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1 **Deep-Water Fan Hierarchy: Assumptions, Evidence, and Numerical Modelling**
2 **Analysis**

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ABSTRACT

9 Submarine fan strata are commonly described and interpreted assuming a nested, hierarchical
10 organisation of elements, from beds, to lobe elements, lobes and lobe complexes. However,
11 describing outcrop and subsurface strata following a particular conceptual method or model is never
12 evidence in itself that the model or method accurately reflects the true nature of the strata. To
13 develop better understanding of and methods for robust hierarchy identification and measurement
14 we developed two metrics, a clustering strength metric that measures how much clustering is present
15 in the spatial distribution of beds on a submarine fan, and a hierarchy step metric that indicates how
16 many clustered hierarchical elements are present in the bed spatial distribution. Both metrics are
17 applied to two quantitative fan models. The first is a very simple geometric model with 10 realisations
18 ranging from a perfectly clustered hierarchy to a indistinguishable-from-random arrangement of beds.
19 The second model, Lobyte3D, is a reduced-complexity process model which uses a steepest descent
20 flow routing algorithm, combined with a simple but physically reasonable representation of flow
21 velocity, erosion, transport and deposition thresholds, to generate detailed 3D representations of
22 submarine fan strata. Application of the cluster strength and hierarchy step metric to the simpler
23 model demonstrates how the metrics usefully characterise how much order and hierarchy is present
24 in the fan strata. Application to four Lobyte3D models with increasingly complex basin-floor
25 topography shows no evidence for true hierarchy, despite clear self-organisation of the model strata
26 into lobes, suggesting that either Lobyte3D is missing key as yet unidentified processes responsible
27 for producing hierarchy, or that interpretations of hierarchy are not realistic.

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INTRODUCTION

31 Submarine fans are among the largest sedimentary accumulations (William, 1970; Posamentier and
32 Kolla, 2003; Talling *et al.*, 2012) and serve as an essential record of Earth history, offering insights into
33 both local and global geological processes (Emmel and Curray, 1984; Pirmez and Imran, 2003; Deptuck

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34 *et al.*, 2008; Picot *et al.*, 2016; Picot *et al.*, 2019; Rabouille *et al.*, 2017). Formed by a complex interplay
35 of turbidity currents, other types of sediment mass flows, and various hydraulic processes, submarine
36 fans are characterized by their complex stratigraphic architectures and depositional patterns (Straub
37 and Pyles, 2012) Submarine fans are also often important reservoirs for the extraction of
38 hydrocarbons and, increasingly importantly, for the sequestration of carbon (Pettingill, Weimer and
39 Anonymous, 2002).

40 Understanding the organization of submarine fan strata is important for unravelling their formative
41 processes and for deciphering the geological history they preserve. Previous studies have proposed
42 hierarchical schemes to describe fan internal organization and characterise spatial and temporal
43 variations in sedimentation patterns (Gardner, 2000; Pyles, 2008; Deptuck *et al.*, 2008; Prelat *et al.*,
44 2009; Prelat *et al.*, 2010) ; Mutti and Normak 1987; Gardner and Borer 2000, Pyles 2007; Deptuck et
45 al. 2008, Prelat et al., 2009; Prelat et al., 2010). However, despite the significant progress made in
46 characterizing submarine fan architecture, quantitative evidence to define hierarchy remains sparse,
47 and aspects of the fundamental mechanisms that would form hierarchical patterns remain poorly
48 defined.

49

50 **Existing Hierarchical Schemes**

51 If submarine fans are hierarchical, they should show some form of systematic pattern of smaller-scale
52 structures nested within and composing larger-scale structures. For example, in a hierarchical fan, fan
53 lobes would be composed of lobe elements that are in turn each composed of many beds, each bed
54 being one turbidite (Figure 1). Various examples of this type of hierarchical arrangement have been
55 interpreted from outcrop, and subsurface data.

