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8 Water discharge and sediment flux intermittency in the fluvial
9 Escanilla Formation, Spain: Implications for changes in
10 stratigraphic architecture

11

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19 **ABSTRACT**

20 Water discharge and sediment flux variations are important parameters controlling the
21 morphodynamical behavior of rivers. Although quantitative estimates for discharge and flux
22 variability are well constrained for modern rivers, far fewer assessments of flow and sediment flux

23 intermittency in ancient fluvial systems from the rock record are available. In this study we explore
24 the relationship between water discharge, sediment flux variability and patterns of changing fluvial
25 stratigraphic architecture in the Middle Eocene Escanilla Formation, Spain. We estimate water
26 discharge intermittency factor (I_{WF}) to range from 0.03 – 0.11 in the HA intervals and from 0.10 –
27 0.32 in the LA intervals. Sediment flux intermittency factor (I_{SF}) is in the range of 0.008 – 0.01 in
28 the HA intervals and from 0.01 – 0.03 in the LA intervals. Consequently, we suggest that high
29 amalgamation (HA) intervals were most likely deposited under more intermittent and short-lived
30 intense precipitation events, while low amalgamation (LA) intervals were the result of less
31 intermittent flows spread throughout the year. Overall, our estimates are consistent with values
32 from modern ephemeral rivers typically found in arid to semi-arid climatic conditions, which is in
33 agreement with available proxy data for the Middle Eocene climatic context of the studied alluvial
34 system. Our data highlights the important connection between hydroclimate, river
35 morphodynamics and landscape evolution, and has implications to predict river flow and sediment
36 transport across the Earth’s surface in the geological past.

37

38 Keywords: Middle Eocene, Escanilla Formation, paleohydraulics, intermittency

39

40 INTRODUCTION

41 The response of river systems to changing hydroclimates is of increasing importance for predicting
42 floods hazards and its impact on growing urbanization in the context of global climate
43 perturbations. Water discharge (hereafter referred to as “discharge”) and sediment flux (hereafter
44 referred to as “flux”) in rivers are correlated to mean annual precipitation, which is linked to
45 prevalent climatic conditions [Langbein and Schumm, 1958; Syvitski and Milliman, 2007;

46 [Hansford et al., 2020](#)]. However, rivers in semi-arid to subhumid tropics display a wide range of
47 discharge variability depending on the balance between precipitation and evapotranspiration with
48 many rivers showing pronounced runoff seasonality and inter-annual variability [[Alexander et al.,](#)
49 [1999](#); [Fielding et al., 2009, 2011, 2018](#)]. Discharge and flux variability are further important as
50 they can play a key role in controlling landscape evolution and the consequent sedimentary record
51 of rivers [e.g., [Allen et al., 2013](#); [Plink-Bjorklund, 2015, 2017](#); [Fielding et al., 2018](#); [Hansford et](#)
52 [al., 2019, 2020](#); [Lyster et al., 2022](#)]. Seasonal discharge variability, in particular, has been found
53 to influence preserved stratigraphy and sedimentology and thus plays an important role in the
54 construction of fluvial bodies both in ancient and modern environments [[Fielding et al., 2018](#);
55 [Lyster et al., 2022](#)]. Discharge variability is also crucial to bedrock rivers through its role in
56 controlling bedrock river incision and continental erosion thereby driving the resulting flux of
57 sediments into depositional basins [[Lague et al., 2005](#) and references therein].
58 Sediment flux, depending on grain size, in rivers is typically more intermittent than discharge
59 variation [[Allemand et al., 2023](#)]. For instance, bedload sediments are typically transported only
60 during floods when there is enough shear stress for such sediments to be entrained and transported
61 [[Phillips and Jerolmack, 2014](#); [Phillips et al., 2018](#); [Allemand et al., 2023](#)]. The frequency of
62 discharge events and quantity of sediment transported is thus an important parameter to assess the
63 efficiency of sediment transport, and the ability of fluvial systems to convey environmental signals
64 from sources to sinks in both modern and ancient systems [e.g., [Castelltort and Van den Driessche,](#)
65 [2003](#); [Armitage et al., 2011](#); [Simpson and Castelltort, 2012](#); [Romans et al., 2016](#); [Tofelde et al.,](#)
66 [2021](#)].
67 Modern river streamflow conditions are typically described in terms of the presence or duration of
68 flow and are a fundamental metric in classifying rivers as perennial and non-perennial (intermittent

69 and ephemeral) [e.g., [Poff, 1996](#); [Bond et al., 2010](#); [Eng et al., 2015](#); [Sauquet et al., 2021](#)]. Further,
70 climate plays a primary role in influencing streamflow patterns, in addition to other factors such
71 as topography and vegetation [e.g., [Beaufort et al., 2019](#)], such that the more arid the climate,
72 higher is the probability of a fluvial system to be non-perennial [e.g., [Sauquet et al., 2021](#)]. While
73 changes in flow patterns in modern rivers can be easily recorded using gauging stations, there exist
74 currently few studies, such as e.g., [Hayden et al., \(2021\)](#), which explicitly quantify flow variability
75 or intermittency in the rock record.

76 Simply put, the temporal distribution of flow and sediment transport in a river is referred to as its
77 intermittency. Two extreme cases can be identified: a highly intermittent system is characterized
78 by repeated or prolonged intervals of no flow or sediment transport, while a non-intermittent
79 system is characterized by continuous flow or sediment transport [[Lyster et al., 2022](#)]. To study
80 sediment fluxes and basin infilling over extended geological timeframes, [Paola et al. \(1992\)](#)
81 introduced a dimensionless intermittency factor ranging from zero to one. This factor serves as a
82 means of scaling instantaneous sediment transport rates to longer term sediment fluxes or
83 depositional volumes in geological applications. The chosen averaging time should be
84 considerably longer than individual channel-forming events (instantaneous conditions), yet
85 relatively shorter than the overall geological timescale (mean conditions). The most
86 straightforward approach is to assume that flow is intermittently characterized by a sequence of
87 bankfull channel-forming conditions [[Paola et al., 1992](#)]. Consequently, discharge or flux
88 intermittency factor can be calculated relative to a longer timescale, such as the number of days in
89 a year. For instance, an intermittency of 120 days yields an intermittency factor of 0.33 or 33 % of
90 a year. The intermittency factor therefore corresponds to the cumulative occurrence of these
91 channel-forming conditions and is precisely described as the proportion of a selected time interval

92 necessary for a constant channel-forming flow to transport an equivalent amount of water or
93 sediment as the river hydrograph accomplishes during that time period [Paola et al., 1992]. The
94 lower the intermittency factor, the more intermittent the discharge or flux is relative to annual or
95 longer-term measures of water and sediment budget.

96 In this study, we for the first time explore a potential relationship between observed changes in
97 fluvial stratigraphic architecture in the Escanilla Formation, Spain, and river discharge and flux
98 variability that we have reconstructed from the sedimentary record. To perform such a quantitative
99 assessment, we estimated discharge and flux intermittency and their respective intermittency
100 factors. We further compare intermittency factors to those from modern rivers and classify the
101 Middle Eocene Escanilla rivers as either perennial or non-perennial and collectively discuss these
102 results within the framework of the observed stratigraphic changes, the paleo-hydroclimate
103 context, and implications for interpreting changes in fluvial stacking patterns recorded in alluvial
104 sedimentary successions.

