Can homogeneous nucleation resolve the inner core nucleation paradox?

Alfred J. Wilson

School of Earth and Environment, University of Leeds a.j.wilson1@leeds.ac.uk

Dario Alfè

Department of Earth Sciences, University College London London Centre for Nanotechnology, Thomas Young Centre, University College London Dipartimento di Fisica "Ettore Pancini", Universita' di Napoli d.alfe@ucl.ac.uk

Andrew M. Walker

Department of Earth Sciences, University of Oxford and rew.walker@earth.ox.ac.uk

Christopher J. Davies

School of Earth and Environment, University of Leeds c.davies@leeds.ac.uk

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¹ Highlights

² Can homogeneous nucleation resolve the inner core nucleation para-

3 dox?

⁴ Alfred J. Wilson, Dario Alfè, Andrew M. Walker, Christopher J. Davies

- Nucleation paradox shows inner core must be supercooled ≥700 K to
 6 freeze.
- Atomistic models in this study simulate Fe-rich liquids to characterise
 nucleation.
- Si and S both reduce nucleation rates whilst O and C increase rates.
- 3% C can reduce supercooling needed to 612 K which is close to resolv ing paradox.

nucleation paradox? 13 Alfred J. Wilson^a, Dario Alfe^{b,c,d}, Andrew M. Walker^e, Christopher J. 14 Davies^a 15 ^aSchool of Earth and Environment, University of Leeds, Woodhouse, Leeds, LS2 9JT, UK^bDepartment of Earth Sciences, University College London, 5 Gower Place, London, WC1E 6BS, UK ^cLondon Centre for Nanotechnology, Thomas Young Centre, University College London, 17-19 Gordon Street, London, WC1H 0AH, UK ^dDipartimento di Fisica "Ettore Pancini", Universita' di Napoli "Federico II", Monte S. Angelo, Napoli, 80126, Italy ^eDepartment of Earth Sciences, University of Oxford, S Parks Rd, Oxford, OX1 3AN. UK

Can homogeneous nucleation resolve the inner core

16 Abstract

12

The formation of Earth's solid inner core is thought to mark a profound change in the evolution of the deep Earth and the power that is available to generate the geomagnetic field. Previous studies generally find that the inner core nucleated around 0.5-1 billion years ago, but neglect the fact that homogeneous liquids must be cooled far below their melting point in order for solids to form spontaneously. The classical theory of nucleation predicts that the core must be undercooled by several hundred K, which is incompatible with estimates of the core's present-day temperature. This "inner core nucleation paradox" therefore asserts that the present inner core should not have formed, leaving a significant gap in our understanding of deep Earth evolution. In this paper we explore the nucleation process in as yet untested

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iron-rich systems which may comprise the Earth's early core. We find that 1 mol.% Si and S increase the supercooling required to freeze the inner core compared to pure iron by 400 K and 1000 K respectively. 3 mol.% C reduces the inner core nucleation temperature to only 612 (\pm 139) K, which is close to resolving the paradox but still requires that the inner core formed recently.

17 Keywords: Inner Core, Nucleation, Molecular Dynamics

18 **1. Introduction**

The Earth's magnetic field is produced by the geodynamo in the liquid 19 outer core. The majority of the convective power which drives the present 20 dynamo is from inner core growth (Labrosse, 2015; Nimmo, 2015a; Davies, 21 2015), where light elements partitioned to the liquid create a positive buoy-22 ancy anomaly at the innermost outer core. This field shields the Earth's 23 surface from potentially harmful space weather events and solar radiation. 24 Palaeomagnetic records suggest that the geodynamo could have been ex-25 tant for at least the last 3.4 Gyrs (Tarduno et al., 2010). Prior to inner core 26 growth, the geodynamo must have been powered by other means such as sec-27 ular cooling, radiogenic heating or precipitation of light elements (O'Rourke 28 and Stevenson, 2016; Hirose et al., 2017; Badro et al., 2018; Wilson et al., 29 2022). Because it presents such a fundamental change in regimes, the nucle-30 ation of the inner core is perhaps the most important event in the thermal 31 history of the core and might present an observable signature in the paleao-32 magnetic record (Biggin et al., 2015; Bono et al., 2019; Zhou et al., 2022; 33

Davies et al., 2022). Despite this the age of the inner core is unknown and
controversy over the thermal conductivity of the core has led to a wide range
of inner core age estimates (e.g. Nimmo, 2015b; Labrosse, 2015; Driscoll and
Davies, 2023) from 1 Ga to 500 Ma.

Adding to the controversial timing of inner core formation, a more recent problem has come to light. Theory and atomic scale simulations predict that there is a substantial barrier to the formation of new solid in liquid iron under core conditions (Huguet et al., 2018; Davies et al., 2019; Wilson et al., 2021) that means substantial supercooling is expected to be needed before inner core formation.