56 Deptuck et al. (2008) used ultra-high-resolution boomer seismic imagery with a vertical resolution of
57 approximately 1 m to define a hierarchical classification for 20 lobes in a late Pleistocene submarine

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58 fan offshore from East Corsica. The classification scheme defined four types of unit starting with a bed
59 or bed-set deposited from single flows, with systematic lateral compensational offsets up to 500 m.
60 Bed-sets stack to form lobe elements, which, in turn, stack to create composite lobes. Composite lobes
61 are separated by disconformable surfaces, abrupt vertical shifts in acoustic facies, or the presence of
62 thin drapes, all resulting from compensational stacking of lobe-elements with lateral offsets ranging
63 from 500 to 2000 m triggered by local avulsion (Deptuck et al. 2008). Composite lobes fed by the same
64 primary conduit stack to form lobe complexes, which frequently exhibit 3-5km lateral shifts between
65 their thickest regions, interpreted to arise from large-scale channel-mouth avulsions. Abandoned
66 composite lobes may be covered by several meters of hemipelagic drape, which may subsequently be
67 eroded by later flows.

68 Based on well-exposed Permian deposits in the Tanqua depocenter of the Karoo Basin, South Africa
69 Prelat et al. (2009) proposed a different four-fold hierarchical classification focused on the properties
70 and geometry of fine-grained interlobe architectural units, which separate more sand-prone bodies.
71 The lowest hierarchical level is single depositional event beds up to 0.5 m thick and hundreds of meters
72 wide. Lobe elements up to 5m thick are composed of stacked beds and form the next higher
73 hierarchical level. Genetically linked vertically stacked lobe elements, separated by fine-grained units
74 typically less than 2 cm thick but occasionally up to 2m thick in topographic lows, create lobes up to 5
75 m thick with widths exceeding 20 km. Finally, lobe complexes are composed of stacked lobe bodies,
76 up to 50 m thick and 40 km wide fed by a single upstream channel.

77 Macdonald *et al.*, (2011) focused on the process sedimentology and internal architecture of lobe
78 deposits in the Carboniferous Ross Sandstone Formation, to propose a three-order hierarchy of bed-
79 sets, lobe-elements, and composite lobes. Lobe-elements are formed by upward-thickening packages
80 of bed-sets, often with basal mudstone units indicative of depositional shutdown. Mudstone
81 thicknesses relate to the lateral distance and duration of avulsion separating compensationally-
82 stacked lobe-elements.

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83 (Cullis *et al.*, 2018) systematically reviewed and compared a representative selection of the most
84 widely adopted deep-marine hierarchy schemes, to assess the principal characteristics of each
85 hierarchical classification, the common diagnostic criteria used to attribute deposits to given
86 hierarchical orders, and the causes of similarity and variability between different schemes. The review
87 revealed recurrent observations underlying all the classification schemes, recommended that
88 hierarchical relationships be categorised based on primary sedimentological observations, rather than
89 through predefined schemes and concluded that a universal process-based hierarchy cannot be
90 established. This is because of the difficulty in to reconcile the different hierarchical schemes arising
91 partly from differences between the underlying studies such as the data types, scales of interest,
92 specific environmental settings and in the significance given to the diagnostic criteria, as well as from
93 the adoption of non-standard terminology.

94 Straub and Pyle (2012) used a modified version of the compensation index to test for statistically
95 significant differences in compensation between different scales in hierarchically-classified strata.
96 They also examined compensation variations between predominantly channelized and unchannelized
97 submarine fan strata in each hierarchical class to test how compensation varies spatially. Their results
98 suggest that hierarchical divisions based on compensation are justified, and that compensation
99 increases along a longitudinal transect through distributive submarine fans.