105 **GEOLOGICAL BACKGROUND**

106 **The Escanilla sediment routing system**

107 The Escanilla sediment routing system, located in the Pyrenees, is preserved sediment routing
108 system, of mid- to late Eocene age (ca. 41 – 34 Ma), that linked catchment regions of the high
109 Pyrenees, via the Sis- and Gurb paleovalleys, to depositional sinks in the south Pyrenean foreland
110 Basin (Fig. 1) [Bentham et al., 1993; Labourdette & Jones 2007; Labourdette 2011; Michael et al.,
111 2013]. Extensive paleocurrent data suggests that these two paleovalley systems sourced sediments
112 from the axial zone of the Pyrenees with a confluence of these two systems in the Viacamp area
113 (Fig. 1). From there sediments were transported downstream towards the west, via the Ainsa Basin
114 [Vincent 2001; Whittaker et al., 2011; Parsons et al., 2012; Michael et al., 2013], (Fig. 1). The

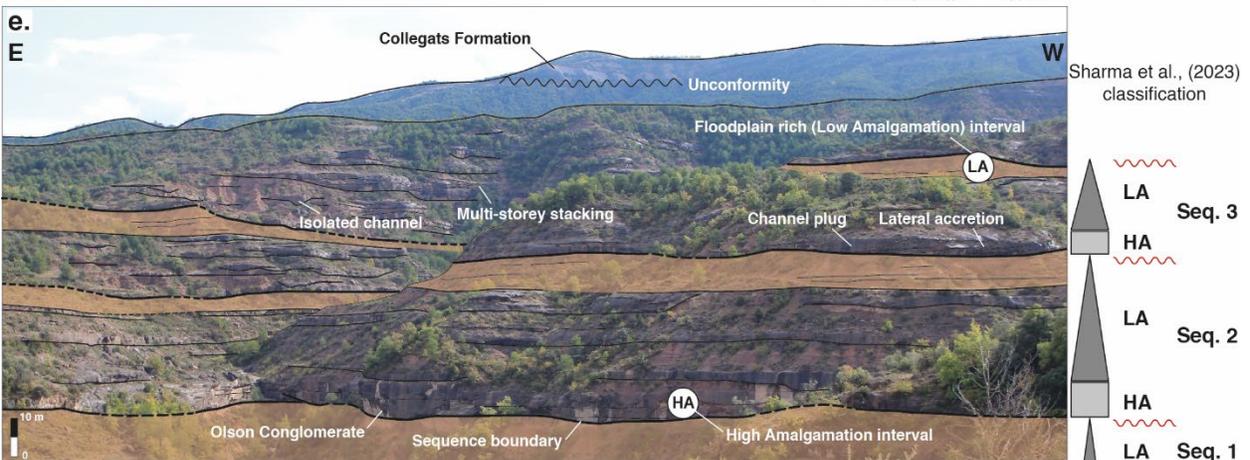
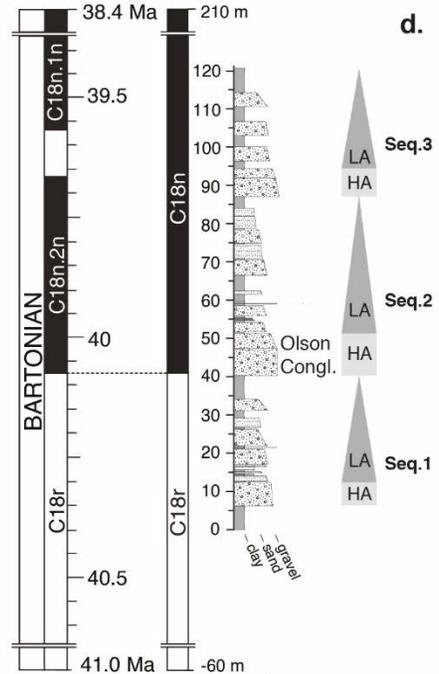
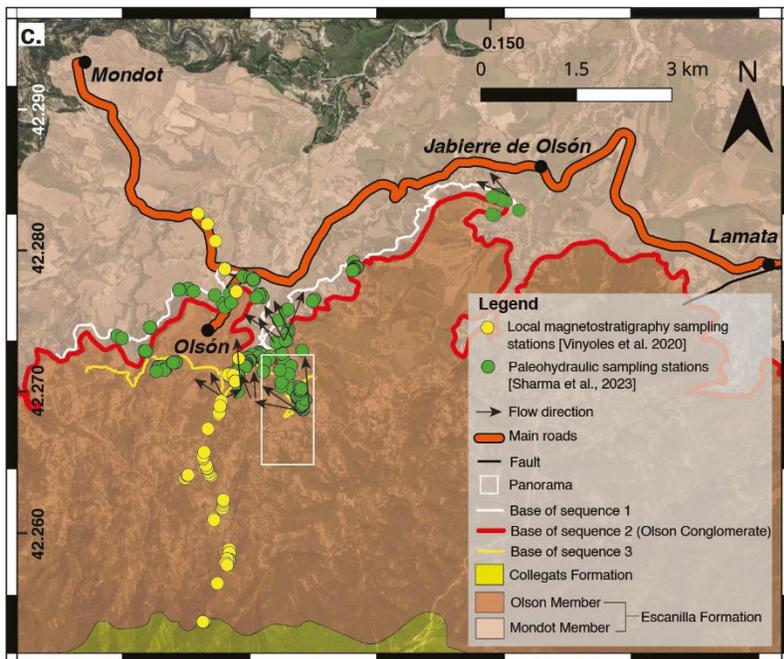
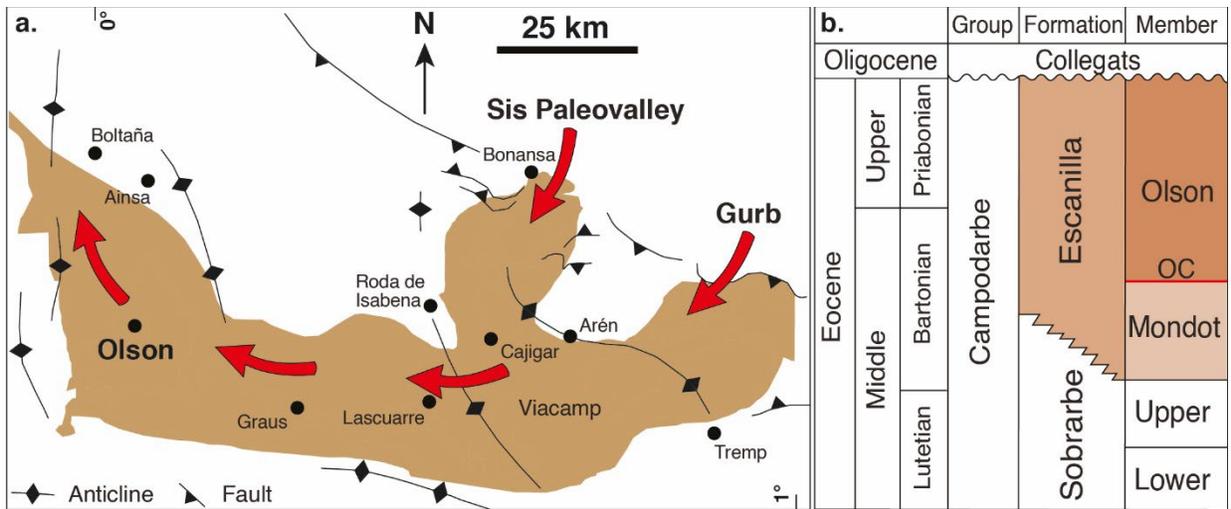
115 entire Escanilla sediment routing system has been extensively mapped within a single source-to-
116 sink framework through a range of provenance tools such as clast lithologies, heavy minerals, U-
117 Pb geochronology of detrital zircons, apatite fission track analysis, paleocurrent analysis, magneto-
118 and biostratigraphy, and has been explained in detail by [Michael et al. \(2013, 2014b\)](#) and
119 references therein.

120 **The Escanilla Formation at Olson – fining upward sequences**

121 Within the southern Ainsa Basin, the Escanilla Formation has a maximum preserved thickness of
122 ~1000 m and is divided into the Mondot and Olson Members [[Bentham et al., 1992, 1993](#); [Dreyer
123 et al., 1992](#); [Kjemperud et al., 2004](#); [Labourdette and Jones 2007](#); [Labourdette 2011](#)]. Previously,
124 several stratigraphic sequences consisting of laterally amalgamated and vertically stacked channels
125 have been described by [Labourdette and Jones \(2007\)](#), and [Labourdette \(2011\)](#). This study focuses
126 on 3 fining-upward sequences at Olson, recently described by [Sharma et al., \(2023\)](#), with each
127 sequence having a thickness around 35 – 45 m. Each fining-upward sequence consists of a high
128 amalgamation (HA) interval which is defined as a 5 to 12 m thick and 600 to 2000 m wide complex
129 of laterally and vertically amalgamated channel bodies in multiple stories, and a low amalgamation
130 (LA) interval which is defined as a floodplain-dominated interval consisting of isolated channel
131 bodies (less amalgamated) that are 2 to 4 m thick and 100 to 500 m wide [[Sharma et al., 2023](#)].
132 Recent work in the Middle Eocene fluvial Escanilla Formation, Spain, has documented cyclical
133 variations in instantaneous water discharge and bedload sediment flux relative to changes in
134 stratigraphic architecture, i.e., from high amalgamation (HA) to low amalgamation (LA) intervals
135 within several fining upward sequences is indicative of an upstream climate control on fluvial
136 stacking pattern [[Sharma et al., 2023](#)].