Classical nucleation theory (CNT, e.g. Christian, 2002) describes the ther-44 modynamics of nucleation and states that for a liquid to freeze it must be 45 supercooled. This is because whilst the liquid will be thermodynamically 46 unfavourable compared to the solid for a system below its melting temper-47 ature, the interface between the first solid and the remaining liquid comes 48 with an energetic penalty. Only when a critical nucleus size is exceeded will 49 the energetic preference for the solid phase outweigh the energetic penalty 50 due to the interface. Nuclei which grow larger than this will become increas-51 ingly likely to continue to grow, leading to the system freezing. Huguet et al. 52 (2018) used CNT to describe the supercooling needed to freeze liquid iron in 53 the core. Applying existing calculations of interfacial energy and enthalpy 54 of fusion of iron (Zhang et al., 2015) to define the balance of energies, the 55 authors found that a supercooling on the order of 1000 K was needed for 56

⁵⁷ spontaneous nucleation. Huguet et al. (2018) estimated the allowed super-⁵⁸ cooling by finding the largest feasible present-day separation of separation of ⁵⁹ isentrope and melting curve at the centre of the Earth whilst preserving an ⁶⁰ intersection at the inner core boundary (ICB). It is this miss-match between ⁶¹ the predicted and allowed supercooling of the core which is the inner core ⁶² nucleation paradox.

Following the discovery of the paradox, several studies have examined 63 the problem in hopes of a resolution. Davies et al. (2019) directly observed 64 homogeneous nucleation in molecular dynamic simulations of Fe and FeO 65 systems at extreme supercooling and extrapolated results to Earth-like con-66 ditions, confirming the existence of the paradox. Others have probed the 67 relevant conditions with molecular dynamic simulations of pure Fe to char-68 acterise the size distribution of sub-critical (those which re-melt) nucleation 69 events (Wilson et al., 2021). Both approaches, find that these simple sys-70 tems reproduce the original prediction of Huguet et al. (2018) with a 675 -71 807 K supercooling requirement for spontaneous homogeneous nucleation of 72 the inner core. A metadynamic approach shows that metastable iron phases 73 may lower the nucleation barrier in a two-step nucleation process (Sun et al., 74 2022) but much of this reduction is owed to a lower melting temperature and 75 this metastable phase has not been reported in molecular dynamic studies 76 of the same systems (Davies et al., 2019; Wilson et al., 2021). A recent laser 77 driven shock experiment study on the melting curve of iron has suggested 78 that the paradox does not exist and that the nucleation barrier is far lower 79

than previously thought for planetary interiors (Kraus et al., 2022). This assertion is based on the freezing of a sample in only a few nanoseconds, far faster than predicted by CNT, but used Fe foils with impurities, which might lower interfacial energies, and an experimental configuration which provides heterogeneous nucleation sites. Both of these effects can reduce the nucleation barrier and increase nucleation rates but would not be present in the core.

All prior studies have focused almost exclusively on pure iron systems 87 with the exception of Davies et al. (2019) who found $Fe_{0.9}O_{0.1}$ had little ef-88 fect on the required supercooling due to almost equal but opposite effects of 89 reducing the nucleation barrier and melting point depression. The composi-90 tion of the core is to be expected far more complex, with an overall density 91 deficit of $\sim 10\%$ attributed to dissolved light elements (Anderson, 2002) and 92 the density contrast between outer and inner core requiring compositional 93 variation within the core (Davies et al., 2015). Silicon, sulphur, carbon and 94 oxygen are all candidate light elements in the core (Hirose et al., 2021) due 95 to their solubility in liquid iron at high temperature and their abundance in 96 the mantle, although their effects on nucleation are unlikely to be similar. 97 For example, because silicon and sulphur do not strongly partition to the 98 solid (Alfè et al., 2002b; Alfe et al., 2000), they are expected to depress the 99 melting curve of Fe less than carbon and oxygen, which do (Li et al., 2019; 100 Alfè et al., 2007). 101

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This study will examine whether iron-rich binary alloys with compositions

thought to be relevant to Earth's core are capable of spontaneous homoge-103 neous nucleation at supercooling which would resolve the inner core nucle-104 ation paradox. We only consider homogeneous nucleation because there are 105 no obvious solid surface on which iron can first nucleate at the centre of the 106 core. We will first describe the methods used to simulate supercooled liquids 107 and characterise nucleation within them following our previous work (Wil-108 son et al., 2021). We will then present predictions of critical nucleus sizes for 109 Fe_xO_{1-x} , Fe_xC_{1-x} , Fe_xSi_{1-x} and Fe_xS_{1-x} at x = 1 and 3 mol. %. Finally, we 110 will compare the rate at which the critical events are achieved to a revised 111 estimate of the geophysically viable supercooling in the core. 112

113 2. Methods

This study aims to define the supercooling required to freeze iron-rich 114 systems under the conditions of Earth's core. CNT is applied to describe 115 the thermodynamic process of supercooled liquids freezing. In order to char-116 acterise nucleation, we require models which accurately describe molecular 117 dynamic behaviour whilst having the computationally efficiency to perform 118 simulations of many thousands of atoms running for long periods of time and 119 thus generate useful statistics. Embedded atom models (EAMs) are used for 120 these simulations and first principles calculations define the parameters of 121 these models. To frame these calculations at relevant pressure and temper-122 atures, equations of state and melting curves must also be calculated for 123 these models. We use the methodology of Wilson et al. (2021) expanded 124

to binary systems to identify nuclei, calculate nucleation rates and predict
waiting times for systems to freeze.