100

101 **Numerical Stratigraphic Forward Modelling as a Tool for Analysis of Submarine Fan Hierarchy**

102 Numerical stratigraphic forward modelling has emerged as a useful tool for unravelling the
103 complexities of sedimentary system (Paola, 2000; Burgess, 2013). By simulating the interplay between
104 sediment transport, deposition, and erosion processes, these models provide valuable insights into
105 the formation of stratigraphic patterns. Reduced-complexity models aim to capture the simplest
106 possible set of processes that may be responsible for a specific stratigraphic pattern, while also

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107 reducing computational cost, allowing multiple model runs and intensive analysis of model results, in
108 this case to explore the emergence of hierarchical patterns within submarine fan systems.

109 This study utilizes the reduced-complexity stratigraphic forward model, Lobyte3D version 2.2, to
110 investigate the hierarchical organization of submarine fan deposits. Lobyte3D is a three-dimensional
111 reduced-complexity numerical stratigraphic forward model, developed to help understand how and
112 why stacking patterns evolve in submarine fan depositional systems (Burgess *et al.*, 2019). Lobyte3D
113 has been modified from its original form with new representations of key depositional processes, and
114 most importantly, the addition of erosion as a function of flow velocity (Mackie et al., in review). In
115 this paper Lobyte3D is used examine the architecture of submarine strata to to (1) access if there is
116 any definite criteria to interpret lobes and (2) describe patterns present within each lobes. And (3)
117 perform clustering analysis on the flow centroid to quantitatively identify and define lobes.

118

119

MODEL FORMULATION AND METHODOLOGY

120 **Lobyte3D Formulation**

121 Lobyte3D version 2.2 calculates turbidity flow routing, erosion and deposition, and the resulting
122 stacking patterns that evolve as sediment accumulates on a submarine-fan surface. Transport and
123 deposition are calculated on a simple orthogonal 50 by 50 km x-y grid with a cell edge dimension of
124 100m. Each model run consisted of 1000 flow events. Sediment enters the model at y0 at the top of a
125 submarine slope. All the sediment volume in one flow event is moved downslope as one single depth-
126 averaged packet of sediment in one model grid cell at each iteration following a steepest gradient
127 descent down the slope. Deposition starts in the cell where depth-averaged flow velocity into the
128 lowest adjacent cell is equal to or less than a specified sediment threshold velocity. Flow velocity is
129 calculated such that.

130

$$v_f = v_i + (a * \emptyset) \quad (1)$$

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131 where V_f is the flow velocity, V_i is the velocity of the flow at the previous time step, a is the flow
132 acceleration and \emptyset is the flow acceleration proportion taken to be 0.5

133 The flow acceleration a is given by.

$$134 \quad a = v_m - v_i \quad (2)$$

135 and the maximum velocity V_m converts shear velocity into whole flow velocity as a function of
136 topographic gradient and is given by

$$137 \quad v_m = \frac{v_s}{\sqrt{\sigma}} \quad (3)$$

138 where V_s is the maximum shear velocity and σ is the basal friction coefficient.

139 Flow erosion rate is calculated as

$$140 \quad \varepsilon_r = v_{se} * \frac{a}{b} \quad (4)$$

141 where v_{se} is the settling velocity and a and b can be calculated as

$$142 \quad a = C_e * Z^5 \quad (5)$$

$$143 \quad b = 1 + \frac{C_e}{0.3} * Z^5 \quad (6)$$

144 where C_e is the erosion rate constant, and Z is the tractive stress which is calculated as follows.

$$145 \quad Z = Re^6 * \frac{v_s}{v_{se}} \quad (7)$$

146 where Re is the particle Reynold number.

147 Four scenarios of Lobyte3D with varying degrees of complexity in the initial topography was used to
148 model 1000 flow events. They include concave flat floor with no noise, very smoothed noise,
149 smoothed noise, and raw noise. Each flow interrupts background hemipelagic deposition occurring at
150 a rate of 0.02 m ky⁻¹. A flow repeat time of 1000 years will be maintained through each model run

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151 representing a 1 My of flow history and deposition. Input parameters for the model include the initial
152 topography, distribution of the grain-size, deposition threshold velocity to commence dispersive flow
153 and deposition, concentration of the sediment, total volume of sediment transported by the flows
154 (Table1).

