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COVER SHEET

Dear Editors,

This manuscript has been sent for consideration for publication in Journal of Sedimentary Research (JSR) special edition. We think this is a concise report of exciting research results that will be of interest to a broad range of Earth Scientists interested to understand more about the architecture of submarine fans, for example, whether hierarchy as interpreted by several author occur in submarine fan. We have adopted a reduced complexity numerical modelling approach because this allows exploration of the simplest-case processes allowing us to build fundamental understanding of how strata accumulate and record Earth-surface process signals.

Please note that, despite having undergone peer-review, the manuscript has yet to be formally accepted for publication. Subsequent version of this manuscript may have slightly different content. If accepted, the final version of this manuscript will be available via the 'Peer-reviewed Publication DOI' link on the right-hand side of this webpage. Please feel free to contact any of the authors; we welcome feedback.

Yours sincerely,

Ibrahim Tinni Tahiru

Journal of Sedimentary Research

Deep-Water Fan Hierarchy: Assumptions, Evidence, and Numerical Modelling Analysis

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Abstract:	Submarine fan strata are commonly described and interpreted assuming a nested, hierarchical organisation of elements, from beds, to lobe elements, lobes and lobe complexes. However, describing outcrop and subsurface strata following a particular conceptual method or model is never evidence in itself that the model or method accurately reflects the true nature of the strata. To develop better understanding of and methods for robust hierarchy identification and measurement we developed two metrics, a clustering strength metric that measures how much clustering is present in the spatial distribution of beds on a submarine fan, and a hierarchy step metric that indicates how many clustered hierarchical elements are present in the bed spatial distribution. Both metrics are applied to two quantitative fan models. The first is a very simple geometric model with 10 realisations ranging from a perfectly clustered hierarchy to a indistinguishable-from-random arrangement of beds. The second model, Lobyte3D, is a reduced-complexity process model which uses a steepest descent flow routing algorithm, combined with a simple but physically reasonable representation of flow velocity, erosion, transport and deposition thresholds, to generate detailed 3D representations of submarine fan strata. Application of the cluster strength and hierarchy step metric to the simpler model demonstrates how the metrics usefully characterise how much order and hierarchy is present in the fan strata. Application to four Lobyte3D models with increasingly complex basin-floor topography shows no evidence for true hierarchy, despite clear self-organisation of the model strata into lobes, suggesting that either Lobyte3D is missing key as yet unidentified processes responsible for producing hierarchy, or that interpretations of hierarchy are not realistic.

Deep-Water Fan Hierarchy: Assumptions, Evidence, and Numerical Modelling Analysis

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ABSTRACT

Submarine fan strata are commonly described and interpreted assuming a nested, hierarchical organisation of elements, from beds, to lobe elements, lobes and lobe complexes. However, describing outcrop and subsurface strata following a particular conceptual method or model is never evidence in itself that the model or method accurately reflects the true nature of the strata. To develop better understanding of and methods for robust hierarchy identification and measurement we developed two metrics, a clustering strength metric that measures how much clustering is present in the spatial distribution of beds on a submarine fan, and a hierarchy step metric that indicates how many clustered hierarchical elements are present in the bed spatial distribution. Both metrics are applied to two quantitative fan models. The first is a very simple geometric model with 10 realisations ranging from a perfectly clustered hierarchy to a indistinguishable-from-random arrangement of beds. The second model, Lobyte3D, is a reduced-complexity process model which uses a steepest descent flow routing algorithm, combined with a simple but physically reasonable representation of flow velocity, erosion, transport and deposition thresholds, to generate detailed 3D representations of submarine fan strata. Application of the cluster strength and hierarchy step metric to the simpler model demonstrates how the metrics usefully characterise how much order and hierarchy is present in the fan strata. Application to four Lobyte3D models with increasingly complex basin-floor topography shows no evidence for true hierarchy, despite clear self-organisation of the model strata into lobes, suggesting that either Lobyte3D is missing key as yet unidentified processes responsible for producing hierarchy, or that interpretations of hierarchy are not realistic.

INTRODUCTION

Submarine fans are among the largest sedimentary accumulations (William, 1970; Posamentier and Kolla, 2003; Talling *et al.*, 2012) and serve as an essential record of Earth history, offering insights into both local and global geological processes (Emmel and Curray, 1984; Pirmez and Imran, 2003;

Deptuck *et al.*, 2008; Picot *et al.*, 2016; Picot *et al.*, 2019; Rabouille *et al.*, 2017). Formed by a complex interplay of turbidity currents, other types of sediment mass flows, and various hydraulic processes, submarine fans are characterized by their complex stratigraphic architectures and depositional patterns (Straub and Pyles, 2012) Submarine fans are also often important reservoirs for the extraction of hydrocarbons and, increasingly importantly, for the sequestration of carbon (Pettingill, Weimer and Anonymous, 2002).

Understanding the organization of submarine fan strata is important for unravelling their formative processes and for deciphering the geological history they preserve. Previous studies have proposed hierarchical schemes to describe fan internal organization and characterise spatial and temporal variations in sedimentation patterns (Gardner, 2000; Pyles, 2008; Deptuck *et al.*, 2008; Prelat *et al.*, 2009; Prealat *et al.*, 2010) ; Mutti and Normak 1987; Gardner and Borer 2000, Pyles 2007; Deptuck et al. 2008, Prelat et al., 2009; Prelat et al., 2010). However, despite the significant progress made in characterizing submarine fan architecture, quantitative evidence to define hierarchy remains spares, and aspects of the fundamental mechanisms that would form hierarchical patterns remain poorly defined.

Existing Hierarchical Schemes

If submarine fans are hierarchical, they should show some form of systematic pattern of smaller-scale structures nested within and composing larger-scale structures. For example, in a hierarchical fan, fan lobes would be composed of lobe elements that are in turn each composed of many beds, each bed being one turbidite (Figure 1). Various examples of this type of hierarchical arrangement have been interpreted from outcrop, and subsurface data.

Deptuck et al. (2008) used ultra-high-resolution boomer seismic imagery with a vertical resolution of approximately 1 m to define a hierarchical classification for 20 lobes in a late Pleistocene submarine

fan offshore from East Corsica. The classification scheme defined four types of unit starting with a bed or bed-set deposited from single flows, with systematic lateral compensational offsets up to 500 m. Bed-sets stack to form lobe elements, which, in turn, stack to create composite lobes. Composite lobes are separated by disconformable surfaces, abrupt vertical shifts in acoustic facies, or the presence of thin drapes, all resulting from compensational stacking of lobe-elements with lateral offsets ranging from 500 to 2000 m triggered by local avulsion (Deptuck et al. 2008). Composite lobes fed by the same primary conduit stack to form lobe complexes, which frequently exhibit 3-5km lateral shifts between their thickest regions, interpreted to arise from large-scale channel-mouth avulsions. Abandoned composite lobes may be covered by several meters of hemipelagic drape, which may subsequently be eroded by later flows.

Based on well-exposed Permian deposits in the Tanqua depocenter of the Karoo Basin, South Africa Prelat et al. (2009) proposed a different four-fold hierarchical classification focused on the properties and geometry of fine-grained interlobe architectural units, which separate more sand-prone bodies. The lowest hierarchical level is single depositional event beds up to 0.5 m thick and hundreds of meters wide. Lobe elements up to 5m thick are composed of stacked beds and form the next higher hierarchical level. Genetically linked vertically stacked lobe elements, separated by fine-grained units typically less than 2 cm thick but occasionally up to 2m thick in topographic lows, create lobes up to 5 m thick with widths exceeding 20 km. Finally, lobe complexes are composed of stacked lobe bodies, up to 50 m thick and 40 km wide fed by a single upstream channel.

Macdonald *et al.*, (2011) focused on the process sedimentology and internal architecture of lobe deposits in the Carboniferous Ross Sandstone Formation, to propose a three-order hierarchy of bed-sets, lobe-elements, and composite lobes. Lobe-elements are formed by upward-thickening packages of bed-sets, often with basal mudstone units indicative of depositional shutdown. Mudstone thicknesses relate to the lateral distance and duration of avulsion separating compensationally-stacked lobe-elements.

(Cullis *et al.*, 2018) systematically reviewed and compared a representative selection of the most widely adopted deep-marine hierarchy schemes, to assess the principal characteristics of each hierarchical classification, the common diagnostic criteria used to attribute deposits to given hierarchical orders, and the causes of similarity and variability between different schemes. The review revealed recurrent observations underlying all the classification schemes, recommended that hierarchical relationships be categorised based on primary sedimentological observations, rather than through predefined schemes and concluded that a universal process-based hierarchy cannot be established. This is because of the difficulty in to reconcile the different hierarchical schemes arising partly from differences between the underlying studies such as the data types, scales of interest, specific environmental settings and in the significance given to the diagnostic criteria, as well as from the adoption of non-standard terminology.