137 **Regional climate during the Middle Eocene**

138 The Escanilla Formation at Olson encompasses the Middle Eocene Climatic Optimum (MECO),
139 a global warming event at ~ 40 Ma. Geochemical proxies from the Escanilla Formation suggest
140 regional climatic conditions in the south-central Pyrenees to be dry, arid, and devoid of much
141 vegetation [Sharma et al., 2023]. In other localities more to the East of the Ebro Basin,
142 (northeastern Spain), other proxies such as palynological, pollen taxa and floral diversity
143 [Cavagnetto and Anadón 1996; Haseldonckx, 1972] suggest warm and humid climatic conditions.
144 For instance, Middle Bartonian vegetation from the eastern Ebro basin was characterized by a
145 diverse mangrove swamp-type vegetation along the coast which subsequently disappeared by the
146 Priabonian [Cavagnetto and Anadón 1996]. Such differences in regional climate could be due to a
147 phase of climate transitioning, expressed differently in different regions, from a warm tropical
148 Early Eocene Climatic Optimum to a colder and arid early Oligocene [López-Blanco et al., 2000;
149 Cantalejo et al., 2015]. Collectively, this makes the Escanilla Formation at Olson an ideal locality
150 to test for the link between discharge, transport intermittency and different stratigraphic stacking
151 patterns and architecture under greenhouse conditions of the Middle Eocene.



153 Figure 1. (a) Map of the Escanilla paleo-sediment routing system in the southern Pyrenees, Spain, and
 154 showing the main tectonic structures. Figure modified after Michael et al. (2014a). Red arrows mark the
 155 water discharge and sediment transport direction of the Escanilla system away from the source regions of
 156 Sis- and Gurb paleovalleys. (b) Lithostratigraphic framework of the Escanilla Fm at Olson consists of two
 157 main Members – the Mondot and the Olson Member with the Olson Conglomerate (OC; red line) at the
 158 transition between the two Members. (c) Geological map of the southern Ainsa basin encompassing the
 159 Escanilla Formation around the village of Olson. The ‘Olson Conglomerate (OC)’ is marked in red as a
 160 basin wide, laterally extensive amalgamated channel body lying in-between the Mondot and Olson
 161 Members of the Escanilla Formation. This map was prepared using QGIS Desktop 3.22.8 ([https:// qgis.
 162 Org/ en/ site/](https://qgis.org/en/site/)). (d) Studied composite section of the Escanilla Fm with the local magnetostratigraphic
 163 interpretation by Vinyoles et al. (2020) correlated to the Geomagnetic Polarity Time Scale (GPTS 2020)
 164 [Ogg, 2020]. The 90 thickest normal magnetozone C18n in the local magnetostratigraphic interpretation
 165 includes C18n.1n, C18n.1r, and C18n.2n. I Panorama of the studied sequences 2, and 3 (sequence 1 lies
 166 below). At the base of the panorama lies a thick floodplain dominated interval terminating the LA interval
 167 of sequence 1, and above which lies the high amalgamation (HA) interval corresponding to the OC. Above
 168 the HA interval lies the floodplain dominated low amalgamation (LA) interval.

169

170 METHODS

171 The concept of discharge intermittency can most simply be expressed through a discharge
 172 intermittency factor (I_{WF}) which has been defined by Paola et al., (1992) as:

$$173 \quad I_{WF} = \frac{\Sigma Q_w}{Q_{w(cf)} \Sigma t} \quad (1)$$

174 Where, Q_w is the total water discharge over the averaging time period, such as a year, $Q_{w(cf)}$ is the
 175 instantaneous channel-forming water discharge, and Σt is the averaging time period (e.g., 1 year).

176 Following Eq. 1, flux intermittency factor (I_{SF}) can be expressed as:

177
$$I_{SF} = \frac{\Sigma Q_s}{Q_{s(cf)} \Sigma t} \quad (2)$$

178 Where, Q_s is the total sediment flux over the period of interest and $Q_{s(cf)}$ is the instantaneous
179 channel forming sediment flux. Σt is the timespan equal to 1 year [Paola et al., 1992].

180 These calculations require estimates for both channel forming discharges and longer-term water
181 budgets, and similarly, sediment transport capacities and longer-term sediment flux rates. For
182 instantaneous discharge and flux conditions in the Escanilla Formation we use the recently
183 published palaeohydrological reconstructions for the HA and LA units of Sharma et al., (2023),
184 which are based on field measurements of channel geometries and sediment caliber. However,
185 drainage area, precipitation, and total volumetric sediment flux estimates are required to
186 approximately estimate the total water and sediment budget available to the Escanilla system.

187

188 **Drainage area estimates**

189 Catchment area of ancient sediment routing systems are often hard to accurately constrain due to
190 tectonic changes and erosion of the hinterland [Eide et al., 2018; Brewer et al., 2021]. However,
191 the Escanilla system's source area is relatively well-constrained: A total drainage area upstream
192 of Olson, based on the mapping of the Escanilla system by Michael et al. (2014a), was estimated
193 to be in the range of 2500 – 5500 km² with an average value of approximately 4000 km². This
194 estimate is similar to that proposed by Brewer et al., (2021) for the Escanilla system. The value
195 includes a combined average area of approximately 2050 km² from the Sis and Gurb catchment
196 areas (2088 km² is suggested by Michael et al. (2014a)) while the downstream region until Olson
197 constitutes an area of approximately 1950 km².

198 **Total water budget and water discharge estimates**

199 ***Total water budget***

200 Total water budget for the Escanilla Fm was estimated using two end members of mean annual
201 precipitation rates ($\sim 0.3 \text{ m yr}^{-1}$ and $\sim 1.0 \text{ m yr}^{-1}$). In the first instance, [Sharma et al., 2023](#) estimated
202 mean annual precipitation (MAP) (Fig. 2), using the chemical index of weathering (CIW) of
203 paleosol samples from the Escanilla Formation, which gave values ranging between 0.25 m yr^{-1}
204 and 0.57 m yr^{-1} (average value of 0.33 m yr^{-1}). It is important to note here that these MAP values
205 are based only on samples from the LA interval due to the absence of floodplain in the HA
206 intervals. Multiplying average total drainage area of 4000 km^2 by average mean rainfall results in
207 an average total water budget of $13 \times 10^8 \text{ m}^3 \text{ yr}^{-1}$ with minimum and maximum values of $7 \times 10^8 \text{ m}^3$
208 yr^{-1} and $31 \times 10^8 \text{ m}^3 \text{ yr}^{-1}$ respectively. These values are maxima because they do not include water
209 loss due to infiltration or evapotranspiration but are reasonable first-order estimates.