127 2.1. Classical Nucleation Theory

The rate per unit volume at which nuclei spontaneously form (I) in a supercooled liquid is

$$I(r) = I_0 \exp\left(\frac{-\Delta G(r)}{k_B T}\right),\tag{1}$$

where r is the radius of the nucleus, I_0 is a prefactor scaling the kinetics of the system, ΔG is the free energy associated with forming the nucleus, k_B is the Boltzmann constant and T is temperature. As discussed earlier, ΔG is comprised of a favourable term associated with converting liquid to solid and an unfavourable term associated with forming an interface between the states. For a sphere

$$\Delta G(r) = \frac{4}{3}\pi r^3 g^{sl} + 4\pi r^2 \gamma, \qquad (2)$$

where γ is the interfacial energy and g^{sl} is the difference between the free energy of the solid and the liquid $(g^{sl} = g^s - g^l)$. g^{sl} can be approximated through the enthalpy of fusion, h_f and an accommodation for second order non-linearity in the temperature dependence, h_c ,

$$g^{sl} = h_f \frac{\delta T}{T} \left(1 - h_c \delta T \right).$$
(3)

 g^{sl} varies with temperature and supercooling ($\delta T = T - T_m$) whilst γ is constant to a first approximation. This means that under CNT, the scaling of g^{sl} with T is what drives the exponential relation of nucleation rate with temperature in Eq. 1. Liquids must be supercooled to freeze because no part of ΔG is favourable otherwise, furthermore, Eq. 1 shows that at the melting temperature, the nucleation rate of all nuclei is infinitesimally small.

The nucleation barrier (Eq. 2) is dominated by γ at small r because of 146 high surface area to volume ratio. All nuclei must grow from a single atom 147 through all smaller nuclei sizes before a system can be completely frozen. 148 The value of ΔG increases with r to a peak at which point the probability 149 of continued growth is equal to that of remelting. This is the critical size, 150 r_c , beyond which, the continued growth of a nucleus becomes exponentially 151 more likely and so will usually result in the system freezing. r_c is found by 152 evaluating the peak of the barrier, where the gradient of ΔG with respect to 153 radius is zero 154

$$\frac{\delta \Delta G}{\delta r} = 0 \tag{4}$$

155 gives

$$r_c = \frac{-2\gamma}{g^{sl}}.$$
(5)

Combining Eq. 1-3 with Eq. 5 then gives the rate at which the critical event
 occurs, the inverse of which is the average waiting time between critical events

$$\tau_w = \tau_0 \exp\left(\frac{\Delta G(r_c)}{k_B T}\right),\tag{6}$$

158 where

$$\tau_0 = \frac{z}{NS},\tag{7}$$

159 and

$$z = \left(\frac{\frac{4}{3}\pi r_c^3 g^{sl}}{k_B T}\right)^{-1/2}.$$
(8)

Here, S, N and z are the rate of nuclei growth, number of available nucleation sites and Zeldovich factor, respectively. With this formulation, once we know the thermodynamic properties of the system we can evaluate the value of δT compatible with the available incubation time for the inner core. We use CMD simulations to observe sub-critical ($r < r_c$) nuclei and record I, the distributions of which inform the thermodynamic quantities in Eq. 2 (see section 2.4 for details).

167 2.2. Molecular dynamics

Simulations must contain tens of thousands of atoms and be observed 168 for several nanoseconds in order to provide useful statistics (many orders of 169 magnitude larger and longer than possible with first principles calculations) 170 because larger nuclei are significantly more rare than smaller ones (Eq. 1). 171 Embedded atom models define these large scale classical molecular dynamic 172 simulations and are fit to first principles molecular dynamics simulations for 173 high accuracy. First principles calculations provide trajectories, energies and 174 pressures which are fit using embedded atom models. We follow the work of 175 Davies et al. (2019) and Wilson et al. (2021) using existing EAM parameters 176 for pure iron (Alfè et al., 2002a) and fitting for the additional components 177

178 (Eq.s 9-15).

EAMs define the total energy of a system (E) through the sum of energies contributed by each atom (i) from the pairwise interaction with other atoms (j)

$$E = \sum_{i=1}^{N_{Fe}} E_i^{Fe} + \sum_{i=1}^{N_X} E_i^X + \sum_{i=1}^{N_{FeX}} E_i^{FeX}.$$
 (9)

For the binary systems considered here this consists of iron-iron, iron-solute and solute-solute interactions. Each of these energies includes a repulsive term (Q), which depends on the separation of the pair (r_{ij}) , and an embedded term (F) which depends on the electron density between the pair (ρ_{ij})

$$E_{i}^{Fe} = Q_{i}^{Fe} + F^{Fe}(\rho_{i}^{Fe}) = \sum_{j=1, j\neq i}^{N_{Fe}} \epsilon^{Fe} \left(a^{Fe}/r_{ij}\right)^{n^{Fe}} - \epsilon^{Fe} C^{Fe} \sqrt{\rho_{i}^{Fe}}, \quad (10)$$

