

1 *The following manuscript is non-peer reviewed preprint and is under consideration for publication*
2 *in Boundary Layer Meteorology.*

3

4 **Approaching coherent turbulence and the roll-cell transition** 5 **with Lagrangian coherent structures and objective fluxes**

6 **Nikolas Aksamit^{1,2} • Marwan Katurji² □ Jiawei Zhang³**

7 Received: DD Month YEAR/ Accepted: DD Month YEAR/ Published online: DD Month YEAR
8 © Springer Science + Business Media B. V.

9 **Abstract**

10 We present the first analysis of objective and material vortices in Large Eddy Simulations
11 of atmospheric boundary layer turbulence. We extract rotating fluid features that maintain
12 structural coherence over time for near-neutral, transitional, and convective boundary
13 layers. In contrast to traditional analysis of coherent structures in turbulent boundary layers,
14 we provide the first objective (frame-indifferent) identification of temporally coherent
15 vortex boundaries that are responsible for organizing tracer distributions. We compare
16 these rotating structures with qualitative descriptions of horizontal rolls and convective
17 cells arising from decades of observational studies. We also quantify their contribution to
18 turbulent fluxes of heat under varying atmospheric stability. Using recently developed tools
19 from the theory of objective transport barriers, we derive connections between the relative
20 orthogonality of objective momentum and heat transport with the presence of rolls and
21 cells. This suggests the relationship between momentum and heat transport through vortex
22 surfaces may help explain the physics behind roll-cell transitions.

23 **Keywords** Heat Flux • Lagrangian Coherent Structures • Large Eddy Simulation • Stability
24 Analysis • Vortex Identification

✉ Nikolas Aksamit
nikolas.aksamit@uit.no

¹ Department of Mathematics and Statistics, UiT - The Arctic University of Norway, Tromsø, 9037, Norway

² marwan.katurji@canterbury.ac.nz School of Earth and Environment, University of Canterbury, Christchurch, 8041, New Zealand

³ Jiawei.Zhang@scionresearch.com Scion, New Zealand Forest Research Institute, Rotorua 3010, New Zealand

25 **1 Introduction**

26 Various geometries of fluid-organizing structures in atmospheric turbulence are evident at
27 scales from millimetres to thousands of kilometres. Such features can be seen in swirls of
28 smoke rising off a match head, the patterning of cloud streets in the atmospheric boundary
29 layer, and synoptic scale cyclones in the troposphere. In the atmospheric boundary layer
30 (the first 2km above ground level), convection results in the development of two prevalent
31 structures - the horizontal convective roll and the convective cell (Moeng and Sullivan
32 1994; Svensson et al. 2017; Yagi et al. 2017; Jayaraman and Brasseur 2021). In weakly
33 convective and neutral boundary layers, significant horizontal shear outweighs convective
34 forcing, causing horizontal rolls to dominate the flow as quasi-streamwise vortices (Young
35 et al. 2002). In a highly convective (unstable) boundary layer, open convective cells
36 dominate the flow, similar to Rayleigh-Bénard convection, with updrafts around the
37 boundaries of polygonal cells, and downdrafts in the center (Moeng and Sullivan 1994;
38 Salesky et al. 2017). The physical mechanisms driving the transition from rolls to
39 convective cells are poorly understood, especially in intermediate atmospheric stability
40 regimes when the relative role of both mechanical and buoyancy forces is important
41 (Salesky et al. 2017; Jayaraman and Brasseur 2021).

42 This transition is of fundamental interest in fluid dynamics as the physical fluid transport
43 mechanisms are changing. For boundary layer meteorology, the two structures have
44 different impacts on turbulent transport, with rolls generating more efficient turbulent
45 momentum transport than cells (Salesky et al. 2017). The transience and quasi-coherence
46 of these different features also contribute to mean flux values that inhibit surface energy
47 balance closure (Foken et al. 2011; Mauder et al. 2020). Furthermore, understanding heat
48 and momentum transport during this transition is critical for turbulence resolving numerical
49 weather prediction tools such as Large Eddy Simulation (LES) models, as the performance
50 of subgrid scale parameterizations still need to be assessed (Schalkwijk et al. 2015; Lehner
51 and Rotach 2018).

52 Previous observational and numerical investigations have studied the presence and the
53 development of horizontal convective rolls and polygonal convective cells under varying

54 surface heat flux conditions (Deardorff 1972; LeMone 1973, 1976; Grossman 1982;
55 Weckwerth et al. 1997, 1999; Khanna and Brasseur 1998; Park and Baik 2014). Salesky et
56 al. 2017) performed the first systematic LES study on the transition of rolls to cells. Their
57 work analyzed 14 large-eddy simulations ranging from neutral to highly convective
58 boundary layers through relative eddy flux contributions (e.g., quadrant analysis), mean
59 vertical profiles, and the statistical symmetries of the vertical velocity field. While certain
60 turbulent flux behaviour was ascribed to roll or cells, this statistical analysis fell short of
61 calculating any fluxes corresponding to individual structures as they did not delimit the
62 actual surfaces of these three-dimensional vortices. Over a smaller range of stabilities,
63 (Jayaraman and Brasseur 2021) also performed a detailed LES study of convective
64 influence on horizontal rolls from a statistical standpoint, but again lacked analysis of the
65 actual geometric structures.

66 To study the behaviour and impact of rolls and cells, being able to accurately identify their
67 boundaries in a given flow is of fundamental interest as our understanding of these features
68 originates from visual evidence of tracers (water vapor) that have been organized by fluid
69 structures in the atmosphere. Some the earliest systematic evidence of rolls and cells was
70 made possible with airborne imagery and satellite remote sensing (e.g., Christian and
71 Wakimoto 1989; Young et al. 2002). Thus, it is intuitive to study these structures from the
72 geometric fluid structure perspective, if possible. This approach, however, contrasts with
73 the common approach of seeking evidence of structures through their statistical imprints
74 on profiles or velocity distributions.

75 To accurately identify and study the atmospheric structures that organize tracer
76 distributions in the ways we have classically observed, we need to utilize structure
77 identification diagnostics that define features that are experimentally observable. By this
78 we mean coherent structure diagnostics which are used to evaluate the existence and
79 behaviour of fluid structures should define the same observable structures highlighted by
80 passive tracers. Developing structure identification diagnostics that maintain experimental
81 verifiability has not been of great concern to the boundary layer meteorology community,
82 but it is something that one needs to consider when developing structure identification
83 methods. This disconnect is evident if one compares standard boundary layer diagnostics

84 that identify coherent structures with what is required to describe material deformation of
85 a fluid as follows.

86 The organization of passive tracers in any fluid (e.g., heat, trace gases, or water vapor),
87 whether in cloud streets, streaks, or convective plumes is the result of the material
88 deformation of the fluid. After several decades of debate, it was widely accepted as a
89 fundamental axiom of continuum mechanics that material deformation of any fluid is
90 indifferent to the position of the observer, and thus indifferent to Euclidean frame changes
91 (Gurtin 1981). That is, to identify an influential coherent structure in the atmosphere, our
92 identification methods need to be indifferent to any changes in reference frame of the form

$$93 \quad \mathbf{y}(t) = \mathbf{Q}(t)\mathbf{x}(t) + \mathbf{b}(t)$$

94 where $\mathbf{x}(t)$ and $\mathbf{y}(t)$ are position vectors in a given reference frame, $\mathbf{Q}(t)$ is a time-
95 varying three-dimensional rotation, and $\mathbf{b}(t)$ is a time-varying translation. For example,
96 the same cloud geometry will appear in photographs whether they are taken from a tripod
97 in a field, a moving car, or from a circling airplane. In this way, one can also see that the
98 dimensions and structure of our material features of interest should also be indifferent to
99 the reference frame. A frame-indifferent scalar value transforms as $P(x) = \tilde{P}(y)$, and a
100 frame-indifferent vector transforms as $\tilde{v} = Qv$ (Truesdell and Noll 2004). Frame-
101 indifference is often referred to as *objectivity* and any material flow feature diagnostic
102 should satisfy this benchmark (Drouot 1976; Drouot and Lucius 1976; Astarita 1979; Lugt
103 1979).

104 Conceptual models of hairpin vortices, rolls, thermal plumes, and cells describe material
105 fluid features and are ubiquitous in the meso- and micro-meteorology literature. There has
106 been limited connection, however, between numerically-simulated vortices and those
107 experimentally observed in the laboratory or atmosphere. One cause for this may stem from
108 the lack of objectivity of the common tools for coherent structure identification. Wind
109 velocity, components of Reynolds decompositions, and products of fluctuating velocity
110 components (e.g., Reynolds stress, turbulence kinetic energy, quadrant analysis products)
111 are known to not actually be experimentally-observable and thus cannot describe material
112 behaviour, or fluid-deforming structures (Speziale 1998; Kaszás et al. 2023). On the other

113 hand, measurements of atmospheric state parameters such as temperature, pressure, and
114 humidity are frame indifferent scalars, and can provide clues to the presence of structures
115 in meteorological station measurements.

116 The study and understanding of heat and momentum transport for process-based analyses
117 in the atmospheric boundary layer has been strongly influenced by the spatial and temporal
118 scale of data that has been classically available. Temporally-resolved point measurements
119 of wind and scalars from meteorological towers facilitate statistical studies of fluxes of
120 heat and momentum that harness some temporal averaging with Reynolds decomposition
121 and eddy-covariance or with flux-profile methods (Foken 2008). There is no doubt that we
122 have a significantly better understanding of ABL turbulence thanks to the idea of turbulent
123 fluxes, and non-objective coherent structure identification methods, such as quadrant
124 analysis. Our goal here is to introduce the advantages of a complementary way of studying
125 fluid behaviour that is rigorously linked to the material behaviour of fluid, instead of
126 statistical signatures arising from the presence of those structures.

127 For spatially resolved velocity fields, the most used vortex identification methods employ
128 diagnostic scalar fields, such as the Q -, λ_2 -, Δ - and λ_{ci} -parameters (Hunt et al. 1988; Jeong
129 and Hussain 1995; Zhou et al. 1999; Adrian et al. 2000; Gao et al. 2011). Iso-surfaces of
130 Q , λ_2 , Δ and λ_{ci} are not frame-indifferent and hence the structures they define cannot
131 predict observed material tracer patterns (Haller 2005, 2020). As mentioned before, this
132 lack of self-consistency means such structures may be correlated with measured scalar
133 concentrations or turbulent fluxes (e.g., Westerweel et al. 2009; Eisma et al. 2021), but
134 there can be no causal description of an observable fluid structure. Several modifications
135 of these vortex diagnostics can make them objective (e.g., Liu et al. 2019a, b), but as there
136 is a missing connection to material mixing and transport, identifying the right vortex is
137 strongly dependent on the user. The subjectivity associated with user-defined values for
138 these non-objective diagnostics was recently highlighted by Dong and Tian (2020).

139 We describe rolls and cells as frame-indifferent, material, and rotationally coherent
140 Lagrangian structures for nearly neutral, transitional, and highly convective boundary
141 layers. This work provides the first objective description of cells and rolls in Large Eddy

142 Simulations of the ABL. We first verify that the features we define do indeed resemble
143 qualitative descriptions of rolls and cells in section 3.1. In section 3.2, we discuss the role
144 these rotationally coherent structures play in the advective and turbulent transport of heat
145 when compared with the surrounding incoherent turbulent atmosphere. Lastly, we compare
146 objective heat and momentum transport for varying atmospheric stability, and draw a
147 connection between structure formation, mechanical and thermal influences, and alignment
148 of diffusive fluxes.

149 **2 Methods**

150 **2.1 Rotationally Coherent Lagrangian Coherent Structures**

151 Lagrangian coherent structures (LCS) behave as the hidden skeleton of fluid flow (Peacock
152 and Haller 2013). Acting as the finite time analogue of invariant manifolds from the
153 mathematical field of time-dependent dynamical systems, LCSs have been mathematically
154 derived as the most influential transport barriers that exhibit specific characteristics (Haller
155 2023). For any arbitrary material surface in an unsteady fluid (i.e., a two-dimensional
156 surface consisting of infinitesimal fluid particles that deforms with the flow), advective
157 transport across that surface will be zero because the surface deforms under advection, by
158 definition. As such, there are infinitely many material barriers to advective transport. LCS
159 are material surfaces that maintain structural coherence over a finite time interval with
160 exceptional behaviour, such as being maximally repelling or attracting surfaces (hyperbolic
161 LCS), or local maximizers of shear among material surface that maintain rotational
162 coherence (elliptic LCS).