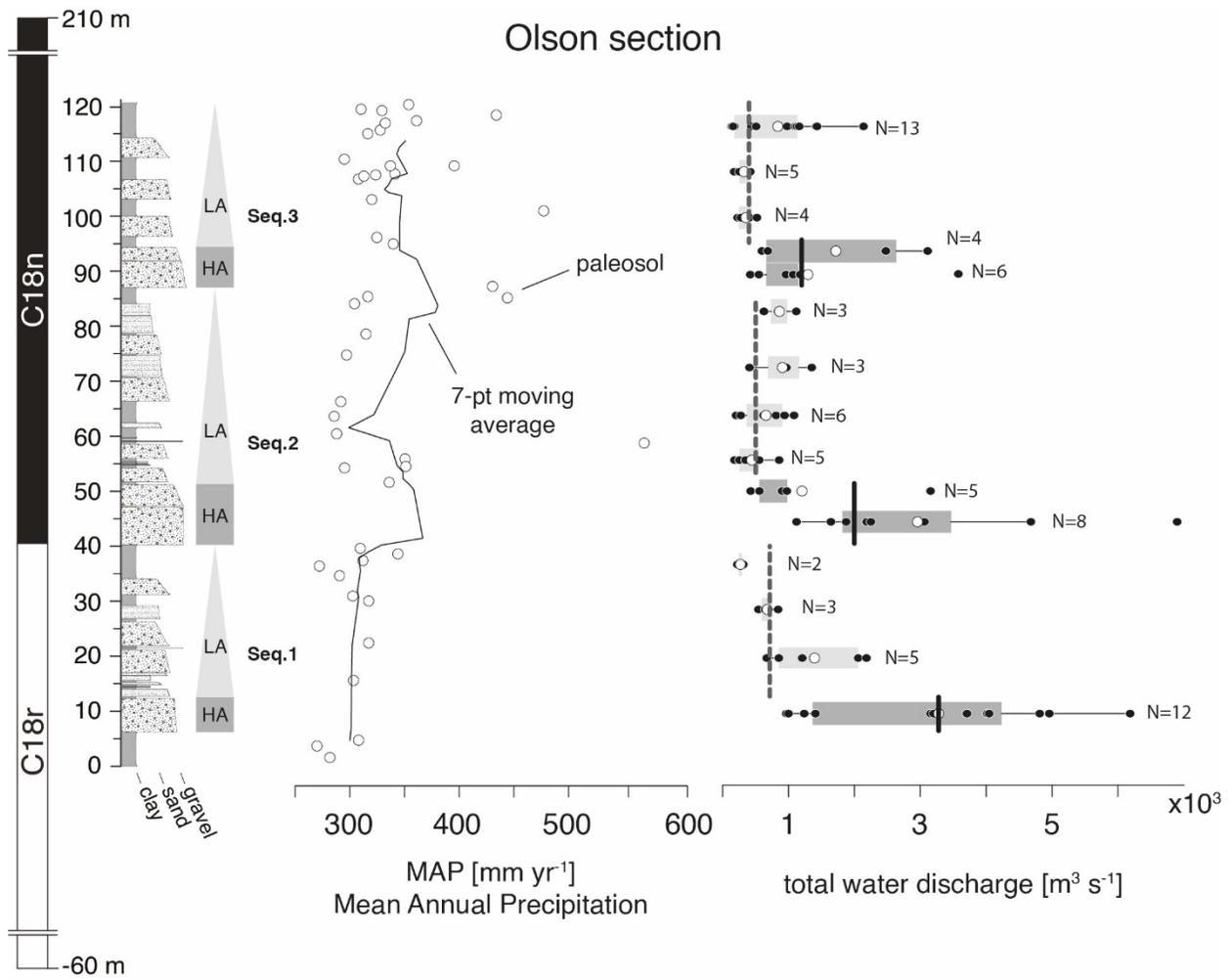
210 In the second instance, Eocene MAP estimates for northern Spain predicted by [Tardif et al. \(2021\)](#)
211 can be used to estimate the total water budget. These MAP estimates are in the range of 0.8 m yr^{-1}
212 1 to 1.4 m yr^{-1} with an average value of 1.1 m yr^{-1} equivalent to an average total water budget of
213 $4 \times 10^9 \text{ m}^3 \text{ yr}^{-1}$ with minimum and maximum values of $2 \times 10^9 \text{ m}^3 \text{ yr}^{-1}$ and $7 \times 10^9 \text{ m}^3 \text{ yr}^{-1}$ respectively.

214

215 *Water discharge estimates*

216 Detailed water discharge, in $\text{m}^3 \text{ s}^{-1}$, for the three sequences at Olson was estimated by [Sharma et](#)
217 [al., \(2023\)](#), using a combination of channel dimensions such as bankfull depth and width, and
218 paleoslope estimates (Fig. 2). HA intervals have an average discharge rate of $2200 \pm 550 [\text{m}^3 \text{ s}^{-1}]$
219 (average value \pm standard error, $N = 45$) in HA intervals, and a discharge rate of $700 \pm 200 [\text{m}^3 \text{ s}^{-1}]$
220 1 ($N = 49$) in the LA intervals which corresponds to a 3-fold increase of volumetric discharge
221 during HA intervals. However, it is important to note that these estimates represent instantaneous

222 bank full flow conditions (channel forming conditions) and do not represent average annual flow
 223 conditions.



224
 225 Figure 2. Stratigraphic log of the studied section at Olson and depicting the three fining upward sequences,
 226 each consisting of a high amalgamation (HA) and low amalgamation (LA) interval. Also shown are the
 227 mean annual precipitation (MAP) and total water discharge estimates for the Escanilla Formation. Black
 228 vertical bars denote the average value in HA intervals while grey bars denote the average value in LA
 229 intervals.

230 **Estimating discharge intermittency factor**

231 Discharge estimates, in $\text{m}^3 \text{s}^{-1}$, for the three sequences at Olson from both end members, were first
232 converted into $\text{m}^3 \text{day}^{-1}$. Discharge intermittency (Q_{WI}) was then calculated by dividing the average
233 total available water budget by discharge estimates in $\text{m}^3 \text{day}^{-1}$ to obtain the intermittency ratio as
234 the number of days per year that channel forming discharge would be required to equal the
235 estimated annual water budget. Discharge intermittency factor (I_{WF}) was calculated relative to the
236 number of days in a year.

237 **Total sediment budget and sediment flux estimates**

238 Bankfull volumetric sediment flux and the resulting total sediment flux for the Escanilla Formation
239 was calculated using two different approaches involving bedload and sand-fraction sediment flux
240 estimates.

241 ***Total sediment budget***

242 The total volumetric sediment flux available in the Escanilla system during the 41.6 – 39.1 Ma
243 time interval has previously been estimated by [Michael et al. \(2013\)](#) using an approach
244 extrapolating the outcrop extent of the sediment routing system, where linear interpolation of
245 cross-sectional areas in the downstream direction is used to constrain the cumulative depositional
246 volume. The most significant uncertainty acknowledged by [Michael et al. \(2013\)](#) arises from the
247 estimated cross-sectional width of the Escanilla system fairway. This mass balance framework
248 resulted in a total depositional volume of $246000 \pm 20000 \text{ m}^3 \text{ yr}^{-1}$, a value range which we use for
249 this study.

250

251 ***Estimating bedload sediment flux and resulting total sediment flux***

252 Bedload sediment flux for the gravel grain size fraction was estimated by [Sharma et al., 2023](#) (Fig.
253 4). Since gravel fraction makes up 25 % of the total sediment flux in the Ainsa area of the Escanilla

254 system in the Ainsa Basin, as documented by [Michael et al. \(2013\)](#) using a modelling approach
255 involving transformation of volumetric depositional volumes into a mass balance framework,
256 bedload sediment flux was accordingly used to calculate the total sediment flux.

257 ***Estimating sand-fraction sediment flux and resulting total sediment flux***

258 Sand-fraction sediment flux was estimated using the model of [Engelund and Hansen \(1967\)](#). Non-
259 dimensional sediment flux per unit width (q_t^*) was calculated as:

$$260 \quad q_t^* = (0.05/C_f) \times (\tau_*)^{2.5} \quad (1)$$

261 Where C_f is the friction factor and is calculated as:

$$262 \quad C_f = (gH_{bf}S)/U^2 \quad (2)$$

263 Where g is gravitational acceleration, H_{bf} is bankfull flow depth, S is riverbed slope and U is flow
264 velocity. These values have been previously estimated for the Escanilla Formation by [Sharma et](#)
265 [al., \(2023\)](#).

