

The manuscript is a non-peer reviewed preprint submitted to EarthArXiv.

SENSITIVITY ANALYSIS OF GLOBAL KINEMATICS ON MANTLE STRUCTURE USING AUTOMATICALLY GENERATED ADJOINT THERMOCHEMICAL CONVECTION CODES

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Sensitivity Analysis of Global Kinematics on Mantle Structure Using Automatically Generated Adjoint Thermochemical Convection Codes

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SUMMARY

Within the past 30 years, numerical models of mantle convection have been able to predict observations on Earth and planets, and among them tectonics. The possibility of building inverse problems in global geodynamics became concrete, and often involve the development of adjoint codes. Such tools provide efficient ways to estimate sensitivities of misfit functions relative to control parameters, like errors on predicted velocities relative to mantle 3D structure. One issue to build an adjoint code is that such code is problem specific in many cases, while forward codes are versatile. We propose here a way to build adjoint codes that are exact adjoints of forward codes through an automated process. Using the automatic differentiation translator TAF (Giering and Kaminski (2003)) and incorporating specific implementations for MPI communications, we generate two adjoint codes of the 3D spherical thermomechanical mantle convection code StagYY (Tackley (2008)). We first present a benchmarking example computing the sensitivities of a thermal state to initial conditions with a 3D spherical thermochemical model. We then compute the sensitivities of present-day plate velocities relative to guessed temperature distribution in the mantle. The sensitivities reflect either the intrinsic sensitivity of the problem (sensitivity

17 to upper mantle structure) and the errors made in reconstructing the thermal structure of
18 the mantle (deepest mantle structure). Both codes successfully pass the rigorous and de-
19 manding gradient test, also called Taylor test. We show that our workflow for automatic
20 generation of adjoint codes for StagYY provides a sustainable and adaptive method to
21 engage in inverse modelling and sensitivity computations of 3D global geodynamics.

22 **Key words:** Adjoint, Automatic differentiation, inverse methods, mantle convection

23 1 INTRODUCTION

24 Modelling the flow within planetary mantles remains a horizon limited by both modelling capabili-
25 ties (theory, experiments and computers) and observations. Quantitatively describing the link between
26 what we observe at the surface of planets through geological mapping, geophysical probing, on one
27 side, and geochemical databases, on the other side, faces challenges: building dynamic models that
28 are predictive enough and inverse methods capable of dealing with complex models and both het-
29 erogeneous and sparse databases. In the past 20 years, geodynamic models of mantle convection and
30 lithosphere dynamics have made a leap forward by including 3D fine resolution, multi-physics and
31 more appropriate rock rheologies (Tackley (2012)). Therefore, they became more and more predictive
32 for fundamental aspects of Earth's geology and geophysics (Tackley (2000); Coltice et al. (2017)).

33 In the late 1990's beowulf computer clusters took mantle convection to a new stage: it was possible
34 to generate 3D spherical models at high convective vigor although rheological approximations were
35 crude (Bunge et al. (1996)). Capitalizing on geodynamics of the 1980's, a generation of models used
36 tectonic plate kinematics as surface boundary conditions (Bunge et al. (2000); Zhong et al. (2000)).
37 They predicted the large-scale temperature field that could be compared with tomographic models that
38 had also made decisive progress at the time (Grand et al. (1997)). (Bunge et al. (2003)) proposed an
39 inverse methodology with these forced models, using the tomographic images as the target quantity
40 and 3D temperature field in the past as the control variable. The goal was to retrieve the 3D thermal
41 history of the mantle through the Cenozoic. The method relies on an adjoint code, which provides in
42 one step the sensitivity of a misfit function to the full set of control variables (Talagrand (1997)). In
43 order to realise an inversion, both forward and adjoint code have to be embedded with a minimisation
44 scheme. In (Bunge et al. (2003)), the adjoint code was built by solving adjoint equations with similar
45 solvers as the forward code, neglecting the treatment of strong lateral viscosity variations or stress-
46 dependent rheologies. The same year, (Ismail-Zadeh et al. (2003)) also proposed an inverse approach
47 to a similar inverse problem, solving the adjoint equation for temperature and accounting for pressure

48 and temperature dependent viscosity in the inversion scheme. This work was further developed in
49 a subsequent paper (Ismail-Zadeh et al. (2004)). This was a first step for a lineage of studies (Liu
50 and Gurnis (2008); Liu et al. (2008); Ghelichakhan and Bunge (2018); Colli et al. (2018)). Initial
51 thermal conditions and rheological parameters are the two ingredients for predicting a geodynamical
52 evolution (initial chemical composition could also be considered). The latter has been the focus of
53 inverse methods in lithosphere modeling using surface deformation, stresses and gravity as targets
54 (Baumann et al. (2014); Reuber et al. (2020)).

55 In the past 10 years, the parameterisation of 3D spherical models of mantle convection improved
56 to generate surface tectonics self-consistently, which opened the way to study global tectonics and
57 thermal mantle structure together (Cramer et al. (2014); Coltice et al. (2019)). The recipe relies on
58 a rheological approximation of mechanical properties of rocks. Exponential temperature-dependent
59 viscosity allows a strong lid to form as long as viscosity contrasts are larger than 10^3 . Combining
60 it with a yield stress formulation generates strain localization on narrow boundaries and a strong
61 toroidal velocity component (Tackley (2000)). Such models produce Earth's like area-age distributions
62 (Coltice et al. (2012)), plate size distributions (Mallard et al. (2016)), supercontinent cycles (Rolf et
63 al. (2014)), transform-like structure (Langemeyer et al. (2021)), plate reorganizations (Coltice et al.
64 (2019)), and hotspot properties (Arnould et al. (2020)). Capitalizing on the forecasting behavior of
65 these models (Coltice and Shephard (2018)), two groups have developed inverse methods targeting
66 surface observations to unravel deep properties. (Bocher et al. (2016); Bocher et al. (2018)) proposed
67 Bayesian data assimilation strategies to infer the internal temperature evolution from heat flow and
68 kinematics at the surface in synthetic 2D models. These Kalman filter methods employ the forward
69 convection code and exploit statistical properties of convective flows to fit the data. (Worthen et al.
70 (2014); Ratnaswamy et al. (2015); Li et al. (2017)) have proposed adjoint-based strategies to evaluate
71 quantitatively the trade-off between rheology and internal temperature when fitting surface kinematics.
72 They solve adjoint equations in 2D models focused on subduction.

73 An adjoint code is built by differentiating the forward code and reversing the chain rule of elemen-
74 tary actions (Talagrand (1991); Talagrand (1997)). Changing the target quantities and/or the control
75 variable means that each new geodynamic inverse problem requires its specific adjoint code develop-
76 ment, although the forward code remains the same. The core of the adjoint code can however be very
77 similar if two problems involving the exact same control variables. The loss of versatility of adjoint
78 codes relative to forward codes can restrict the variety of geodynamic problems to be studied. There-
79 fore, we propose here a framework for automatically generating and maintaining adjoint codes for
80 multi-geometry, multi-physics convection code StagYY (Tackley (2008)). We adapt the forward code
81 StagYY and the automatic differentiation translator TAF (Giering and Kaminski (2003)) to generate

82 tangent linear and adjoint codes. We describe here the methodology and realise an exacting bench-
83 marking (ensuring that the adjoint code is the exact adjoint of the forward code) with gradient tests on
84 3D spherical thermochemical convection cases with and without non-linear rheology. We do not re-
85 alise here inversions here but rather focus on the evaluation of outcomes of adjoint codes. We compute
86 the sensitivities of plate velocities to the 3D temperature field in a mantle flow model with plate-like
87 behavior. We explore how sensitivities depend on the guessed temperature distribution in the mantle
88 and rheological parameters.