163 LCS have proven beneficial for furthering our understanding of coherent atmospheric
164 structures and transport barriers, but this is still a nascent field of research (see e.g.,
165 Tallapragada et al. 2011; Olascoaga et al. 2012; Rutherford et al. 2012; BozorgMagham
166 and Ross 2015; Wang et al. 2017). Specific examples include studies on zonal jets (Beron-
167 Vera et al. 2012), atmospheric rivers (Garaboa-Paz et al. 2015), and the polar vortex (Serra
168 et al. 2017). Of particular relevance to the ABL are the studies identifying LCS in
169 laboratory boundary layers using two-dimensional Particle Image Velocimetry (Green et
170 al. 2007; Pan et al. 2009; Wilson et al. 2013; He et al. 2016; Eisma et al. 2021), predicting

171 downdraft and significant shear events in near-surface doppler lidar measurements at the
172 Hong Kong International Airport (Tang et al. 2011; Knutson et al. 2015), studying
173 atmospheric Karman Vortex street from satellite wind measurements (Günther et al. 2021),
174 and understanding aerosol dispersion patterns in the stratosphere (Aksamit et al. 2021).
175 The above research all relied on two-dimensional projections of velocity fields to describe
176 inherently three-dimensional phenomena. Only recently have studies of elliptic LCS and
177 objective momentum and heat transport barriers been successfully conducted in fully three-
178 dimensional turbulent experimental and numerical flows (Neamtu-Halic et al. 2019;
179 Aksamit and Haller 2022; Aksamit et al. 2023).

180 To study rolls and cells in ABLs of varying stability, we utilized time-resolved three-
181 dimensional velocity fields to identify candidate vortices as regions of strong fluid
182 coherence and material rotation. Specifically, in a given velocity field $\mathbf{v}(\mathbf{x}, t)$, fluid particle
183 trajectories $\mathbf{x}(t; t_0, \mathbf{x}_0)$ originating at some initial position \mathbf{x}_0 at time t_0 are generated by
184 the differential equation

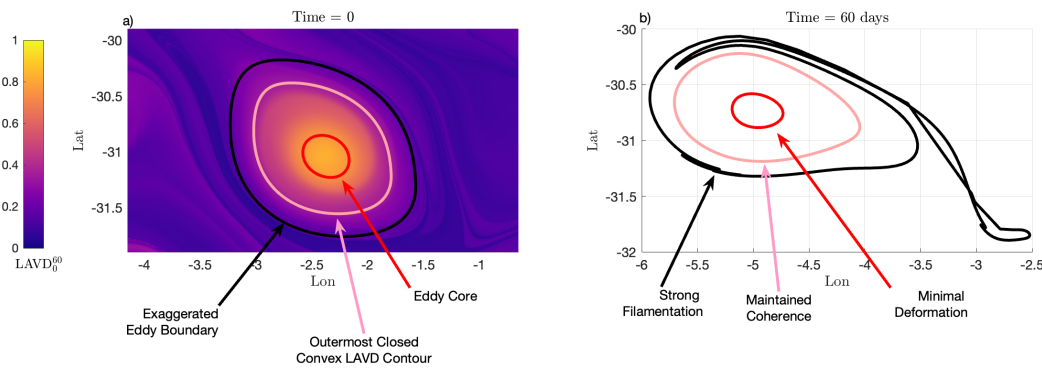
$$185 \quad \dot{\mathbf{x}} = \mathbf{v}(\mathbf{x}, t).$$

186 These trajectories define the flow map $\mathbf{F}_{t_0, t}(\mathbf{x}_0) = \mathbf{x}(t; t_0, \mathbf{x}_0)$, which is the unique
187 function that maps fluid particle positions from their initial position and time, to their
188 position at some time t , according to the velocity field $\mathbf{v}(\mathbf{x}, t)$. To detect elliptic LCSs
189 over a time window $[t_0, t_1]$, we utilize the *Lagrangian-Averaged Vorticity Deviation*
190 (*LAVD*) (Haller et al. 2016). This is defined as the mean of the magnitude of the difference

191 of the pointwise vorticity $\omega = \nabla \times \mathbf{v}$ along a trajectory from the spatial mean of vorticity
 192 at each time step. Formally, to obtain the time t_0 location of elliptic LCSs, we calculate

193
$$\text{LAVD}_{t_0}^t(\mathbf{x}_0) = \frac{1}{|t_1 - t_0|} \int_{t_0}^t |\boldsymbol{\omega}(\mathbf{x}(s; \mathbf{x}_0), s) - \bar{\boldsymbol{\omega}}(s)| ds$$

194 where the overbar indicates a spatial mean. This quantity is objective for a given fluid
 195 volume of interest, but exact values depend on how that domain is defined. For our
 196 experiments, we consistently use the entire spatial domain of our LES.



197 **Fig 1:** Example of time evolution of fluid particles surrounding an elliptic LCS (red) in a 2D ocean flow over
 198 60 days

199 In recent years, *LAVD* has been used as a diagnostic to identify the boundaries of coherent
 200 oceanic eddies and vortices (Abernathey and Haller 2018; Beron-Vera et al. 2019) and
 201 quantify the transport of fluid inside these coherent structures over pan-oceanic distances.
 202 In Figure 1, we illustrate the dynamic behaviour of an *LAVD*-identified ocean surface
 203 current eddy in the Agulhas Rings region as computed from geostrophic ocean surface
 204 currents that are freely available from the Copernicus Environment Monitoring Service
 205 (CMEMS, 2019). The *LAVD* field was computed over 60 days of fluid advection, and the
 206 boundary of the materially coherent eddy at time $t = 0$ is identified in pink as the
 207 outermost closed convex *LAVD* contour surrounding a local *LAVD* maximum (Figure 1a).
 208 In Figure 1a, we also include a level-set contour corresponding to a higher *LAVD* value in
 209 the eddy core in red, and a spatially magnified version of the pink eddy boundary in black.
 210 This magnified contour is thus outside the boundary of what we predict is a materially
 211 coherent eddy. In Figure 1b, we plot the final position of the fluid particles corresponding

212 to each contour after 60 days of advection. As an appropriately chosen elliptic LCS, both
 213 the pink boundary and the central core remain minimally deformed though they have
 214 undergone significant rotation and the eddy center has traveled nearly 250 km through open
 215 ocean. As it was originally drawn outside of the material eddy boundary, the outermost
 216 black contour exhibits significant filamentation after 60 days.

217 We can extend this analysis to three-dimensional flows where locations of elliptic LCSs
 218 can be identified as smooth cylindrical *LAVD* level-surfaces that surround a one-
 219 dimensional *LAVD* ridge (Neamtu-Halic et al. 2019). In the present work we rely on the
 220 relaxed coherent Lagrangian vortex criteria utilized by Aksamit et al. (2023) in rotating
 221 Rayleigh-Bénard convection by not seeking a central *LAVD* ridge or enforcing a cylindrical
 222 shape. Neglecting these requirements comes with a computational advantage, while still
 223 capturing material rotational features. In fact, Aksamit et al. (2023) showed that any
 224 arbitrary *LAVD* level-surface exhibits exceptional momentum and heat transport blocking
 225 behaviour orthogonal to its surface, even though the calculation of *LAVD* does not consider
 226 these fields. Furthermore, the ability of arbitrary *LAVD* surfaces to organize the transport
 227 of momentum and heat was largely independent of the length of the integration time $[t_0, t_1]$,
 228 with shorter intervals resulting in better flux limiting behaviour.

229 **2.2 Objective and non-objective Fluxes**

230 For a scalar concentration c that satisfies the classic advection-diffusion equation with
 231 diffusivity $\kappa > 0$, the instantaneous diffusive transport through an evolving material surface
 232 $M(t)$ is an objective quantity that can be written as

$$233 \quad \Sigma(t, M) = \int_{M(t)} \kappa \nabla c \cdot \mathbf{n} \, dA \quad (1)$$

234 with $\mathbf{n}(\mathbf{x}, t)$ being a smooth unit normal vector field along $M(t)$. In contrast to the
 235 convective scalar flux through the surface, $\mathbf{v}c \cdot \mathbf{n}$, diffusive scalar transport through a
 236 surface in eq (1) does not change with varying reference frames and can be thought of as a
 237 physical property intrinsic to the surface and the flow. This idea is of particular relevance
 238 to micrometeorology where a given flow may be characterized by choosing M to be a fixed
 239 (non-material) horizontal plane, and then calculating the vertical convective scalar flux at

240 that height at each time (Stull, 1988). This vertical convective scalar flux is not actually a
241 frame-indifferent quantity, and therefore not an intrinsic quantity of the flow as it depends
242 on the user.

243 Similarly, the convective transport of momentum, $\rho\mathbf{v}(\mathbf{v} \cdot \mathbf{n})$, varies between reference
244 frames and is an insufficient benchmark to quantify the momentum transport through a
245 given surface in a given flow. To circumvent this problem, Haller *et al.* (2020) introduced
246 the instantaneous diffusive transport of linear momentum $\mathbf{f}(\mathbf{x}, t) = \rho\mathbf{v}(\mathbf{x}, t)$ through
247 $M(t)$,

$$248 \quad \psi(t, M) = \int_{M(t)} \nu \rho \nabla^2 \mathbf{v} \cdot \mathbf{n} dA \quad (2)$$

249 The integrands of equations (1) and (2) thus provide objective vector fields for quantifying
250 the magnitude and alignment of diffusive heat and momentum transport for arbitrary
251 surfaces in a flow. This frame-indifferent and individual feature-focused approach to
252 quantifying heat and momentum flux has helped explain the relative influences of Coriolis
253 and convective forces on specific vortices in direct numerical simulations of rotating
254 Rayleigh-Bénard flow (Aksamit et al. 2023). We apply a similar approach to suggest a
255 spatially and temporally resolved objective diagnostic that predicts the dominance of rolls
256 and cells and is based on the underlying physics of heat and momentum transport.

257 In turbulent boundary layers, distinguished flow features that advect heat (plumes, vortices,
258 etc.) appear as structures with limited mixing with the surrounding fluid. The boundaries
259 of such features, across which the mixing of heat is limited, can be identified by locally
260 maximal temperature gradients. That is, they are surfaces across which diffusive transport
261 is maximized, meaning the temperature gradient is normal to these surfaces. In contrast,
262 Lagrangian coherent structures have been correlated with diffusive momentum transport
263 barriers that constrain the distributions of momentum (Haller et al. 2020; Aksamit et al.
264 2023). The surfaces of these structures are then tangent to the objective momentum
265 transport vector field.

266 Given this theoretical difference in flux vector orientation, Aksamit et al. (2023) used the
267 inner product of diffusive heat and momentum flux vector fields to quantify the relative
268 agreement of momentum and heat transport barriers in rotating Rayleigh-Bénard

269 convection. The more closely aligned that instantaneous barriers of heat and momentum
 270 are, the closer to zero the inner products of objective heat and momentum flux vectors on
 271 those surfaces are. In their work, the distribution of momentum and heat flux vector
 272 alignments helped explain the varying roles of Coriolis enhanced and convection
 273 dominated structures in organizing the flow. We seek to extend these findings to ABLs
 274 where heat and momentum alignment can in turn be used to diagnose the presence of cells
 275 and rolls, and describe transitional behaviour, in an objective way.

276 *2.2.1 Non-objectivity of turbulent momentum and heat flux*

277 In this section, we highlight a fundamental difference between our approach, and
 278 traditional turbulent flux-based flow diagnostics. The behaviour of turbulent flows is often
 279 characterized by Reynolds decomposition and the Reynolds stress tensor, which is frame-
 280 indifferent (objective) only if one removes the same average values from every point of the
 281 flow field (Speziale 1979). When quantifying turbulent fluxes at a chosen height or through
 282 a chosen surface, researchers typically rely on instantaneous or time-averaged turbulence
 283 covariances (e.g., $w'\theta'$ or $u'w'$). In contrast to the full Reynolds stress tensor, $w'\theta'$ and $u'w'$
 284 are actually not frame-indifferent, and thus cannot describe material behaviour of the flow.
 285 That is, these values cannot predict experimentally observable structures that organize
 286 tracers, such as rolls and cells. This can be seen in the following way.