155 For each model run, model behaviour was analysed by plotting each down-slope flow route and area
156 of deposition in map view. Avulsion points were identified when the apex of flow deposition shifted
157 substantially from the location of the apex of the previous flow.

158 Table 1: Lobyte3D input parameters

| S/N | Parameter | Value |
|-----|--|-------------------------|
| 1 | Hemipelagic deposition rate, per time step, m My ⁻¹ | 0.02 |
| 2 | Diffusion coefficient, m ² per My. | 0.0 |
| 3 | Density (kg/m ³) of the ambient fluid | 1.00 |
| 4 | Erosion rate constant (m/s) | 1.3 x 10 ⁻¹⁰ |
| 5 | Basal friction coefficient | 0.004 |
| 6 | D50 (m) median grain diameter (medium/fine sand) | 0.00025 |
| 7 | Grain density in kg/m ³ siliciclastic quartz/feldspar | 2660 |
| 8 | Depositional velocity threshold (m/s) to commence dispersive flow and deposition | 0.1 |
| 9 | Flow acceleration/deceleration coefficient | 0.5 |
| 10 | Total flow thickness, fluid and sediment mix (m) | 100 |
| 11 | Flow COG proportion | 0.10 |

| | | |
|----|---|-------|
| 12 | Volumetric sediment concentration | 0.01 |
| 13 | Minimum flow thickness (m) | 0.001 |
| 14 | Proportion of the height of ponding topographic lows to fill when flow is trapped | 1.00 |
| 15 | Flow Radiation Factor | 2.0 |
| 16 | Number of fractions in the depositional fraction profile | 13 |

159

160 Clustering Analysis and Hierarchy Metrics

161 Clustering analysis is a numerical technique to classify data, originally developed as a natural sciences
 162 method to make taxonomy more objective. (Everitt *et al.*, 2011), but now widely applied in earth
 163 sciences (Simpson, Thatcher and Savage, 2012; Takahashi *et al.*, 2019) to identify patterns, group
 164 similar objects, and uncover underlying structures within data. Cluster analysis partitions data based
 165 on their similarities or dissimilarities, and often provides valuable insights into the organization and
 166 relationships within the data (Everitt *et al.*, 2011). Clustering, unlike other classification techniques,
 167 does not rely on preset classes and class-labelled samples, so is a relatively more objective method
 168 (Jiawei Han, 2011).

169 Data point separation distances, or dissimilarity, are a fundamental aspect of many clustering
 170 analyses, quantified using a wide range of dissimilarity measures (Gower and Legendre, 1986), often
 171 in matrix form. Dissimilarity matrices capture pairwise dissimilarities, the distances between individual
 172 data points, such that

$$173 \quad D = \begin{bmatrix} 0 & & & & & \\ d(2,1) & 0 & & & & \\ d(3,1) & d(3,2) & 0 & & & \\ \vdots & \vdots & \vdots & & & \\ d(n,1) & d(n,2) & \cdots & \cdots & 0 & \end{bmatrix}$$

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174 Where $d(i, j)$ is the measured dissimilarity between objects i and j . since $d(i, j) = d(j, i)$, and
175 $d(i, i) = 0$. Analysis of a dissimilarity matrix allows distinction between randomly distributed data
176 where a broad spread of dissimilarity distances is expected, and clustered data, where the distances
177 have a narrower range of values reflecting the specific distances within and between clusters; in
178 clustered data, many of the dissimilarity distances are relatively small because many points occur in
179 close proximity within the clusters.