89 **2 THE FORWARD MANTLE CONVECTION CODE: STAGYY**

90 **2.1 30 years of StagYY code development**

91 The simulation code StagYY originated in 1992 and has been expanded and enhanced since then. Orig-
92 inally called Stag3D and written in Fortran 77 to model infinite Prandtl number, variable-viscosity con-
93 vection in 3D Cartesian geometry, the first resulting publication was (Tackley (1993)). Subsequently,
94 Stag3D was enhanced to include phase transitions (Tackley (1996)) and to track chemical variations
95 using a marker-in-cell technique (Tackley (1998)). It was used to produce some of the first 3D mod-
96 els of self-consistent plate tectonics, using strain-rate-weakening or plastic rheology (Tackley (1998);
97 Tackley (2000)). Next, two-dimensional cylindrical geometry was added as an option, as were the
98 abilities to model melting-induced chemical differentiation (Xie and Tackley (2004)) and couple core
99 evolution to the mantle (Nakagawa and Tackley (2004))

100 Stag3D was transformed into StagYY by converting to Fortran 90 and adding 3-D spherical ge-
101 ometry (Tackley (2008)). A new 2-D spherical approximation, the spherical annulus, was also im-
102 plemented (Hernlund and Tackley (2008)). Subsequent enhancements include coupling to plate mo-
103 tion histories (Bello et al. (2015)), visco-elasticity (Patočka et al. (2017)), a more advanced melting
104 treatment that can produce continental crust in addition to the previously-implemented oceanic crust
105 (Jain et al. (2019)) and multiple impacts (Borgeat and Tackley (2022)). StagYY has been applied to
106 model Earth and various planets including including Mars (Keller and Tackley (2009)), Venus (Ar-
107 mann (2012)) and super-Earths (Tackley et al. (2014)).

108 Besides the benchmarking of the code presented in some of the publications cited above, such
109 as (Tackley (2008)), StagYY was part of community benchmarking initiatives (Crameri et al. (2011);
110 Tosi et al. (2015)).

111 2.2 Equations

112 The truncated anelastic approximation is assumed (see details in (Tackley (2008)) and (Ricard et al.
113 (2022))) for more on compressibility approximations, leading to the following set of equations for
114 conservation of mass:

$$115 \quad \nabla \cdot (\bar{\rho} \mathbf{v}) = 0, \quad (1)$$

116 momentum

$$117 \quad \nabla \cdot \underline{\underline{\sigma}} - \nabla p = \rho \vec{g}, \quad (2)$$

118 and energy

$$119 \quad \rho C_p \frac{DT}{Dt} = -\bar{\alpha} \bar{\rho} T v_r + \nabla \cdot (k \nabla T) + \bar{\rho} H + \underline{\underline{\sigma}} : \underline{\underline{\dot{\epsilon}}}, \quad (3)$$

120 where \mathbf{v} is velocity, v_r being the radial component, p is pressure, $\underline{\underline{\sigma}}$ is the deviatoric stress tensor and
121 $\underline{\underline{\dot{\epsilon}}}$ the strain-rate tensor (the latter two are given by standard expressions in Cartesian or spherical polar
122 coordinates with variable viscosity), and physical properties are density ρ , gravitational acceleration
123 vector \vec{g} , specific heat capacity C_p , thermal expansivity α , thermal conductivity k and internal heating
124 rate H . Overbars denote reference state properties that are dependent on depth only. StagYY can
125 be run using either dimensional or non-dimensional units, in which case the physical properties are
126 relative to reference values and the Rayleigh number is incorporated into the right-hand side of the
127 momentum equation (see (Tackley (2008))); further to this, the Boussinesq approximation allows for
128 setting all material properties except viscosity equal to 1 and deleting the adiabatic heating and viscous
129 dissipation terms in the energy equation (the first and last terms on the right-hand side, respectively).

130 Probably the most important physical property is viscosity, which appears in the stress expression
131 and can vary by many orders of magnitude. In StagYY it can be dependent on temperature, pressure,
132 stress, composition, and accumulated strain, with choices of viscosity laws for these various depen-
133 dencies.

134 When compositional variations are tracked, the following must be satisfied:

$$135 \quad \frac{DC_i}{Dt} = 0 \quad (4)$$

136 where C_i is the fraction of compositional component i .

137 Partial melting is also implemented, as well as melt-solid segregation and intrusive and extrusive
138 magmatism. For details of the latest treatment see (Jain et al. (2019)).

139 **2.3 Numerical methods**

140 A finite volume discretization is used, with velocity components and pressure defined on a staggered
141 grid (Patankar(1980); Ogawa et al. (1991)). Both cartesian and spherical grids are implemented, and in
142 both two and three dimensions. For three-dimensional spherical geometry covering a complete sphere,
143 the yin-yang spherical grid is used (Kageyama and Sato (2004)), which covers the sphere using two
144 overset patches similar to the construction of a tennis ball - here the minimum overlap version is
145 used. For two-dimensional spherical geometry, the spherical annulus geometry is used (Hernlund and
146 Tackley (2008)).

147 The momentum and pressure equations are solved simultaneously using either a geometric multi-
148 grid solver or (in 2-D) a choice of direct solvers. In the case of nonlinear rheology (plasticity or
149 dislocation creep), Picard iterations are used to converge on the correct viscosity. The energy equation
150 is time-stepped explicitly.

151 Tracers (markers) are used to track compositional information, both for bulk composition and
152 trace-element composition, and may optionally also track temperature and/or viscosity. They are ad-
153 vected using a 4th-order Runge-Kutta method. See (Tackley and King (2003)).

154 **2.4 Implementation**

155 StagYY is written in Fortran using features introduced up to Fortran 2013. It may be compiled in
156 isolation, or linked to one or more libraries, the main ones being MPI (for parallelisation), HDF5
157 (for input/output), and PETSc, MUMPS and UMFPACK (for direct solvers). Parallelisation uses a
158 three-dimensional domain decomposition; when using the yin-yang grid the maximum azimuthal de-
159 composition is currently limited to 8 ways.

160 **3 AUTOMATIC GENERATION OF ADJOINT CODE OF STAGYY**

161 **3.1 Principles of automatic differentiation**

162 Algorithmic Differentiation (AD), also known as Automatic Differentiation, holds significant poten-
163 tial for geodynamicists seeking to analyze derivatives in the context of their algorithms, such as those
164 embedded in software like StagYY. This technique enables the computation of function derivatives
165 (for instance the sensitivity of the difference between plate velocities and those predicted by a geo-
166 dynamic model as a function of the 3D temperature field) directly from algorithmic source code. The
167 core concept of AD rests on recognizing that even the most intricate algorithms can be deconstructed
168 into a sequence of elementary operations. These operations, which manipulate numerical values, can
169 be differentiable, yielding local Jacobian information (Talagrand (1991)). By applying the chain rule,

170 we can aggregate these local Jacobians to obtain the complete derivative of the algorithm. This deriva-
171 tive takes the form of a product of Jacobian matrices. Notably, the associativity property of matrix
172 multiplication empowers us to compute this matrix product in various orders.

173 Two prominent orders are particularly relevant: the forward order and the reverse order (see Fig.1).
174 The forward order, also termed forward mode in the AD context, mimics the original algorithm's pro-
175 gression. In contrast, the reverse mode initiates its calculation from the Jacobian of the final elemen-
176 tary operation. The selection between these modes hinges on the characteristics of the function under
177 consideration. In instances where the function is scalar, meaning it produces a solitary pertinent out-
178 come (dependent variable) through mapping from multiple independent parameters, the reverse mode
179 proves advantageous. This is the case when the problem evaluates a cost function. This preference
180 arises because the reverse mode begins with a scalar sensitivity, which quantifies the derivative of the
181 final result concerning itself (typically equal to one). Consequently, the reverse mode predominantly
182 involves matrix-vector multiplications.