Straub and Pyle (2012) used a modified version of the compensation index to test for statistically significant differences in compensation between different scales in hierarchically-classified strata. They also examined compensation variations between predominantly channelized and unchannelized submarine fan strata in each hierarchical class to test how compensation varies spatially. Their results suggest that hierarchical divisions based on compensation are justified, and that compensation increases along a longitudinal transect through distributive submarine fans.

Numerical Stratigraphic Forward Modelling as a Tool for Analysis of Submarine Fan Hierarchy

Numerical stratigraphic forward modelling has emerged as a useful tool for unravelling the complexities of sedimentary system (Paola, 2000; Burgess, 2013). By simulating the interplay between sediment transport, deposition, and erosion processes, these models provide valuable insights into the formation of stratigraphic patterns. Reduced-complexity models aim to capture the simplest possible set of processes that may be responsible for a specific stratigraphic pattern, while

also reducing computational cost, allowing multiple model runs and intensive analysis of model results, in this case to explore the emergence of hierarchical patterns within submarine fan systems.

This study utilizes the reduced-complexity stratigraphic forward model, Lobyte3D version 2.2, to investigate the hierarchical organization of submarine fan deposits. Lobyte3D is a three-dimensional reduced-complexity numerical stratigraphic forward model, developed to help understand how and why stacking patterns evolve in submarine fan depositional systems (Burgess *et al.*, 2019). Lobyte3D has been modified from its original form with new representations of key depositional processes, and most importantly, the addition of erosion as a function of flow velocity (Mackie et al., in review). In this paper Lobyte3D is used examine the architecture of submarine strata to to (1) access if there is any definite criteria to interpret lobes and (2) describe patterns present within each lobes. And (3) perform clustering analysis on the flow centroid to quantitatively identify and define lobes.

MODEL FORMULATION AND METHODOLOGY

Lobyte3D Formulation

Lobyte3D version 2.2 calculates turbidity flow routing, erosion and deposition, and the resulting stacking patterns that evolve as sediment accumulates on a submarine-fan surface. Transport and deposition are calculated on a simple orthogonal 50 by 50 km x-y grid with a cell edge dimension of 100m. Each model run consisted of 1000 flow events. Sediment enters the model at y0 at the top of a submarine slope. All the sediment volume in one flow event is moved downslope as one single depth-averaged packet of sediment in one model grid cell at each iteration following a steepest gradient descent down the slope. Deposition starts in the cell where depth-averaged flow velocity into the lowest adjacent cell is equal to or less than a specified sediment threshold velocity. Flow velocity is calculated such that.

$$v_f = v_i + (a * \emptyset) \qquad (1)$$

where V_f is the flow velocity, V_i is the velocity of the flow at the previous time step, a is the flow acceleration and Ø is the flow acceleration proportion taken to be 0.5

The flow acceleration a is given by.

$$a = v_m - v_i \qquad (2)$$

and the maximum velocity V_m converts shear velocity into whole flow velocity as a function of topographic gradient and is given by

$$v_m = \frac{v_s}{\sqrt{\sigma}} \qquad (3)$$

where V_s is the maximum shear velocity and σ is the basal friction coefficient.

Flow erosion rate is calculated as

$$\varepsilon_r = v_{se} * \frac{a}{b} \qquad (4)$$

where v_{se} is the settling velocity and a and b can are calculated as

$$a = C_e * Z^5 \qquad (5)$$

$$b = 1 + \frac{C_e}{0.3} * Z^5 \qquad (6)$$

where C_e is the erosion rate constant, and Z is the tractive stress which is calculated as follows.

$$Z = Re^6 * \frac{v_s}{v_{se}} \qquad (7)$$

where R_e is the particle Reynold number.

Four scenarios of Lobyte3D with varying degrees of complexity in the initial topography was used to model 1000 flow events. They include concave flat floor with no noise, very smoothed noise, smoothed noise, and raw noise. Each flow interrupts background hemipelagic deposition occurring at a rate of 0.02 m ky^{-1}. A flow repeat time of 1000 years will be maintained through each model run

151 representing a 1 M_y of flow history and deposition. Input parameters for the model include the initial
152 topography, distribution of the grain-size, deposition threshold velocity to commence dispersive
153 flow and deposition, concentration of the sediment, total volume of sediment transported by the
154 flows (Table1).

155 For each model run, model behaviour was analysed by plotting each down-slope flow route and area
156 of deposition in map view. Avulsion points were identified when the apex of flow deposition shifted
157 substantially from the location of the apex of the previous flow.

158 Table 1: Lobyte3D input parameters

S/N	Parameter	Value
1	Hemipelagic deposition rate, per time step, m My^{-1}	0.02
2	Diffusion coefficient, m2 per My.	0.0
3	Density (kg/m^3) of the ambient fluid	1.00
4	Erosion rate constant (m/s)	1.3×10^{-10}
5	Basal friction coefficient	0.004
6	D50 (m) median grain diameter (medium/fine sand)	0.00025
7	Grain density in kg/m3 siliciclastic quartz/feldspar	2660
8	Depositional velocity threshold (m/s) to commence dispersive flow and deposition	0.1
9	Flow acceleration/deceleration coefficient	0.5
10	Total flow thickness, fluid and sediment mix (m)	100
11	Flow COG proportion	0.10

12	Volumetric sediment concentration	0.01
13	Minimum flow thickness (m)	0.001
14	Proportion of the height of ponding topographic lows to fill when flow is trapped	1.00
15	Flow Radiation Factor	2.0
16	Number of fractions in the depositional fraction profile	13

159

160 **Clustering Analysis and Hierarchy Metrics**

161 Clustering analysis is a numerical technique to classify data, originally developed as a natural
162 sciences method to make taxonomy more objective. (Everitt *et al.*, 2011), but now widely applied in
163 earth sciences (Simpson, Thatcher and Savage, 2012; Takahashi *et al.*, 2019) to identify patterns,
164 group similar objects, and uncover underlying structures within data. Cluster analysis partitions data
165 based on their similarities or dissimilarities, and often provides valuable insights into the
166 organization and relationships within the data (Everitt *et al.*, 2011). Clustering, unlike other
167 classification techniques, does not rely on preset classes and class-labelled samples, so is a relatively
168 more objective method (Jiawei Han, 2011).

169 Data point separation distances, or dissimilarity, are a fundamental aspect of many clustering
170 analyses, quantified using a wide range of dissimilarity measures (Gower and Legendre, 1986), often
171 in matrix form. Dissimilarity matrices capture pairwise dissimilarities, the distances between
172 individual data points, such that

173
$$D = \begin{bmatrix} 0 & & & & \\ d(2,1) & 0 & & & \\ d(3,1) & d(3,2) & 0 & & \\ \vdots & \vdots & \vdots & & \\ d(n,1) & d(n,2) & \cdots & \cdots & 0 \end{bmatrix}$$

174 Where $d(i,j)$ is the measured dissimilarity between objects i and j. since $d(i,j) = d(j,1)$, and
175 $d(i,i) = 0$. Analysis of a dissimilarity matrix allows distinction between randomly distributed data
176 where a broad spread of dissimilarity distances is expected, and clustered data, where the distances
177 have a narrower range of values reflecting the specific distances within and between clusters; in
178 clustered data, many of the dissimilarity distances are relatively small because many points occur in
179 close proximity within the clusters.

180 Here we use a metric termed clustering strength to distinguish between clustered *xyz* data, and a
181 randomly distributed set of *xyz* points. Clustering strength is calculated from the centroid separation
182 distances such that

183
$$CSI = \left(\sum_{i=1}^{N} I(d_i \leq T) \right) \Big/ N$$

184 where *N* is the number of bed centroids, d_i is the separation distance between centroid point i and
185 another centroid, *T* is a threshold distance, and *I* is an indicator function that returns 1 if or 0,
186 depending the logical condition $d_i \leq T$. For a threshold distance that is 1% of the maximum
187 dissimilarity distance in the system, values of clustering strength will approach zero as the degree of
188 randomness in *xyz* points increase, and the value will always be higher for clustered data.

189 Once a degree of non-random clustering has been identified, the nature of the clustering can be
190 assessed, specifically whether there is any hierarchical element such that smaller clusters
191 themselves cluster to form larger clusters, and so on (e.g. Figure 1). Hierarchical Agglomerative
192 Clustering Analysis (Gordon, 1987) is a bottom-up clustering analysis approach that starts with
193 individual data points, merging them into new clusters based on their dissimilarity values, until all

194 points are within one cluster. Euclidean dissimilarity distances were used because these most
195 effectively measure bed centroid spatial relationships in xyz coordinate space, and the complete
196 linkage method was selected because it has low sensitivity to outliers, and is relatively robust in
197 noisy data (Jiawei Han, 2011), so a good choice to identify hierarchy levels.