180 Here we use a metric termed clustering strength to distinguish between clustered xyz data, and a
181 randomly distributed set of xyz points. Clustering strength is calculated from the centroid separation
182 distances such that

$$183 \quad CSI = \left(\sum_{i=1}^N I(d_i \leq T) \right) / N$$

184 where N is the number of bed centroids, d_i is the separation distance between centroid point i and
185 another centroid, T is a threshold distance, and I is an indicator function that returns 1 if or 0,
186 depending the logical condition $d_i \leq T$. For a threshold distance that is 1% of the maximum dissimilarity
187 distance in the system, values of clustering strength will approach zero as the degree of randomness
188 in xyz points increase, and the value will always be higher for clustered data.

189 Once a degree of non-random clustering has been identified, the nature of the clustering can be
190 assessed, specifically whether there is any hierarchical element such that smaller clusters themselves
191 cluster to form larger clusters, and so on (e.g. Figure 1). Hierarchical Agglomerative Clustering Analysis
192 (Gordon, 1987) is a bottom-up clustering analysis approach that starts with individual data points,
193 merging them into new clusters based on their dissimilarity values, until all points are within one
194 cluster. Euclidean dissimilarity distances were used because these most effectively measure bed
195 centroid spatial relationships in xyz coordinate space, and the complete linkage method was selected
196 because it has low sensitivity to outliers, and is relatively robust in noisy data (Jiawei Han, 2011), so a
197 good choice to identify hierarchy levels.

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198 Hierarchical cluster analysis results are plotted as a dendrogram, with cluster separation distance on
199 the Y-axis, and cluster number on the x-axis. The actual degree of hierarchy present in the dendrogram
200 can be assessed quantitatively by extracting dissimilarity distances between dendrogram bifurcation
201 points, and analysing these for clustering also; a hierarchical example should show clustering in these
202 bifurcation distances, because bifurcations should occur at specific scales reflecting the size and
203 separation distance of the various hierarchical elements. The hierarchy step metric is then the number
204 of distinct clusters identified in the dendrogram bifurcation point distances, typically 1 for
205 indistinguishable from random points with little or no clustering, and otherwise a number
206 representing the number of hierarchical levels present in the data.

207

208

RESULTS

209 **Synthetic Lobe Model Results**

210 To provide a well-understood definitively hierarchical baseline for the analysis, eleven synthetic fan
211 lobe models were constructed and analysed, each comprising 1000 beds, with 40 beds in a lobe
212 element, five lobe elements per lobe, and five lobes in total. These models are range from perfectly
213 deterministic and hierarchical, with distinct lobes and lobe elements composed of beds arranged in a
214 simple retrogradational stacking pattern, to a completely stochastic example with a stochastic
215 distribution of bed centroids (Figure 2). The entirely deterministic fan arrangement follows the three
216 or four-fold hierarchy described in (Gervais *et al.*, 2006; Deptuck *et al.*, 2008; Prelat, Hodgson and
217 Flint, 2009) (Figure 1). A random offset is added to each x and y coordinate in the deterministic model,
218 and the magnitude of the added random element ranges from 0.05 to 0.5. For example, a model with
219 a random element of 0.2 has a random offset of each x and y coordinate ranging from -0.1 to 0.1.

220 For each synthetic fan lobe model, cluster strength was calculated, and also hierarchy step values were
221 derived from dendrogram analysis (Figure 3). The cluster strength values range from a high of 5.7×10^7

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222 ³ for the completely deterministic hierarchically clustered fan, to 1.0×10^{-5} for the entirely random bed
223 centroid points, and the decrease in the metric value is quite sharp as the magnitude of random point
224 offset increases (Figure 4A). The dendrogram hierarchy analysis shows a similar pattern. The two least-
225 random-component models yield a hierarchy step value of 3, an accurate measurement of the number
226 of hierarchical levels built in to each model (Figure 4B). In contrast, the models with a random offset
227 value of 0.2 and greater have a hierarchy step value of 1 indicating that a random offset of 0.2 or more
228 is enough to remove any detectable hierarchy.