266 Using the model of [Engelund and Hansen \(1967\)](#), total nondimensional shear stress (τ_*) is related
267 to bankfull flow depth (H_{bf}), slope (S), submerged specific sediment density ($R = 1.65$ for quartz
268 in water) and median grain size (D_{50}) as:

$$269 \quad \tau_* = (H_{bf}S)/(RD_{50}) \quad (3)$$

270 Since, $q_t^* = Q_s/W(RgD_{50}^3)^{0.5}$ [[Engelund and Hansen, 1967](#)], Bankfull sediment flux (Q_s) was then
271 calculated using Eq. 4 as:

$$272 \quad Q_s = q_t^* \times W \times (RgD_{50}^3)^{0.5} \quad (4)$$

273 Where W is the flow width. A median grain size of 0.25 mm (fine-medium grain size fraction) was
274 considered while calculating the sand-fraction sediment flux. Channel-belt widths estimated by
275 [Sharma et al. \(2023\)](#), using the relationship $W = 8.8H_{bf}^{1.82}$ [[Bridge and Mackey, 1993](#)], where used
276 to calculate Bankfull sediment flux (Q_s). Similar to the gravel fraction, sand-fraction also makes

277 up 25 % of the total sediment flux [Michael et al., 2013] and values were accordingly used to
278 calculate the resulting total sediment flux in the Ainsa Basin.

279 **Estimating sediment flux intermittency factor**

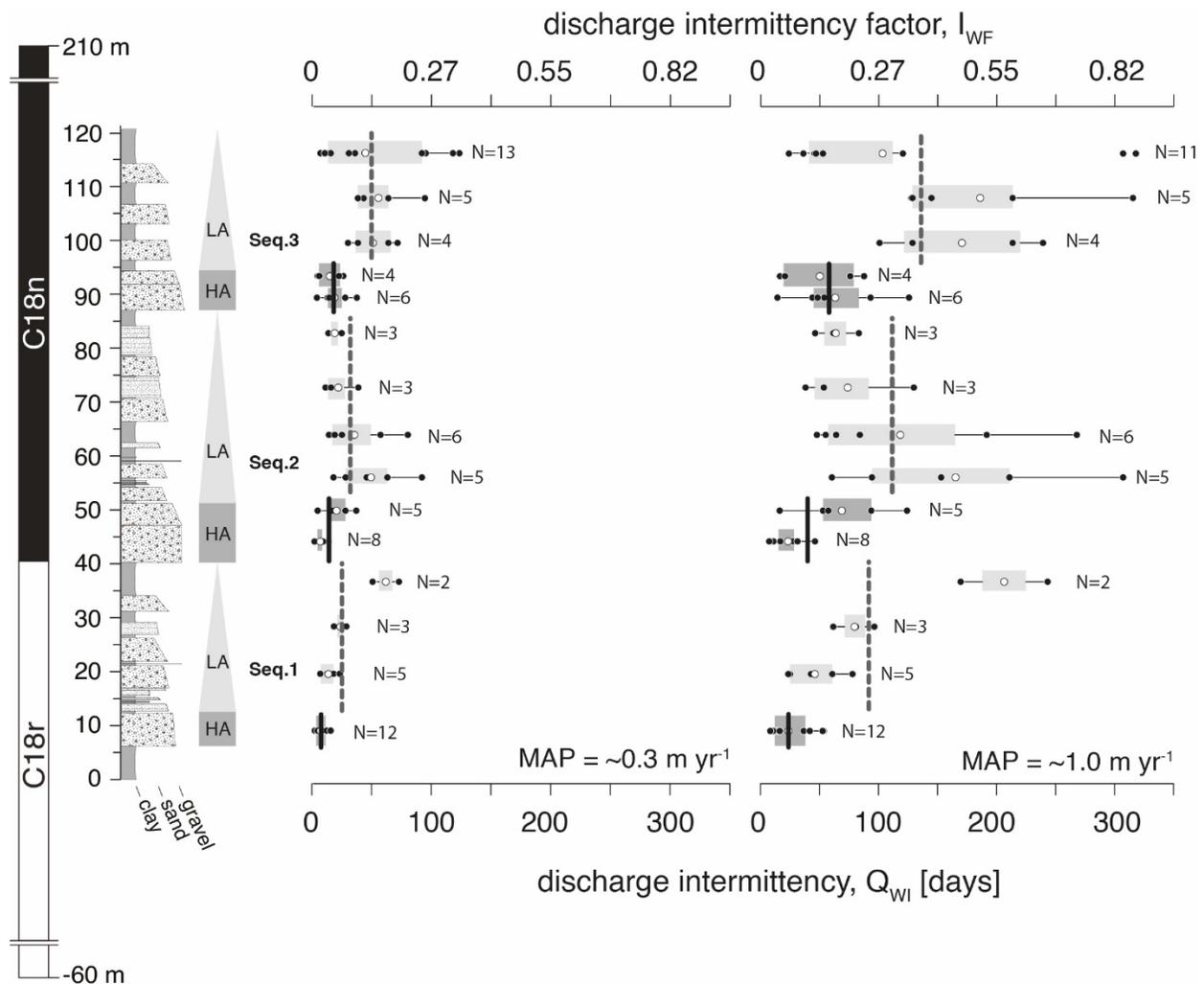
280 Total sediment flux estimates, in $\text{m}^3 \text{s}^{-1}$, from both approaches (bedload- and sand-fraction) were
281 first converted into $\text{m}^3 \text{day}^{-1}$. Flux intermittency (Q_{SI}) for each approach was then obtained by
282 dividing the total available annual sediment budget by the sediment flux in $\text{m}^3 \text{day}^{-1}$ to obtain the
283 flux intermittency, expressed in terms of the number of days in a year. Flux intermittency factor
284 (I_{SF}) was then estimated using the same approach used to estimate discharge intermittency factor.
285 Uncertainty on all results reported in this study consist of the standard error of the mean (SE)
286 calculated as $SE = \frac{SD}{\sqrt{n}}$, where SD is the standard deviation and n is sample size. Uncertainty
287 propagation was carried out using the uncertainties package on Python (Spyder version 4.0.1),
288 which is a free, cross-platform program that transparently handles calculations with numbers
289 involving uncertainties.

290 **RESULTS**

291 **Water discharge intermittency factor (I_{WF})**

292 Bankfull water discharge intermittency, estimated using the first end member ($\sim 0.3 \text{ m yr}^{-1}$ MAP),
293 in the HA intervals is 12 ± 2 days (average value \pm standard error, $N = 35$), equivalent to an
294 intermittency factor of 0.03 or 3 % of a year, while LA intervals have an intermittency of 39 ± 4
295 days ($N = 49$), equivalent to an intermittency factor of 0.10 or 10 % of a year and represent a 3-
296 fold increase in intermittency factor in the LA intervals over HA intervals (Fig. 3), again noting
297 that an increase in the numerical value of the intermittency factor (I_{WF}) implies a decrease in the
298 temporal intermittency of water discharge – i.e., water flow is relatively more constant through the
299 year in the LA intervals.

300 Discharge intermittency, based on the second end member ($\sim 1.0 \text{ m yr}^{-1}$ MAP), in the HA intervals
301 is 40 ± 5 days ($N = 35$), equivalent to an intermittency factor of 0.11 or 11 % of a year, while LA
302 intervals have an intermittency of 119 ± 13 days ($N = 47$), equivalent to an intermittency factor of
303 0.32 or 32 % of a year and represents an almost 3-fold increase in discharge intermittency factor.
304 Overall, discharge intermittency values from both end-members suggest that flow during HA
305 intervals was more intermittent (likely concentrated within a few days in a year) while flow during
306 LA intervals was less intermittent and more likely to be characterized by non-bankfull perennial
307 flow. Any increase in precipitation in the source area would result in a higher water budget
308 translating overall into a higher discharge intermittency factor (I_{WF}), i.e., less intermittent flow.
309 The Escanilla system is consistent with lower discharge intermittency in temporal sense under
310 increased precipitation and supports evidence from modern rivers that climatic conditions such as
311 the amount and timing of precipitation have a first-order control on flow variability [e.g., [Buttle et](#)
312 [al., 2012](#); [Eng et al., 2015](#)]. In contrast higher flow intermittencies (i.e., a few days a year) in HA
313 intervals more typical of ephemeral (intermittent) streams where flows are typically short, intense,
314 and associated with periods of intense rainfall [e.g., [Piccard and High, 1973](#); [Mabbut, 1977](#)].