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$$E_{i}^{X} = Q_{i}^{X} + F^{X}(\rho_{i}^{X}) = \sum_{j=1, j \neq i}^{N_{X}} \epsilon^{X} \left(a^{X}/r_{ij} \right)^{n^{X}} - \epsilon^{X} C^{X} \sqrt{\rho_{i}^{X}}, \qquad (11)$$

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$$E_{i}^{FeX} = Q_{i}^{FeX} = \frac{1}{2} \sum_{i=1}^{N_{Fe}} \sum_{j=1, i \neq j}^{N_{X}} \epsilon^{FeX} \left(a^{FeX} / r_{ij} \right)^{n^{FeX}}, \qquad (12)$$

where ϵ , a, n and C are free parameters specific to each interaction. The electron densities are also defined in terms of a radial separation

$$\rho_i^{Fe} = \sum_{j=1, j \neq i}^{N_{Fe}} \left(a^{Fe} / r_{ij} \right)^{m^{Fe}} + \rho_i^{FeX}, \tag{13}$$

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$$\rho_i^X = \sum_{j=1, j \neq i}^{N_x} \left(a^x / r_{ij} \right)^{m^X} + \rho_i^{FeX}, \tag{14}$$

191

$$\rho_i^{FeX} = \sum_{j=1, j \neq i}^{N_x} \left(a^{FeX} / r_{ij} \right)^{m^{FeX}}, \qquad (15)$$

¹⁹² and include an additional parameter m^{Fe} , m^X and m^{FeX} for each class of ¹⁹³ interaction. Details of first principles calculations, fitting of EAMs and sub-¹⁹⁴ sequent validation can be found in the supplementary information.

¹⁹⁵ Davies et al. (2019) present a model for the FeO system which we adopt ¹⁹⁶ here, negating the need for fitting this system. EAMs were further vali-¹⁹⁷ dated through the mean square root of the fluctuations in energy differences ¹⁹⁸ between configurations evaluated through EAM potentials and independent ¹⁹⁹ DFT simulations (not used for the fitting procedure). For Fe_{0.97}Si_{0.03}, Fe_{0.97}S_{0.03} ²⁰⁰ and Fe_{0.97}C_{0.03} at 6000 K these are 0.245, 0.325 and 0.360 eV per cell respec-²⁰¹ tively, which is less than k_BT (0.517 eV).

CMD simulations were conducted using the LAMMPS package (Plimp-202 ton, 1995) within the canonical ensemble. Systems contain 21296 atoms with 203 periodic boundary conditions and trajectories calculated via the Verlet al-204 gorithm. Uniquely random initial configurations of iron atoms interspersed 205 with each impurity are evolved for 2 ps at 10000 K to remove any pre-existing 206 structure in the liquid. The system is then cooled to the desired tempera-207 ture over 1 ps and then evolved for 1 ns, recording atom positions every 208 100 steps. Volumes are adjusted for each temperature and composition ac-209

cording to Birch–Murnaghan 3rd order equations of state (Birch, 1947) also
calculated using the EAMs.

212 2.3. Melting temperatures and equations of state

Melting temperatures are necessary to evaluate Eq. 3 and frame the 213 supercooling of a system more generally. We calculate self-consistent melting 214 temperatures for the systems studied here through coexistence simulations. 215 These involve simulating conditions close to a point on the melting curve with 216 regions of both solid and liquid within a single system. When the system is 217 allowed to evolve under the microcanonical ensemble some portion of either 218 phase will convert to the other in order to establish an equilibrium whilst 219 maintaining constant energy and the temperature of the system will adopt 220 a point on the melting curve. Melting point depression for Si, C and O are 221 presented in table 1 and Fig. 1. The value of O is taken from Davies et al. 222 (2019) and other systems are polynomials fit to our coexistence simulation 223 results. 224

225 2.4. Nuclei identification

The conditions of interest for nucleation the Earth's inner core involve a maximum volume of 17.62×10^{18} m³ and a maximum waiting time on the order of 1 Gyrs. These are not volumes or waiting times which are accessible to molecular dynamic simulation and so the critical event cannot be observed. Instead we record sub-critical nuclei, the frequency of which is directly sampling *I*. Solid-like arrangements of atoms are identified within

the supercooled liquid as in our previous study (Wilson et al., 2021) which 232 in turn uses a previously developed method for categorising local bonding 233 environments via local order parameters (Van Duijneveldt and Frenkel, 1992; 234 Rein ten Wolde et al., 1996; Persson et al., 2011). Nuclei are comprised 235 of solid like atoms within bonding distance of one-another (as defined by 236 the full width of the first peak of the radial distribution function). Nuclei 237 sharing at least half of their atoms with another in an adjacent timestep are 238 considered to be a time evolution of the same nuclei. This information allows 239 the frequency and growth rate of each nuclei size to be recorded. 240

