloud-based storage and route data through post-processing algorithms. Cloud storage

allows data to be easily visualized through supplementary web applications (optional pathway, top).

2.4 Case study location: Beaufort, North Carolina

Our case study location for assessing the utility of this new sensor framework for measuring the incidence and drivers of chronic floods is Beaufort, North Carolina (Figure 3). Beaufort is a historic small town on the southeastern coast of North Carolina and a popular tourist destination. Downtown Beaufort is a hub of activity during the summer months, but roadway flooding has rendered shops and restaurants inaccessible during high-tide events in recent years. Water levels at the local tide gauge (NOAA 8656483) surpassed the NOAA HTF threshold on one day in 2000, four days in 2019, and is projected to surpass the threshold 6-15 days by 2030 (Sweet et al., 2020).

Working with Beaufort officials, we installed a single SuDS pressure logger and gateway in June 2021 at the location of a flood hotspot on Front Street, the main waterfront roadway in Beaufort (Figure 3B). This portion of Front Street is protected by bulkheads, which according to local officials, are rarely overtopped during high-tide events. Therefore, stormwater infrastructure was hypothesized to play a large role in chronic roadway floods. The stormwater network at this location consists of two storm drains located on opposite sides of the street that connect to an outfall one block to the southeast. This outfall empties into Taylors Creek, a tidal creek connected to the Atlantic Ocean via Beaufort Inlet. The pressure logger was installed in the drain on the south side of the street and the gateway on a neighboring light post (Figure 1A). The pressure transducer was positioned just above the bottom of the storm drain, at the elevation of the bottom of the outfall pipe (3.14 feet below the top of the roadway), such that the transducer records air pressure when the drain is completely empty of water. To visually confirm roadway flooding and capture a larger range of flood extent, we pointed the camera at the storm drain across the street, which is at a slightly lower elevation (Figure 3B). A NOAA tide gauge (8656483) is located 1 km west of the SuDS, which allows for robust comparison of measured flood frequency with those estimated using local flood proxies (i.e., when tide gauge water levels exceed the NWS minor flood or NOAA HTF threshold). Data from a NWS station 2 km north of the SuDS (Beaufort Smith Field, KMRH) was used to analyze precipitation patterns during observed flood events (Figure 3A).

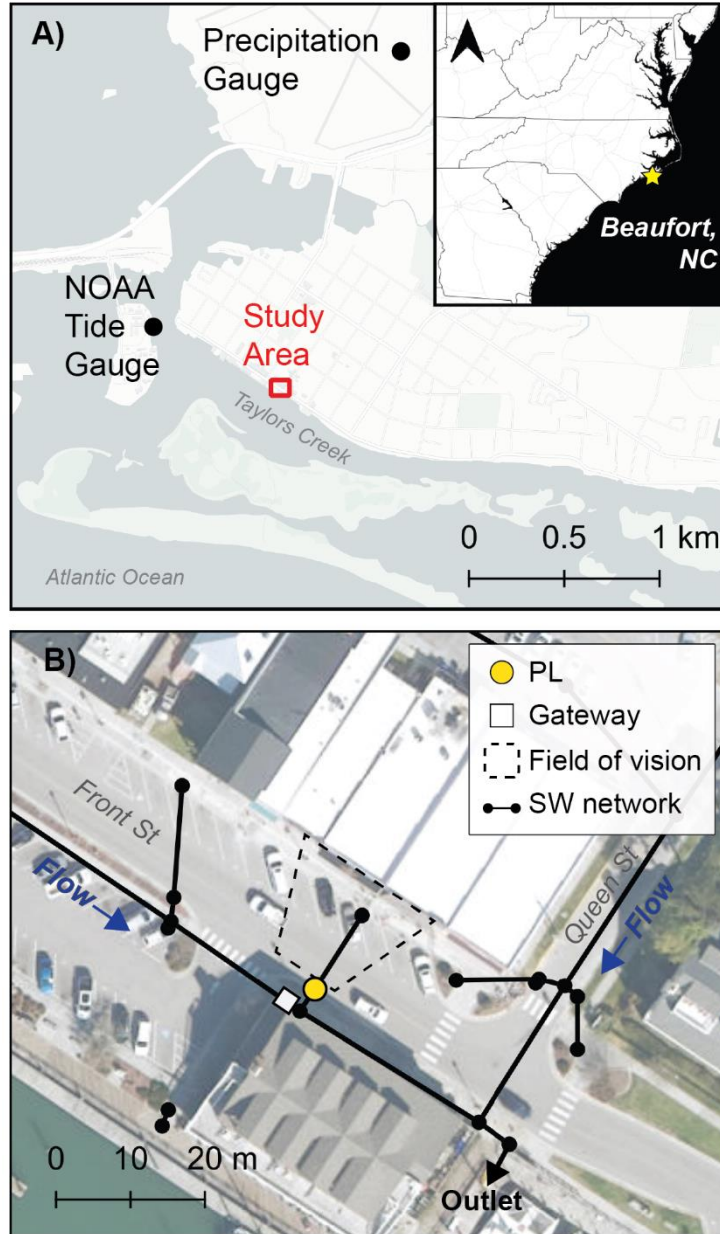


Figure 3. **A)** Overview map of Beaufort, NC and the location of a local NOAA tide gauge (8656483). **B)** Map of the study area showing the stormwater (SW) network (and designed flow direction), location of the SuDS pressure logger (PL), gateway, and field of view for the camera.