229

230 **Lobyte3D Model Results**

231 Lobyte3D was run with four different initial topographies defining scenarios with no noise, very
232 smoothed noise, smoothed noise, and raw noise. Strike-oriented cross-sections, 3D views of the
233 channel, bed and lobe stacking patterns, and bed centroid maps from these different initial
234 topographies are used to understand how variations in initial topography control avulsion, fan
235 stacking, and the hierarchical organization of the modelled submarine fan strata.

236 *Avulsion Cycle Processes*

237 The avulsion process is key to forming lobes and therefore key to generating any stratal hierarchy
238 present, so it is important to understand exactly how avulsion occurs in the model. Evolving flow
239 routing shows substantial changes during avulsion, bypassing previous mounded depositional
240 topography, and cutting a new section of channel that bypasses sediment further into the basin to the
241 point where the initial basin floor slope is low enough to decelerate the flow enough to trigger
242 deposition.

243 Analysis of the first avulsion in the no noise case reveals the detail of how avulsion occurs in Lobyte3D.
244 Prior to flow 190, deposition was backstepping up the basin-margin slope, partially backfilling the
245 mouth of the previously cut channel (Figure 5). Upslope backstepping occurred due to flow interaction

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246 at the channel-lobe transition, with strata deposited from previous flows triggering flow deceleration
247 and further deposition. As strata backstep upslope, depositional relief at the channel mouth on the
248 proximal mound edge increased, and magnitude of deceleration when flows reach this depositional
249 topography also increased. Each time a flow encounters a mound that has been built by previous
250 flows, the flow will continue to follow the steepest available down-slope route, and therefore tend to
251 divert left or right to climb over the lowest-relief part of the mound. Flow velocity prior to climbing
252 the depositional mound tends to increase through time as deposition backsteps up the basin-margin
253 slope, and by flow 190, the flow had sufficient remaining velocity after climbing the depositional
254 mound (Figure 5) to continue to flow, accelerate down from the crest of the mound, and start to cut
255 a new channel. Flow routing through the new channel bypasses the positive topography produced by
256 the previous lobe deposition, defines a new route further into the basin (Figure 5b), and starts to
257 deposit a new lobe, defining an avulsion event.

258 Rather obviously this is a much-simplified representation of what actually happens in deep-water
259 depositional systems. For instance, several processes have been investigated to produce instability
260 that results in avulsion-threshold circumstances. Channel sinuosity, channel lengthening, channel
261 thalweg and levee aggradation, and channel-relief reduction are some of these causes (Kolla, 2007;
262 Prelat, Hodgson and Flint, 2009; Groenenberg *et al.*, 2010). In this analysis we assume that this
263 modelled avulsion process is sufficiently realistic and representative enough of the real physical
264 process to form the basis for at least initial numerical experiment exploration of how this behaviour
265 influences fan lobe geometry stacking and potential hierarchy.

266

267 *Flow Routing and Stacking Patterns*

268 All four modelled scenarios generated a multi-km-scale submarine fan (Figure 7) consisting of
269 interbedded turbidite event beds and background hemipelagic strata organised as more-or-less
270 discrete lobes (Figure 8) broadly comparable to typical observed submarine-fan bathymetry and

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271 successions (Romans *et al.*, 2009; Romans *et al.*, 2011; Prelat, Hodgson and Flint, 2009; Prelat and
272 Hodgson, 2013). The no noise initial topography produces the most systematic lobe stacking with a
273 simple compensational stacking pattern and lobe boundaries clearly defined by a few meters of
274 hemipelagic sediments (Figure 8A). Each lobe is composed of around 60-to-200 mostly contiguous,
275 spatially-clustered backstepping flow events. Lobes have a simple stacking pattern, separated by
276 progressive lateral 1-2km shift in focus of deposition, and a mean duration of 114 ky (Figure 8A).