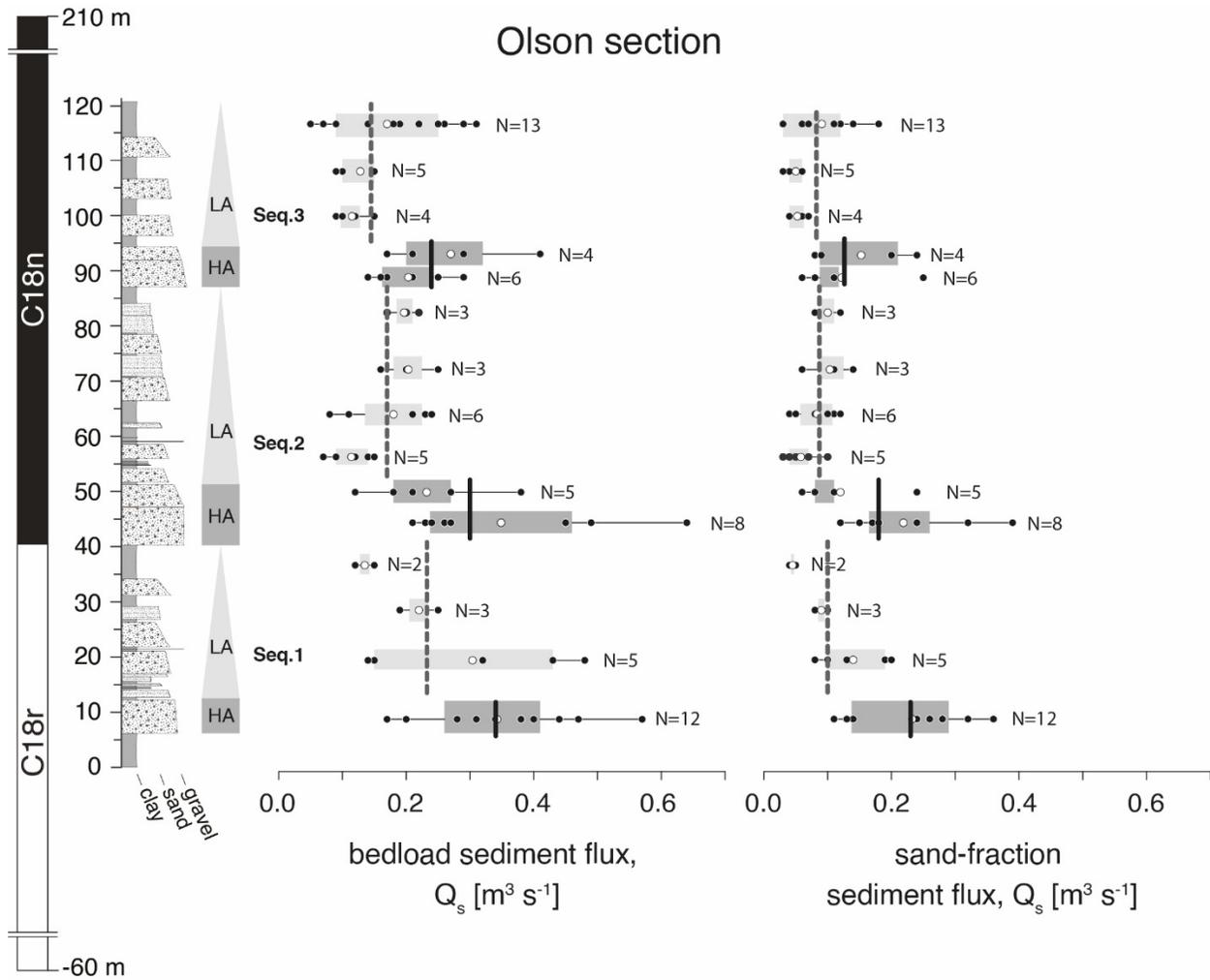


315
 316 Figure 3. Discharge intermittency (Q_{WI}) and intermittency factor (I_{WF}) estimates from two end-members
 317 having MAP of $\sim 300 \text{ mm yr}^{-1}$, and $\sim 1000 \text{ mm yr}^{-1}$. Values are strongly dependent on precipitation rate
 318 such that the more water is available, the less intermittent the fluvial system becomes. Black vertical bars
 319 denote the average value in HA intervals while grey bars denote the average value in LA intervals.

320 Sediment flux estimates

321 Non-dimensional unit sediment flux, q_t (Eq. 1), based on the model of [Engelund and Hansen](#)
 322 ([1967](#)), was estimated to be 63.5 ± 21 (average value \pm standard error, $N = 35$) for the HA intervals
 323 and 61 ± 20 ($N = 49$) for the LA intervals. This would imply bankfull sediment flux using the sand
 324 fraction (Eq. 4) for HA intervals to be $0.2 \pm 0.06 \text{ m}^3 \text{ s}^{-1}$ and $0.1 \pm 0.02 \text{ m}^3 \text{ s}^{-1}$ for the LA intervals,

325 i.e., a 2-fold increase in sediment flux during HA intervals. This compares well to the 1.5-fold
 326 increase in bedload sediment flux in the HA intervals recently documented by [Sharma et al. \(2023\)](#)
 327 (Fig. 4).

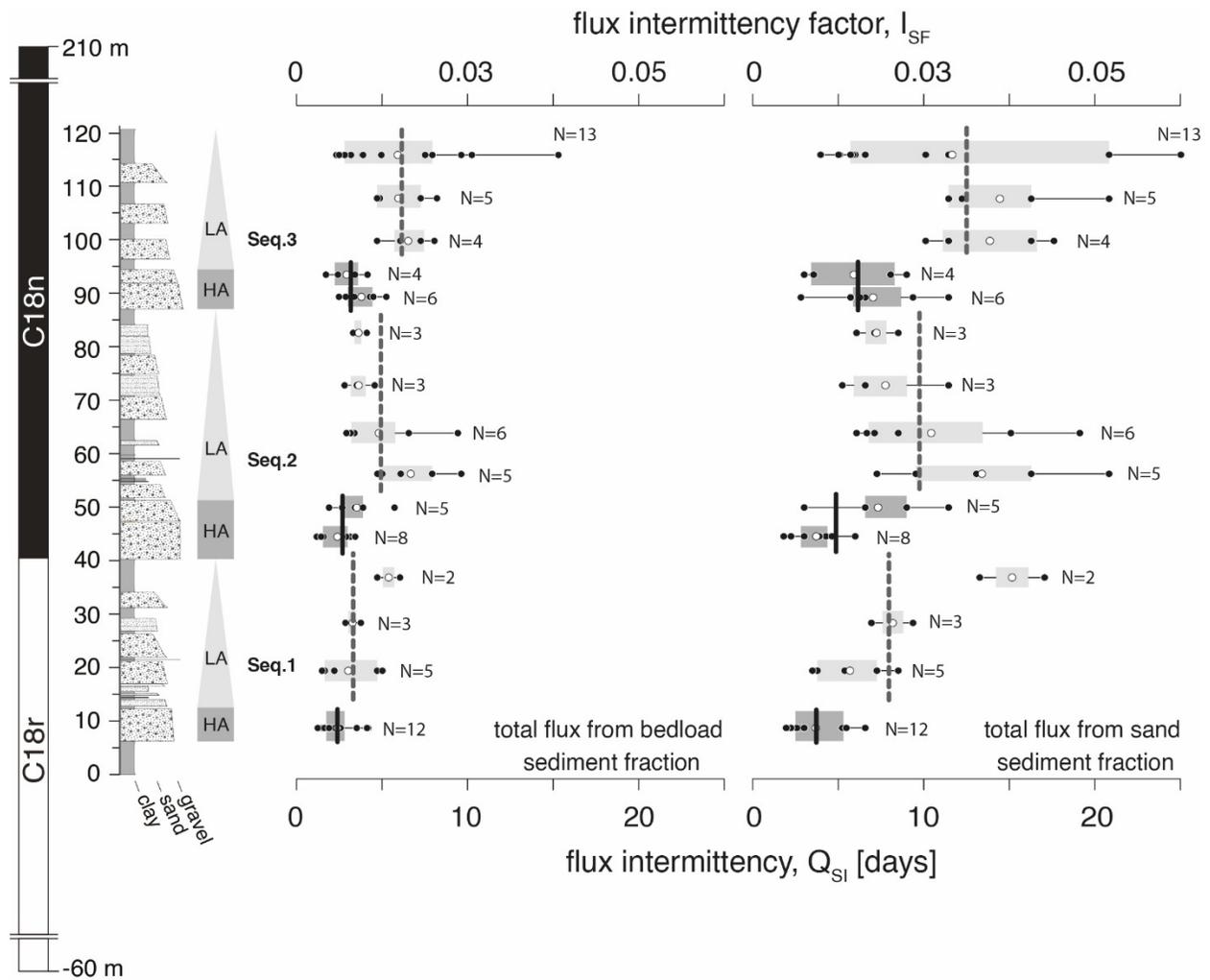


328
 329 Figure 4. Bedload sediment flux calculated by [Sharma et al. \(2023\)](#), using the Meyer-Peter and Muller
 330 equation, and sand-fraction sediment flux calculated using the [Engelund and Hansen \(1967\)](#) model. Black
 331 vertical bars denote the average value in HA intervals while grey bars denote the average value in LA
 332 intervals.