183 The forward mode corresponds to the tangent linear model (Fig.1 middle row), while the reverse
184 mode corresponds to the adjoint model (Fig.1 bottom row). When confronted with scenarios featuring
185 only a handful of independent parameters but yielding numerous dependent outcomes, the forward
186 mode usually exhibits superior performance. This is when for instance one seeks to compute the
187 gradient of the surface velocities of the convection model with respect to a limited set of material
188 properties (viscosity parameters).

189 In the realm of AD, two primary methodologies have emerged. The first approach, known as AD
190 by operator overloading (e.g. (Walther and Griewank (2012))), exploits a distinctive feature within
191 programming languages. This feature allows the customization of individual operations, such as '*',
192 to encompass additional computations for derivatives. In contrast, source-to-source AD tools adopt a
193 different strategy. These tools, such as TAF (Giering and Kaminski (1998)) or TAPENADE (Hascoët
194 and Pascual (2013)), generate novel derivative code within a specific programming language. This
195 process mirrors the functioning of compilers, reading and parsing the existing code, analyzing its
196 structure, and transforming its internal representation before reconstructing it (unparsing). The ensuing
197 transformation adheres to either forward or reverse mode principles, yielding tangent linear or adjoint
198 code correspondingly.

199 While the implementation of AD by operator overloading as an automated tool is relatively easy
200 compared to source-to-source AD, it comes at the expense of heightened resource demands in terms of
201 memory and runtime for the resulting program. It is noteworthy that a multitude of AD tools now offer
202 support for a range of different source code languages. The application of AD in geodynamics poses
203 several challenges. These encompass the computational efficiency of the derivative code, compatibility

204 with language standards of the source code, and accommodation for parallel computing like OpenMP,
205 MPI, and coarray Fortran. Addressing these challenges is paramount to unlocking the full potential of
206 Automatic Differentiation.

207 **3.2 TAF: source-to-source translator**

208 Transformation of Algorithms in Fortran (TAF) presents a valuable source-to-source AD tool, as de-
209 tailed in (Giering and Kaminski (2002a)). TAF notably accommodates a wide spectrum of the Fortran
210 standard, spanning from FORTRAN-77 through Fortran-2018. This versatility empowers TAF to gen-
211 erate both adjoint and tangent linear codes through reverse and forward modes, respectively.

212 The adjoint code excels in efficiently computing gradients, which find application in gradient-
213 based optimization techniques. This is the case for geodynamic inversions, such as finding mantle
214 convection initial conditions to generate an accurate prediction of a temperature structure interpreted
215 from a tomographic model (Bunge et al. (2003); Liu et al. (2008)). Furthermore, this adjoint code
216 can undergo differentiation once more. This subsequent differentiation generates code primed for the
217 computation of the Hessian matrix. Within the realm of inversion problems, the inverse Hessian fur-
218 nishes the uncertainty covariance matrix of the outcomes, thereby facilitating the proper utilization of
219 the results in a meaningful manner.

220 The influence of source-to-source AD, demonstrated through TAF, resonates across a diverse spec-
221 trum of scientific domains. These domains include climatology (Blessing et al. (2014)), oceanography
222 (Heimbach et al. (2005)), satellite remote sensing (Blessing and Giering (2021)), and engineering
223 (Othmer et al. (2006)). Such versatility underscores the utility of TAF and analogous tools in address-
224 ing an array of complex problems that span multiple fields.

225 **3.3 Taping and checkpointing**

226 Given that the StagYY code, much like other advanced models in the geosciences domain, involves
227 inherently solving nonlinear equations, the process of linearization is contingent on the prevailing
228 system state (such as mantle temperature field in most cases). Consequently, for the propagation of
229 sensitivities using reverse mode (i.e., the adjoint model), access to the system state becomes impera-
230 tive. However, it is important to note that the adjoint model functions in reverse, navigating from the
231 final state to the initial state. This contrasting operational directionality prompts a challenge: the states
232 required for adjoint computations must be provided in the reverse order compared to their original
233 computation sequence. In this context, two primary strategies exist: taping and recomputation.

234 Taping entails the storage of states either in memory or on external storage like disk. This stored
235 data is then accessed when needed. On the other hand, an alternative approach involves recomputing

236 a specific state based on an available initial or intermediate state (often referred to as a checkpoint).
237 While the former demands additional memory or disk resources, the latter necessitates extra com-
238 putational time. In practice, a judicious combination of both strategies, termed checkpointing, has
239 demonstrated optimal outcomes. This approach minimizes the demand for substantial supplementary
240 memory resources by introducing a modest increase in computational time (Griewank and Walther
241 (2000); Giering and Kaminski (2002b)).

242 Within the StagYY framework, a pragmatic approach has been taken. TAF "store"-directives have
243 been integrated at the onset of the time-stepping loop and at various other strategic points. These
244 directives effectively mitigate the need for default recomputations that arise from TAF, thus optimizing
245 the sensitivity propagation process.

246 **3.4 MPI**

247 In the context of parallel computing in StagYY, the Message Passing Interface (MPI) plays a crucial
248 role as the library of routines for enabling parallelism. It's important to note that, since MPI is not
249 inherently integrated into the programming language, Automatic Differentiation (AD) tools must pos-
250 sess the capability to handle MPI library calls. This introduces a distinctive challenge that has given
251 rise to three distinct approaches. One prevalent approach involves the implementation of MPI commu-
252 nication within separate, higher-level routines often referred to as 'wrapper' routines. These wrappers
253 consolidate multiple individual communications for updating border grid points across neighboring
254 domains in domain decomposition scenarios. The adjoint routines for these wrappers are manually
255 crafted and AD-specific directives are inserted that provide the necessary information for the AD tool.
256 This strategy has been successfully employed in parallelizing models like the global ocean-atmosphere
257 circulation model MITgcm (Heimbach et al. (2005)). An alternative and more generalized approach
258 has been proposed by (Utke et al. (2009)), extending frequently used MPI-library routines with addi-
259 tional arguments that carry essential information required for adjoint computation. Adjoint and tan-
260 gent routines are then incorporated into an Adjoinable MPI (AMPI) library to enable the generation
261 of proper calls to the modified MPI routines.

262 The third approach, employed in this context, entails the direct differentiation of MPI library calls
263 by TAF. This methodology demands an additional global analysis of data transfer between processes,
264 due to the low-level nature of MPI (one has to explicitly provide the details of the message passing).
265 While collective communications, being group based and synchronized are relatively straightforward
266 to implement, point-to-point (P2P) communications, especially non-blocking ones, pose a substantial
267 challenge as they involve direct communication between two specific processes and involves asyn-
268 chronicity. These non-blocking P2P communications consist of multiple MPI library calls, making

269 their differentiation intricate. In the case of StagYY, which employs both collective and non-blocking
 270 P2P communications, the specific challenges of differentiating MPI library calls have been addressed.
 271 This intricate process is further detailed in an upcoming paper (Giering (2023)).

272 3.5 Changes to StagYY to apply TAF

273 Automatic Differentiation (AD) assumes a critical premise: that the algorithm under scrutiny behaves
 274 akin to a well-defined function, consistently producing the same outcomes for a given set of input
 275 values, which represent the control variables in our geodynamic problems. To make this work seam-
 276 lessly, we have incorporated specialized interface routines. These routines serve as bridges between
 277 StagYY algorithms and the AD tool. They ensure that necessary initializations occur before an algo-
 278 rithm kicks into gear, they define the essential connections between inputs and outputs of the function,
 279 and they guarantee that the initial state is faithfully restored each time the function is invoked. Using
 280 pseudo-random numbers does not guarantee exact reproducibility between two runs. In this context,
 281 we switched them off to ensure the fidelity of these properties.

282 In order to help TAF to generate efficient adjoint code, directives have been inserted in STagYY
 283 in addition to the aforementioned “store”-directives which support the data flow analysis and ensure
 284 that the code generated by TAF is efficient and accurate.