287 Decompose the velocity field into a mean and fluctuating part

$$288 \quad v(x, t) = \bar{v} + v'(x, t)$$

289 where averaging must be performed over ensembles of experiments with the same initial
 290 and boundary conditions, indexed by α :

$$291 \quad \bar{v} = \frac{1}{N} \sum_{\alpha=1}^N v^\alpha.$$

292 Recall, Euclidean frame-changes, or physical changes of an observer's reference frame can
 293 be written as

$$294 \quad \mathbf{y}(t) = \mathbf{Q}(t)\mathbf{x}(t) + \mathbf{b}(t)$$

295 where x and y are positions, $\mathbf{Q}(t)$ is a three-dimensional rotation, and $\mathbf{b}(t)$ is a translation
 296 vector. By differentiating the frame-change with respect to time, we observe the
 297 transformation of velocity vectors between frames as,

$$298 \quad \tilde{\mathbf{v}} = \dot{\mathbf{Q}}(t)\mathbf{x}(t) + \mathbf{Q}(t)\mathbf{v}(t) + \dot{\mathbf{b}}(t)$$

299 We can then write a fluctuating velocity vector in the new frame as

$$300 \quad \tilde{\mathbf{v}}' = \dot{\mathbf{Q}}(t)\mathbf{x}(t) + \mathbf{Q}(t)\mathbf{v}(t) + \dot{\mathbf{b}}(t) - \frac{1}{N} \sum_{\alpha=1}^N \dot{\mathbf{Q}}(t)\mathbf{x}(t) + \mathbf{Q}(t)\mathbf{v}^\alpha + \dot{\mathbf{b}}(t)$$

301 As we are averaging over an ensemble of experiments that undergo the same time-varying
 302 frame change, we can simplify this equation by moving terms with no dependence on α
 303 outside the summation, resulting in the following form

$$304 \quad \tilde{\mathbf{v}}' = \dot{\mathbf{Q}}(t)\mathbf{x}(t) + \mathbf{Q}(t)\mathbf{v}(t) + \dot{\mathbf{b}}(t) - \dot{\mathbf{Q}}(t)\mathbf{x}(t) - \dot{\mathbf{b}}(t) - \mathbf{Q}(t) \left[\frac{1}{N} \sum_{\alpha=1}^N \mathbf{v}^\alpha \right]$$

$$305 \quad = \mathbf{Q}(t)[\mathbf{v}(t) - \bar{\mathbf{v}}].$$

306 This is precisely the form necessary for fluctuating velocity vectors to be frame indifferent
 307 when a Reynolds decomposition is performed with ensemble averages.

308 Researchers often invoke the ergodic hypothesis that ensemble and temporal averages are
 309 equivalent. That is, for large enough N and M , $\frac{1}{N} \sum_{\alpha=1}^N \mathbf{v}^\alpha(x, t) = \frac{1}{M} \sum_{i=1}^M \mathbf{v}(x, t_i)$. While
 310 this may be true, \mathbf{Q} and \mathbf{b} are also time dependent, and we are left with

$$311 \quad \tilde{\mathbf{v}}' = \dot{\mathbf{Q}}(t)\mathbf{x}(t) + \mathbf{Q}(t)\mathbf{v}(t) + \dot{\mathbf{b}}(t) - \frac{1}{M} \sum_{i=1}^M \dot{\mathbf{Q}}(t_i)\mathbf{x}(t_i) + \mathbf{Q}(t_i)\mathbf{v}(x(t_i), t_i) + \dot{\mathbf{b}}(t_i)$$

312 which does not simplify as above. Spatial averaging creates similar issues as the fluctuating
 313 velocity would transform as

$$314 \quad \tilde{\mathbf{v}}' = \dot{\mathbf{Q}}(t)\mathbf{x}(t) + \mathbf{Q}(t)\mathbf{v}(t) + \dot{\mathbf{b}}(t) - \frac{1}{M} \sum_{i=1}^k \dot{\mathbf{Q}}(t)\mathbf{x}_i + \mathbf{Q}(t)\mathbf{v}(x_i, t) + \dot{\mathbf{b}}(t)$$

315 Furthermore, the individual components of the fluctuating velocity vector, and individual
 316 terms in the Reynolds stress tensor are not frame indifferent scalar values, even for
 317 ensemble averaging. This can be seen term by term by writing $\mathbf{Q} = [q_{ij}]$ and $\tilde{\mathbf{v}}'_i = q_{i1}\mathbf{v}'_1 +$
 318 $q_{i2}\mathbf{v}'_2 + q_{i3}\mathbf{v}'_3$. Then, $\tilde{\mathbf{v}}'_i = \mathbf{v}'_i$ only for \mathbf{Q} being the identity matrix, not for any rigid-body
 319 rotation, so the fluctuating velocity component values \mathbf{v}'_i are not frame indifferent. As
 320 temperature is a frame indifferent scalar, this implies $\mathbf{v}'_i\theta'$ and $\overline{\mathbf{v}'_i\theta'}$ are also frame
 321 dependent for each component i . Furthermore, one can expand

$$322 \quad \overline{\mathbf{v}'_i\mathbf{v}'_j} = (q_{i1}\mathbf{v}'_1 + q_{i2}\mathbf{v}'_2 + q_{i3}\mathbf{v}'_3)(q_{j1}\mathbf{v}'_1 + q_{j2}\mathbf{v}'_2 + q_{j3}\mathbf{v}'_3),$$

323 and conclude individual terms of instantaneous and time-averaged Reynolds stress are also
 324 not objective.

325 This lack of objectivity has wide implications for studies that attempt to identify turbulent
 326 coherent structures through quadrant analysis and contours of $u'w'$ (for a review of this

327 approach, see Wallace 2016)). From the fundamental axioms of continuum mechanics, no
328 such structure will ever have a causal relationship with fluid deformation. As we will also
329 discuss in the Results, structures identified using Reynolds stress and turbulent heat flux
330 level-sets are not even reliably correlated with fluid deformation. This issue is further
331 complicated in mildly complex terrain where buoyancy and shear forces become non-
332 orthogonal and there is no a-priori known temporal scale for averaging (Serafin et al. 2018).

333 **2.3 Large Eddy Simulations**

334 Observational and numerical studies indicate that $-z_i/L$ is well correlated with the
335 dominance of rolls and cells, with small values associated with roll and large values
336 associated with cells. The transitional values are more disputed, but previous LES studies
337 suggest that the transition from rolls to cells begins around $15 < -z_i/L < 25$ for flat,
338 horizontally homogeneous terrain (Deardorff 1972; Khanna and Brasseur 1998; Salesky et
339 al. 2017). Initial investigations suggested $-z_i/L = 25$ to be too small for our simulations,
340 and we settled on a slightly larger value where transitional behaviour became more
341 pronounced. Accordingly, we compare objective fluxes of momentum and heat across
342 Lagrangian coherent structures for three ABL simulations $-z_i/L \in \{6.7, 29.2, 589.2\}$. For
343 each stability regime, the PALM (Parallelized Atmospheric Large eddy simulation Model)
344 model (Maronga et al. 2020) using incompressible Navier-Stokes equation with
345 Boussinesq approximation is used in this work to generate boundary layer simulation data.
346 The turbulence recycling method is used to reduce the computational cost in the main
347 simulations (Maronga et al. 2020). To do so, for each of the three main simulations, the
348 model first used a pre-cursor simulation to prepare the turbulence inflow data for the main
349 simulation. Detailed pre-cursor run configurations can be found in Table 1a. The pre-cursor
350 simulations run long enough to make sure that the turbulent flow field has reached quasi-
351 equilibrium. The turbulent flow field from the pre-cursor runs were then used in the
352 respective main simulations as the upwind turbulence inflow in the main simulation
353 domain. Two nested domains were used in all the main simulations to resolve finer
354 turbulence structures (Table 1b). For each stability regime, we calculate $LAVD$ in volumes
355 of 500 m, 2500 m, 125 m corresponding to the streamwise, spanwise, and vertical
356 dimensions.

357 Table 1a. Configuration for the precursor run simulations

	Domain size (x,y,z) (km)	Grid resolution (x,y,z) (m)	Simulation time
Near neutral	12.3x12.3x6.9	64x64x54	24h
Transitioning			24h
Convective			4h

358

359 Table 1b. LES Configuration

	Domain size (x,y,z) (km)	Grid resolution (x,y,z) (m)	Simulation time	z_i	$ L $	$-z_i/L$
Near neutral	D01:	D01:	1.5h (Only the last hour was used in the analysis.)	2268	336.1	6.7
Transitioning	24.5x24.5x6.9	64x64x54		3713	127.1	29.2
Convective	D02: 8.2x8.2x3.5 D03: 6.1x6.1x2.3	D02: 32x32x18 D03: 16x16x9		2345	3.98	589.2

360 **3 Results**

361 **3.1 Describing Vertical Fluid Motion with Frame Dependent Structures**

362 To help motivate our Lagrangian coherent structure approach, we start with a simple
 363 example from the near-neutral ABL simulation. As shown in section 2.2.1, components
 364 of fluctuating velocity vectors and Reynolds stress components are not frame-indifferent,
 365 and cannot describe the material fluid structures responsible for coherent motions. There
 366 may still, however, be correlations between the location of coherent fluid motions and
 367 their imprint on these diagnostic fields. We investigate these potential correlations in a
 368 simple test of describing vertical motion of fluid near the surface of a near-neutral
 369 boundary layer.

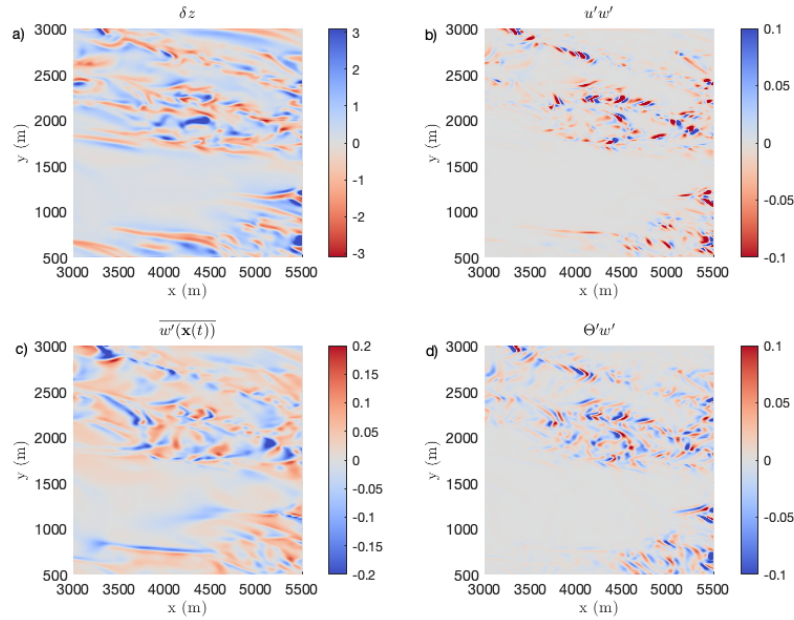
370 Quadrant analysis is a common Eulerian turbulent coherent structure diagnostic, that
 371 focuses on the fluctuating values of streamwise and vertical windspeed

372
$$u' = u - \bar{u}, w' = w - \bar{w},$$

373 and isolates large magnitude Reynolds stress ($u'w'$) events (Lu and Willmarth 1973).

374 These events are then separated into quadrants depending on the sign of the fluctuating

375 components u' and w' , with quadrants two and four, termed ejections and sweeps,
 376 contributing disproportionately to the total Reynolds stress.