Following Wilson et al. (2021), we use I recorded from CMD simulations to predict r_c . By considering a single T, Eq. 1 can be expressed as

$$-\ln\left(I_T(r)\right) \propto \Delta G_T(r). \tag{16}$$

Using this approach we can interpret nucleation rates as the portion of Eq. 244 2 where $r < r_c$ (because the critical event will never occur within practi-245 cal durations). The absolute magnitude of ΔG remains poorly constrained, 246 meaning that g^{sl} , γ and I_0 cannot be calculated yet. Instead, we fit this 247 distribution via

$$\Delta G_T(r) = 4/3\pi r^3 A + 4\pi r^2 B,$$
(17)

where A and B are variables at each T. Once fit, this distribution then predicts $r_c = -2B/A$ in the same way as Eq. 5. Once r_c is known at all temperatures, the temperature dependence of r_c is described by combining ²⁵¹ Eq. 5 and 3 to give

$$r_c(T) = \frac{-2\gamma}{h_f \frac{\delta T}{T_m} (1 - h_c \delta T)}.$$
(18)

Predictions of $r_c(T)$ are fit with h_f , h_c and γ being free parameters. This leaves only τ_0 remaining to populate Eq. 6, where N and S are recorded directly from simulations and z is calculated from h_f and h_c (Eq. 7).

255 3. Results

CMD simulations were used to calculate melting curves, equations of 256 state and to characterise nucleation rates. Coexistence simulations of liquid 257 and solid were preformed at 13 volumes (corresponding to 200-400 GPa), 10 258 temperatures (5000-7000 K) and 4 solute concentrations (1-7 mol. %) for 250 each system (Si, S and C). O bearing systems were only analysed for crit-260 ical radius to confirm the result of Davies et al. (2019), further assessment 261 was not warranted as this study uses the same EAM. Calculation of melting 262 temperature (Fig. 1) is necessary due to the lack of relevant published melt-263 ing curves (in terms of precise composition) and the requirement to frame 264 sub-critical nuclei information in terms of supercooling. For the FeO system 265 we adapt the result of Davies et al. (2019) at 323 GPa, extrapolating all 266 points such that the pure Fe result agrees with the 6490 K value of Alfè et al. 267 (2002b) at 360 GPa (from which the Fe EAM originates). Results in this 268 study are evaluated at 360 GPa because the centre of the Earth will have 269 experienced the longest incubation time for nucleating the inner core. At low 270 solute concentration (1 mol. %) all systems see a melting point depression 271

of ~ 50 K. At 5 mol. % concentration, FeSi and FeS systems have a similarly 272 small $\frac{dT_m}{dx}$ whilst FeO and FeC remain approximately linear over this compo-273 sitional range. This is because Si and S are partitioned equally between solid 274 and liquid (Alfè et al., 2007), meaning the effect on free energies of solid and 275 liquid is similar and balanced. The opposite is true of C and O, where both 276 are more strongly partitioned to the liquid (Li et al., 2019) implying greater 277 melting point depression. Melting point depression for O bearing systems 278 found by Davies et al. (2019) is greater than the effect we find for systems 279 with C. 280



Figure 1: Melting temperatures of FeSi, FeS, and FeC (maroon, purple and green circles respectively) systems calculated via coexistence simulation at 360 GPa. All systems take a pure Fe melting temperature from Alfè et al. (2002a) (black triangle) which also provides the same Fe EAM used here. Davies et al. (2019) is shown for comparison (grey triangles and line) and is adjusted to match the pure Fe 360 GPa value.

To characterise nucleation we perform CMD calculations of supercooled systems at 5-10 temperatures and 1-3 solute concentrations in order to record the properties of sub-critical nuclei. For sufficient statistics to be gathered, we run these calculations with between 80 and 200 random initial configurations per temperature and composition, resulting in ~6000 calculations totalling more than 50 million cpu hours.

Figure 2 shows nucleation rates in systems containing Si, S and C. Those with C have produce nuclei $\sim 20\%$ faster than those containing Si and S for similar supercooling, suggesting that the nucleation barrier is lower (ΔG is smaller). It is helpful to express these results in terms of a notional radius

$$\tilde{r} = \left(\frac{N^{nuc}v_{par}}{\frac{4}{3}\pi}\right)^{1/3},\tag{19}$$

where $v_{par} = V/N^{atoms}$, V is the volume of the system, N^{atoms} is the number of atoms in the system and N^{nuc} is the number of atoms in the nuclei. Whilst \tilde{r} is framed in terms of spherical nuclei, shapes can vary from this significantly as we discuss below.



Figure 2: Nucleation rates of sub-critical nuclei for 1 mol.% Si, S and C systems (orange, magenta, light green) at similar supercooling. Size is shown as notional radius (Eq. 19). Si and S bearing systems nucleate slower than those containing O for all nuclei sizes. Whilst the functional form of these results is not important, a first order observation is that systems with C nucleate faster than others.