3 Results and Discussion

3.1 Flood measurements

Over the course of five months (June 22, 2021 to November 30, 2021), the SuDS captured 14,770 measurements of storm drain water levels and 38,616 images. There were four data gaps in storm drain water levels during the study period due to battery depletion in the

pressure logger (8/14 - 8/19, 9/20 - 9/22, 10/14 - 10/15, 10/25 - 11/04), totaling 21 days of missing data (13% of study period). Based on camera images, two roadway flood events occurred during these data gaps (10/29 and 11/4); however, because we do not have in situ knowledge of stormwater capacity from the pressure loggers, we do not include these floods in our calculation of flood frequency or discussion of flood drivers below.

On every day of measurement, the SuDS pressure logger recorded water from the tidal creek (receiving water body) entering the storm drain with each rising tide. Hence, the stormwater network was always at reduced drainage capacity at high tide, meaning that the network of pipes and catch basins could not convey runoff from the roadway to the tidal creek as designed during a rain event. We identified 24 discrete flood events where water levels surpassed the elevation of the top of the storm drain and then receded back into the drain. Using this definition of a flood event, it is possible to have more than one event in a day. However, given this definition, not all of the detected floods extended onto the roadway and impacted roadway functioning. As illustrated by the roadway cross-section in Figure 4, flood extent during 11 flood events was limited to parking spaces (water level < 2.8 ft NAVD88), six extended into the roadway (2.8 ft < water level < 3.15 ft NAVD88), and an additional seven flood events overtopped the curb and extended onto the sidewalk (water level > 3.15 ft NAVD88).

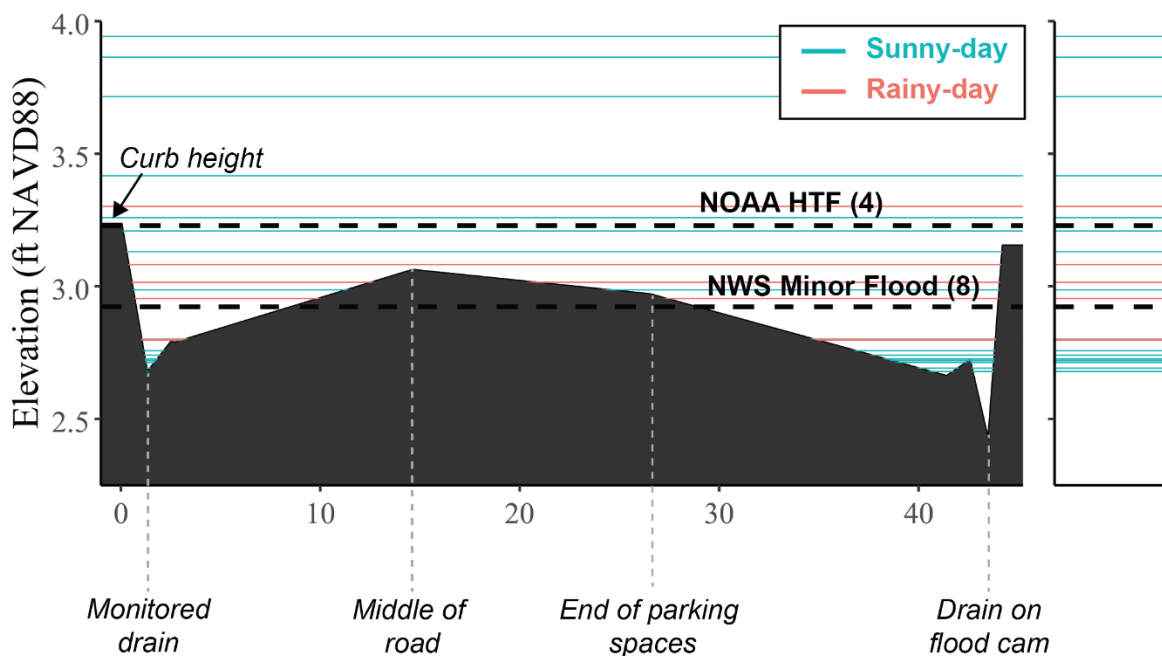


Figure 4. Cross section of the roadway and maximum water levels during flood events measured by the SuDS pressure logger in Beaufort, NC between June 22 and November 30, 2021. Here we define a flood event as water levels surpassing the elevation of the top of the storm drain. The color of horizontal lines indicates the type of flood event. NOAA and NWS flood thresholds are shown as dotted lines; the number in parentheses indicates the number of times water levels at the Beaufort NOAA tide gauge exceeded these thresholds during the measurement period (see text for detailed comparison). Water levels above the monitored drain are interpolated across the roadway, but the spatial extent was also confirmed using camera images (e.g., Figures 5 and 6).