285 4 RESULTS

286 4.1 Benchmarking preamble

287 In this section we present 2 cases of automatically generated 3D spherical convection adjoint codes and
 288 their benchmarking. The methodology to test the quality of adjoint codes is the gradient test (Navon et
 289 al. (1992); Andersson et al. (1994)), sometimes called Taylor test (Charpentier and Ghemires (2000)),
 290 an exacting benchmark for adjoint codes. It ensures the adjoint code is the exact adjoint of the forward
 291 code. Convergence of finite-difference towards the computed adjoint is not enough or not straightfor-
 292 ward in the numerical context, because of the multiple factors which influence the computation of the
 293 finite-difference approximation. Obtaining the exact adjoint of the forward code, providing the exact
 294 numerical gradients is a key for an optimization process. Note that we do not perform optimization
 295 procedures to solve an inverse problem in the following work but we perform sensitivity evaluations.

296 We define a cost function $\mathcal{J}(\mathbf{x})$ for a state \mathbf{x} . The gradient test relies on a Taylor expansion of the
 297 cost function for a perturbed state $\mathbf{x} + \alpha\delta\mathbf{x}$:

$$298 \mathcal{J}(\mathbf{x} + \alpha\delta\mathbf{x}) = \mathcal{J}(\mathbf{x}) + \alpha\langle\nabla\mathcal{J}, \delta\mathbf{x}\rangle + \alpha^2\mathcal{O}(\delta\mathbf{x}^2), \quad (5)$$

where α is a scalar defining the intensity of the perturbation, $\delta\mathbf{x}$ a random perturbation vector comensurate with \mathbf{x} and $\langle \nabla \mathcal{J}, \delta\mathbf{x} \rangle$ the sensitivity of \mathcal{J} to a perturbation in \mathbf{x} . The latter is given by running the adjoint code while $\mathcal{J}(\mathbf{x})$ and $\mathcal{J}(\mathbf{x} + \alpha\delta\mathbf{x})$ are computed with the forward code. The residue being

$$\mathcal{R}(\alpha) = \mathcal{J}(\mathbf{x} + \alpha\delta\mathbf{x}) - \mathcal{J}(\mathbf{x}) - \alpha\langle \nabla \mathcal{J}, \delta\mathbf{x} \rangle \quad (6)$$

has therefore to scale with α^2 . This test does multiple things at once. It helps to identify the range for which the truncated Taylor expansion is a good approximation to the gradient ($\mathcal{R}(\alpha) \sim \alpha^2$ range), the range where the finite-differences approximation is the numerically best-possible approximation to the gradient ($\mathcal{R}(\alpha) \sim \text{const.}$ range), and the range where α is too small to make a difference numerically in $\mathcal{J}(\mathbf{x} + \alpha\delta\mathbf{x})$ ($\mathcal{R}(\alpha) \sim \alpha$ range). If these ranges can be identified, there is confidence that the finite-differences-approximation of the gradient would converge to the gradient computed with the adjoint if there were no limitations in numerical representation.

4.2 A benchmarking example

We generate automatically an adjoint code to illustrate and benchmark the workflow. The goal of the following test is to explore specific capabilities that could be used for mantle convection inverse problems, but using a simplified abstract case, which targets the computation of the sensitivities of an initial temperature field to the error between a predicted state and a known temperature field. The corresponding adjoint code would be relevant to the published strategies for inferring past mantle circulation (Bunge et al. (2003); Ismail-Zadeh et al. (2003); Ismail-Zadeh et al. (2004); Liu and Gurnis (2008)). The test we implement focuses mainly on transport of heat and composition. The code uses the multi-grid solver of StagYY, the yin-yang-layout of the grid and the tracer ratio method.

In the adjoint code, the specific heat field is the control variable, being in this case the local temperature times the cell volume (the problem hereafter being incompressible and in its non-dimensional form). The cost function evaluates the heat difference between the predicted state and the reference state:

$$\mathcal{J}^T = \sum_i^{\mathcal{V}} (T(x_i) - T_0(x_i))^2 \Delta V(x_i), \quad (7)$$

where T is the final volume-centered temperature in the model, T_0 the targeted final volume-centered temperature field, (x_i) the coordinates of the cell center and ΔV the value of the local volume (the global volume being V). The summation is over full volume \mathcal{V} . Such adjoint code could in principle be used to retrieve the initial conditions to match a final temperature structure deduced from seismic tomography (Bunge et al. (2003); Ismail-Zadeh et al. (2003); Ismail-Zadeh et al. (2004); Liu et al. (2008)). This adjoint code generated by TAF is 270 399 lines while the forward code is 75 960 lines.

Parameter	Non dimensional value
Rayleigh number	10^6
Heat production rate	35
Top temperature	0
Basal temperature	1
Depth of basal layer	0.3
Viscosity of basal layer	50
Buoyancy ratio of basal layer	1
Number of cells	786 432
Number of tracers	8 000 000
Average resolution	90 km

Table 1. Non dimensional parameters of the convection model used for benchmarking the adjoint code

330 A fraction of the increased number of lines comes from the fact that the adjoint code has one line for
 331 one variable declaration whereas the forward code can have one line of several variable declarations.

332 We perform a gradient test to verify the adjoint code is the exact adjoint of the forward code. For
 333 this benchmarking case, we specifically choose an abstract case for 2 goals: being easily computed
 334 so it has to be small enough; using a variety of the code capabilities so it has to be complex enough.
 335 The rheological complexity is explored in the following geodynamic application. We choose an in-
 336 compressible 3D spherical convection model with a composition-dependent viscosity, the goal being
 337 here to focus on the time-dependent transport sections of the code (temperature and composition). We
 338 consider two materials here: ambient mantle and a deep dense and more viscous layer. The properties
 339 of this layer are set to typical values suitable to study the stability of a primordial dense viscous layer
 340 on a planet (such as in (Kreielkamp et al., (2002))). We solve the composition evolution equation us-
 341 ing the tracer ratio method. The set of parameters for the model is in Table 1. The forward calculation
 342 corresponds to the convection evolution from a designed initial condition and runs over 10 time steps
 343 equivalent to a dimensionless time of 10^{-5} (equivalent of 3 My), being enough to start develop the
 344 instabilities (see Fig.2). More timesteps would require to implement specific strategies for taping to
 345 optimize computing speed, which is not the goal here. Fig.2 shows the initial and final temperature
 346 and compositions fields for the trial and the targeted temperature field.

347 The sensitivity obtained running the adjoint code is shown in Fig. 3. In the volume section, we
 348 identify that heating the initial state would decrease the cost function and we can identify areas in
 349 upwellings that should be cooled off. For the gradient test, we compute $\mathcal{R}(\alpha)$ for a variety of α
 350 between 10^{-15} to 10^{-4} , using a vector $\delta\mathbf{x}$, which individual components are random numbers ranging

351 from 0 to 1. The cost function for this case is 3.561. $\mathcal{R}(\alpha)$ reaches the machine ε for *alpha* around
 352 10^{-12} . $\mathcal{R}(\alpha)$ decreases as α^2 for larger values of α and becomes more linear as the machine ε is
 353 reached.

354 Without optimization, this automatically generated adjoint code passes the gradient test. This ad-
 355 joint runs 11 times slower than the forward code, the latter running in 39 seconds over 32 cores on an
 356 AMD Ryzen Threadripper 3990X processor.

357 **4.3 Sensitivity of surface kinematics to convective mantle temperature structure**

358 *4.3.1 Forward problem*

We now automatically generate an adjoint code to estimate the sensitivity of surface velocities to temperature anomalies in the mantle-lithosphere system. We consider here a 3D spherical convection model with plate-like behavior, which we will use for instantaneous calculation of mantle flow and surface kinematics. Viscosity depends exponentially on temperature and depth:

$$\mu(z, T) = \mu_0(z) \exp \frac{E_a}{T}$$

359 with μ being the dimensionless viscosity, $\mu_0(z)$ the viscosity prefactor, E_a the activation energy, and
 360 T the absolute dimensionless temperature.