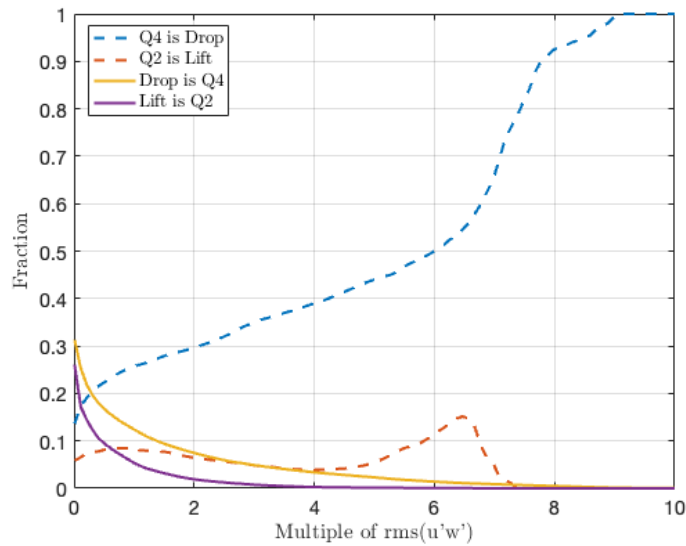


377 **Fig 2:** Comparison of the 10-second vertical change of fluid particle position (a), kinetic momentum flux (b),
 378 Lagrangian-averaged vertical velocity fluctuations (c), and kinetic heat flux (d) in a near-neutral atmospheric
 379 boundary layer at $z = 5$ metres

380 In turbulent boundary layers, ejections and sweeps are often used to describe near-
 381 surface signatures of the bursting-cycle, a theoretical process of coherent fluid moving
 382 away from the surface and the in-rush of turbulent fluid to replace it (Kline et al. 1967;
 383 Wallace 2016). In Figure 2 we present streamwise-spanwise planes at 5 metres above the
 384 surface in a near-neutral boundary layer. In Figure 2a, we present the 10 second vertical
 385 displacement of fluid by initializing a 1500×1500 grid of fluid particles at $z = 5$ metres,
 386 and advecting them backwards in time from t_0 to $t_0 - 10s$. The resulting contour plot in
 387 Fig 2a shows the vertical height change for fluid particles with blue shading indicating
 388 fluid dropping from an initially higher position, and red corresponding with fluid rising
 389 from a lower position in forward time. We then compare this material fluid deformation to

390 the instantaneous t_0 fields of $u'w'$, and $\Theta'w'$ in Figures 2b and 2d, calculated from ten
 391 second averaging over the plane of observation.

392 There is some qualitative agreement between regions of large vertical change in fluid
 393 trajectories with the largest magnitudes of $u'w'$ and $\Theta'w'$, suggesting larger turbulent
 394 fluxes may occur during significant vertical transport of fluid. It is immediately clear,
 395 however, that there is no direct connection between the magnitude, or sign, of values in
 396 2b or 2d with what the fluid was doing immediately prior to t_0 . Even at short time scales,
 397 $u'w'$ and $\Theta'w'$ cannot determine if nearby air is rising or falling.



398 **Fig 3:** Connection between quadrant analysis designated events of varying threshold and the actual vertical
 399 motion of fluid particles from Figure 2

400 For an additional comparison, we also perform a Reynolds decomposition for each
 401 grid cell in our flow spanning the ten seconds of fluid advection, as one would do if
 402 sampling at separate meteorological stations throughout the domain. Though this results in
 403 a non-physical reference frame change, it gives the greatest advantage for vertical velocity
 404 fluctuations to accurately describe relative motion of nearby fluid. We then average w'
 405 along the same 10-second trajectories used in 2a, to see if descending or ascending fluid
 406 consistently experience the same fluctuating value on its path. Contours of this diagnostic
 407 in Figure 2c show qualitatively more similar features to the actual fluid elevation change,
 408 such as more elongated features in the streamwise direction, but there is still not a direct

409 match. In fact there are many examples of large positive Lagrangian-averaged w' in 2c that
410 corresponds with descending fluid in 2a.

411 We quantify these qualitative descriptions of turbulent fluctuations and vertical fluid
412 motion in Figure 3. We refer to any fluid that descends by more than 1 metre in the ten
413 seconds prior to t_0 as a true drop, and all fluid particles that ascend by more than 1 metre
414 as a true lift. This is a liberal description of significant vertical fluid motion, as can be seen
415 from the distribution of δz in Figure 2a.

416 When performing quadrant analysis, the user must choose a Reynolds stress
417 magnitude threshold (“quadrant hole”) above which quadrant 2 and quadrant 4 features are
418 defined as ejections, or sweeps, respectively. There is a wide range of values available in
419 the literature, so we instead investigate all thresholds between 0.001 and 10 times the root
420 mean square of $|u'w'|$. The fraction of instantaneous sweeps that correspond with true
421 drops varies from 15% to 100% at a hole size of nine times the r.m.s.. For the majority of
422 hole sizes, less than 50% of sweeps corresponded with fluid that is actually descending
423 significantly. Ejections were less successful at identifying rising fluid as less than 20% of
424 ejections actually corresponded with lifting fluid.

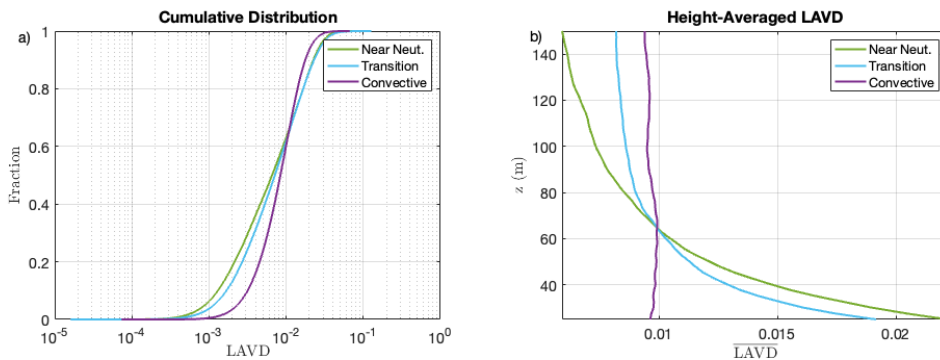
425 In Figure 3, we also show the fraction of drops and lifts that could be identified as
426 sweeps or ejections. For the smallest Reynold stress threshold, sweeps were maximally
427 effective at diagnosing descending fluid with approximately 30% of drops identified.
428 Ejections nearly matched this accuracy, but more quickly decreased in accuracy as
429 quadrant hole size increased.

430 This simple example shows the disconnect between an intuitive interpretation of
431 fluctuating velocity terms, a very common method of coherent structure identification, and
432 the true fluid behaviour. It is through this seeming dissonance that we differentiate our
433 research from other approaches. Rather than looking at coherence in turbulent velocity
434 fields or time series to suggest the presence of an atmospheric structure or behaviour, we
435 define coherence with respect to the material deformation of the fluid, and use those
436 structures to investigate the role of rolls and cells. With the actual fluid surfaces in hand,

437 we can determine their influence on turbulent heat fluxes, and better understand the physics
438 of their origin.

439 3.2 LAVD in the atmospheric boundary layer

440 We calculated *LAVD* over ten second windows spanning sixty minutes of simulated
441 boundary layer flow. For computational economy, we randomly selected 10 second
442 intervals in each minute of the sixty-minute datasets. A ten second integration interval was
443 empirically chosen to balance the computational expense of Lagrangian particle tracking
444 with feature resolution. Integration times from two to sixty seconds were also investigated.
445 As with previous *LAVD* studies of heat transport barriers, structure geometry and flux
446 barrier behaviour was found to be robust over a wide range of integration times. We show
447 an example of this in the appendix.

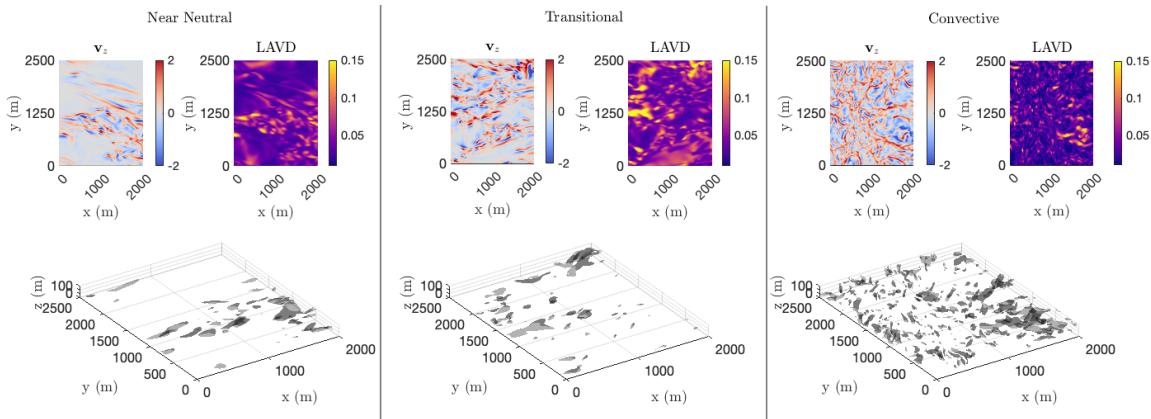


448 **Fig 4:** Empirical cumulative distributions of LAVD and height-averaged values of LAVD for the three
449 stability simulations

450 Some general properties of the transition from shear-dominated to convection-
451 dominated flows can be seen in bulk flow behaviour described in Figure 4. Figure 4a shows
452 empirical cumulative distribution functions (CDF) of *LAVD* for the three cases, and Figure
453 4b shows height-averaged values of *LAVD*. In the near-neutral case, the surface-shear
454 dominance is clear as highly rotational fluid is concentrated near the surface, with the
455 largest mean *LAVD* values below 60 metres out of the three experiments. The CDF reveals
456 that more fluid undergoes minimal rotation and is not part of a coherent vortex in the near-

457 neutral case than in the transitional or convective case. That is, strong rotation in the fluid
 458 is isolated to relatively rare, but strong near-surface vortices.

459 For the strongly convective case, we see that convective mixing results in a much more
 460 uniform distribution of *LAVD* values across all heights. The relatively smaller influence of
 461 shear no longer restricts the formation of coherent Lagrangian vortices to the near surface
 462 region, though a slight decrease in average *LAVD* is evident above 65 metres. The CDF of
 463 *LAVD* shows a shift away from extreme values, and is more concentrated around a mean
 464 value of 10^{-2} . The transitional case reveals more rotational structures between 65 and 150
 465 metres above the surface than the near-neutral simulation, but lower average *LAVD* in the
 466 near surface region. This exists as an intermediate step between the convective and neutral
 467 regimes. These profiles also reveal a relative enhancement of upper level mixing possible
 468 with the onset of convection, and a complimentary dampening of roll-formation that
 469 decreases near-surface fluid rotation begins as temperature gradients increase.



470 **Fig 5:** Comparison of vertical velocity and *LAVD* on $z = 25\text{ m}$ streamwise-spanwise planes, as well as
 471 *LAVD* level-sets for the three stability regimes