Simulations containing $\geq 5 \mod \%$ solute often produced liquid regions 295 enriched in the solute. This means that the system then contains at least 296 two liquids, one Fe rich and another solute rich. The formulations of CNT 297 and free energy differences applied here are not appropriate to describe these 298 conditions. Because of this we choose not to include these concentrations 299 here and focus on the cases where the liquid compositions remain consis-300 tently homogeneous. Despite not including these results, we observe the 301 same phenomena of liquid phase separation in first principles calculates of 302 smaller systems at the same conditions. 303

All simulations see non-spherical nuclei at small sizes (Fig. 3). CNT 304 typically assumes a spherical geometry (e.g. Christian, 2002) despite this 305 formulation being intended for vapour-liquid systems. Spheres are energeti-306 cally preferred due to a minimisation of surface area compared to other ge-307 ometries. Many solids exhibit preferred growth directions in crystal lattices 308 where the energetic benefit of forming a non-spherical crystal can outweigh 309 the minimised surface area of a spherical nucleus. The anisotropic nature 310 of these situations can largely be ignored (Christian, 2002) provided that a 311 consideration of geometry is still applied. In a previous study, we retained 312 the spherical treatment of CNT equations, however, the distributions pro-313 duced here via Eq. 16 from CMD simulations produce greater $\frac{\delta \Delta G}{\delta r}$ at small 314 r compared to spherical geometry which is assumed by standard CNT. 315



Figure 3: Surface area to volume ratio for sub-critical nuclei at ~400 K supercooling ($r_c > 20$ Å). Systems containing 3 mol.% Si, S and C (orange, pink and green circles) are shown as well as the spherical case (black dashed line, 3r) for comparison. Also shown are example nuclei from the C bearing system for reference. Surface area to volume ratios are similar for all systems and approach spherical before the critical size.

Whilst non-spherical small nuclei were apparent with the pure Fe system, 316 we find the departure from sphericity to be more pronounced in impure 317 systems. Despite this, as nuclei grow, they incorporate a greater number of 318 defects, randomising the preferred growth direction and becoming spherical 319 before reaching the critical size. This is true in both pure and light element 320 bearing systems, where the pure Fe systems which freeze are best described 321 as defect rich hexagonally close packed (hcp) structure (Wilson et al., 2021). 322 These defects are randomly distributed and disrupt the structure of the nuclei 323 but are able to relax from the structure to form the energetically favoured 324

phase given time. When nuclei first form, they contain few defects and so are most likely to have a single preferred growth in the direction of the basal plane as platelets, as is generally the case with hcp metals and alloys (Bergman et al., 2003). This is the mechanism which promotes dendritic growth in hcp structured materials and leads to small nuclei becoming elongate here.

For completeness we include a description of non-spherical geometries. 330 The surface area to volume ratio of these geometries follows a power law 331 decay, the same as a sphere, only with a greater initial gradient. We there-332 for apply Eq. 16 with $\Delta G = VA + \omega VB$ in place of Eq. 2, where V is 333 volume of the nuclei, A and B are proxies for the free energy contributions 334 and ω is the surface area to volume ratio $\omega = \frac{s}{V} = \alpha V^{-\beta/3}$, using α and β 335 as fitting parameters. All results here include this modification. Despite this 336 accommodation, the geometry of larger nuclei becomes increasingly spheri-337 cal towards the critical size and the temperature dependence of r_c remains 338 appropriately described by Eq. 18. 339

Through Eq. 16, nucleation rates recorded from MD simulations allow 340 the prediction of critical radius (Fig. 4) following the methods of Wilson 341 et al. (2021). For Si and S systems, the critical nuclei predicted are 10-342 100% larger than in the pure case at the same supercooling. The O bearing 343 system matches the extrapolated result of Davies et al. (2019) where nuclei 344 are $\sim 10\%$ smaller than the pure Fe case for 10 mol.% O. C is more efficient 345 at producing smaller nuclei than O. 1 mol.% C gives a similar result to 10 346 mol.% O for moderate supercooling, but is less efficient at small supercooling. 347

Extrapolation of these results to 200 K supercooling (where Huguet et al. (2018) proposed the paradox would be resolved) suggests that the small C concentrations would not reduce the barrier to nucleation compared to Fe. 3 mol.% C provides smaller critical nuclei over the 10 mol.% O case at all T studied, being ~20% smaller than the pure Fe case.



Figure 4: Critical radii sizes predicted at different δT from distributions of nuclei sizes in CMD simulations. Coloured points are the results of this study and the fits are shown as solid lines. The pure Fe results of Wilson et al. (2021) (thick black line) is shown for comparison as well as the results of Davies et al. (2019) (dashed lines). Larger critical radii than the pure Fe system are found in Si and S bearing systems, which represents a reduced nucleation rate and an increased barrier to nucleation. O and C bearing systems present increased nucleation rates relative to the pure system. Davies et al. (2019) and Wilson et al. (2021) are shown for comparison where the latter uses the same methods applied here.