361 $\mu_0(z)$ is chosen (1) to obtain a reference dimensionless viscosity is 1 for a non-dimensional tem-
 362 perature of 0.64 at zero pressure, the expected temperature at the base of the cold boundary layer
 363 before the realization of the calculation, and (2) to allow for a viscosity jump at 660 km as expected
 364 from geoid inversions (Ricard et al. (1993)), although this depth could be extended deeper (Rudolph et
 365 al. (2015)). This specific value is selected prior to the calculation to align with the anticipated temper-
 366 ature at the base of the upper boundary layer. To prevent excessive variations in viscosity, a maximum
 367 non-dimensional viscosity of 10^4 is enforced as a cutoff. Consequently, before performing the calcu-
 368 lation, it is expected that there will be a viscosity contrast of 10^4 across the upper boundary layer.
 369 Following the calculation, the average non-dimensional temperature at the base of the upper boundary
 370 layer is determined to be 0.75, indicating that it is somewhat hotter than initially anticipated. However,
 371 it remains stable. Consequently, as illustrated in Figure 2, the typical non-dimensional viscosity in the
 372 upper mantle, excluding the slabs is around 10^{-1} .

373 The viscosity is also stress dependent, as we include a yield stress formulation so high strain
 374 rates can localize in the boundary layer to generate analogs of plate-boundaries (Coltice et al. (2017)).
 375 The yield stress depends weakly on depth here. The parameters used for the convection model are
 376 presented in Table 2 and are set to generate plate-like behavior at statistical steady-state.

377 We will use here two guesses for the temperature field. We will use a constant temperature in order

Parameter	Non dimensional value
Rayleigh number	10^6
Heat production rate	35
Top temperature	0.12
Basal temperature	1.12
Temperature for the viscosity of reference (1)	0.64
Viscosity jump factor at depth 0.227 (660 km)	30
Activation energy	8
Yield stress at the surface	10^4
Yield stress depth derivative	0.025
Number of cells	6 258 688
Average resolution	45 km

Table 2. Non dimensional parameters of the convection model used predicting Earth surface velocities

378 to evaluate the sensitivity of a model without any information (here we use a temperature guess of 0.7
379 similar to the average temperature obtained in the following model). We will also use a temperature
380 field build by imposing the plate motion model of (Seton et al. (2012)) over a convection model. This
381 setup, called hereafter 'nudged', is very similar to (Coltice and Shephard (2018)). Therefore, we refer
382 to this paper for more details on the modelling of the temperature field.

383 Predicting global kinematics by computing whole mantle flow has been a challenge since more
384 than 40 years ago (Hager and O'Connell (1979)). (Ricard and Vigny (1989)), (Becker and O'Connell
385 (2001)) or (Conrad and Lithgow-Bertelloni (2002)) achieved accurate plate motion predictions, albeit
386 with slightly different guessed density models within the Earth's mantle, using radially a constant vis-
387 cosity structure and prescribing a priori plate geometry and rigidity. (Stadler et al. (2010)), (Alisic et
388 al. (2012)) and (Ghosh and Holt (2012)) accurately predicted plate motions based on a guessed tem-
389 perature field derived from seismology, considering lateral viscosity variations, internal deformation
390 of plates and variable strength of plate boundaries. Our model differs from these studies two notewor-
391 thy manners: (1) we allow rigid plates or plate boundaries to emerge self-consistently from local force
392 balance while these studies impose the plate layout a priori; and (2) our model treats these temperature
393 fields as outputs given by running the "nudged" convection model, meaning that there is a degree of
394 self-consistency between the density structure and the self-organized state of the system, while the
395 previously mentioned studies use guesses of the density structure by converting seismic anomalies or
396 imposing the location of slabs in the mantle.

397 We derive below the sensitivity structure of plate kinematics to the 3D temperature field, which
 398 contributes to the flow through both buoyancy anomalies and viscosity contrasts.

399 4.3.2 *Adjoint code and gradient test*

400 The full temperature field is the control variable, as in the first adjoint code. The cost function of the
 401 second code is

$$402 \quad \mathcal{J}^{\mathbf{v}} = \frac{1}{S} \sum_i^S \langle \mathbf{v}(x_i) - \mathbf{v}_0(x_i), \mathbf{v}(x_i) - \mathbf{v}_0(x_i) \rangle \Delta S(x_i), \quad (8)$$

403 where $\mathbf{v}(x_i)$ is the velocity at the volume center, $\mathbf{v}_0(x_i)$ the target velocity at the volume center.
 404 The summation is over the surface of the model S , $\Delta S(x_i)$ being the local elemental surface. The
 405 generated adjoint code gives the sensitivity to the initial temperature field of the full flow difference
 406 with respect to the plate kinematic model of (Seton et al. (2012)) for consistency. Since there is no
 407 covariance weighting in the cost function, the misfit being of the order of magnitude of the velocity
 408 itself, high velocities can dominate the misfit here. This adjoint code generated by TAF is 270 034
 409 lines. Since the control variable is the same as in the benchmarking case, the core of this generated
 410 adjoint code is very similar to that of the benchmarking example.

411 4.3.3 *Sensitivity of uniform temperature structure*

412 We first set a uniform temperature structure. As a consequence, the predicted surface velocities are
 413 only null vectors, the cost function representing then the mean squared surface velocity. The uniform
 414 thermal state implies there is not cold boundary layer where yielding can occur. Running the adjoint
 415 code on that setup offers a way to evaluate the location of temperature anomalies that contribute to
 416 generate the expected kinematics. However, given the non-linear relationship between temperature
 417 and velocity in the present model, it should not be mistaken as the kernels used in (Forte and Peltier
 418 (1991)) or (Vigny et al. (1991)).

419 The sensitivity fields depicted in Fig. 7 show the upper mantle dominates the signal over the lower
 420 mantle by more than an order of magnitude in the presence of the viscosity jump at 660 km. At this
 421 depth, the average sensitivity changes sign. Hence, in the upper mantle negative temperature anomalies
 422 would reduce the cost function, while in the lower mantle positive anomalies would be required. This
 423 prediction is consistent with slabs in the upper mantle being the essentials in driving plate motions
 424 (Conrad and Lithgow-Bertelloni (2002); Coltice et al. (2019)). The sensitivity structure observed in
 425 the cross section (right column of Fig. 7) suggests creating temperature contrasts in the upper mantle
 426 across plate boundary locations would be favorable to decrease the cost function. Such temperature
 427 distribution does not corresponds to typical convection planform. It shows further interpretation should

428 be done with the awareness that the adjoint is a linear estimate of the sensitivity around the guessed
429 state (Talagrand (1997)). We see here that such a distant guess from the awaited solution combined
430 with a non-linear rheology is not appropriate for starting an inversion process.

431 Increasing the yield stress by a factor of 2 has the effect of decreasing the sensitivities while
432 keeping the structure similar (second row of Fig. 7). This means that temperature anomalies should
433 be stronger to impact more the flow than with a smaller yield stress. It is consistent with the fact that
434 stronger buoyancy forces are required to generate larger stresses so that yielding is reached to generate
435 plate boundaries and surface mobility. The average sensitivities as a function of depth has a similar
436 behavior as the lower yield stress case.