The 24 measured flood events in Beaufort can be classified into two types based on drivers, which we identify using imagery, the shape of the stormwater hydrograph, and local precipitation data. The first type of flooding – “sunny-day flooding” – is caused by high water levels in the tidal creek which fill the stormwater network until water overtops onto the street (Figure 5A). The shape of the storm drain hydrographs for these floods are smooth and periodic, following the predicted tide (Figure 5B). The second type of flooding – “rainy-day flooding” – occurs during rain storms. In almost all cases, these floods occur when the capacity of the stormwater network is reduced by elevated water levels in the tidal creek such that runoff floods the roadway (Figure 6A). The storm drain hydrographs for this type of flooding are characterized by sharp increases in water level above the longer period fluctuations, which coincide with rain events (Figure 6B-C). We do not classify these floods further based on tidal influence primarily because we found that rainy-day floods occurred at all stages of the tide (rising, peak, and ebbing) and it is unclear to what extent high groundwater contributes to flood occurrence or extent. The six storms that resulted in rainy-day flooding were short-lived with somewhat intense precipitation (duration: 25 minutes – 2.4 hours, amount: 0.45 – 1.58 inches), but all storms were below the 1 year return period based on Atlas 14 point precipitation frequency estimates for the nearby Morehead City NWS Station (NWS, 2022). Hence, the rainy-day floods that we observe are primarily driven by SLR.

Using these definitions, we observed 18 sunny-day and 6 rainy-day flood events over the five-month study. The two types of flood events had distinctly different flood durations and magnitudes (Figure 7A). Sunny-day flood events were long in duration (median duration = 86.6 min) and led to the highest magnitude of flooding during the study period (1.27 feet above the top of the storm drain). Rainy-day flooding was much shorter in duration (median duration = 10.9 min) and spanned a smaller range of flood magnitudes (0.1 - 0.6 feet above the top of the storm drain).

A)



B)

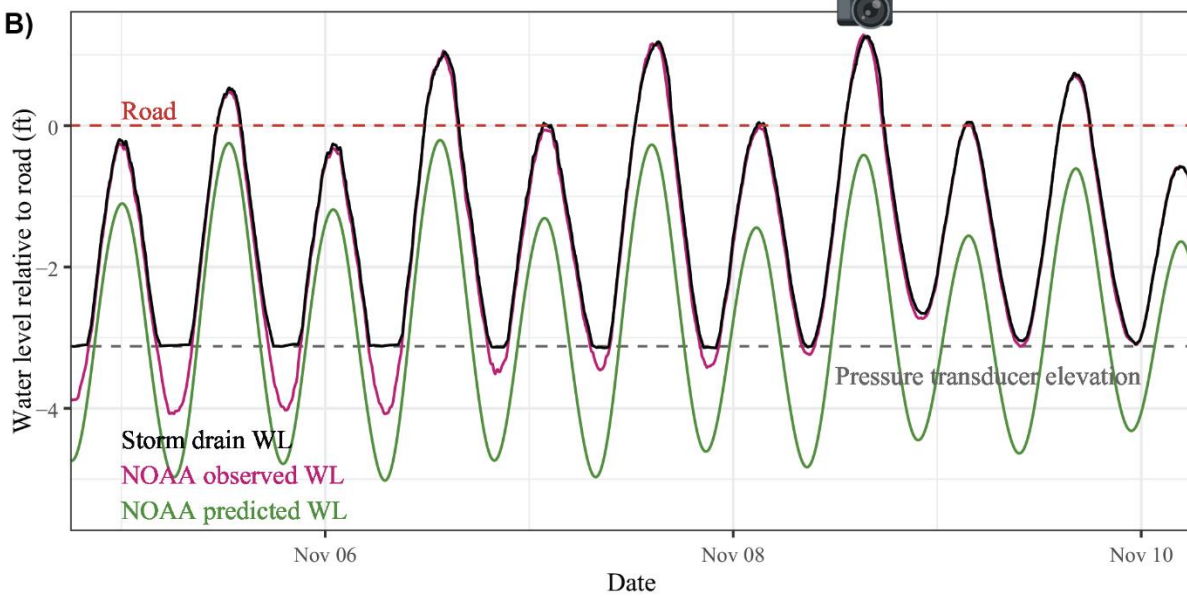
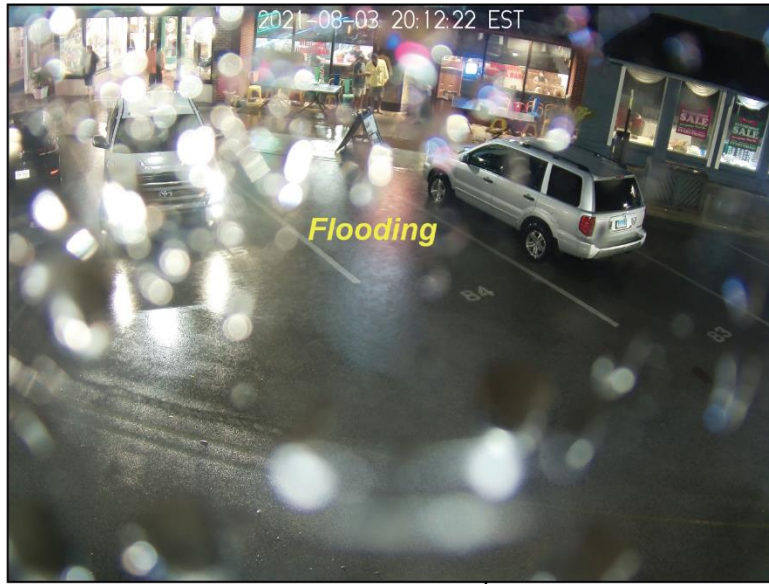
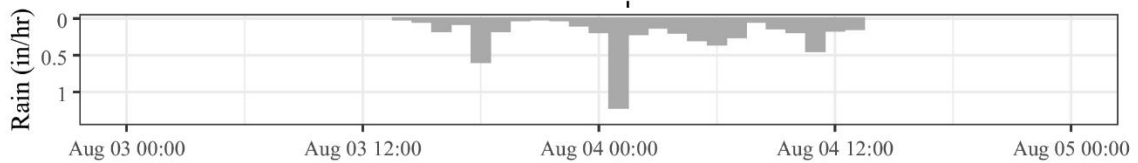