333 **Sediment flux intermittency factor (I_{SF})**

334 Sediment flux intermittency, based on bedload flux, in the HA intervals is 3 ± 0.2 days (average
335 value \pm standard error, $N = 35$), equivalent to an intermittency factor of 0.008 or 0.8 % of a year,
336 while LA intervals have an intermittency of 5 ± 0.4 days ($N = 49$), equivalent to an intermittency
337 factor of 0.01 or 1 % of a year (Fig. 5).

338 Intermittency based on sand-fraction sediment flux, in the HA intervals is 5 ± 0.5 days ($N = 35$),
339 intermittency factor of 0.01 (1 % of a year), while LA intervals have an intermittency of 11 ± 0.8
340 days ($N = 49$) i.e., an intermittency factor of 0.03 (3 % of a year) (Fig. 5). These data suggest that
341 events moving sediment through the Escanilla system happened more intermittently than water
342 transport and likely occurred on just a few days in a year. Again, HA intervals are reconstructed
343 to have lower sediment flux intermittency factor (i.e., more intermittent sediment transport) than
344 LA intervals.



345
 346 Figure 5. Sediment flux intermittency (Q_{SI}) and intermittency factor (I_{SF}) based on total flux estimated from bedload-
 347 fraction, and sand-fraction sediment flux. Black vertical bars denote the average value in HA intervals while
 348 grey bars denote the average value in LA intervals.

349
 350 **DISCUSSION**

351 These results provide new insights into how water discharge and sediment transport evolved
 352 relative to alluvial channel stratal architecture in the Middle Eocene Escanilla Formation. We find
 353 that discharge and flux intermittency factor is systematically lower in HA intervals and higher in
 354 LA intervals (Fig. 3, 5). Given that we do not have evidence for very large changes in mean annual

355 rainfall during this period (e.g., Fig. 2), we instead hypothesize these could be due to changes in
356 the distribution of rainfall and storminess at these timescales.

357 According to paleogeographic reconstructions from [Hay et al. \(1999\)](#), the Pyrenees were situated
358 approximately at 35° N during the Eocene period. This particular latitude is recognized to be
359 vulnerable to climate changes induced by astronomical factors with some studies suggesting that
360 orbital variations could impact precipitation and evaporation patterns at such latitudes [[Cantalejo](#)
361 [et al., 2014](#)]. For instance, in the Middle Eocene (Late Lutetian) Ainsa System submarine fan
362 deposits, cyclical variations in relatively coarser and finer-grained sediments reflects a strong
363 relation to the 400-kyr eccentricity cycles [[Cantalejo et al., 2014; 2020](#)]. In the continental
364 Escanilla Formation, 400-kyr eccentricity cycles have recently been proposed to influence
365 sediment depositional patterns from HA to LA intervals due to cyclical variations in sediment flux
366 and water discharge [[Sharma et al., 2023](#)].

367 These new intermittency results indicate that sediments during the deposition of HA intervals were
368 on average transported within 4 days, most likely suggesting that HA intervals were deposited
369 under concentrated ‘bursts’ of sediment flux probably under high-frequency convective storms
370 over the Pyrenees during summertime [[Callado and Pascual, 2005; Llasat et al., 2021](#)], while
371 sediment transport in LA intervals took on average 8 days but represent a much larger spread in
372 the number of days over which sediments were transported (Fig. 5).

373 Collectively, this suggests a strong link between eccentricity cycles, discharge and flux rates, and
374 their respective intermittencies in the Escanilla Formation such that eccentricity maxima most
375 likely corresponds to higher flux and discharge, and potentially more stormy conditions that
376 resulted in concentrated flow events (more intermittent flow) during the deposition of HA

377 intervals. Contrary to this, eccentricity minima most likely corresponds to lower discharge and
378 flux in the Escanilla system under calm climatic conditions with less intermittent flow conditions.

379

380 **Sediment flux intermittency (I_{SF}) to water discharge intermittency (I_{WF}) ratio**

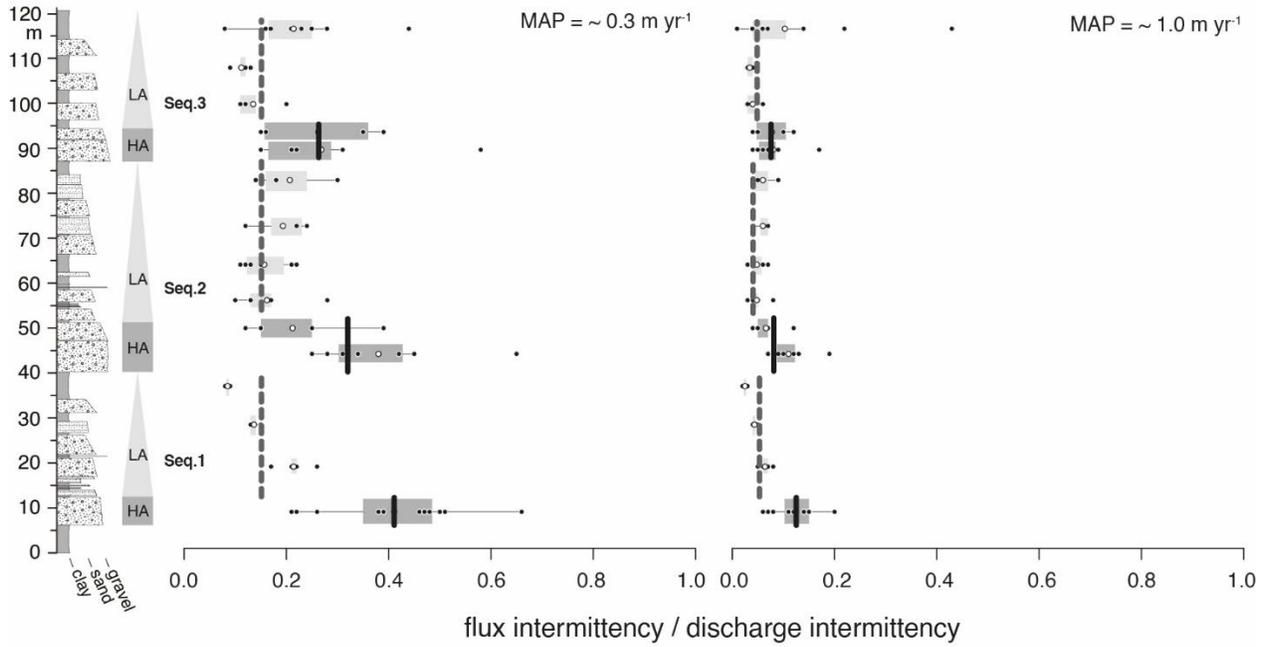
381 For an MAP value of $\sim 0.3 \text{ m yr}^{-1}$, the ratio of sediment flux intermittency factors (from bedload
382 flux) to water discharge intermittency is 0.33 and 0.17 in the HA and LA intervals, i.e., 33% and
383 17% of the water discharge intermittency factor (Fig. 6). For the same MAP, the ratio of sediment
384 flux intermittency factor (from sand fraction sediment flux) to water discharge intermittency factor
385 is 0.52 and 0.43 in the HA and LA intervals, i.e., 52% and 43% of the water discharge intermittency
386 factor (Fig. 6).

387 For an MAP value of $\sim 1.0 \text{ m yr}^{-1}$, we obtain similar trends: 10% and 5% of the water discharge
388 intermittency factor for HA and LA intervals (Fig. 6). And 16% and 13% of sediment flux
389 intermittency for HA and LA intervals (Fig. 6).