437 The rms of the adjoint field (first column, third row in Fig. 7) shows that the removing the viscosity
438 jump at 660 km smooths out sensitivity contrast between upper and lower mantle. Deeper thermal
439 anomalies impact surface velocities. The magnitude of the sensitivity is smaller by more than 3 orders
440 of magnitude than with a viscosity jump, meaning that the cost function is less sensitive to a local
441 given temperature anomaly than in the model with a viscosity jump. This is consistent with the fact
442 that the sensitivity without a viscosity jump is more distributed within the whole mantle. The changes
443 of sign of the average sensitivity with depth suggests that reducing the cost function would be favored
444 by hotter anomalies in the shallow and lower mantle, while cold anomalies around 500 km. Although
445 these differences with the layered viscosity case, the cross section in Fig. 7 shows that the structure of
446 the adjoint field remains similar.

447 4.3.4 *Sensitivity of nudged temperature structure*

448 We compute the sensitivity of the nudged temperature structure. We use a forward model run to com-
449 pute the full 3D velocity field in response to the "nudged" temperature field. No plate structure or
450 velocities are imposed here. Both plate boundary positions and kinematics are predictions of the for-
451 ward model. The comparison between this prediction and the velocities from the plate reconstructions
452 show the mismatch between the model and the observations. The sensitivities obtained by running the
453 adjoint code estimate the correction to improve the prediction. Fig. 8 shows that the forward run rep-
454 resents consistently the main ridge and trench systems but fails in expressing the African rift and the
455 smaller scale connection between convergent plate boundaries in the East Pacific system. Velocities are
456 consistent in direction and magnitude in major areas of the world (Atlantic, Indian and Pacific ocean).
457 However, the Pacific plate is slower than expected and the convergence directions across South Amer-
458 ica is deviated towards the South compared to what is expected. Unlike the previous uniform state,
459 this one closely aligns with the expected state, as it accurately reproduces the key characteristics of

460 plate motions. As a reminder for the reader, plate boundaries in this model emerge self-consistently in
461 the numerical solution and are not prescribed by the modeler through weaker areas.

462 The sensitivity structure is shown in Fig.9 for the reference model (top row) and for a model in
463 which the yield stress value is twice the reference (bottom row). Both adjoint rms sensitivity profiles
464 show 3 peaks in sensitivity: in the lithosphere, in the mid-mantle and at the bottom of the mantle. Areas
465 where the model is the most sensitive represent a combination of errors in the temperature structure
466 and intrinsic sensitivity of the surface velocities to these areas (surface velocities are in principle less
467 sensitive to the deeper mantle as shown in the previous subsection).

468 The computed sensitivity show that small temperature changes in the lithosphere have a strong
469 impact on the cost function. Because forces in the lithosphere dominate the force balance (slab pull
470 corresponds to pressure gradients within the lithosphere), it is expected that small alteration of this bal-
471 ance modify the surface flow. From the significantly higher RMS sensitivity compared to the average,
472 we anticipate that for a plate, heating up a ridge and cooling down a trench could yield comparable
473 effects.

474 While previous uniform guessed states predict a low sensitivity to lower mantle thermal structure,
475 the nudged guesses show a comparable sensitivity of the upper and lower mantle structure. Our in-
476 terpretation lies in the way the nudged temperature field is built: plate kinematics is more precise for
477 recent times, and consequently, we expect the upper mantle structure to be represented with greater
478 consistency than the deeper mantle. Therefore the deep mantle thermal structure is probably the less
479 consistent with the surface flow, which would need the more correction for a better fit. An area in
480 which the structure is consistent with the prediction would have a low sensitivity, while an area in
481 which the structure is not consistent would have a high sensitivity. It is then expected that the deeper
482 mantle is a place of high sensitivity. The mid-mantle is the area where slabs that enter the more vis-
483 cous lower mantle tend to flatten and fold. Therefore this area generates major structures for the global
484 organization of the flow. The viscosity change which impacts the most the flow in this area is the sub-
485 ject of debates (Rudolph et al. (2015)) and therefore small errors on its parameterization could result
486 in generating erroneous deep slab structures. The change of sign of the average sensitivity in the ref-
487 erence model shows that reducing the cost function would require heating up the base of the mantle
488 while increasing the amount of cold anomalies between 1000 and 2000 km. Fig.9 which matches cross
489 section in Fig.5) reveals that the thermal structure beneath plate boundaries and in the environment
490 of slabs dominate the sensitivity signal. The same figure shows that surface velocities are not very
491 sensitive to plume structures.

492 Increasing the yield stress in the model shows a similar overall structure but specific differences.
493 First of all, and consistently with the uniform structure cases, the sensitivity is lower. Stronger temper-

494 ature anomalies would be required to lower the cost function compared to the reference model. The
495 high yield stress model is more sensitive to cold temperature changes in the top boundary layer. The
496 signal is now more confined in the top and bottom regions of the model, for the same reasons as advo-
497 cated in the previous paragraph. Contrarily to the reference model, with a high yield stress cooling the
498 deeper mantle and heating up the 1000 km-2000 km area are predicted to decrease the cost function.
499 It suggests that resolving these areas in mantle reconstructions can be strongly dependent on the given
500 rheological structure.

501 **5 DISCUSSION AND CONCLUSIONS**

502 We have presented here the development of the automatic generation of adjoint codes for the sophis-
503 ticated parallel multi-geometry thermochemical convection code StagYY. As opposed to inversions
504 which require combining forward and adjoint calculations embeded into an optimization scheme, we
505 have focused on the direct output of adjoint codes: sensitivities with a specific application to how
506 surface velocities are sensitive to the 3D thermal structure of the mantle. The generation of adjoint
507 codes relies on implementing point to point MPI automatic differentiation in TAF, and the adaptation
508 of StagYY code being mostly inserting TAF directives. We have created this workflow to make sure
509 the adjoint code is the exact adjoint of the forward code. Solving adjoint equations does not give such
510 guarantee. The gradient test, also called Taylor test, is the exacting validation test for such property,
511 which is fundamental to make sure adjoint codes give the best estimates in a minimization/inversion
512 process. A finite difference check of the adjoint is not enough to benchmark an adjoint code. The
513 specific dependence of the finite-difference convergence needs to be evaluated.

514 Another reason to use automatic differentiation is that changing the control variable (or cost func-
515 tion but in a very moderate manner) requires the development of a new adjoint code: one sensitivity
516 problem needs one specific adjoint code. To finish with, StagYY has 20 years of evolution and will
517 evolve. New physics, new solvers, new methods will be added to it (grain size dynamics, melting,...)
518 implying following changes in adjoint codes. Maintaining the code structure which is prerequisite for
519 differentiation, we can generate new adjoint codes automatically. Since we expect a multitude of in-
520 verse problem for mantle convection/plate tectonics modelling, the automatic differentiation approach
521 remains versatile, sustainable and efficient.

522 We have presented here a benchmarking test focused on generating an adjoint code that can be
523 used to recover initial conditions knowing a final temperature distribution, which has been proposed
524 as an inverse problem for mantle convection, using tomographic models as thermal proxies. We have
525 used tracers to track the composition in such models introducing a coupling between composition and
526 momentum equations.

527 We then generated an adjoint code to compute the sensitivity of surface velocities to the internal
528 3D thermal structure of a mantle convection calculation with plate-like behavior, introducing com-
529 plexities in system equations and numerical methods. After performing a gradient test, we have com-
530 puted model sensitivities with two different temperature structure: uniform and nudged with a plate
531 kinematic model. The uniform temperature distribution show that the presence of a viscosity jump
532 at 660 km make the surface velocities poorly sensitive to lower mantle temperature anomalies, while
533 the value of the yield stress impacts the magnitude of the sensitivity (low yield stress means high
534 sensitivity). The nudged temperature structure suggest that lower mantle structure predictions are dif-
535 ficult to realize because of uncertainties in the rheological parameterization and in plate kinematic
536 models before 50 My. The upper boundary layer expresses the stronger sensitivities, consistently with
537 the dominance of forces like slab pull, ridge push, and lithospheric/crustal thickness anomalies, all of
538 them generating pressure gradients in the boundary layer.