Figure 5. A series of “sunny-day” flood events measured in November 2021 in Beaufort, NC. A) Photo of the flooded roadway during the highest observed water level on November 8, 2021, and B) measured water levels above the storm drain pressure transducer relative to the road surface.

A)



B)



C)

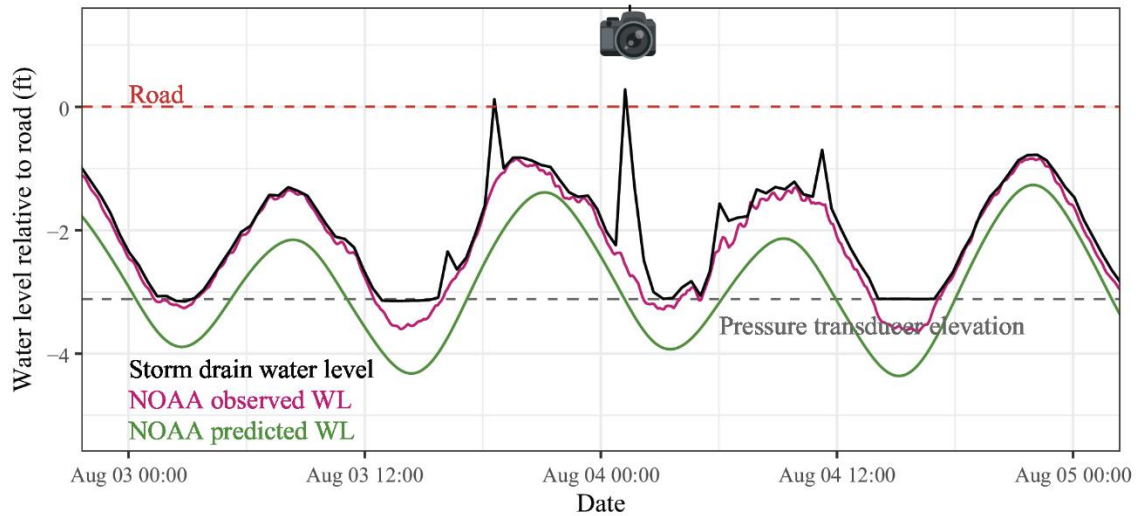


Figure 6. Two “rainy-day” flood events on August 3 and 4, 2021 in Beaufort, NC. **A)** Photo of the flooded roadway during the August 3 flood event, **B)** 1-hr rain intensity from the Beaufort Smith Field precipitation gauge (see Figure 3A), and **C)** measured water levels above the storm drain pressure transducer relative to the road surface.

3.2 Comparison with tide gauge data and flood thresholds

Generally, storm drain water levels agreed well with NOAA tide gauge observations; for our entire data record (flood and non-flood events), the RMSE of storm drain water levels compared to NOAA gauge water levels was 0.23 ft (2.7 inches) and 0.2 ft (2.4 inches) excluding days when it rained. During sunny-day flood events, there was very strong agreement between observations (RMSE = 0.1 ft), whereas during rainy-day floods, storm drain water levels diverged greatly from tide gauge observations (RMSE = 1.81 ft). The NOAA HTF flood threshold for the Beaufort tide gauge is 3.23 ft NAVD88 (Sweet et al., 2022), which spans just above the crest of the roadway at the location of the SuDS (Figure 4). The NWS minor flood threshold is slightly lower at 2.92 ft NAVD88, which according to the NWS corresponds to the elevation where at the west end of Front Street begins to flood (<https://water.weather.gov/ahps2/hydrograph.php?wfo=mhx&gage=bftn7>). Using SuDS data, we measured 18 floods below the NOAA HTF flood threshold, 5 of which were rainy-day floods. Similarly, we measured 12 flood events below the NWS minor flood threshold, two of which were rainy-day floods. If we use these thresholds and the NOAA tide gauge water levels to determine flood frequency for the same time period as the SuDS measurements, we find four discrete exceedances of the NOAA HTF threshold and eight exceedances of the NWS minor flood threshold (Figure 4). Note that due to battery outages in the SuDS pressure logger (Section 3.1), we omit two tide-gauge exceedances of the NWS minor flood threshold from this total (i.e., we did not capture two floods with the SuDS that were otherwise detected as tide gauge exceedances of the NWS minor flood threshold). It is not surprising that our measured flood incidence is higher than the proxy provided by the NOAA HTF threshold given that this threshold is not intended to capture land-based sources of flooding: here, rainfall runoff and reduced capacity in stormwater infrastructure. The NWS minor flood threshold is impact-based, meaning that it reflects the elevation of vulnerable infrastructure, but it is calibrated empirically to NOAA tide gauge water levels and therefore also does not encapsulate the effects of land-based sources. Although the data in this study only span five months, the rainy-day events constitute 25% of all floods. Hence, while flood proxies that rely exclusively on tide gauge water levels for determining flood incidence (i.e., the NWS and NOAA HTF thresholds) are useful for forecasting high tide events, the actual flood frequency may be significantly higher in areas where the stormwater network has reduced capacity.