198 Hierarchical cluster analysis results are plotted as a dendrogram, with cluster separation distance on
199 the Y-axis, and cluster number on the x-axis. The actual degree of hierarchy present in the
200 dendrogram can be assessed quantitatively by extracting dissimilarity distances between
201 dendrogram bifurcation points, and analysing these for clustering also; a hierarchical example should
202 show clustering in these bifurcation distances, because bifurcations should occur at specific scales
203 reflecting the size and separation distance of the various hierarchical elements. The hierarchy step
204 metric is then the number of distinct clusters identified in the dendogram bifurcation point
205 distances, typically 1 for indistinguishable from random points with little or no clustering, and
206 otherwise a number representing the number of hierarchical levels present in the data.

207

208 **RESULTS**

209 **Synthetic Lobe Model Results**

210 To provide a well-understood definitively hierarchical baseline for the analysis, eleven synthetic fan
211 lobe models were constructed and analysed, each comprising 1000 beds, with 40 beds in a lobe
212 element, five lobe elements per lobe, and five lobes in total. These models are range from perfectly
213 deterministic and hierarchical, with distinct lobes and lobe elements composed of beds arranged in a
214 simple retrogradational stacking pattern, to a completely stochastic example with a stochastic
215 distribution of bed centroids (Figure 2). The entirely deterministic fan arrangement follows the three
216 or four-fold hierarchy described in (Gervais *et al.*, 2006; Deptuck *et al.*, 2008; Prelat, Hodgson and
217 Flint, 2009) (Figure 1). A random offset is added to each x and y coordinate in the deterministic

model, and the magnitude of the added random element ranges from 0.05 to 0.5. For example, a model with a random element of 0.2 has a random offset of each x and y coordinate ranging from -0.1 to 0.1.

For each synthetic fan lobe model, cluster strength was calculated, and also hierarchy step values were derived from dendogram analysis (Figure 3). The cluster strength values range from a high of 5.7×10^{-3} for the completely deterministic hierarchically clustered fan, to 1.0×10^{-5} for the entirely random bed centroid points, and the decrease in the metric value is quite sharp as the magnitude of random point offset increases (Figure 4A). The dendogram hierarchy analysis shows a similar pattern. The two least-random-component models yield a hierarchy step value of 3, an accurate measurement of the number of hierarchical levels built in to each model (Figure 4B). In contrast, the models with a random offset value of 0.2 and greater have a hierarchy step value of 1 indicating that a random offset of 0.2 or more is enough to remove any detectable hierarchy.

Lobyte3D Model Results

Lobyte3D was run with four different initial topographies defining scenarios with no noise, very smoothed noise, smoothed noise, and raw noise. Strike-oriented cross-sections, 3D views of the channel, bed and lobe stacking patterns, and bed centroid maps from these different initial topographies are used to understand how variations in initial topography control avulsion, fan stacking, and the hierarchical organization of the modelled submarine fan strata.

Avulsion Cycle Processes

The avulsion process is key to forming lobes and therefore key to generating any stratal hierarchy present, so it is important to understand exactly how avulsion occurs in the model. Evolving flow routing shows substantial changes during avulsion, bypassing previous mounded depositional topography, and cutting a new section of channel that bypasses sediment further into the basin to

the point where the initial basin floor slope is low enough to decelerate the flow enough to trigger deposition.

Analysis of the first avulsion in the no noise case reveals the detail of how avulsion occurs in Lobyte3D. Prior to flow 190, deposition was backstepping up the basin-margin slope, partially backfilling the mouth of the previously cut channel (Figure 5). Upslope backstepping occurred due to flow interaction at the channel-lobe transition, with strata deposited from previous flows triggering flow deceleration and further deposition. As strata backstep upslope, depositional relief at the channel mouth on the proximal mound edge increased, and magnitude of deceleration when flows reach this depositional topography also increased. Each time a flow encounters a mound that has been built by previous flows, the flow will continue to follow the steepest available down-slope route, and therefore tend to divert left or right to climb over the lowest-relief part of the mound. Flow velocity prior to climbing the depositional mound tends to increase through time as deposition backsteps up the basin-margin slope, and by flow 190, the flow had sufficient remaining velocity after climbing the depositional mound (Figure 5) to continue to flow, accelerate down from the crest of the mound, and start to cut a new channel. Flow routing through the new channel bypasses the positive topography produced by the previous lobe deposition, defines a new route further into the basin (Figure 5b), and starts to deposit a new lobe, defining an avulsion event.

Rather obviously this is a much-simplified representation of what actually happens in deep-water depositional systems. For instance, several processes have been investigated to produce instability that results in avulsion-threshold circumstances. Channel sinuosity, channel lengthening, channel thalweg and levee aggradation, and channel-relief reduction are some of these causes (Kolla, 2007; Prelat, Hodgson and Flint, 2009; Groenenberg *et al.*, 2010). In this analysis we assume that this modelled avulsion process is sufficiently realistic and representative enough of the real physical process to form the basis for at least initial numerical experiment exploration of how this behaviour influences fan lobe geometry stacking and potential hierarchy.

Flow Routing and Stacking Patterns

All four modelled scenarios generated a multi-km-scale submarine fan (Figure 7) consisting of interbedded turbidite event beds and background hemipelagic strata organised as more-or-less discrete lobes (Figure 8) broadly comparable to typical observed submarine-fan bathymetry and successions (Romans *et al.*, 2009; Romans *et al.*, 2011; Prelat, Hodgson and Flint, 2009; Prelat and Hodgson, 2013). The no noise initial topography produces the most systematic lobe stacking with a simple compensational stacking pattern and lobe boundaries clearly defined by a few meters of hemipelagic sediments (Figure 8A). Each lobe is composed of around 60-to-200 mostly contiguous, spatially-clustered backstepping flow events. Lobes have a simple stacking pattern, separated by progressive lateral 1-2km shift in focus of deposition, and a mean duration of 114 ky (Figure 8A).

The very smooth noise initial topography produces similar but slightly more complex lobe stacking pattern (Figure 8B). These lobes consist of around 50 to 130 aggradational and backstepping beds with a lateral lobe separation distance of 2-4 km and a mean duration of 83 ky (Figure 8B, Figure 9B). The smooth noise initial topography case still shows some discrete lobes, but lobe structure and stacking are more complex (Figure 7C). Where distinct enough to measure, lobes consist of 35-70 contiguous spatially clustered flow events, with lateral lobe separation distance ranging from 0.5 to 2 km and a mean duration of 50 ky (Figure 8C, Figure 9C). Finally, the raw noise initial topography shows the most complex lobe stacking pattern lacking any clear trend (Figure 7D, Figure 9D). These lobes are even more difficult to define. Where discrete enough to define, lobes consist of 5 to 270 aggradational and backstepping stacked beds with a separation distance of 1 to 3 km, but also the highest gradual lateral shift within each lobe (Figure 8D) and a mean duration of 112 ky.

Quantification of Clustering and Hierarchy in Lobyte3D Results

Cluster strength values for the four Lobyte3D models range from 2.51×10^{-3} to 1.14×10^{-3} (Figure 4A) and the smoothed noise initial topography generates the highest clustering strength, suggesting that smoothed noise in the basin-floor topography can enhance clustering relative to the case with the simplest no-noise topography. In contrast, the raw noise basin-floor topography model has the lowest clustering strength (Figure 4A) due to the irregular topography disrupting the regular stacking and avulsion pattern required for clustering. All four model runs generate strata with a hierarchical step value of 1, indicating that no hierarchy is detectable in the spatial distribution of bed centroids, despite the clustering. This suggests that although the clustering produces clear lobe structures, particularly in the no noise and smoothed noise cases, this bed-lobe distinction is not enough to define a hierarchy measured by this dendogram-derived metric.

DISCUSSION

Reduced complexity models

Reduced complexity models are, by design, very much simplified representations of the complex processes that generate real strata (Liang et al., 2015). Consequently, results from reduced complexity models must be used carefully, and not over interpreted or assumed to have predictive power beyond what is reasonably supported by their constituent process representations. However, these models also have some substantial advantages over more complex models, particularly their lower computational cost, and perhaps most importantly, the fact that if a reduced complexity model demonstrates a particular emergent behaviour, the process representation in the model is quite likely to be the simplest possible representation of that process.