277 The very smooth noise initial topography produces similar but slightly more complex lobe stacking
278 pattern (Figure 8B). These lobes consist of around 50 to 130 aggradational and backstepping beds with
279 a lateral lobe separation distance of 2-4 km and a mean duration of 83 ky (Figure 8B, Figure 9B). The
280 smooth noise initial topography case still shows some discrete lobes, but lobe structure and stacking
281 are more complex (Figure 7C). Where distinct enough to measure, lobes consist of 35-70 contiguous
282 spatially clustered flow events, with lateral lobe separation distance ranging from 0.5 to 2 km and a
283 mean duration of 50 ky (Figure 8C, Figure 9C). Finally, the raw noise initial topography shows the most
284 complex lobe stacking pattern lacking any clear trend (Figure 7D, Figure 9D). These lobes are even
285 more difficult to define. Where discrete enough to define, lobes consist of 5 to 270 aggradational and
286 backstepping stacked beds with a separation distance of 1 to 3 km, but also the highest gradual lateral
287 shift within each lobe (Figure 8D) and a mean duration of 112 ky.

288

289 *Quantification of Clustering and Hierarchy in Lobyte3D Results*

290 Cluster strength values for the four Lobyte3D models range from 2.51×10^{-3} to 1.14×10^{-3} (Figure 4A)
291 and the smoothed noise initial topography generates the highest clustering strength, suggesting that
292 smoothed noise in the basin-floor topography can enhance clustering relative to the case with the
293 simplest no-noise topography. In contrast, the raw noise basin-floor topography model has the lowest
294 clustering strength (Figure 4A) due to the irregular topography disrupting the regular stacking and
295 avulsion pattern required for clustering. All four model runs generate strata with a hierarchical step

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296 value of 1, indicating that no hierarchy is detectable in the spatial distribution of bed centroids, despite
297 the clustering. This suggests that although the clustering produces clear lobe structures, particularly
298 in the no noise and smoothed noise cases, this bed-lobe distinction is not enough to define a hierarchy
299 measured by this dendrogram-derived metric.

300

301

DISCUSSION

302 **Reduced complexity models**

303 Reduced complexity models are, by design, very much simplified representations of the complex
304 processes that generate real strata (Liang et al., 2015). Consequently, results from reduced complexity
305 models must be used carefully, and not over interpreted or assumed to have predictive power beyond
306 what is reasonably supported by their constituent process representations. However, these models
307 also have some substantial advantages over more complex models, particularly their lower
308 computational cost, and perhaps most importantly, the fact that if a reduced complexity model
309 demonstrates a particular emergent behaviour, the process representation in the model is quite likely
310 to be the simplest possible representation of that process.

311 In this case Lobyte3D shows avulsion events that divert deposition into new locations clustering sets
312 of beds to form lobes. Critical elements in the model necessary for this a steepest-descent transport
313 algorithm and a gradient threshold for initiation for turbidite bed deposition. Both these elements are
314 represented in a very simple but physically reasonable way, and do seem to operate to some degree
315 in real submarine fan systems. Given this the resulting lobe formation in the model is probably realistic
316 enough to offer some basic but useful insight in deep-water fan processes and structure. However, it
317 is also important to remember that additional and more realistic representations of key processes, for
318 example more detail in the 3D structure and spatial distribution of each flow and consideration of a
319 range of grain sizes in each flow may generate different avulsion process and different fan structures

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320 (e.g. (Wahab *et al.*, 2022)) and (Hamilton, Strom and Hoyal, 2015) found that uneven topography
321 increases channel avulsion likelihood due to localized variations in sediment concentration, leading to
322 mouth bar formation and hydraulic jumps. Clearly these processes and controls require further
323 investigation with more complex models, but starting with the simplest model seems sensible.