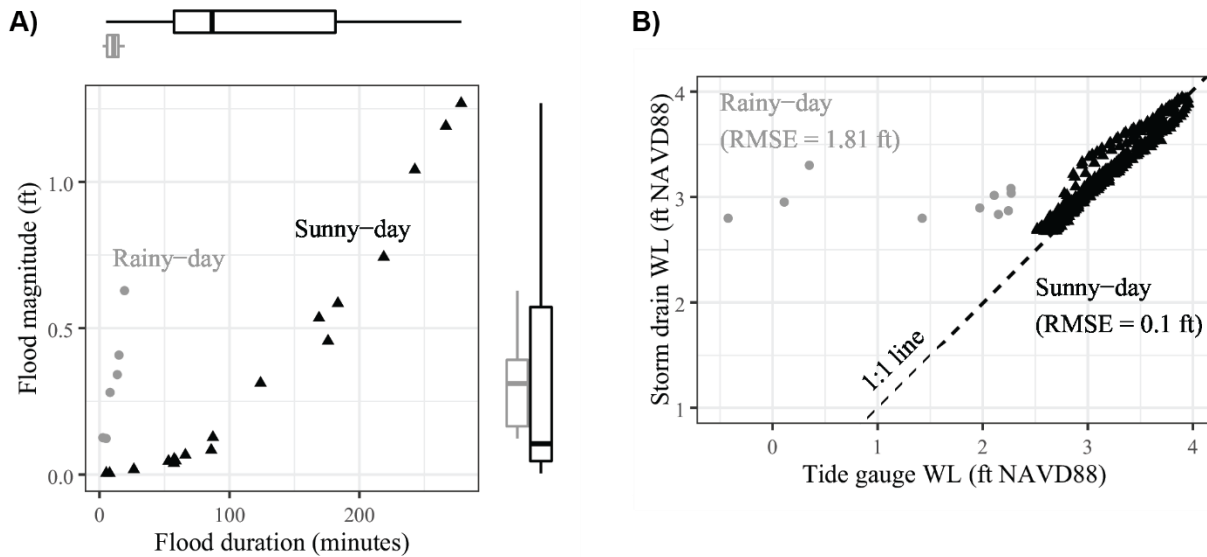


Figure 7. A) Comparison of flood magnitude (i.e., depth of water above the top of the storm drain) and duration for both sunny-day and rainy-day floods, with boxplots showing the distribution of each variable for all floods. **B)** Comparison of measured storm drain water levels during sunny-day and rainy-day floods to water levels recorded at the local NOAA tide gauge.

3.3 Sensor limitations

The SuDS have supplied a rare look at conditions within storm drains prior, during, and after chronic floods in Beaufort, NC. As a low-cost sensor framework, however, there are limitations. First, we found that the low-cost pressure transducer is sensitive to temperature, despite on-board manufacturer supplied corrections, and needs to be calibrated prior to use to ensure data quality. Second, we have documented (and corrected for) drift in the pressure measurements that may be caused by prolonged inundation or intermittent wetting-drying cycles (Figure S2). A more robust pressure transducer would likely eliminate these limitations, albeit at an increase to the sensor cost. We also use NOAA air pressure data to convert the raw pressure data from the in situ pressure transducer to gauge pressure. Future iterations of the SuDS framework could incorporate an atmospheric pressure transducer directly on the gateway. Third, the SuDS framework uses Bluetooth to send data from the pressure logger to the gateway, but the range of this connection is impeded by the metal grate covering the storm drain. This means the gateway and pressure logger must be fairly close to each other (line of sight) for consistent data uploads. Poor Bluetooth connectivity or loss of connectivity can also lead to data loss. Lower bandwidth communications technologies (i.e., LoRa) could be used to extend the distance between the monitored storm drain and gateway and provide more consistent data uploads.

The SuDS are designed to continuously collect data during floods, but real-time communication between the pressure logger and the gateway ceases once the logger becomes submerged. This loss of communications is a common drawback of flood-sensing technologies that rely on wireless communication. But contrary to other technologies, our logger continues to collect water level data while underwater and transfers the data once communications are re-established. The camera incorporated in the gateway also provides real-time photos of the roadway even when the pressure sensor communications are interrupted, and therefore a visual

confirmation of flood incidence and spatial extent. In addition, flooding can be inferred by the last recorded water level and the timing of lost communication: our real-time web app shows a “flooding” banner on the sensor site’s page if communications are lost and the last recorded water level was within 0.5 ft of the roadway surface. Machine learning techniques (e.g., long short term memory) could be useful in prediction of flood depths during sensor communication outages given external data streams of flood drivers (e.g., tide gauge water levels, rainfall intensity), a potentially fruitful avenue for future work. Lastly, the communications gateway requires electricity, so this sensor framework could stop functioning during a major flood event if power is lost for an extended period of time (>1 hr).