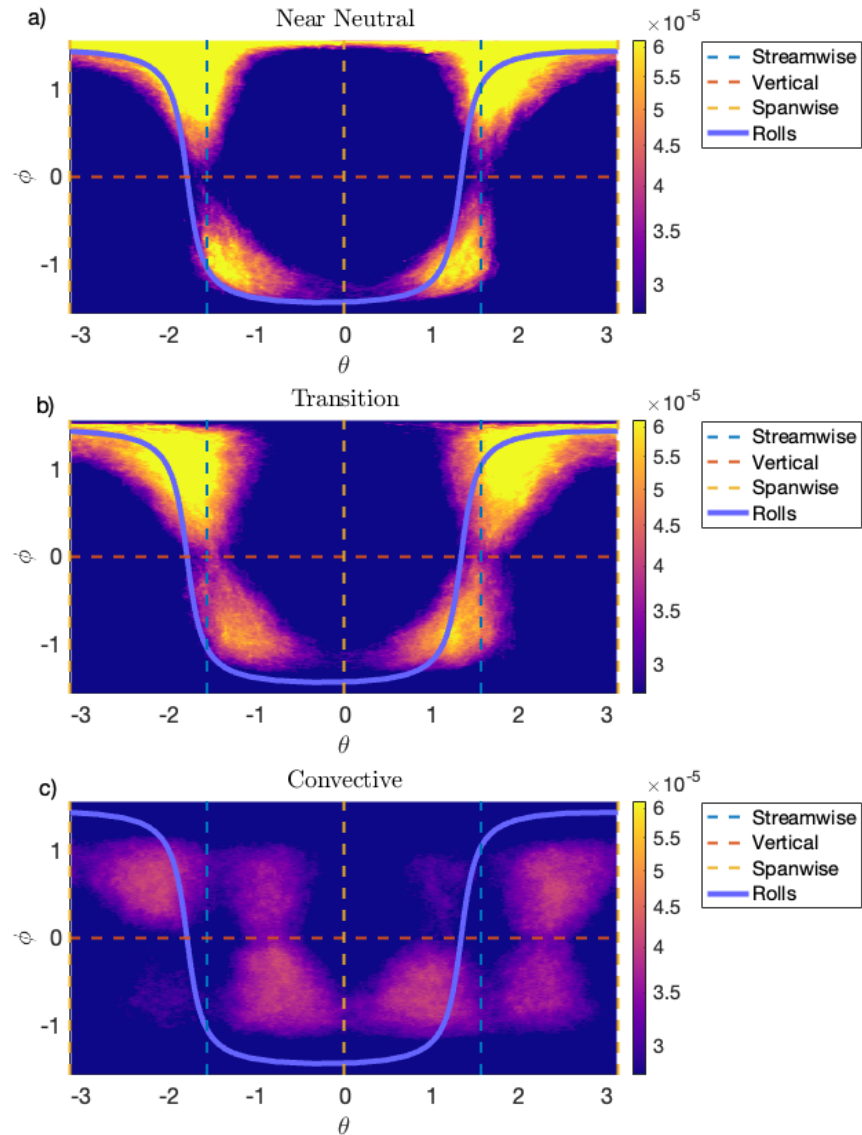
472 This bulk behaviour suggests that *LAVD* is indeed capturing structural changes in the
 473 organization of the ABL as we transition from a nearly-neutral to a highly unstable
 474 atmosphere. One distinct advantage of this approach is the ability to extract the individual
 475 material features, and examine the role that each play in land-atmosphere interactions. For
 476 computational efficiency in our LES dataset, we extracted coherent Lagrangian vortices as
 477 *LAVD* level-sets, similar to the previous analysis of Aksamit et al. (2023), instead of

478 isolating cylindrical shells surrounding co-dimension two *LAVD* ridges. Large *LAVD*
479 values in LES may result from trajectories trapped in rotationally coherent vortices as well
480 as in high shear regions with large vorticity but no apparent vortices. Additionally, there is
481 no standard method for selecting the most appropriate value of an *LAVD* level-set of
482 interest, though it has been shown that this is not of primary importance as any arbitrarily
483 chosen level-set performs as an effective diffusive transport barrier to heat and momentum
484 (Aksamit et al. 2023). We first seek to verify that we can extract influential roll and cell
485 structures via the relaxed *LAVD* level-set criteria as this is not yet known.

486 To analyze our sixty-minute temporally-resolved LES fields, we implemented a fixed
487 *LAVD* level-set value for each type of simulation. From figure 4, we see that the near-
488 neutral and transitional cases have the strongest *LAVD* features immediately above the
489 surface. Additionally, there is not a significant change in mean *LAVD* across all heights in
490 the convective case. We thus suggest an *LAVD* level-set value should be chosen to be
491 significantly large relative to values at the lowest height of investigation if one seeks to
492 extract near-surface horizontal rolls. To achieve this for each stability, we used twice the
493 mean *LAVD* value at 25 metres above the surface (the lower extent of our *LAVD* analysis)
494 as this allows us to limit our near-neutral analysis to exceptional rolls and while still
495 providing a suitable value to identify convective cells.

496 In Figure 5 we display *LAVD* level-sets for the three stabilities calculated in randomly
497 selected ten-second windows. We also compare these structures with the vertical velocity
498 and *LAVD* fields at the $z = 25$ m level. Quasi-linear streamwise organization of features
499 reminiscent of rolls can be clearly seen in Figure 5a for the near-neutral case. There is still
500 some suggestion of linear organization in the transitional case (Figure 5b), but small
501 plumes are also visible throughout the domain. In the unstable atmosphere, features with
502 high *LAVD* values exhibit no streamwise organization and a much more isotropic
503 distribution of vortices. Generalizing beyond this single realization, we can quantify the

504 mean geometry of vortices in each flow by comparing the orientation of *LAVD* surfaces
 505 over the whole sixty-minute periods.



506 **Fig 6:** Heat map distributions of spherical coordinates of coherent Lagrangian vortex surface normal vectors
 507 for the three stability simulations. Distributions are compared to curves that represent streamwise, vertical,
 508 and spanwise oriented cylinders, as well as a perfect cylindrical “roll” oriented 15° from streamwise and
 509 elevated 30° above the surface

510 Specifically, for each integration window, we first extract the roll and cell candidates
 511 as *LAVD* level-sets at our chosen thresholds, and calculate unit surface normal vectors for
 512 a triangulation of the surfaces. By definition, these vectors are aligned with the *LAVD*

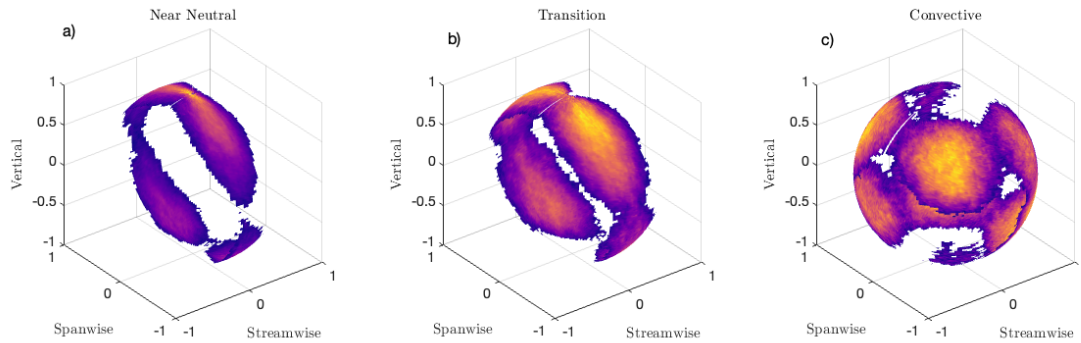
513 gradient on each vortical feature. It is widely suggested that horizontal rolls are quasi-linear
514 tube-like features that are oriented between 10° and 30° in the streamwise-spanwise plane
515 away from the streamwise direction (Banghoff et al. 2020), and may be elevated
516 approximately 30° above the surface (Zhou et al. 1999). We use this description as a
517 baseline with which to compare the orientations of our coherent Lagrangian vortices.

518 By translating each surface unit normal vector to the origin and converting to spherical
519 coordinates, we can compare the distribution of the orientation of surface tangent spaces
520 in the azimuth-elevation plane. With this novel approach, idealized cylindrical vortices will
521 have a distinct signature depending on the direction their rotational axis. We can then
522 compare how closely our vortices approximate these idealized structures.

523 In Figure 6, we provide heatmap distributions of the fraction of coherent Lagrangian
524 vortex normal vectors for the three stabilities on a 200×200 grid spanning the azimuth-
525 elevation plane. We also include the theoretical signatures of vertical, spanwise, and
526 streamwise oriented cylinders. We also include the trace of a horizontal cylindrical roll that
527 is rotated away from perfect streamwise alignment. Comparing the three experiments we
528 see that *LAVD* level-sets in near-neutral stability most closely match the idealized roll
529 suggesting not only that PALM is generating the correct structures observed in neutral
530 stability experiments, but that *LAVD* can also be used to extract individual experimentally-
531 verifiable structures in ABL turbulence.

532 The transitional scenario shows qualitatively similar orientations as the near-neutral
533 rolls, but with a larger degree of scatter. This compliments the findings in Figure 4 that,
534 while the structural organization of turbulence may appear similar, increased convection is
535 modifying the spatial distribution of vortical features as well as their actual shape. Vortices
536 in the convective case shows the widest range of surface-normal orientations, with no
537 distinct alignment with any specific direction. There is an increased probability of normal
538 vector orientations closer to the idealized vertical cylinder than in the near-neutral or
539 transitional cases, but it is not the dominant orientation for the convective case. This

540 suggests a much less linear orientation of cells in convective turbulence, and a more
541 random distribution of cell shapes.



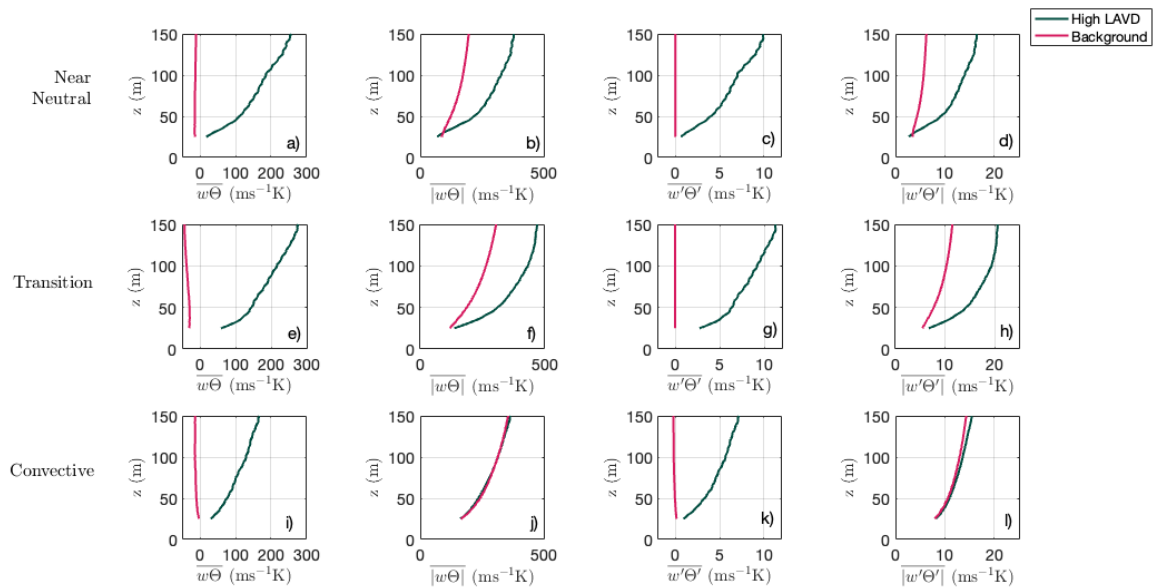
542 **Fig 7:** Three-dimensional visualization of coherent Lagrangian vortex surface normal vectors distributions
543 in spherical coordinates of for the three stability simulations. Corresponding ABL directions are labeled to
544 interpret the direction that surface normal vectors are typically oriented. The presence of rolls as influential
545 Lagrangian structures is evident in the near neutral and transitional case

546

547 In Figure 7 we supplement these heat map distributions by mapping them into
548 spherical coordinates with a fixed radius of one. To aid in visualization, we remove values
549 below a single fixed threshold ($2 \times 10^{-7}\%$) for all three cases. This leaves the
550 approximate orientation of the surface of only the most common vortices. The near-neutral
551 case has the narrowest distribution of surface normal vectors, suggesting we are
552 consistently extracting a recurrent roll structure throughout the whole sixty minutes of
553 simulation. In Figure 6 it is also easier to see the slight elevation angle away from the
554 surface in the near neutral case, though the central axis is closer to 15° than an idealized
555 30° . As mentioned before, the transitional case has a slightly wider distribution of
556 orientations, though the influence of the roll-structure is still visible. Once we move to the
557 strongly convective case, it is much harder to determine a typical orientation of the surface
558 of a typical vortex, again suggesting a much more isotropic distribution of turbulent
559 coherent structures.