539 The generation of adjoint codes is a first step towards solving optimisation problems and therefore
540 to embed models together with observations. For a given problem, the adjoint code which is automat-
541 ically generated can require some optimisation, mostly on memory use and choices of checkpointing
542 and recomputation. Also the development of an optimisation procedure that can handle the fact that
543 mantle convection problems can be non-linear and non-Gaussian, especially when using non-linear
544 rheologies, is a step to make. Another difficulty is the size of such problems with non-linear rheolo-
545 gies and high resolution in 3D. Adjoint created with TAF typically require a computational time of
546 about 2 to 5 times of that of the forward code, where the adjoint run includes the computation of the
547 cost function, which is necessary for non-linear problems and we hope to overcome the worse per-
548 formance of the presented codes in the near future. But still, together with the model approximations
549 (rheology, compressibility) and sparsity of data (no direct observation of Earth's interior), computing
550 time will be the most limiting factors towards global geodynamic inversions.

551 **ACKNOWLEDGMENTS**

552 **DATA AVAILABILITY**

553 The data used for running the test and making the figures are available in the following repository:
554 <https://osf.io/dpzv8/>

555 The convection code StagYY is the property of P.J.T. and Eidgenössische Technische Hochschule
556 (ETH) Zürich. Researchers interested in using StagYY should contact P.J.T. (paul.tackley@erdw.ethz.ch),
557 and N.C. (nicolas.coltrice@ens.fr) for the TAF compliant version of StagYY.

558 The adjoint code was generated with TAF. A TAF license is available from FastOpt.

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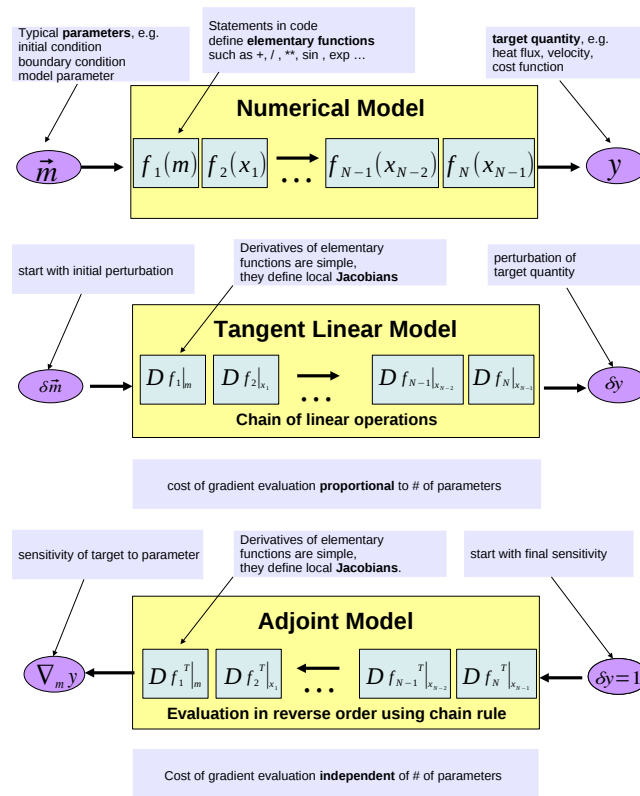


Figure 1. Top: diagram of operations for the forward numerical model to differentiate. Centre: diagram of operations differentiated in forward mode, corresponding to the tangent-linear code. Bottom: diagram of operation in reverse mode, corresponding to the adjoint code.

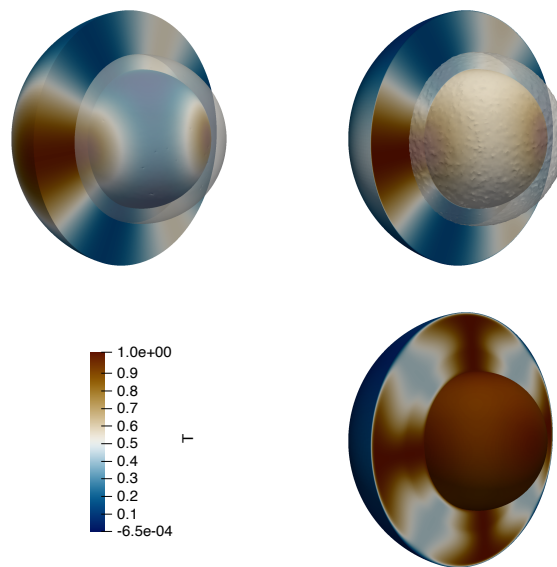


Figure 2. Setup for the gradient test of the automatically generated adjoint code 1. Top left: Initial condition (lateral spherical harmonic degree 3); Top right: final temperature field and isosurface showing the top of the dense layer. Bottom image: targeted temperature field after 10 time steps.

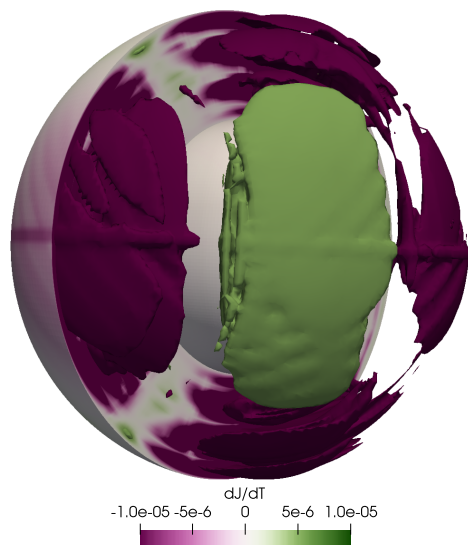


Figure 3. Volume section of the local sensitivity field $d\mathcal{J}^T/dT$. The color is saturated to identify positive values (the initial local temperature should be increased to increase the cost function) and negative values (the initial local temperature should be decreased to increase the cost function).

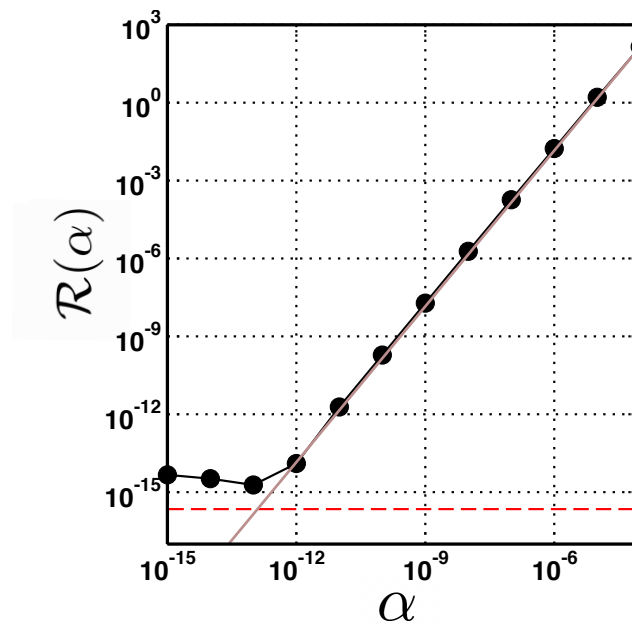


Figure 4. Gradient test for the benchmarking adjoint code 1, showing the relationship between α and $\mathcal{R}(\alpha)$. Computed values are in black circles. The red horizontal dashed line corresponds to the value of machine ε . The brown line corresponds to α^2 that $\mathcal{R}(\alpha)$ has to match to pass successfully the gradient test.