3.4 Implications for community engagement and hazard communication

The SuDS sensor framework presented here can contribute to enhanced flood awareness and public safety in the near-term, as well as improved resilience to climate change in the long-term. Local officials typically block off flooded roads to protect public safety, but with chronic flooding, it is not always evident when roads will need to be closed and when they can be reopened. The SuDS framework can be used to notify emergency management officials when water levels begin to approach the roadway (i.e., sensor communications are lost due to flooding) or once water levels have receded (i.e., communications resume). Such alerts reduce the risk of vehicle damage and minimize the duration of disruptions, as the road can be reopened promptly. Local residents can also view images in real-time on the web app to determine if they can travel safely or need to adjust their plans (“Flood Cam” tab in Figure 8).

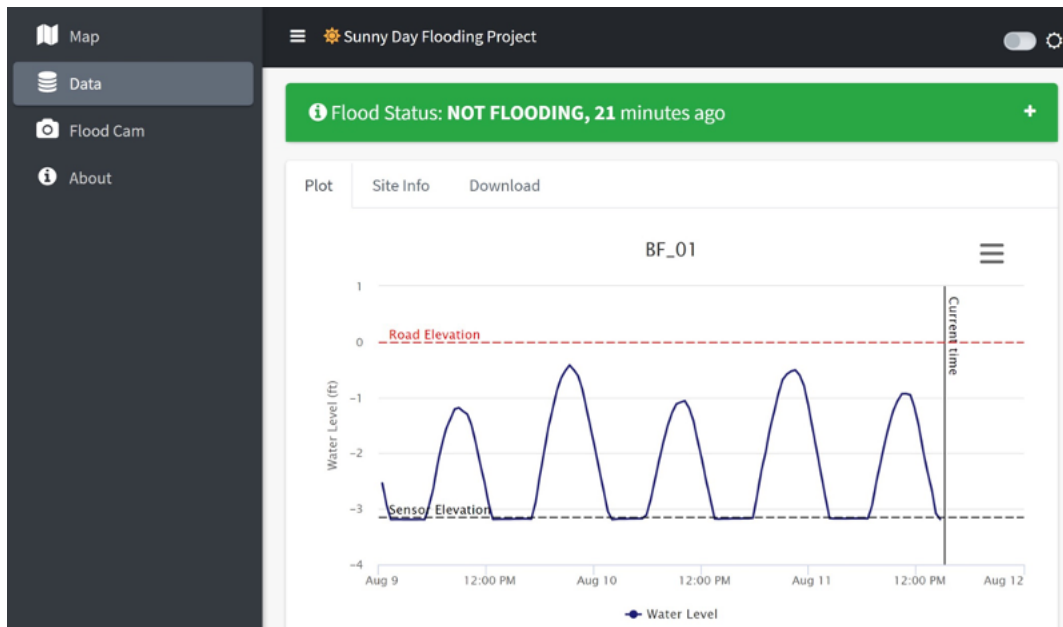


Figure 8. Screenshot of the SuDS web app showing live water level data from the monitored storm drain in Beaufort, NC. This web app also shows sample sites (and flooding status) on an overview map (“Map” tab), real-time images from SuDS gateway cameras (“Flood Cam” tab), and information about the project (“About” tab).

The SuDS framework can be used to support broader public engagement and education efforts concerning the impacts of climate change. Unlike many climate impacts, chronic coastal flooding is visible, frequent, and can be directly linked to SLR. For example, the SuDS framework could be integrated into a community science project to document the extent and disruptions associated with tidal floods (e.g., King Tides Project, n.d.). Informational signs near the SuDS can raise awareness around the issue of chronic flooding and the impacts of SLR.

As communities increasingly prepare for higher sea levels, a stronger understanding of the incidence and drivers of chronic flooding can inform evidence-based adaptation plans and investments. First, data from the SuDS framework can help identify the relative contributions of rainfall and high-water levels in receiving water bodies. Such evidence is valuable because some adaptation strategies may only combat flooding from one source. For example, higher bulkheads can prevent overtopping, but will not prevent water from entering through the stormwater network. Second, the SuDS framework can improve estimates of future flood frequency by identifying the range of conditions that lead to flooding. Adaptation strategies designed for extreme events, such as high sand dunes, will have little effect or exacerbate smaller floods along the back-side of islands or bays. With greater evidence on how chronic flooding will evolve into the future, communities can assess their needs and priorities and allocate resources accordingly.

Finally, the SuDS framework is purposefully open-source and low-cost, with the goal of enabling broader adoption by researchers and community members alike. Chronic coastal flooding is ubiquitous in low-lying coastal communities, and many questions remain about its drivers and impacts. By monitoring flooding where people live and by capturing flooding from multiple drivers, this sensor framework can enable widespread progress in understanding the causes of such events and devising potential solutions.