Fits to the temperature dependence of r_c using Eq. 18 give the thermo-353 dynamic quantities for each system, shown in table 1. Figure 5 shows τ_0 354 where these parameters are used to evaluate z. The remaining components 355 of z are the rate at which nuclei grow (S) and the number of nucleation sites 356 present at any given time (N, unrelated to terms in EAM models). The 357 variability across compositions and the temperatures relevant to inner core 358 incubation is within several orders of magnitude, and far less than the vari-359 ance between values applied by previous studies (Christian, 2002; Huguet 360 et al., 2018; Davies et al., 2019). Holding τ_0 constant (as a mean of all sys-361 tems and temperatures) does not greatly impact the waiting time results 362 presented here and has been the approach of most applications of CNT pre-363 viously. For completeness, we choose to include a temperature dependence 364 in our calculation of Eq. 6. This is a linear fit to the exponent of all τ_0 365 $(\tau_0(T) = 10^{0.02 \times \delta T + 24.89}).$ 366

	T_m	h_f	h_c	γ	$ au_0$	ICN δT
	K	$J m^{-3} \times 10^8$		$\mathrm{J}~\mathrm{m}^{-2}$	$\mathrm{s} \mathrm{m}^{-3}$	K
Fe _{0.99} Si _{0.01}	6439	9.8	3.1×10^{-3}	1.2	2.69×10^{22}	1230(346)
$\mathrm{Fe}_{0.97}\mathrm{Si}_{0.03}$	6362	3.7	$9.6 imes 10^{-3}$	1.4	$6.43 imes 10^{20}$	2040(233)
$Fe_{0.99}S_{0.01}$	6441	47.8	1×10^{-6}	1.1	1.64×10^{21}	1837(1125)
$Fe_{0.97}S_{0.03}$	6347	31.9	1×10^{-4}	1.1	4.29×10^{20}	2131(786)
$Fe_{0.99}C_{0.01}$	6444	57.0	1×10^{-3}	1.005	2.93×10^{23}	711(55)
${\rm Fe_{0.97}C_{0.03}}$	6348	130.0	1×10^{-6}	1.005	4.63×10^{23}	612(139)
Fe^{a}	6522	$7.119^{1}0$	6.069^{-5}	1.02	5.742×10^{44}	807
${\rm Fe}_{0.90}{\rm O}_{0.10}{}^{\rm b}$	5987^{*}	$9.8 imes 10^9$	$7.05 imes 10^{-5}$	1.02	1.26×10^{45}	730

Table 1: Thermodynamic parameters fit to $r_c(T)$ for each composition tested where all evaluations for this study were carried out at 360 GPa. τ_0 varies with temperature but is given here as the value at the temperature which coincides with the supercooling required for inner core nucleation.^{*}Melting temperature is adjusted from the value at 323 GPa to agree with the pure Fe result of (Alfè et al., 2002a). ^aWilson et al. (2021), ^bDavies et al. (2019)



Figure 5: Prefactor to critical event waiting times calculated from values in table 1 and the growth rate (S) and number of nucleation sites (N) recorded from CMD simulations. Temperature dependence is a linear fit (grey line) of all data and the shaded region captures the uncertainty of this fit.

The difference in free energy between solid and liquid defines the energetic benefit to freezing the liquid. A more negative g^{sl} is seen for C bearing systems compared to the pure Fe system and those containing Si and S (Fig. 6). S and Si see a smaller free energy difference at all temperatures when compared to other systems (Fig. 6), agreeing with previous finding that partitioning is approximately evenly between solid and liquid iron (Alfè et al., 2007).



Figure 6: Comparison of $g^{sl}(T)$ from fits to $r_c(T)$ for each system studied. Dashed black line is the pure Fe case from Wilson et al. (2021) using the same methods applied here. Large differences in g^{sl} imply that the structure of nucleating material and the composition of the liquid are largely responsible for differing nucleation behaviour.

374 4. Discussion

Our results shown that nucleation rates in Fe rich liquids containing C are faster than those containing Si or S (Fig.2). Compared to the pure Fe system, critical nuclei sizes are larger in system containing Si and S and smaller in those containing C and O (Fig.4). These finding suggest that systems containing C and O should freeze at higher temperatures (lower supercooling) than a pure Fe system.

To asses whether the systems studied here might resolve the paradox, we 381 must compare the time taken to nucleate at supercooling permitted in the 382 core with the available time to nucleate in the core, the incubation time. 383 The maximum incubation time available for the inner core to form depends 384 on the undercooling available and the minimum age of the inner core. In 385 the most extreme case (referred to as the extreme case hereafter) the inner 386 core nucleated very recently and so the incubation time is the entire dura-387 tion since becoming supercooled to the present day. Huguet et al. (2018)388 estimated a maximum allowable supercooling of ~ 200 K by calculating sep-389 aration between the isentrope and melting curve at the centre of the Earth 390 whilst preserving the intersection of melting curve and temperature profile 391 at the present inner core boundary. To do this, the authors defined a melting 392 curve with Lindemann's law and the result of Anzellini et al. (2013), and an 393 isoentrope from Labrosse (2003), both populated with material properties of 394 the core. By varying the parameters of these functions within their uncer-395 tainty, the authors found that the maximum supercooling at the centre of 396

the core is ~ 200 K. This would translate to a 1 Gyr maximum incubation time if the core is cooling at ~ 200 K Gyr⁻¹.