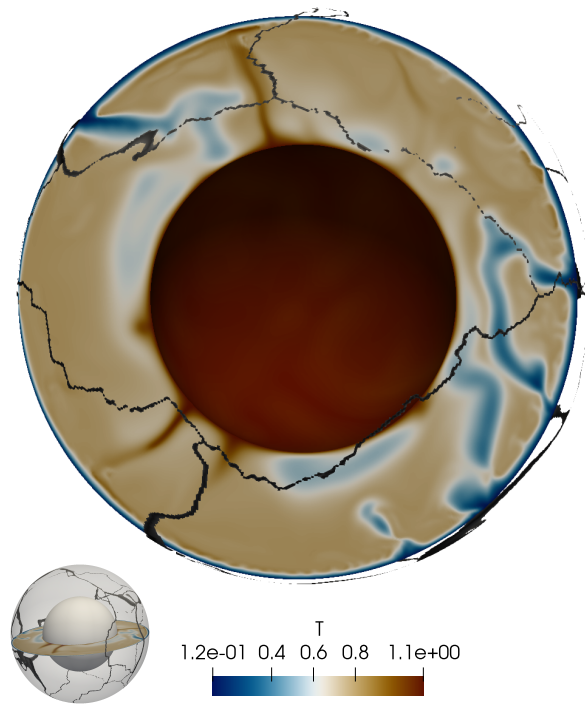


Figure 5. Cross section of the non-dimensional nudged temperature guess. The location of the cross section is shown on the small globe and crosses Northern Chile and the Philippines. Plate boundaries are represented in black. The top of the model shows the South Atlantic ridge. The slab on the left shows subduction below South America. Slabs on the right correspond to Asia-Pacific subduction system in a 3D system.

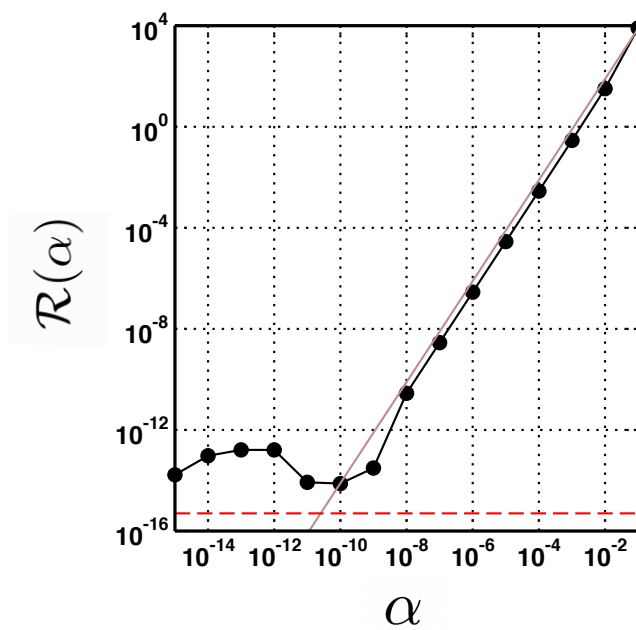


Figure 6. Gradient test for the 'nudged' case, showing the relationship between α and $\mathcal{R}(\alpha)$. Computed values are in black circles. The red horizontal dashed line corresponds to the value of machine ε . The brown line corresponds to α^2 that $\mathcal{R}(\alpha)$ has to match to pass successfully the gradient test.

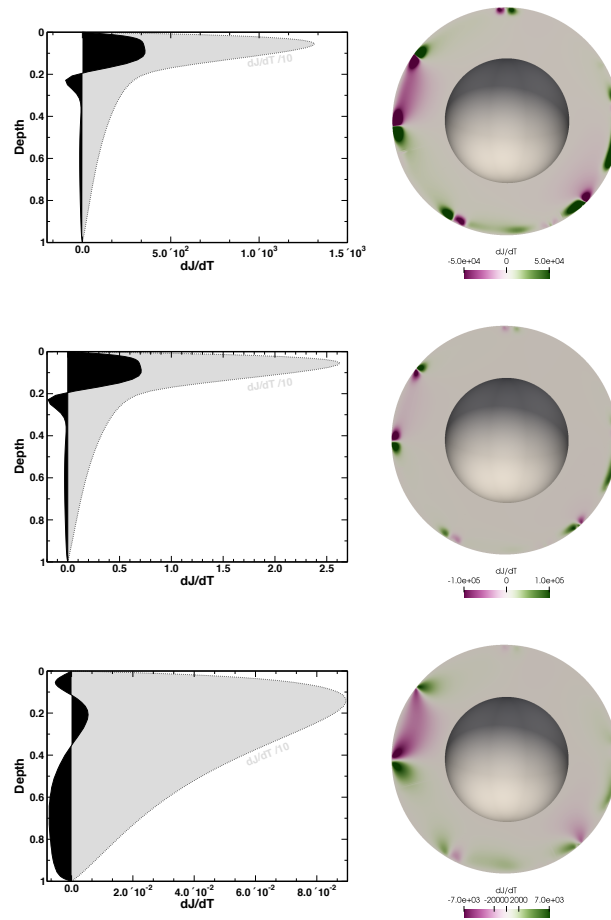


Figure 7. Left column: sensitivity field $d\mathcal{J}^v/dT$ as a function of depth (laterally averaged in black and root-mean square value in gray). Right column: volume section of the local sensitivity field $d\mathcal{J}^v/dT$. The section is identical to that of Fig5. Top row: reference model. Middle row: high yield stress model. Bottom row: model without a viscosity jump. Positive values mean that the local temperature should be increased to increase the cost function and negative values suggest the local temperature should be decreased to increase the cost function.

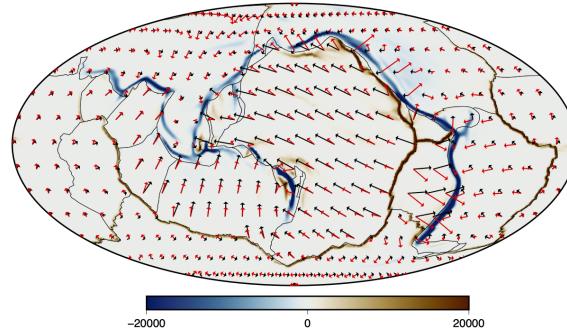


Figure 8. Surface kinematics of the convection model (forward model solving for the velocity field in response to the 3D temperature distribution) vs. plate reconstruction model. Computed velocities are in red together with predicted non-dimensional divergence in colors. Velocities and plate boundaries for the plate reconstruction model are represented in black.

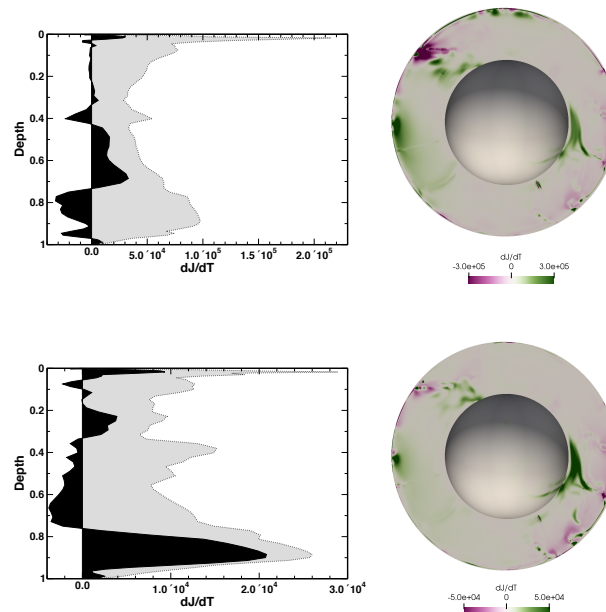


Figure 9. Left column: sensitivity field $d\mathcal{J}^v/dT$ as a function of depth (laterally averaged in black and root-mean square value in gray). Right column: volume section of the local sensitivity field $d\mathcal{J}^v/dT$. The section is identical to that of Fig5. Top row: reference model. Bottom row: model without viscosity jump. Positive values mean that the local temperature should be increased to increase the cost function and negative values suggest the local temperature should be decreased to increase the cost function.