In this case Lobyte3D shows avulsion events that divert deposition into new locations clustering sets of beds to form lobes. Critical elements in the model necessary for this a steepest-descent transport algorithm and a gradient threshold for initiation for turbidite bed deposition. Both these elements

315 are represented in a very simple but physically reasonable way, and do seem to operate to some
316 degree in real submarine fan systems. Given this the resulting lobe formation in the model is
317 probably realistic enough to offer some basic but useful insight in deep-water fan processes and
318 structure. However, it is also important to remember that additional and more realistic
319 representations of key processes, for example more detail in the 3D structure and spatial
320 distribution of each flow and consideration of a range of grain sizes in each flow may generate
321 different avulsion process and different fan structures (e.g. (Wahab *et al.*, 2022)) and (Hamilton,
322 Strom and Hoyal, 2015) found that uneven topography increases channel avulsion likelihood due to
323 localized variations in sediment concentration, leading to mouth bar formation and hydraulic jumps.
324 Clearly these processes and controls require further investigation with more complex models, but
325 starting with the simplest model seems sensible.

326

327 **Influence of initial topography**

328 Lobyte3D models in this analysis show substantial influence of initial topography on flow routing,
329 avulsion, and lobe stacking patterns. Previous studies have shown or interpreted a similar influence
330 of topography in shaping submarine fan evolution and architecture (Groenenberg *et al.*, 2010;
331 Straub and Pyles, 2012; Hamilton, Strom and Hoyal, 2015; Cullis *et al.*, 2018; Ferguson *et al.*, 2020);
332 taken together these results support the hypothesis that initial topography influences lobe switching
333 and avulsion timing (Piper and Normark, 2001; Gervais *et al.*, 2006; Groenenberg *et al.*, 2010;
334 Ferguson *et al.*, 2020). However, the formulation of Lobyte3D is perhaps particularly sensitive to
335 small changes in seafloor topography, especially in terms of flow routing prior to deposition, so
336 further work developing more complex model formulations or testing this effect with other
337 numerical and analogue models is required.

338

Absence of hierarchy

There is no hierarchy present in these Lobyte3D results; all modelled strata show detectable non-random clustering, as indicated by comparison with the entirely synthetic fan models, but all the Lobyte3D models have a hierarchical step value 1. This combination of cluster and hierarchy metric values indicate that no hierarchy is detectable in the spatial distribution of bed centroids, despite the clustering.

Clearly absence of a hierarchy in strata calculated in a reduced complexity numerical model is not necessarily evidence that hierarchy does not occur in real deep-water fan strata. However, nor is interpretation of outcrop and subsurface data following a conceptual model of stratal hierarchy evidence that the deep-water fan strata really are hierarchical. Failure to reproduce hierarchy in a very simple numerical model highlights two end-member possibilities; either hierarchy is a real feature of deep-water fan strata, but occurs by processes not adequately represented in Lobyte3D, or the interpretations of hierarchy in outcrop and subsurface strata are an over-interpretation of limited data with insufficient quantitative evidence to be properly robust.

Avulsion is a key control on hierarchy formation because it is the main process forming clustered entities such as lobes. Avulsion in Lobyte3D happens in a simplified and specific way that likely does not capture the range of different and perhaps more complex mechanisms that operate in real submarine fan systems (Hamilton *et al*., 2015; Ortiz-Karpf *et al.*, 2015; Qi *et al.*, 2022; de Haas *et al.*, 2016). Clearly therefore further modelling and model development is required, with Lobyte3D or other process models including analogue models perhaps, to explore how other avulsion processes might behave differently and produce hierarchical clustering.

Until now, interpretations of hierarchy in submarine fan strata have been mostly qualitative, and this lack of quantitative evidence does mean that conclusions of hierarchy are much more tenuous than has perhaps been recognised. More quantitative analysis is therefore required, but a key challenge is how to analyse limited data, for example one-dimensional vertical sections, to provide metrics that

364 can reliably identify and present or absence of hierarchy developed in three-dimensional strata;
365 most current interpretations do not recognise or account for this uncertainty (Gervais et al. 2006;
366 Deptuck et al. 2008; Prelat et al. 2009; MacDonald et al. 2011), suggesting that hierarchical patterns
367 observed in previous studies are probably not universally applicable to all submarine fan systems
368 (Cullis et al. 2018; Ferguson et al. 2020), and development of further tools for quantification of
369 hierarchy with limited outcrop and subsurface data is essential.

370

371 **CONCLUSIONS**

372 1. Submarine fan strata are commonly described and interpreted to have a nested, hierarchical
373 organisation of elements, but quantitative evidence from outcrop and subsurface data to
374 support this interpretation is limited.
375 2. Two new metrics are defined, calculated and used to identify the degree of hierarchy
376 present in the modelled fan strata. A clustering strength metric measures how much
377 clustering is present in the spatial distribution of Lobyte3D beds, and a hierarchy step metric
378 indicates how many clustered hierarchical elements are present in the bed spatial
379 distribution.
380 3. Both metrics applied to a definitively hierarchical geometric fan model with ten
381 progressively more randomised realisations, shows that the combined metrics can clearly
382 distinguish between hierarchical and non-hierarchical realisations.
383 4. The combined metrics also show that there is no hierarchy present in the four Lobyte3D
384 realisations, suggesting that either Lobyte3D is missing key as yet unidentified processes
385 responsible for producing hierarchy, or that hierarchal interpretations of outcrop and
386 subsurface data are more complicated and less realistic than typically assumed.

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Figure captions

Figure 1: An idealised model of hierarchical stacking patterns with three primary clusters each defining a lobe, and each further subdivided into four lobe-element sub-clusters, each of which is composed of a series of individual turbidite beds.

Figure 2: Centroid plot of synthetic fan models, with a normalised 0-to-1 *xy* coordinate range, and varying degrees of randomness in the bed centroid *xy* coordinates A. Totally deterministic and hierarchical, without random offset, B. moderate randomness with a random element of 0.1, C. significant randomness with a random element of 0.5. D. Totally random model with a random element of 1.0. As randomness increases from 0 to 1, the distinction between clusters diminishes, reflecting a transition from well-defined, hierarchical patterns, to a random arrangement of beds.

Figure 3. Dendograms calculated from a selection of synthetic fan scenarios. A. Totally deterministic and hierarchical model. B. Synthetic model with a random offset of 0.2. C. Synthetic model with a random offset of 0.5. D. Totally stochastic model with a random offset

Figure 4. Measurements of clustering and hierarchy in the synthetic fan models. A. Cluster strength plotted against the maximum random point separation shows that cluster strength decreases sharply from a maximum with no random element in the synthetic fan model, to much lower values for a maximum random offset of 0.1 and greater. B. The hierarchy step metric shows 3 hierarchical levels for maximum random offsets less than 0.1, and only one level, so no evidence of hierarchy, for greater levels of randomness in the synthetic fan models.

Figure 5. Topography from the no noise model showing the lobe (yellow), channel, and sediment flow paths (blue) for pre-avulsion flow 189 (a) and post-avulsion flow 190 (b) at the avulsion node location. Yellow cells indicate the location of deposition of the previous flow. Flow 189 deposits a small part of its sediment load at the channel mouth, diverts and climbs over previously-deposited topography, and decelerates and deposits. Flow 190, in contrast, deposits, ascends, but retains enough velocity to divert, accelerate, and start cutting a new channel, defining a new route to begin to deposit a new lobe.

Figure 6. Plot of the no-noise model topography (solid lines) and flow velocity (dashed lines) versus flow distance along the route of flows 189 (red lines) and 190 (blue lines). Prior to avulsion, flow 189 velocity first reverses sign as it hits an opposite-facing slope on previous depositional mound topography, deposits some sediment in the channel mouth that accretes to the back of the previous depositional mound, then decelerates to near zero velocity climbing the prior topography, below the threshold velocity for continued transport, at which point full flow deposition commences. In contrast, flow 190 has sufficient velocity on the slightly steeper slope such that flow deceleration climbing the mound is insufficient to trigger deposition, leaving sufficient remaining velocity to flow over the mound crest, accelerate down the mound lee slope, and start cutting a new channel that defines a new avulsed route further into the basin.

Figure 7. 3D views for each of the different initial topographies, showing how successive flows in different colours backstep up-slope to form lobes, and then avulse as flows divert around the depositional topography created by previous flows using different initial topography. A. no noise topography, B. very smooth noise, C. smooth noise, and D. raw noise topography. Blue circles show the apex position of each turbidite bed, so show stacking pattern of beds, which is mostly aggradational with a slight retrogradational element.

Figure 8. Strike-oriented cross-section and chronostratigraphic plot a y = 15km, for each of the four initial topographies, showing distinct packages of flow deposits each separated by a hemipelagic unit. A. no noise topography, B. very smooth noise, C. smooth noise, and D. raw noise. Clustering of

beds is evident in all four model runs, but becomes more complex as the degree of smoothing of the noise in the initial topography is reduced. Note different colours in the cross section delineate turbidite beds, and tringle geometries are backfilled channels, and in the chronostratigraphic diagram light blue indicates lobe deposition while pale pink indicates channel erosion.