Acknowledgments

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Open Research

The storm drain water level data used for flood detection and analysis in the study are archived on Zenodo (DOI: 10.5281/zenodo.7135955) and can also be downloaded from our project web app (<https://sunnydayflood.apps.cloudapps.unc.edu>). The software for the SuDS sensor framework are available on GitHub (<https://github.com/sunny-day-flooding-project>) and tutorials are archived on Zenodo (Hayden-Lowe et al., 2022, DOI: 10.5281/zenodo.7017187).

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Supporting Information for

Data from the drain: a sensor framework that captures multiple drivers of chronic coastal floods

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Introduction

The supporting figures in this supplement are related to quality control of pressure transducer measurements, including an example calibration of the pressure transducers used in the SuDS for temperature effects and a graphical explanation of how we identify and correct for drift and assess data quality. Supporting text gives additional details on the procedures for correction of temperature effects and drift, and the deployment of an in situ data logger for comparative assessment of SuDS data quality.

Text S1. Correction of pressure readings for temperature

The pressure transducer used in the SuDS is sensitive to changes in temperature. We correct for the effect of temperature on raw pressure readings by performing a temperature calibration on each transducer in a controlled environment prior to deployment. The procedure involves observing the pressure response to a change in temperature while maintaining a constant water depth (and thus a constant pressure forcing). Transducers are first submerged in an ice bath and then transferred to a bucket of room-temperature water at a known depth (here 40 cm). We log both pressure and temperature as the transducer adjusts to the room-temperature water (Figure S1B, 0-150 sec) and use this data to define a linear relationship for correction of temperature effects (Figure S1A). To test whether this calibration holds over a range of water depths, we change the submersion depth at discrete intervals (Figure S1C, 150 - 300 sec). As shown in Figure S1B, the most significant temperature effects are observed between 0 and 50 seconds (at the constant submersion depth of 40 cm), during which time the water temperature increases from 11 to 19 degrees Celsius.

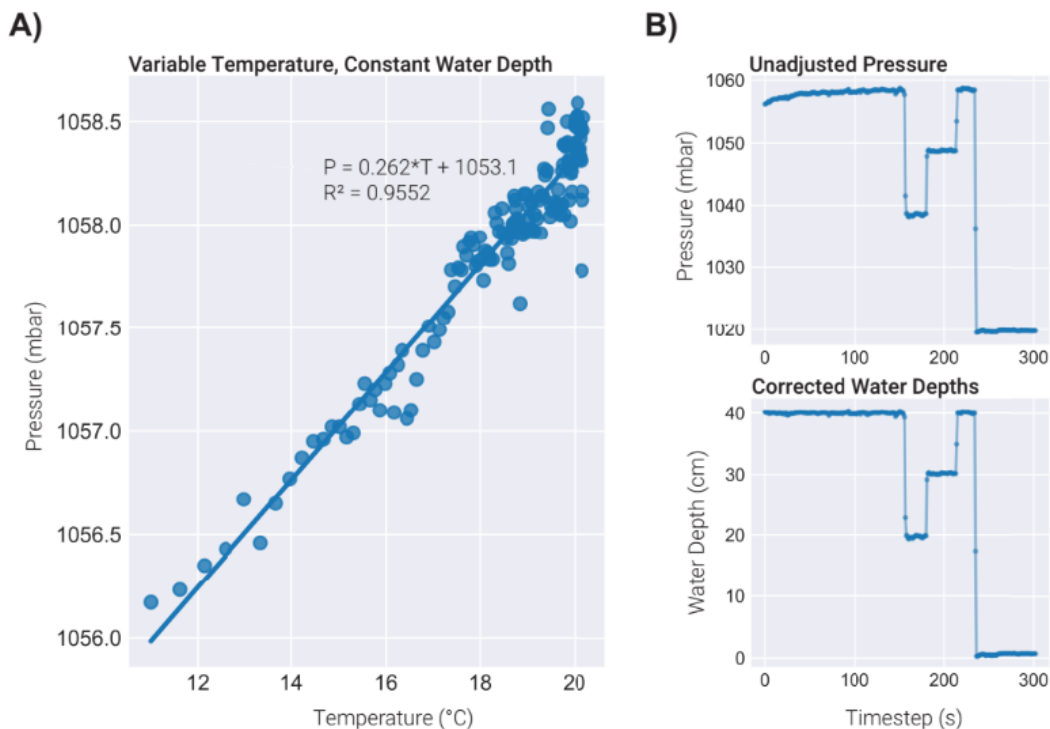


Figure S1. Linear relationship between raw pressure (P) and temperature (T) as measured by the SuDS pressure logger, shown in (A) during the constant 40 cm submersion depth period between 0 and 150 seconds in (B). Water depths corrected for temperature effects and atmospheric pressure are shown in (C).

Text S2. Drift correction and assessment of data quality

Drift detection and correction is performed using atmospherically-corrected pressure data converted to water depth. First, a rolling function that calculates the minimum water depth over the past two days is applied to uncorrected water depth data. These rolling minimum water depth

values are fit with a loess function to smooth the data and account for any short-term variations, such as if the logger is inundated for multiple days. Second, to correct for drift, an offset is applied to the uncorrected water depth data, and this offset is the difference between the surveyed sensor elevation and the smoothed minimum water depth (Figure S2).