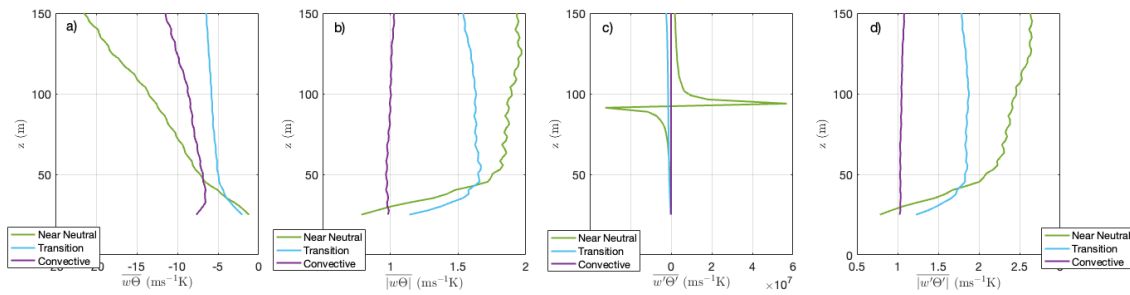
560 3.3 Coherent Lagrangian Vortices and Turbulent Heat Transport

561 Having shown that *LAVD* level-sets can indeed be used to identify the material boundaries
 562 of features that represent experimental descriptions rolls and cells, we now quantify the
 563 role of these vortices in the transport of heat in land-atmosphere interactions. We begin by
 564 investigating the advective and turbulent transport of heat. As mentioned before, advective
 565 and turbulent fluxes vary between different reference frames, and are therefore not
 566 representative of inherent physical processes in the wind, but they are nonetheless widely
 567 studied in boundary layer meteorology and are useful metrics for comparison and model
 568 parameterization. For each simulation, we separate the flow into coherent regions
 569 associated with being inside a coherent Lagrangian vortex, and an incoherent region in the
 570 surrounding turbulent flow. We then calculate the volume-averaged advective transport of
 571 heat ($\overline{w\Theta}$) and volume-averaged vertical turbulent transport of heat ($\overline{w'\Theta'}$) for 60
 572 realizations of *LAVD* fields spanning approximately a 1.5 million cubic metre volume. We
 573 also compare the volume-averaged magnitudes of these two fluxes to account for potential
 574 cancelations of fluxes of different sign.
 575



576 **Fig 8:** Comparison of advective and Turbulent Heat Flux profiles for different stabilities for fluid inside
 577 and outside coherent Lagrangian vortices
 578

579 Figure 8 compares the height-averaged advective and turbulent heat fluxes for the
 580 coherent vortex regions and the surrounding incoherent regions of the flow, while Figure
 581 9 shows the ratio of high and low *LAVD* flux values. In low *LAVD* regions, $\overline{w\Theta}$ and $\overline{w'\Theta'}$
 582 are of much smaller magnitude than the high *LAVD* fluid and typically slightly negative.
 583 One exception is the near-neutral cases, where $\overline{w'\Theta'}$ in the low *LAVD* region changes sign
 584 at approximately 90 metres, as can be clearly seen in Figure 9c. In the near neutral case,
 585 mean vertical advective transport of heat inside a coherent Lagrangian vortex is
 586 approximately 1.2 times stronger, and in the opposite direction, at $z=25$ metres, and 20
 587 times stronger at 150 metres. The amplification of advective heat transport is less
 588 pronounced for the transitional and convective case, but still ranges from two to twelve
 589 times stronger, and away from the surface.



590 **Fig 9:** Profiles of advective and turbulent heat flux ratios for different stabilities for fluid inside and
 591 outside coherent Lagrangian vortices. The values being compared are those in Figure 8

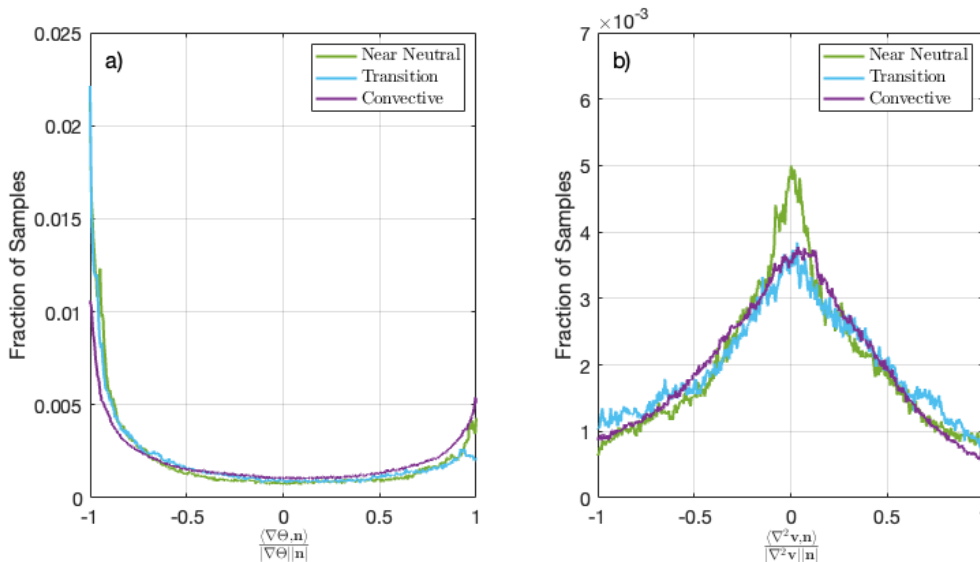
592

593 When ignoring the direction of advective heat transport, and compare only the mean
 594 magnitudes, we find that coherent Lagrangian vortices, rolls and cell, transport heat much
 595 more effectively than the surrounding fluid in the transition and near neutral cases. This is
 596 a significant difference, such that preferential sampling in observational studies and
 597 accurately resolving a statistically representative number of these structures in modeling
 598 studies needs to be considered. For example, a bulk transport coefficient that treats the
 599 entire flow domain homogeneously would inaccurately represent the total flux. For the
 600 convective case, the ratio of advective magnitudes is much closer to one, signifying a
 601 similar ability of coherent vortices and incoherent fluid to transport heat by advection,
 602 though only when neglecting the direction of transport.

603 Volume averages of turbulent fluxes show similar trends, with mean heat flux being
 604 of opposite sign, and much larger inside coherent vortices. The magnitude of turbulent heat
 605 flux inside vortices also increases with height for all stabilities. Neglecting the sign of
 606 turbulent flux, we find a similar trend as in the advective case with near neutral and
 607 transitional vortices containing signatures of much larger turbulent fluxes than the
 608 incoherent regions, and the coherent and incoherent regions having approximately the same
 609 magnitude for the convective case.

610 3.4 Objective Heat and Momentum Transport for roll-cell prediction

611 As discussed above, turbulent and advective fluxes of heat (and momentum) are frame-
 612 dependent diagnostics and insufficient for objectively describing flow physics in thermal
 613 fluids. This, and the common assumptions of horizontally homogeneous and flat terrain,
 614 makes comparisons of turbulent transport of scalars and momentum between different flow
 615 geometries, and their average statistics, highly non-trivial. Furthermore, stability measures
 616 based on turbulent fluxes, such as the Obukhov length, are not robust predictors of the
 617 presence rolls or cells in nonstationary flows.



618 **Fig 10:** Pointwise inner products of normalized diffusive heat flux (panel a) and diffusive momentum flux
 619 (panel b) across select LAVD surfaces from Figure 5 for the three stability regimes

620

621 Instead of focusing on stability as a prescriptive measure, we now seek to explain the
 622 transition from shear-dominated rolls to convective cells by describing the relative

623 influence of objective momentum and heat transport barriers in organizing Lagrangian
624 coherent structures of the flow. Using instantaneous velocity and temperature fields,
625 Aksamit et al. (2023) showed how the alignment of diffusive momentum and heat transport
626 vectors accurately diagnoses the relative influence of Coriolis-enhanced structures and
627 turbulent convective plumes in rotating Rayleigh-Bénard flow. We adapt this theory to
628 differentiate the relative influence of shear and convection generated structures and test it
629 in our ABL simulations. We hypothesize the momentum-heat barrier findings from
630 Aksamit et al. (2023) may be adapted as follows.

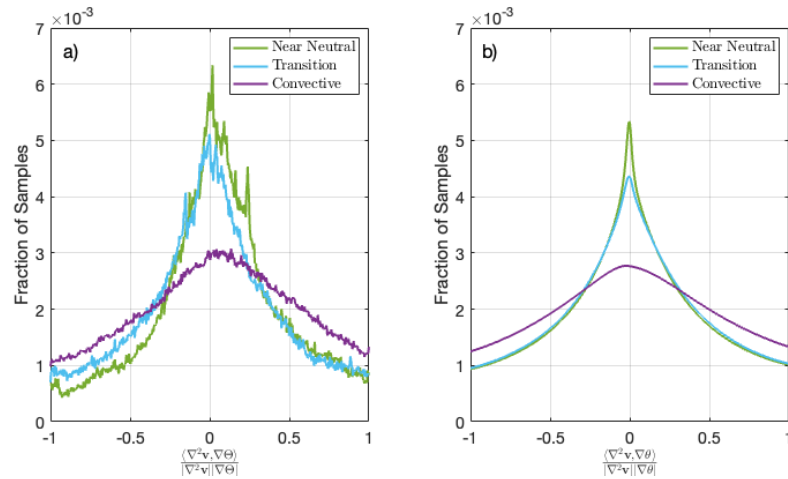
631 In the near-neutral atmosphere, weak temperature gradients do not result in the
632 creation of convective cells, and thus air temperature behaves more like a passive scalar
633 that is organized by Lagrangian coherent structures. Large temperature gradients are
634 generated across surfaces of distinct LCS, and thus LCS are closely aligned with diffusive
635 transport maximizers in the flow. At the same time, momentum plays a significant role in
636 organizing LCSs when convective influences are weak, with diffusive momentum
637 transport barriers closely aligned with Lagrangian coherent structures, and momentum
638 being convected along with the LCSs. In this scenario, gradients of temperature would be
639 orthogonal to the Laplacian of the velocity field as the former is the direction of diffusive
640 heat flux and the latter represents diffusive momentum flux.

641 As the relative influence of shear decreases and convection increases, momentum and
642 heat both compete to modify the velocity field, which in turn modifies the distribution of
643 momentum and heat. As was seen with the decreased influence of the Coriolis force in
644 rotating Rayleigh-Bénard convection, homogeneous regions of heat may become less
645 aligned with momentum when convection becomes more influential (Aksamit et al. 2023).
646 This results in a loss of momentum and heat transport barrier alignment, and a decreased
647 orthogonality of diffusive heat and momentum fluxes.

648 In Figure 10, we start with an individual example and evaluate the inner product of
649 heat and momentum flux vectors ($\nabla\theta$ and Δv , respectively) with surface normal vectors
650 on the *LAVD* level-sets isolated in Figure 5. Figure 10a shows a high degree of alignment
651 between vortex surface normal vectors and diffusive heat flux, suggesting the vortices are
652 effectively constraining the distribution of heat by maximizing the temperature gradient
653 across their borders. The orthogonality of *LAVD* level-set surfaces and the diffusive heat

654 flux decreases with decreasing stability, suggesting a decreased ability to perfectly resolve
 655 heat transport barriers by *LAVD* alone. As mentioned before, *LAVD* was mathematically
 656 derived to identify rotationally coherent vortices, and is independent of heat transport.
 657 Other Lagrangian diagnostics that minimize and maximize diffusive flux (i.e., diffusion
 658 barrier strength, (Haller et al. 2018)) are better suited for this purpose.

659 In Figure 10b, we compare the ability of our rolls and cells to block the objective
 660 transport of momentum across their surface. Vortices in near neutral condition have the
 661 greatest degree of tangency, but it is notable that tangency for the transitional and
 662 convective cases is comparable. This contrasts with the heat-blocking abilities of these
 663 same surfaces that actually decreases from the transitional to convective scenario. It is
 664 encouraging to see how even a rough numerical approximation of objective and material
 665 structures with *LAVD* level-sets can both extract rolls and cells, as well as provide
 666 physically meaningful comparisons of momentum and heat flux through those surfaces.



667 **Fig 11:** Pointwise inner products of normalized diffusive momentum and heat transport vector fields for the
 668 three stability regimes. In panel a) we show the selected inner products on the specific *LAVD* surfaces from
 669 Figure 5. Panel b) displays the bulk inner products for the entire simulations. Orthogonality increases as
 670 shear-driven structures (rolls) exhibit outsized control on the organization of heat distributions

671 The ability of coherent Lagrangian vortices to block momentum and heat transport
 672 varies as we change stability, but we can also investigate the alignment of momentum and
 673 heat barriers themselves in each flow. In Figure 11a we show how momentum and heat
 674 flux vectors align with each other on the same *LAVD* features examined in Figures 5 and

675 10. We find the strongest agreement on vortices in the near-neutral and transition cases,
676 with decreasing alignment as we increase convection. Generalizing to the entire flow, we
677 also calculate inner products of heat and momentum flux vectors for all the datapoints
678 resolved in our large eddy simulations. Figure 11b clearly shows a decreasing alignment
679 of heat and momentum transport with increasing convection, but all three stabilities have
680 a clear orthogonality preference, even when considering vectors not on the surface of
681 coherent Lagrangian vortices. This suggests a general agreement of heat and momentum
682 transport pathways, but that the transport of heat and momentum varies more as convective
683 cells begin to generate their own momentum, and alter the structure of momentum barriers.