Figure 9. Plot of centroids of stacked beds obtained from Lobyte3D with different initial topographies. A: No noise, 3 lobes. b: very smooth noise, 4 lobes. c: smooth noise, 4 – 5 lobes. d: raw noise, 6 lobes. This figure illustrates the impact of four different initial topographies. The plot unveils a distinct pattern in the flow behaviour, characterized by backstepping of flows followed by avulsion events, leading to the deposition of sediment in new locations. Each bar on the plot represents the chronological order of flow deposits, ranging from the earliest to the latest. The visualization provides valuable insights into the dynamic nature of sedimentation processes and the influence of different initial topographies on the stacking patterns of beds.

Figure 10. Measurements of clustering and hierarchy in the four Lobyte3D models, plotted on top of the synthetic fan model values. Note that Lobyte3D data points are plotted at the point on the x-axis where, according to simple linear interpolation, the synthetic fan model would have the same cluster strength value, assuming that the cluster strength is a reasonable measure of the degree of randomness present in the bed centroid *xy* distribution. See text for discussion.

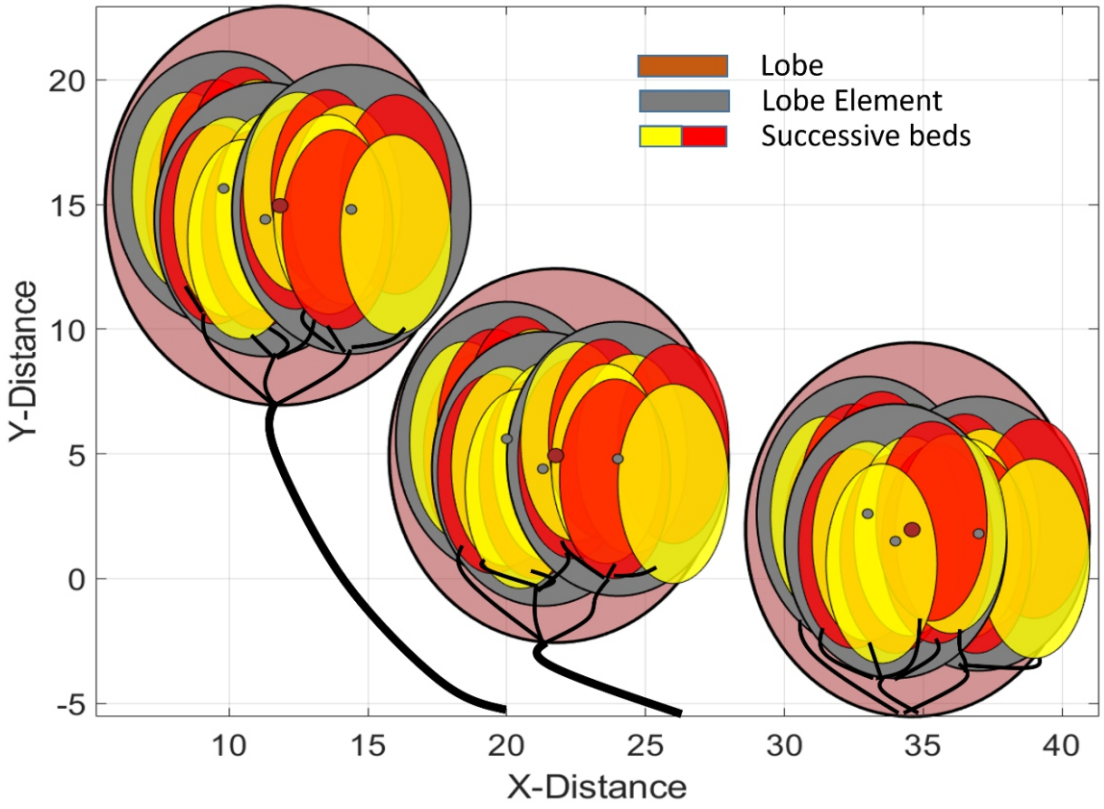

Figure 1

Figure

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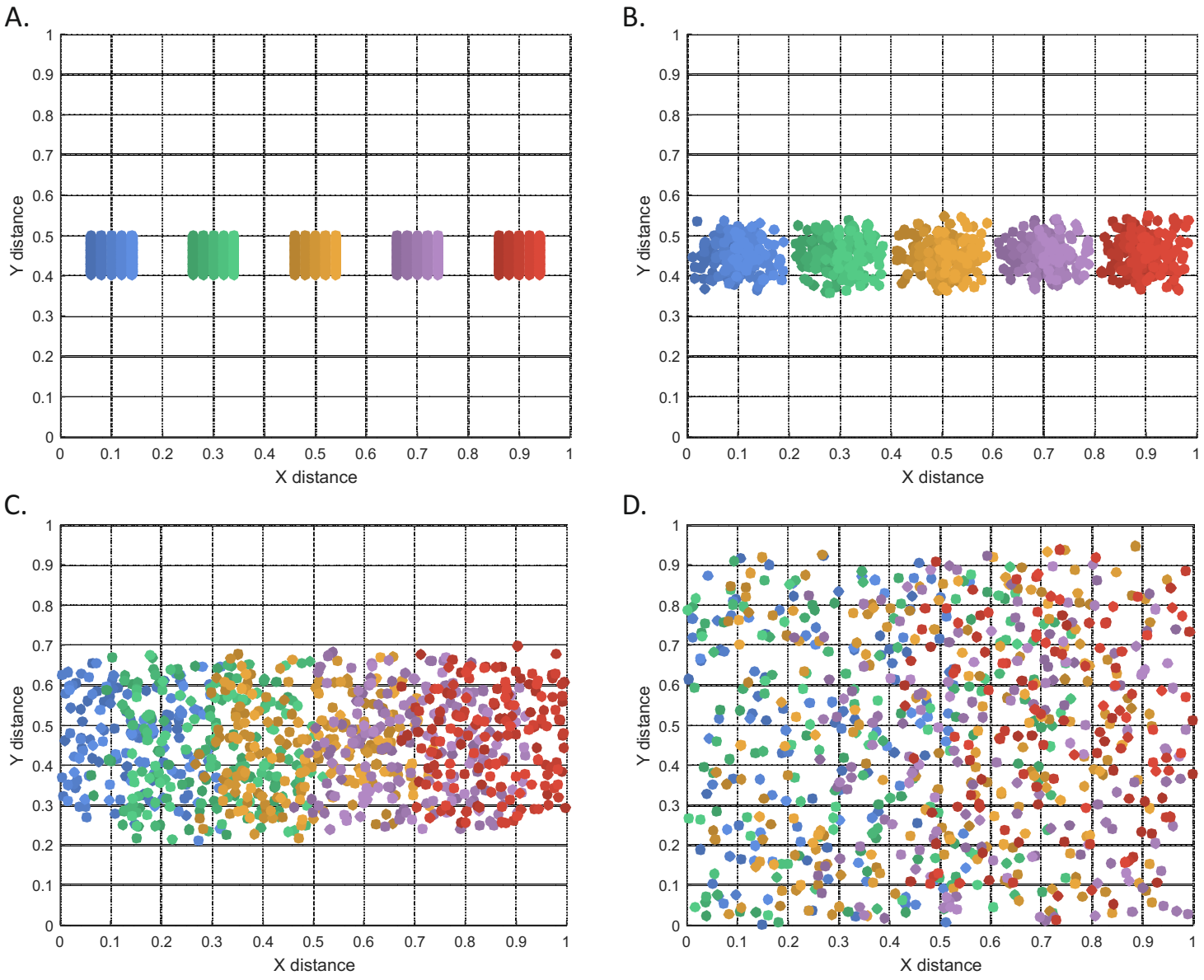