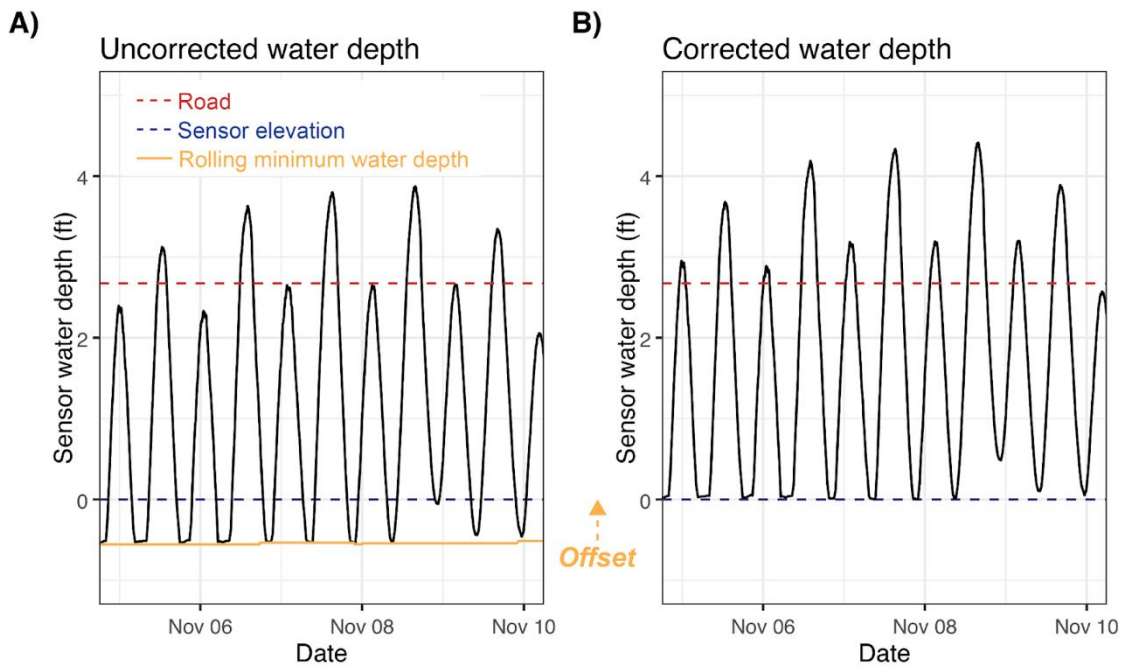


Figure S2. Graphical explanation of pressure sensor drift detection (A) and correction (B)

Text S3. To assess the robustness of our drift correction and quality of pressure data from the SuDS, we deployed an in situ HOBO pressure logger alongside the SuDS pressure logger in Beaufort for a period of one month in September-October 2022, over one year after the initial SuDS deployment. During this deployment, we removed time periods where Bluetooth connectivity issues resulted data loss from the SuDS, so the resulting comparison period was approximately 2 weeks (September 12, 2022 – October 1, 2022). Figure S3 compares atmospherically-corrected pressure data (converted to water depth) between the two sensors. The RMSE between the SuDS and HOBO water levels was 0.154 ft during this comparison period.

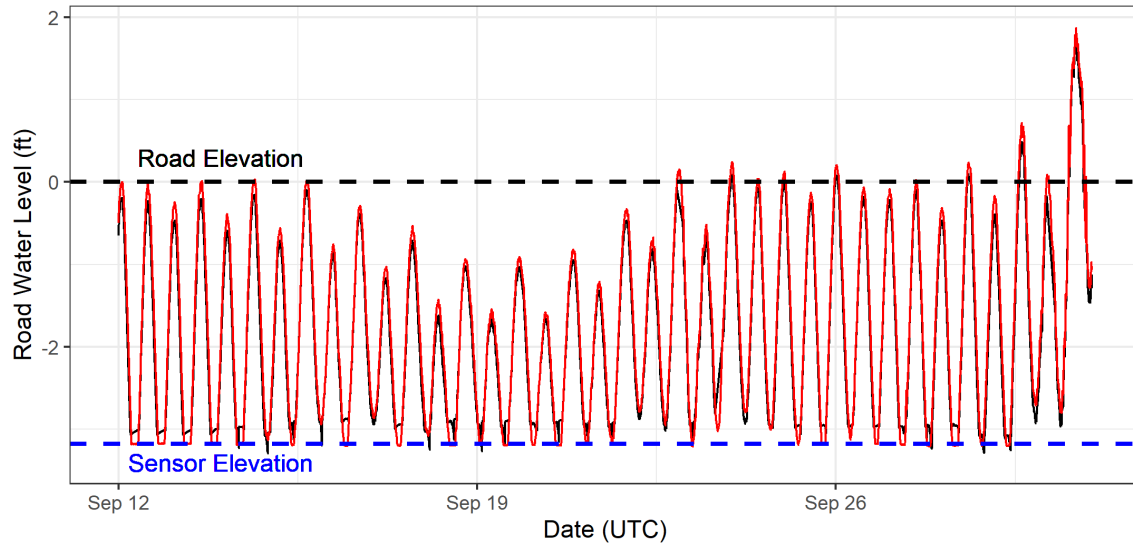


Figure S3. Comparison of data collected by the SuDS pressure logger (black line) and a co-located in situ HOBO data logger (red line)