684 **4 Conclusions and Outlook**

685 The transition from horizontal rolls to convective cells is a complex turbulence
686 organization problem resulting from competing physical influences that are poorly
687 understood. To study the behaviour of the atmospheric boundary layer under varying
688 stabilities, we introduced several new computational tools that identify atmospheric
689 structures as frame-indifferent and material features that exhibit exceptional rotation and
690 temporal coherence. The frame-indifference of our approach allows a physically
691 meaningful comparison with experimentally-observed tracer-organizing structures. This
692 contrasts with previous numerical investigations into ABL structure which rely on
693 statistical descriptions or correlations with frame-dependent diagnostic fields, and do not
694 actually extract temporally coherent fluid surfaces.

695 Being the first study to identify rolls and cells as *LAVD* level-sets, we compared
696 several geometric quantities of our surfaces with classic descriptions from experimental
697 observations. Two novel structure orientation visualization techniques allowed deeper
698 insight into the bulk geometry of coherent Lagrangian vortices for each stability, and opens
699 the door for future comparisons with other studies. We also qualitatively verified that the
700 individual *LAVD* structures we extracted do represent rolls and cells in the existing
701 literature.

702 We found that rolls and cells play an outsized role for turbulent and convective heat
703 fluxes when compared with other turbulent motions. In the near-neutral and transitional
704 atmosphere, high *LAVD* regions showed significant amplification of these spatially

705 averaged fluxes, and their spatially averaged magnitudes, when compared with the
706 surrounding fluid. For the convective atmosphere, the magnitude of convective and
707 turbulent fluxes was more evenly distributed inside and outside coherent Lagrangian
708 vortices, but total fluxes were still significantly larger. This suggests that the strength of
709 turbulence may be more isotropically distributed inside and outside rotational features in
710 the unstable boundary layer, but convective cells play a specific role in directing turbulent
711 and convective fluxes.

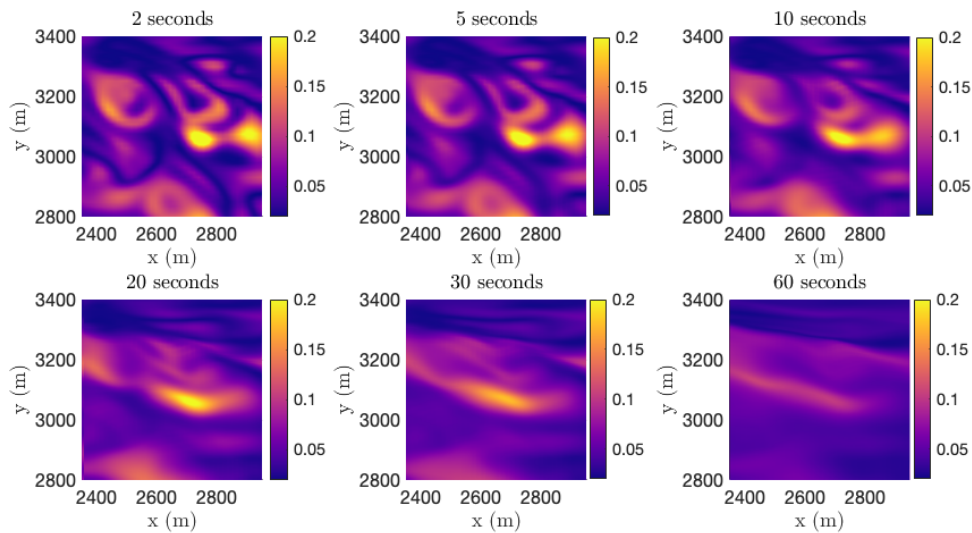
712 Finally, we utilized recent developments in the theory of diffusive momentum and
713 heat transport to describe the roles of shear and convective forces in a manner that is
714 objective, spatially and temporally resolved, and makes no assumptions on the geometry
715 or structure of the flow. The relative alignment of momentum and heat transport barriers
716 was found to correspond with the presence of horizontal rolls or convective cells. This
717 extends previous work that draws connections between mechanical and thermal influences
718 with the type of structures present in rotating Rayleigh-Bénard flow by way of momentum
719 and heat transport.

720 The relationship we found between objectively-defined momentum and heat transport
721 with the roll-cell transition suggests a physics-based understanding of this process may be
722 possible. The dominant influence of momentum barriers in the near-neutral atmosphere,
723 and complex the heat-momentum feedback in the unstable atmosphere provides an intuitive
724 description of this transition from physically meaningful vector fields.

725 By approaching the study of rolls and cells as objective and material structures, and
726 studying momentum and heat transport through objective flux definitions, we do not rely
727 on a given orientation or statistical stationarity to identify relevant fluid features. This may
728 not be of primary concern to boundary layer meteorologists that analyze time series data
729 from meteorological towers. However, when describing physical turbulent phenomena in
730 both spatially resolved numerical simulations and field observations, it is important to
731 consider whether or not diagnostics are meaningful in both scenarios, and if there are
732 fundamental benchmarks that are met in one (e.g., frame-indifference for structure
733 identification) we should at the very least consider this when attempting to discover
734 common ground.

735 Frame-indifferent descriptions of structures and fluxes also removes the need of many
 736 common assumptions for comparing the transport of scalars in ABLs, such as horizontally
 737 homogeneous terrain. In this way, our research is a proof-of-concept for a benchmark
 738 methodology that is suitable for comparing the existence and importance of atmospheric
 739 structures between flows in complex terrain, unsteady and transitional flows, flows around
 740 objects, and many otherwise incomparable situations.

741 5 Appendix



742 **Fig 12:** Effect of increasing integration time for LAVD fields at $z=25$ m. For 2 to 20 seconds, the dominant
 743 rotating structures appear in the same locations, but longer integration times reduce their impact on fluid
 744 trajectories as the material rotation is averaged over longer distances

745 In this appendix we provide a simple qualitative comparison of *LAVD* fields in the near-
 746 neutral boundary layer as calculated on the $z=25$ m plane. We compare advection times
 747 spanning two seconds to 60 seconds in Figure 12. At longer advection times, fluid particles
 748 interact with multiple turbulent coherent flow features, and *LAVD* fields are no longer
 749 representative of structures adjacent to initial fluid particle positions at the beginning of
 750 advection where the *LAVD* values are mapped. From two to ten seconds, there are only
 751 minor differences in *LAVD* fields, while at twenty seconds turbulent motions already begin

752 to obscure and elongate features. Beyond twenty seconds, full detail of the coherent fluid
753 behaviour at the spatial scales resolved in Figure 12 is largely lost.

754 **References**

- 755 Abernathey R, Haller G (2018) Transport by Lagrangian vortices in the eastern Pacific. *J*
756 *Phys Oceanogr* 48:667–685. <https://doi.org/10.1175/JPO-D-17-0102.1>
- 757 Adrian RJ, Meinhart CD, Tomkins CD (2000) Vortex organization in the outer region of
758 the turbulent boundary layer. *J Fluid Mech* 422:1–54.
759 <https://doi.org/10.1017/S0022112000001580>
- 760 Aksamit NO, Haller G (2022) Objective momentum barriers in wall turbulence. *J Fluid*
761 *Mech* 941:1–35. <https://doi.org/10.1017/jfm.2022.316>
- 762 Aksamit NO, Hartmann R, Lohse D, Haller G (2023) Interplay between advective,
763 diffusive, and active barriers in Rayleigh-Bénard flow. *J Fluid Mech* 969:A27.
764 <https://doi.org/10.1017/jfm.2023.563>
- 765 Aksamit NO, Kravitz B, Macmartin DG, Haller G (2021) Harnessing Stratospheric
766 Diffusion Barriers for Enhanced Climate Geoengineering. *Atmos Chem Phys*
767 21:8845–8861. <https://doi.org/doi.org:10.5194/acp-21-8845-2021>
- 768 Astarita G (1979) Objective and generally applicable criteria for flow classification. *J*
769 *Nonnewton Fluid Mech* 6:69–76. [https://doi.org/10.1016/0377-0257\(79\)87004-4](https://doi.org/10.1016/0377-0257(79)87004-4)
- 770 Banghoff JR, Sorber JD, Stensrud DJ, et al (2020) A 10-year warm-season climatology of
771 horizontal convective rolls and cellular convection in Central Oklahoma. *Mon*
772 *Weather Rev* 148:21–42. <https://doi.org/10.1175/MWR-D-19-0136.1>
- 773 Beron-Vera FJ, Hadjighasem A, Xia Q, et al (2019) Coherent Lagrangian swirls among
774 submesoscale motions. *Proc Natl Acad Sci U S A* 116:18251–18256.
775 <https://doi.org/10.1073/pnas.1701392115>
- 776 Beron-Vera FJ, Olascoaga MJ, Brown MG, Koçak H (2012) Zonal jets as meridional
777 transport barriers in the subtropical and polar lower stratosphere. *J Atmos Sci*
778 69:753–767. <https://doi.org/10.1175/JAS-D-11-084.1>
- 779 BozorgMagham AE, Ross SD (2015) Atmospheric Lagrangian coherent structures
780 considering unresolved turbulence and forecast uncertainty. *Commun Nonlinear Sci*
781 *Numer Simul* 22:964–979. <https://doi.org/10.1016/j.cnsns.2014.07.011>
- 782 Christian TW, Wakimoto RM (1989) The Relationship between Radar Reflectivities and
783 Clouds Associated with Horizontal Roll Convection on 8 August 1982. *Mon*
784 *Weather Rev* 117:1530–1544
- 785 Deardorff JW (1972) Numerical Investigation of Neutral and Unstable Planetary
786 Boundary Layers. *J Atmos Sci* 29:91–115
- 787 Dong Y, Tian W (2020) On the thresholds of vortex visualisation methods. *Int J Comput*
788 *Fluid Dyn* 34:267–277. <https://doi.org/10.1080/10618562.2020.1745781>
- 789 Drouot R (1976) Definition d'un transport associe un modele de fluide de deuxieme
790 ordre. *C R Acad Sci Pari Ser A* 282:923–926
- 791 Drouot R, Lucius M (1976) Approximation du second ordre de la loi de comportement
792 des fluides simples. Lois classiques deduites de l'introduction d'un nouveau tenseur
793 objectif. *Arch Mech Stos* 28:189=198