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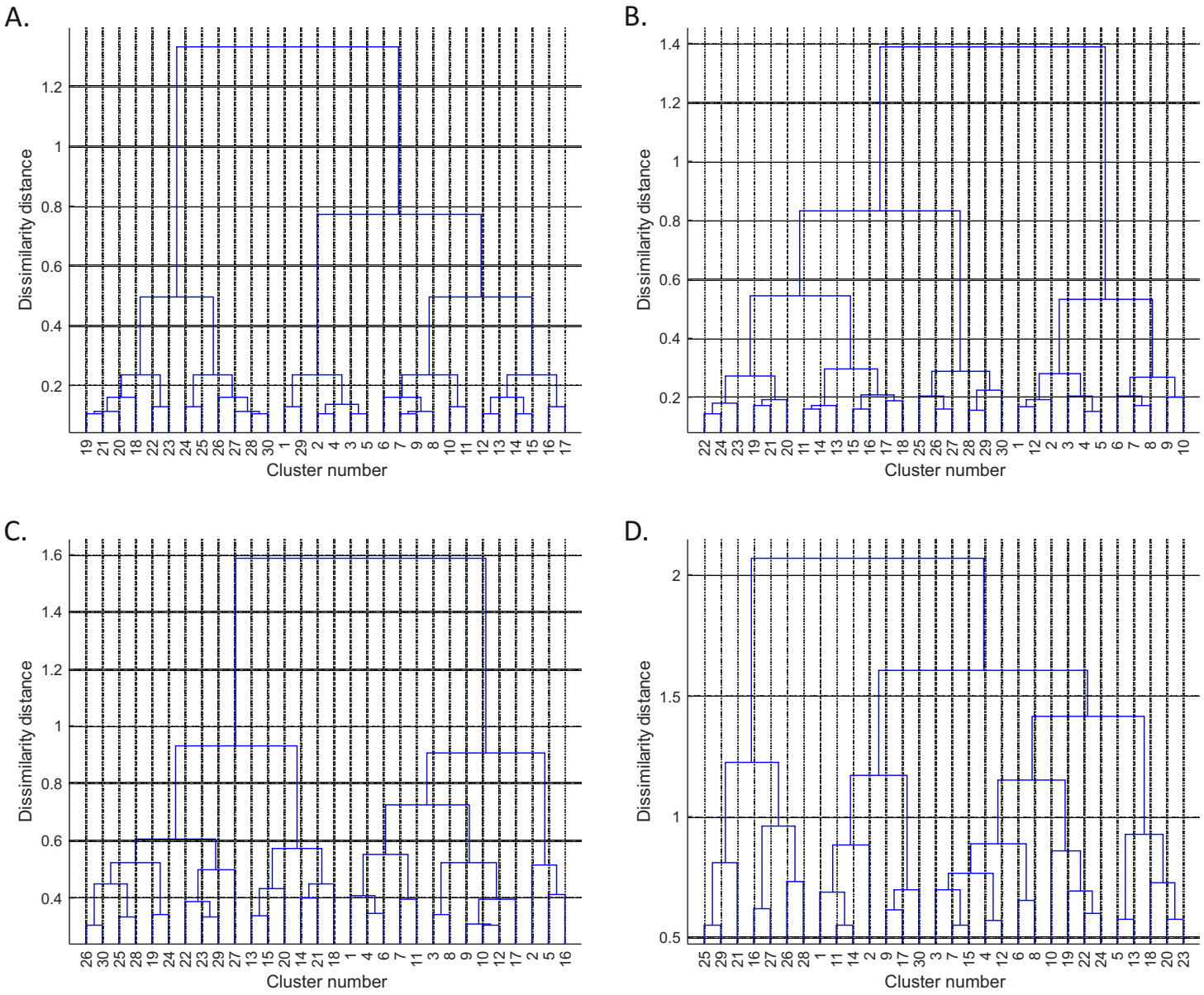

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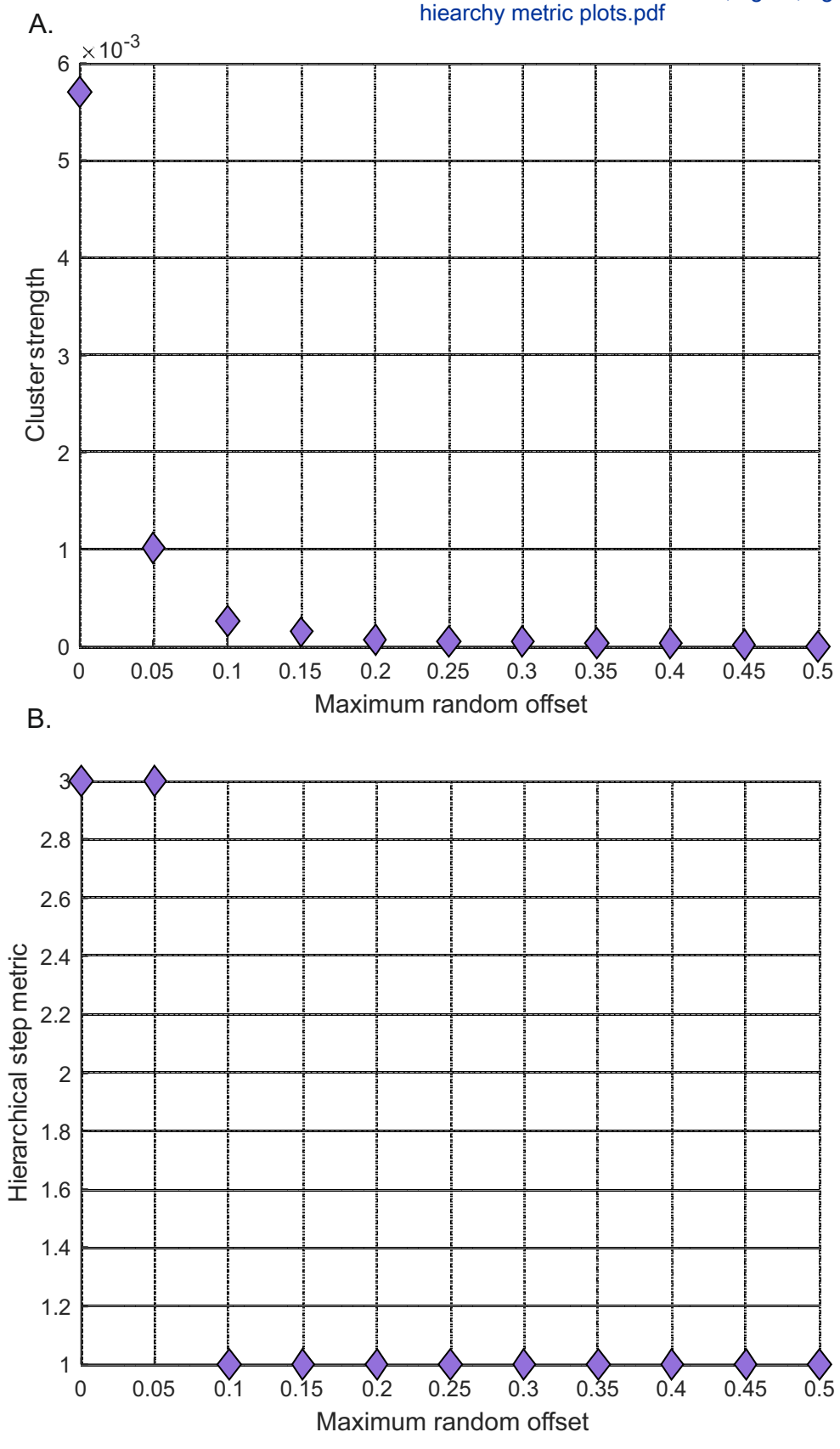

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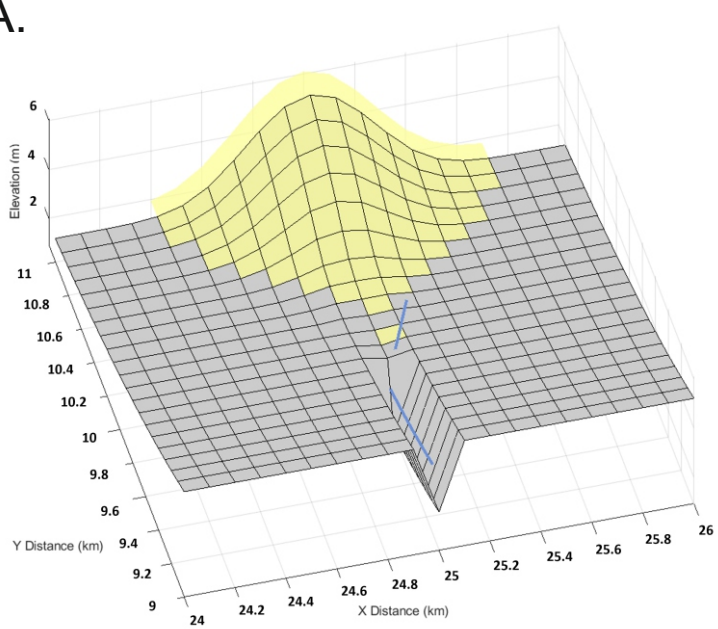