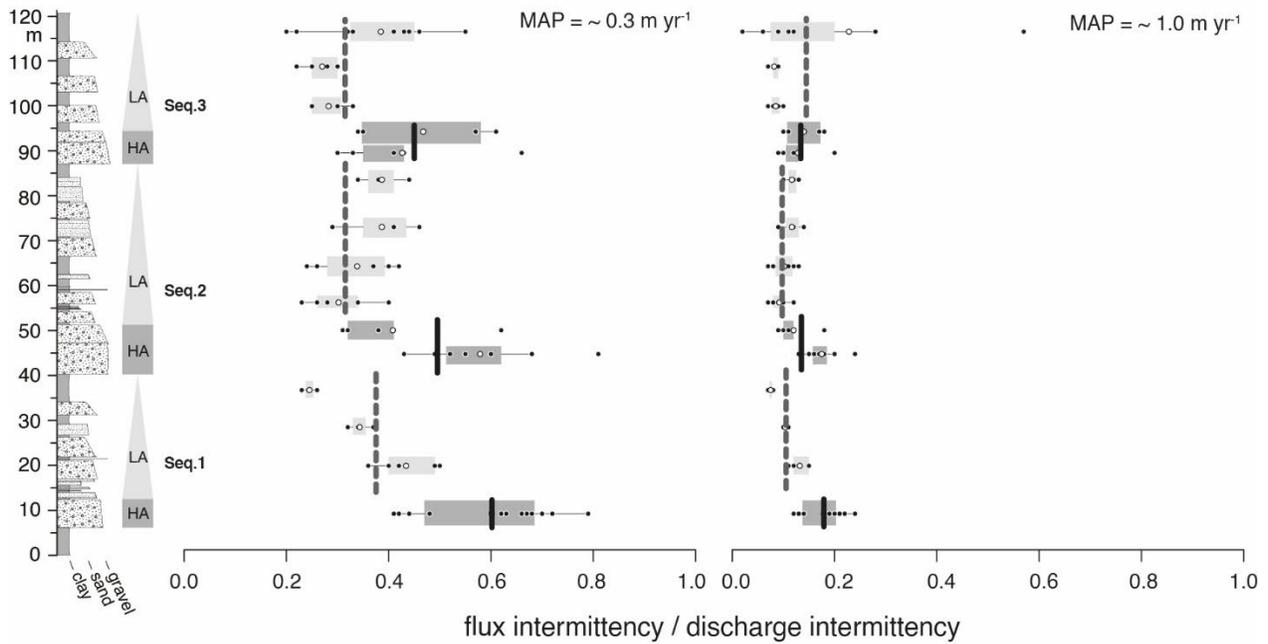
390 This implies that sediment transport intermittencies vary in proportion to the assumed rainfall such
391 that during lower rainfall rates, discharge and flux intermittency are similar in value since the
392 infrequent discharge and sediment transport events happen together. However, as rainfall
393 increases, the total water budget also increases resulting in flow events that do not transport any
394 sediments. The resulting sediment transport intermittency factor, in this case, therefore, constitutes
395 only a small proportion of the discharge intermittency factor.

396 These results also demonstrate how upstream environmental drivers (precipitation) can be
397 predominant factor that determines how sediments are transported in fluvial systems and reinforces
398 the idea that upstream climatic factors play an important role in how sediments are mobilized, and
399 how they influence the resulting depositional architecture (c.f. [Sharma et al. \(2023\)](#)).

BEDLOAD SEDIMENT FLUX



SAND-FRACTION SEDIMENT FLUX



401

402 Figure 6. Ratio of sediment flux intermittency, based on bedload and sand-fraction flux estimates, and water

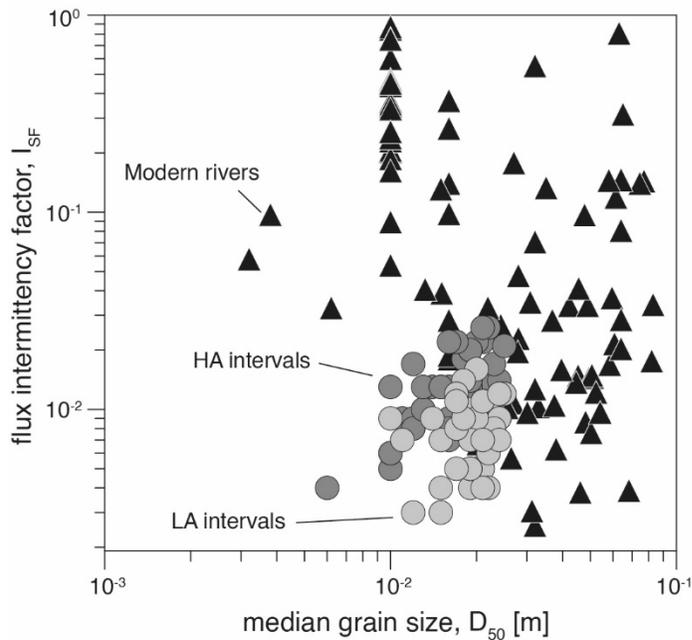
403 discharge intermittency

404

405 **How do our results compare to modern rivers?**

406 To contextualize our findings, we compare them to the flux intermittency factor of 94 gravel
407 bedded modern rivers, having grain size ranging from 0.003 – 0.08 m, with the flux intermittency
408 factor from the HA and LA intervals deduced in this study (Fig. 6). Modern rivers from climatic
409 environments with MAP ranging from 0.4 – 1.2 m yr⁻¹ were selected from the dataset of [Hayden](#)
410 [et al. \(2021\)](#) (see supplementary material).

411 Sediment flux intermittency factors of HA and LA intervals from the Escanilla Formation range
412 from 0.008 to 0.03 with an average value of 0.02 (N = 82), while those from modern rivers have
413 intermittency values ranging from 0.0026 to 0.8 with an average value of 0.14 (N = 94). These
414 results suggest that our results are plausible and similar to sediment flux intermittency values of
415 ephemeral rivers [[Hayden et al., 2021](#)]. It is also expected that sediment flux intermittency
416 factors are lower than corresponding water intermittencies [[Lyster et al., 2022](#)] as not all real-
417 world discharge conditions will transport sediment at maximum capacity.



418

419 Figure 7. Comparison between flux intermittency factor of modern rivers (black triangles), and intermittent rivers
420 (dark grey circles; HA intervals) and perennial rivers (light grey circles; LA intervals) from the Escanilla Formation,
421 having the same median grain size range.

422

423 **CONCLUSIONS**

424 A quantitative approach of estimating discharge and flux variability relative to changes in fluvial
425 stratigraphic architecture provides new insights into how channel stacking pattern in ancient
426 sedimentary successions can be interpreted. Cyclical variations in discharge and flux intermittency
427 correspond to changes in architectural styles such that HA intervals are deposited under more
428 intermittent flow conditions (discharge intermittency of 12 – 40 days per year) which we interpret
429 to be influenced by short and intense precipitation events while LA intervals are deposited under
430 less intermittent flow conditions (discharge intermittency of 39 – 119 days per year). Overall,
431 sediment flux intermittency factor of the Escanilla Formation has values ranging from 0.008 to
432 0.03 (3 – 11 days per year), which are within the same range of values from modern ephemeral
433 rivers (0.0026 to 0.954). These values are typical of rivers found in arid and semi-arid climatic
434 conditions and are consistent with the regional climate at Olson during the Middle Eocene. This
435 further demonstrates the ability of paleohydraulic reconstructions to predict, within acceptable
436 uncertainties, estimates that are consistent with values from modern rivers. Our data suggests that
437 changes in depositional architectures are the result of relatively infrequent sediment transport
438 events and indicate that changing rainfall distributions (as well as magnitudes) significantly
439 influenced sediment routing systems on the Earth's surface in the past.

440

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659 **Author contributions**

660 S.C. designed the project and obtained funding. N.S. computed, interpreted results, and wrote the
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663 **Competing interests**

664 The authors declare no competing interests.

665 **Data availability**

666 All data generated and analyzed in this study has been provided as supplementary material files
667 accompanying this manuscript.