794 Eisma J, Westerweel J, van de Water W (2021) Do coherent structures organize scalar
795 mixing in a turbulent boundary layer? *J Fluid Mech* 929:1–19.
796 <https://doi.org/10.1017/jfm.2021.821>
797 Foken T (2008) *Micrometeorology*. Springer, Berlin
798 Foken T, Aubinet M, Finnigan JJ, et al (2011) Results of a panel discussion about the
799 energy balance closure correction for trace gases. *Bull Am Meteorol Soc* 92:13–18.
800 <https://doi.org/10.1175/2011BAMS3130.1>
801 Gao Q, Ortiz-Dueñas C, Longmire EK (2011) Analysis of vortex populations in turbulent
802 wall-bounded flows. *J Fluid Mech* 678:87–123.
803 <https://doi.org/10.1017/jfm.2011.101>
804 Garaboa-Paz D, Eiras-Barca J, Huhn F, Peérez-Münuzuri V (2015) Lagrangian coherent
805 structures along atmospheric rivers. *Chaos* 25:. <https://doi.org/10.1063/1.4919768>
806 Green MA, Rowley CW, Haller G (2007) Detection of Lagrangian coherent structures in
807 three-dimensional turbulence. *J Fluid Mech* 572:111–120.
808 <https://doi.org/10.1017/S0022112006003648>
809 Grossman RL (1982) An analysis of vertical velocity spectra obtained in the bomex fair-
810 weather, trade-wind boundary layer. *Boundary Layer Meteorol* 23:323–357.
811 <https://doi.org/10.1007/BF00121120>
812 Günther T, Horváth Á, Bresky W, et al (2021) Lagrangian Coherent Structures and
813 Vortex Formation in High Spatiotemporal-Resolution Satellite Winds of an
814 Atmospheric Kármán Vortex Street. *Journal of Geophysical Research: Atmospheres*
815 126:1–23. <https://doi.org/10.1029/2021JD035000>
816 Gurtin ME (1981) *An Introduction to Continuum Mechanics*, 1st edn. Academic Press,
817 San Diego, USA
818 Haller G (2020) Can vortex criteria be objectivized? *J Fluid Mech* 908:.
819 <https://doi.org/10.1017/jfm.2020.937>
820 Haller G (2005) An objective definition of a vortex. *J Fluid Mech* 525:1–26.
821 <https://doi.org/10.1017/S0022112004002526>
822 Haller G (2023) Transport Barriers in Flow Data: Advective, Diffusive, Stochastic and
823 Active Methods. In: *Transport Barriers and Coherent Structures in Flow Data*.
824 Cambridge University Press, Cambridge, UK
825 Haller G, Hadjighasem A, Farazmand M, Huhn F (2016) Defining coherent vortices
826 objectively from the vorticity. *J Fluid Mech* 795:136–173.
827 <https://doi.org/10.1017/jfm.2016.151>
828 Haller G, Karrasch D, Kogelbauer F (2018) Material barriers to diffusive and stochastic
829 transport. *Proceedings of the National Academy of Sciences* 115:9074–9079.
830 <https://doi.org/10.1073/pnas.1720177115>
831 Haller G, Katsanoulis S, Holzner M, et al (2020) Objective barriers to the transport of
832 dynamically active vector fields. *J Fluid Mech* 905:.
833 <https://doi.org/10.1017/jfm.2020.737>
834 He GS, Pan C, Feng LH, et al (2016) Evolution of Lagrangian coherent structures in a
835 cylinder-wake disturbed flat plate boundary layer. *J Fluid Mech* 792:274–306.
836 <https://doi.org/10.1017/jfm.2016.81>
837 Hunt JCR, Wray a a, Moin P (1988) Eddies, streams, and convergence zones in turbulent
838 flows. Center for Turbulence Research, *Proceedings of the Summer Program* 193–
839 208. <https://doi.org/CTR-S88>

840 Jayaraman B, Brasseur JG (2021) Transition in atmospheric boundary layer turbulence
841 structure from neutral to convective, and large-scale rolls. *J Fluid Mech* 913:1–31.
842 <https://doi.org/10.1017/jfm.2021.3>

843 Jeong J, Hussain F (1995) On the Identification of a vortex. *Journal of Fluid Mechanics*
844 285:69–94. <https://doi.org/10.1109/TCT.1956.1086328>

845 Kaszás B, Pedergnana T, Haller G (2023) The objective deformation component of a
846 velocity field. *European Journal of Mechanics, B/Fluids* 98:211–223.
847 <https://doi.org/10.1016/j.euromechflu.2022.12.007>

848 Khanna S, Brasseur JG (1998) Three-dimensional buoyancy- and shear-induced local
849 structure of the atmospheric boundary layer. *J Atmos Sci* 55:710–743.
850 [https://doi.org/10.1175/1520-0469\(1998\)055<0710:TDBASI>2.0.CO;2](https://doi.org/10.1175/1520-0469(1998)055<0710:TDBASI>2.0.CO;2)

851 Kline S, Reynolds W, Schraub F, Runstadler P (1967) The structure of turbulent
852 boundary layers. *J Fluid Mech* 30:741–773

853 Knutson B, Tang W, Chan PW (2015) Lagrangian coherent structure analysis of terminal
854 winds: Three-dimensionality, intramodel variations, and flight analyses. *Advances*
855 *in Meteorology* 2015:. <https://doi.org/10.1155/2015/816727>

856 Lehner M, Rotach MW (2018) Current challenges in understanding and predicting
857 transport and exchange in the atmosphere over mountainous terrain. *Atmosphere*
858 (Basel) 9:. <https://doi.org/10.3390/atmos9070276>

859 LeMone MA (1976) Modulation of Turbulence Energy by Longitudinal Rolls in an
860 Unstable Planetary Boundary Layer. *J Atmos Sci* 33:1308–1320

861 LeMone MA (1973) The Structure and Dynamics of Horizontal Roll Vortices in the
862 Planetary Boundary Layer. *J Atmos Sci* 30:1077–1091

863 Liu J, Gao Y, Liu C (2019a) An objective version of the Rortex vector for vortex
864 identification. *Physics of Fluids* 31:. <https://doi.org/10.1063/1.5095624>

865 Liu J, Gao Y sheng, Wang Y qian, Liu C (2019b) Objective Omega vortex identification
866 method. *Journal of Hydrodynamics* 31:455–463. [https://doi.org/10.1007/s42241-](https://doi.org/10.1007/s42241-019-0028-y)
867 019-0028-y

868 Lu SS, Willmarth WW (1973) Measurements of the structure of Reynolds stress in a
869 turbulent boundary layer. *J Fluid Mech* 60:481–511

870 Lugt HJ (1979) The Dilemma of Defining a Vortex. In: Müller U., Roesner K.G. SB (ed)
871 *Recent Developments in Theoretical and Experimental Fluid Mechanics*. Springer,
872 Berlin, Heidelberg

873 Maronga B, Banzhaf S, Burmeister C, et al (2020) Overview of the PALM model system
874 6.0

875 Mauder M, Foken T, Cuxart J (2020) *Surface-Energy-Balance Closure over Land: A*
876 *Review*. Springer Netherlands

877 Moeng C-H, Sullivan PP (1994) A Comparison of Shear and Buoyancy-Driven Planetary
878 Boundary Layer Flows. *J Atmos Sci* 51:999–1022

879 Neamtu-Halic MM, Krug D, Haller G, Holzner M (2019) Lagrangian coherent structures
880 and entrainment near the turbulent/non-Turbulent interface of a gravity current. *J*
881 *Fluid Mech* 877:824–843. <https://doi.org/10.1017/jfm.2019.635>

882 Olascoaga MJ, Brown MG, Beron-Vera FJ, Koçak H (2012) Stratospheric winds,
883 transport barriers and the 2011 Arctic ozone hole. *Nonlinear Process Geophys*
884 19:687–692. <https://doi.org/10.5194/npg-19-687-2012>

885 Pan C, Wang JJ, Zhang C (2009) Identification of lagrangian coherent structures in the
886 turbulent boundary layer. *Science in China, Series G: Physics, Mechanics and*
887 *Astronomy* 52:248–257. <https://doi.org/10.1007/s11433-009-0033-1>

888 Park SB, Baik JJ (2014) Large-eddy simulations of convective boundary layers over flat
889 and urbanlike surfaces. *J Atmos Sci* 71:1880–1892. [https://doi.org/10.1175/JAS-D-](https://doi.org/10.1175/JAS-D-13-0191.1)
890 [13-0191.1](https://doi.org/10.1175/JAS-D-13-0191.1)

891 Peacock T, Haller G (2013) Lagrangian coherent structures: The hidden skeleton of fluid
892 flows. *Phys Today* 66:41–47. <https://doi.org/10.1063/PT.3.1886>

893 Rutherford B, Dangelmayr G, Montgomery MT (2012) Lagrangian coherent structures in
894 tropical cyclone intensification. *Atmos Chem Phys* 12:5483–5507.
895 <https://doi.org/10.5194/acp-12-5483-2012>

896 Salesky ST, Chamecki M, Bou-Zeid E (2017) On the Nature of the Transition Between
897 Roll and Cellular Organization in the Convective Boundary Layer. *Boundary Layer*
898 *Meteorol* 163:41–68. <https://doi.org/10.1007/s10546-016-0220-3>

899 Schalkwijk J, Jonker HJJ, Siebesma AP, Van Meijgaard E (2015) Weather forecasting
900 using GPU-based large-Eddy simulations. *Bull Am Meteorol Soc* 96:715–723.
901 <https://doi.org/10.1175/BAMS-D-14-00114.1>

902 Serafin S, Adler B, Cuxart J, et al (2018) Exchange Processes in the Atmospheric
903 Boundary Layer Over Mountainous Terrain. *Atmosphere (Basel)* 9:102.
904 <https://doi.org/10.3390/atmos9030102>

905 Serra M, Sathe P, Beron-Vera F, Haller G (2017) Uncovering the edge of the polar
906 vortex. *J Atmos Sci* 74:3871–3885. <https://doi.org/10.1175/JAS-D-17-0052.1>

907 Speziale CG (1998) A review of material frame-indifference in mechanics. *Appl Mech*
908 *Rev* 51:489–504. <https://doi.org/10.1115/1.3099017>

909 Speziale CG (1979) Invariance of turbulent closure models. *Physics of Fluids* 22:1033–
910 1037. <https://doi.org/10.1063/1.862708>

911 Svensson N, Sahlée E, Bergström H, et al (2017) A Case Study of Offshore Advection of
912 Boundary Layer Rolls over a Stably Stratified Sea Surface. *Advances in*
913 *Meteorology* 2017:. <https://doi.org/10.1155/2017/9015891>

914 Tallapragada P, Ross SD, Schmale DG (2011) Lagrangian coherent structures are
915 associated with fluctuations in airborne microbial populations. *Chaos* 21:.
916 <https://doi.org/10.1063/1.3624930>

917 Tang W, Chan PW, Haller G (2011) Lagrangian coherent structure analysis of terminal
918 winds detected by lidar. Part I: Turbulence structures. *J Appl Meteorol Climatol*
919 50:325–338. <https://doi.org/10.1175/2010JAMC2508.1>

920 Truesdell C, Noll W (2004) *The Non-Linear Field Theories of Mechanics*, 3rd edn.
921 Springer

922 Wallace JM (2016) Quadrant Analysis in Turbulence Research: History and Evolution.
923 *Annu Rev Fluid Mech* 48:131–158. [https://doi.org/10.1146/annurev-fluid-122414-](https://doi.org/10.1146/annurev-fluid-122414-034550)
924 [034550](https://doi.org/10.1146/annurev-fluid-122414-034550)

925 Wang N, Ramirez U, Flores F, Datta-Barua S (2017) Lagrangian coherent structures in
926 the thermosphere: Predictive transport barriers. *Geophys Res Lett* 44:4549–4557.
927 <https://doi.org/10.1002/2017GL072568>

928 Weckwerth TM, Horst TW, Wilson JW (1999) An observational study of the evolution of
929 horizontal convective rolls. *Mon Weather Rev* 127:2160–2179.
930 [https://doi.org/10.1175/1520-0493\(1999\)127<2160:AOSOTE>2.0.CO;2](https://doi.org/10.1175/1520-0493(1999)127<2160:AOSOTE>2.0.CO;2)

931 Weckwerth TM, Wilson JW, Wakimoto RM, Crook NA (1997) Horizontal convective
932 rolls: Determining the environmental conditions supporting their existence and
933 characteristics. *Mon Weather Rev* 125:505–526. [https://doi.org/10.1175/1520-
934 0493\(1997\)125<0505:HCRDTE>2.0.CO;2](https://doi.org/10.1175/1520-0493(1997)125<0505:HCRDTE>2.0.CO;2)

935 Westerweel J, Fukushima C, Pedersen JM, Hunt JCR (2009) Momentum and scalar
936 transport at the turbulent/non-turbulent interface of a jet. *J Fluid Mech* 631:199–230.
937 <https://doi.org/10.1017/S0022112009006600>

938 Wilson ZD, Tutkun M, Cal RB (2013) Identification of Lagrangian coherent structures in
939 a turbulent boundary layer. *J Fluid Mech* 728:396–416.
940 <https://doi.org/10.1017/jfm.2013.214>

941 Yagi A, Inagaki A, Kanda M, et al (2017) Nature of Streaky Structures Observed with a
942 Doppler Lidar. *Boundary Layer Meteorol* 163:19–40.
943 <https://doi.org/10.1007/s10546-016-0213-2>

944 Young G, Kristovich D, Hjelmfelt M, Foster R (2002) Rolls, streets, waves, and more: A
945 review of quasi-two-dimensional structures in the atmospheric boundary layer. *Bull*
946 *Am Meteorol Soc* 997–1001

947 Zhou J, Adrian RJ, Balachandar S, Kendall TM (1999) Mechanisms for generating
948 coherent packets of hairpin vortices in channel flow. *J Fluid Mech* 387:353–396.
949 <https://doi.org/10.1017/S002211209900467X>

950