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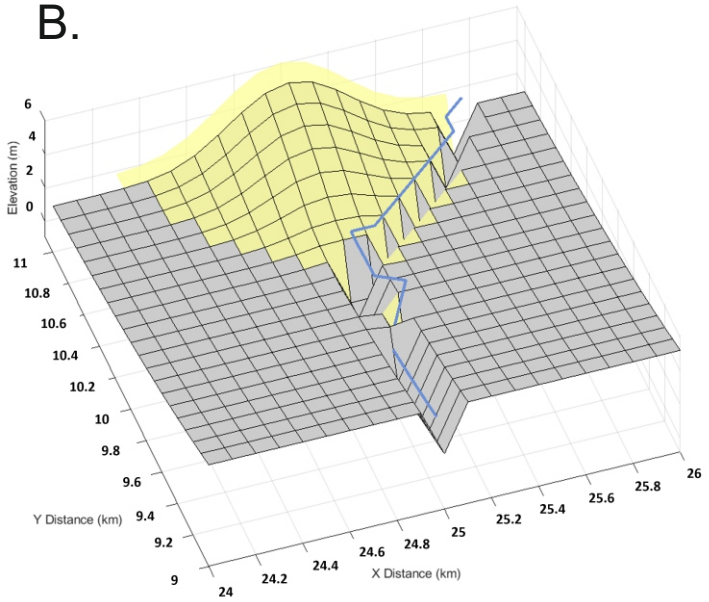

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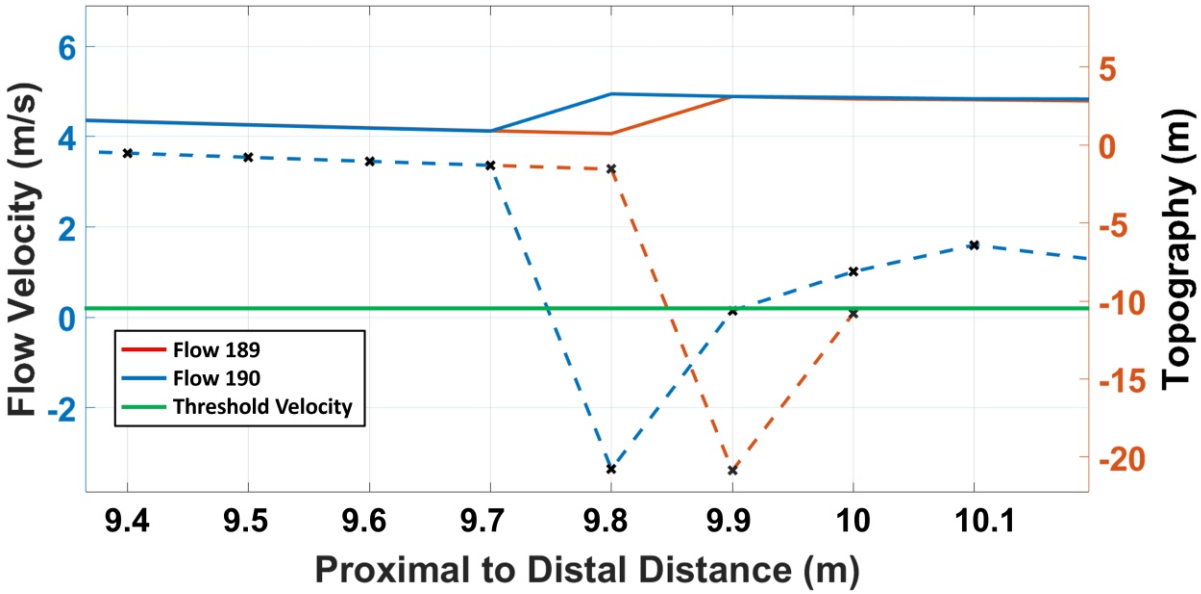

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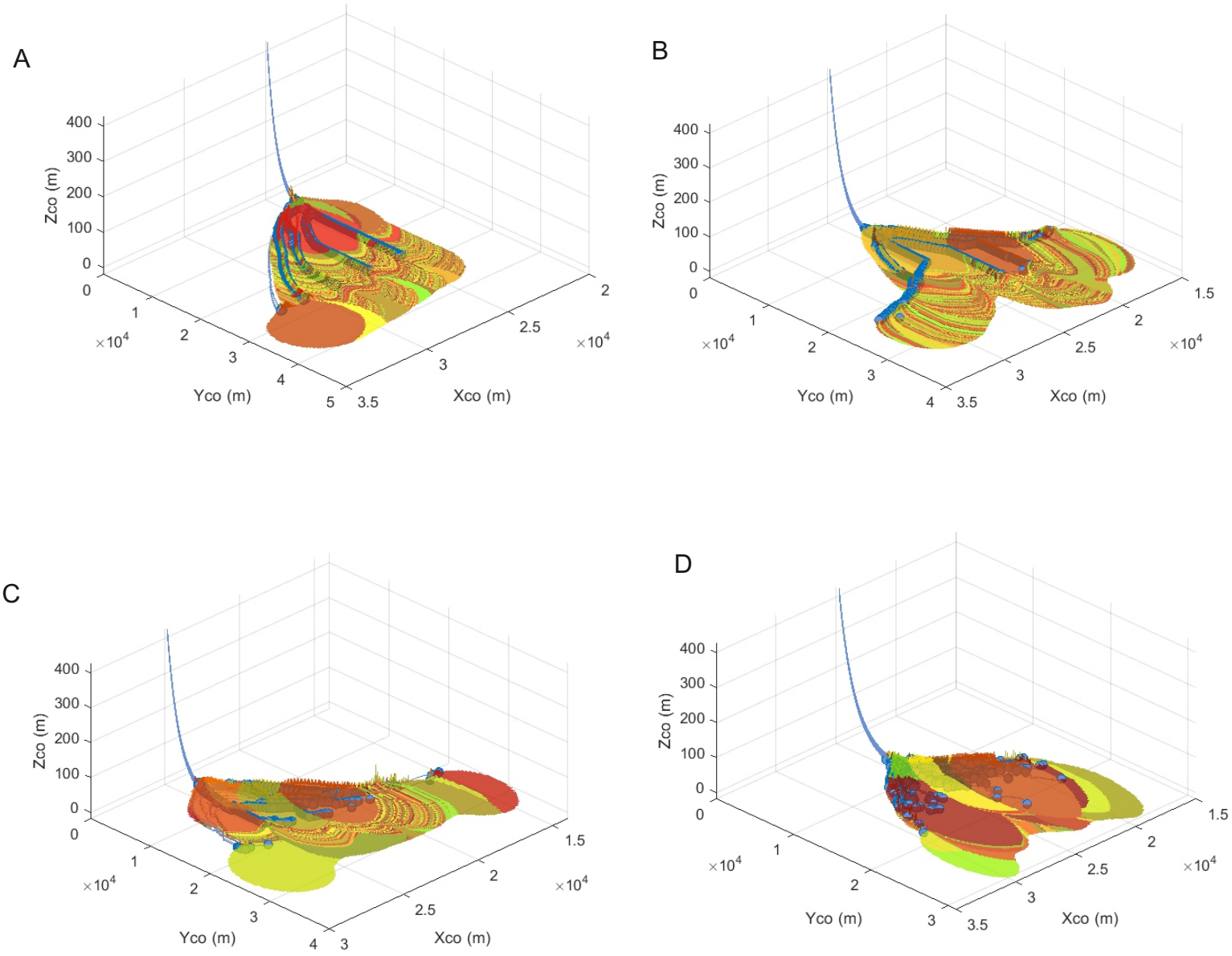