We consider two cases, the extreme case and a more moderate version 390 where the inner core is not required to have nucleated recently. For the 400 extreme case we take a similar approach to Huguet et al. (2018) but explore 401 a greater range of input parameters in these functions. Additionally, if the 402 thermal conductivity of the core is both high and depth dependent then the 403 centre of the core can become thermally stratified (Gomi et al., 2013). In this 404 case the temperature profile of the core would not be isentropic and could 405 be isothermal at an extreme. We vary the parameters of the adiabat and the 406 effect of melting point depression on the melting curves of Alfè et al. (2002c); 407 Sinmyo et al. (2019). These melting curves are chosen to explore different 408 predicted gradients at the ICB. Figure 7 presents some of these combinations, 409 including a case showing the maximum permissible supercooling of 419 K. 410 This means that the extreme case incubation time for the core could be 2.4411 $\times 10^{35}$ s m³, more than double that used by previous studies. For a moderate 412 case, which might offer a resolution to the paradox whilst being plausible 413 to incorporate into thermal histories of the core, we take the extreme case 414 without exploring the uncertainties or melting point depression. With an 415 isothermal inner core the maximum permissible supercooling is ~ 400 K. Most 416 importantly, we consider that the incubation volume is half the radius of the 417 present inner core, implying that the remaining half (87.5% of volume) of the 418 inner core froze slowly as the core cooled. The incubation for this moderate 419

 $_{420}$ case is 1.7×10^{29} s m³, and provides a sense of the time available to not just $_{421}$ resolve the paradox, but do so with the inner core age being compatible with $_{422}$ thermal history models of the core.



Figure 7: Melting curves (solid lines) and core temperature profiles (dotted and dashed lines) with radius. Dotted (dashed) lines represent isentropic (isothermal) regions of the core. Temperature profiles are described by varying the material properties of the core used by Huguet et al. (2018) within uncertainty and also considering thermal stratification of the innermost core. Melting curves from Huguet et al. (2018) (red, blue), Alfè et al. (2002a) (pink) and Sinmyo et al. (2019) (cyan) are also applied (with varying degrees of melting point depression, causing the apparent separation) to find the largest plausible separation of temperature and melting point, and therefore supercooling, at 360 GPa whilst preserving an intersection at the ICB (solid black line).

The duration before a supercooled system will producing a critical event and freeze is presented here as waiting time (Fig. 8). As predicted by a lower nucleation rates, larger critical nuclei and less favourable thermodynamic

properties; Si and S bearing systems require significantly greater supercooling 426 than the pure iron system. In reality these systems would simply freeze via 427 alternate mechanisms, the fluctuations of composition we observe in high 428 solute concentration systems would produce Fe rich regions spontaneously. 429 This would result in an elevated nucleation rate due to a more pure Fe system, 430 meaning that freezing would occur at supercooling closer to that described 431 by the pure Fe case. In the case of FeO systems, our results confirm those of 432 Davies et al. (2019), where 730 K of supercooling is needed to nucleate the 433 inner core. 434



Figure 8: Average waiting time to observe freezing time against δT for different iron-rich liquids. Solid coloured lines are results of this study for systems containing Si (orange, maroon), S (pink, purple) and C (greens) where dark colours are higher solute concentration. Black (grey) line is the Fe (Fe_{0.9}O_{0.1}) systems from previous studies. Black dotted line represents the maximum incubation time (extreme case) available to the nucleate the inner core if the centre of the Earth is supercooled by 419 K at the present day and the core cools at 200 K Gyr⁻¹. Supercooling within the grey hatched region does not present a nucleation paradox.

⁴³⁵ Compared to all other cases considered so far, the FeC system shows a ⁴³⁶ far more efficient reduction of the nucleation barrier, partly due to a smaller ⁴³⁷ depression of the melting curve. 1 mol.% C requires 711 K (\pm 55 K) of ⁴³⁸ supercooling and 3 mol.% requires cooling to 612(\pm 139) K below melting ⁴³⁹ in order to nucleate the inner core for the extreme case, close to the 419 K of permissible supercooling of core to avoid a nucleation paradox. For the moderate case, where incubation time accounts for the core being several hundred million years old, this system requires $649(\pm 148)$ K of supercooling.

443 5. Conclusion

This study examines the effect of light elements commonly considered 444 to be present in the core on the nucleation of the inner core. Both oxygen 445 and carbon can make a reduction to the supercooling required to produce 446 the first solids in the core. The best conceivable solution from the binary 447 systems tested here is within ~ 50 K of resolving the paradox. Other higher 448 concentration ternary or higher order systems may surpass these results and 440 present possible resolutions to the paradox but are beyond the capability of 450 the methodology applied here. It should also be noted that a minimum viable 451 resolution to the paradox still presents significant challenges for the thermal 452 history of the core as it implies a very young inner core which is incompatible 453 with a high thermal conductivity core and consistent geodynamo output. We 454 find that for a more reasonable incubation time, the paradox is ~ 30 K more 455 difficult to resolve. 456

The presence of compositionally distinct regions in our simulations means a breakdown of the thermodynamic theory we apply here. If explored appropriately, these may provide alternate resolutions to the paradox; for example, through local enrichment in elements which reduce the nucleation barrier.

⁴⁶¹ 6. CRediT authorship contribution statement

⁴⁶² DA produced the original embedded atom models for Fe and FeO and pro-⁴⁶³ vided the code for fitting. AJW conducted all simulations, model fitting and ⁴⁶⁴ validation, and analysis. AJW, CD, AMW and DA wrote the manuscript.

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