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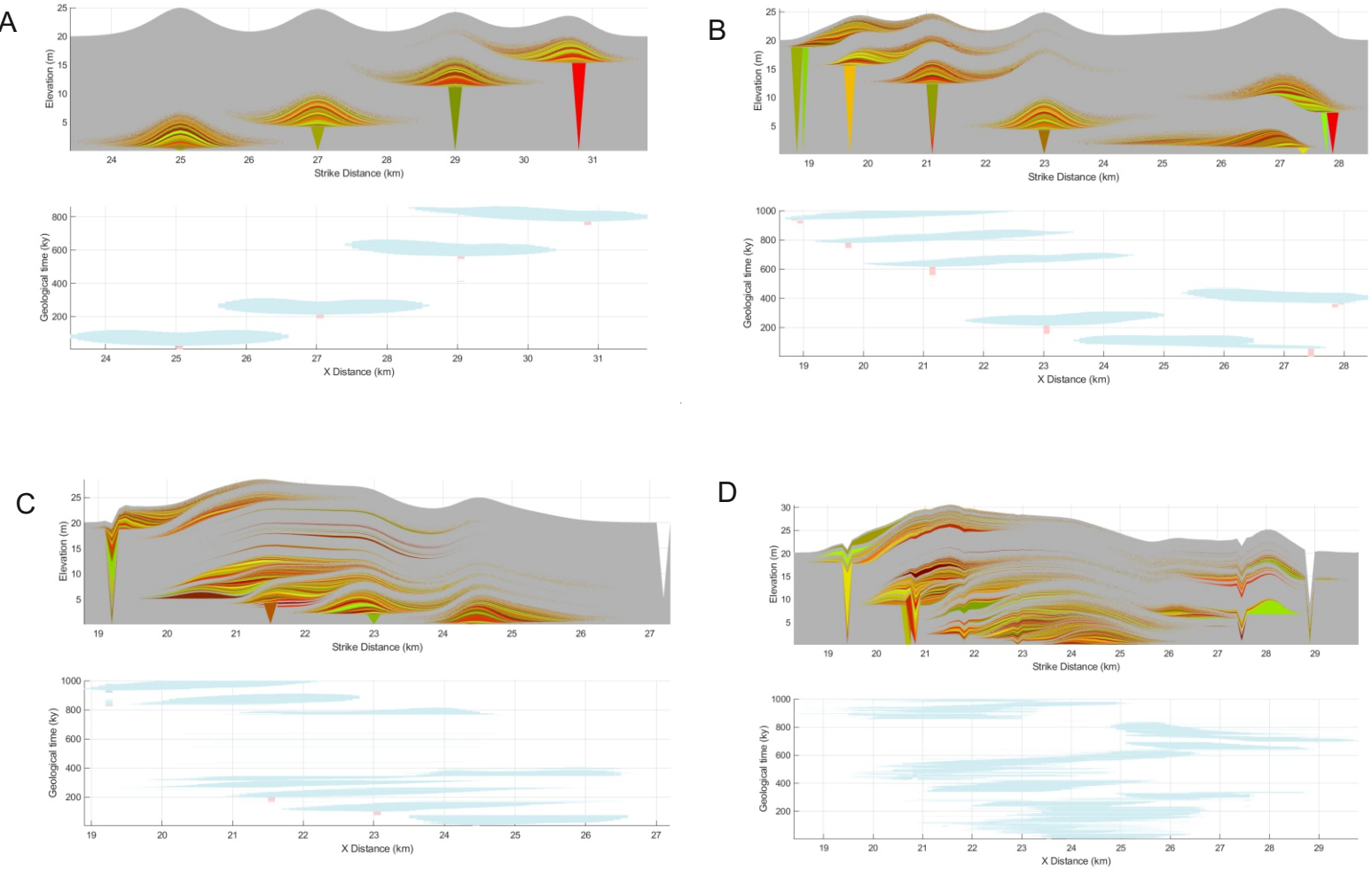

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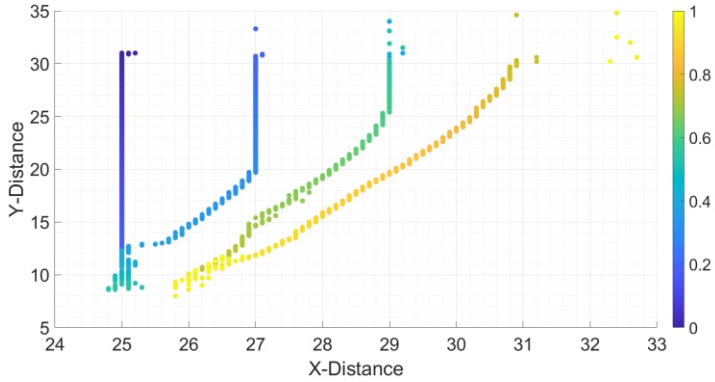

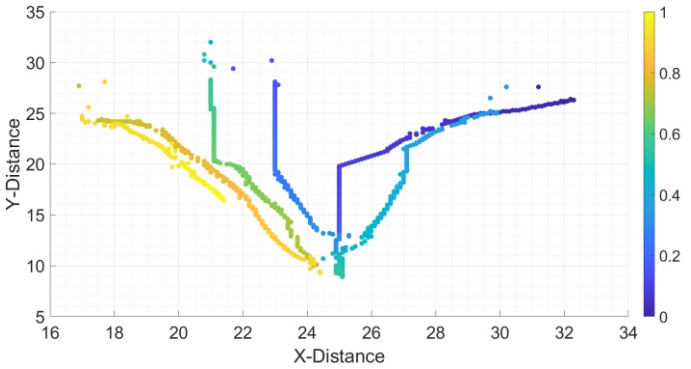

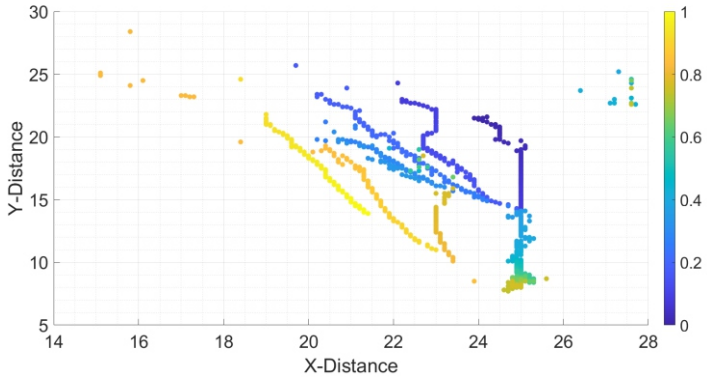

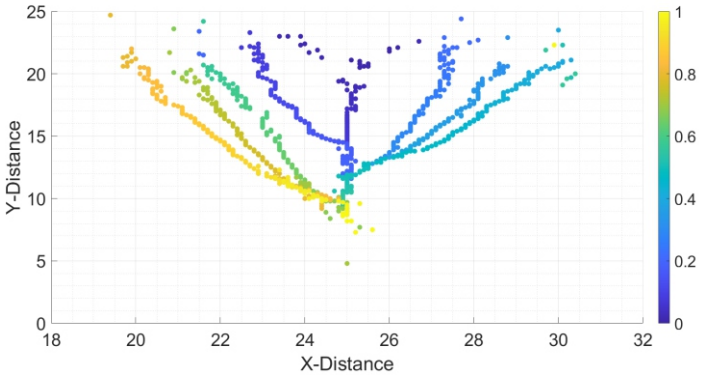

Figure

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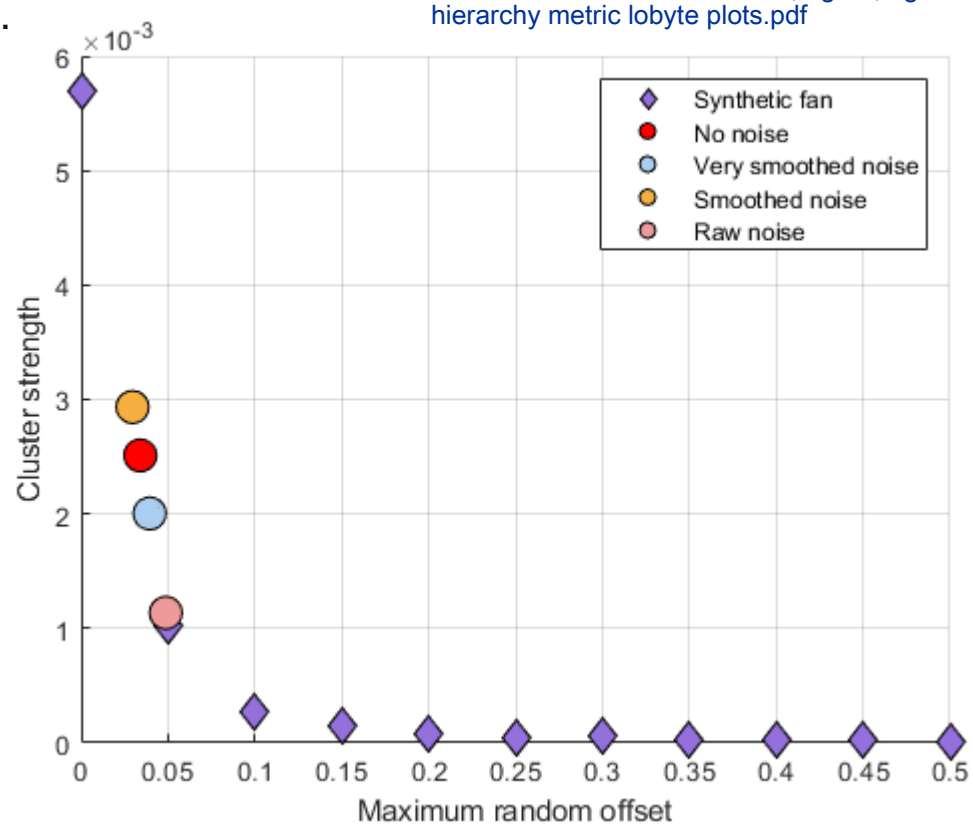
A.



B.