324

325 **Influence of initial topography**

326 Lobyte3D models in this analysis show substantial influence of initial topography on flow routing,
327 avulsion, and lobe stacking patterns. Previous studies have shown or interpreted a similar influence
328 of topography in shaping submarine fan evolution and architecture (Groenenberg *et al.*, 2010; Straub
329 and Pyles, 2012; Hamilton, Strom and Hoyal, 2015; Cullis *et al.*, 2018; Ferguson *et al.*, 2020); taken
330 together these results support the hypothesis that initial topography influences lobe switching and
331 avulsion timing (Piper and Normark, 2001; Gervais *et al.*, 2006; Groenenberg *et al.*, 2010; Ferguson *et*
332 *al.*, 2020). However, the formulation of Lobyte3D is perhaps particularly sensitive to small changes in
333 seafloor topography, especially in terms of flow routing prior to deposition, so further work
334 developing more complex model formulations or testing this effect with other numerical and analogue
335 models is required.

336

337 **Absence of hierarchy**

338 There is no hierarchy present in these Lobyte3D results; all modelled strata show detectable non-
339 random clustering, as indicated by comparison with the entirely synthetic fan models, but all the
340 Lobyte3D models have a hierarchical step value 1. This combination of cluster and hierarchy metric
341 values indicate that no hierarchy is detectable in the spatial distribution of bed centroids, despite the
342 clustering.

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343 Clearly absence of a hierarchy in strata calculated in a reduced complexity numerical model is not
344 necessarily evidence that hierarchy does not occur in real deep-water fan strata. However, nor is
345 interpretation of outcrop and subsurface data following a conceptual model of stratal hierarchy
346 evidence that the deep-water fan strata really are hierarchical. Failure to reproduce hierarchy in a very
347 simple numerical model highlights two end-member possibilities; either hierarchy is a real feature of
348 deep-water fan strata, but occurs by processes not adequately represented in Lobyte3D, or the
349 interpretations of hierarchy in outcrop and subsurface strata are an over-interpretation of limited data
350 with insufficient quantitative evidence to be properly robust.

351 Avulsion is a key control on hierarchy formation because it is the main process forming clustered
352 entities such as lobes. Avulsion in Lobyte3D happens in a simplified and specific way that likely does
353 not capture the range of different and perhaps more complex mechanisms that operate in real
354 submarine fan systems (Hamilton *et al.*, 2015; Ortiz-Karpf *et al.*, 2015; Qi *et al.*, 2022; de Haas *et al.*,
355 2016). Clearly therefore further modelling and model development is required, with Lobyte3D or
356 other process models including analogue models perhaps, to explore how other avulsion processes
357 might behave differently and produce hierarchical clustering.

358 Until now, interpretations of hierarchy in submarine fan strata have been mostly qualitative, and this
359 lack of quantitative evidence does mean that conclusions of hierarchy are much more tenuous than
360 has perhaps been recognised. More quantitative analysis is therefore required, but a key challenge is
361 how to analyse limited data, for example one-dimensional vertical sections, to provide metrics that
362 can reliably identify and present or absence of hierarchy developed in three-dimensional strata; most
363 current interpretations do not recognise or account for this uncertainty (Gervais *et al.* 2006; Deptuck
364 *et al.* 2008; Prelat *et al.* 2009; MacDonald *et al.* 2011), suggesting that hierarchical patterns observed
365 in previous studies are probably not universally applicable to all submarine fan systems (Cullis *et al.*
366 2018; Ferguson *et al.* 2020), and development of further tools for quantification of hierarchy with
367 limited outcrop and subsurface data is essential.

368

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CONCLUSIONS

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1. Submarine fan strata are commonly described and interpreted to have a nested, hierarchical organisation of elements, but quantitative evidence from outcrop and subsurface data to support this interpretation is limited.

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2. Two new metrics are defined, calculated and used to identify the degree of hierarchy present in the modelled fan strata. A clustering strength metric measures how much clustering is present in the spatial distribution of Lobyte3D beds, and a hierarchy step metric indicates how many clustered hierarchical elements are present in the bed spatial distribution.

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3. Both metrics applied to a definitively hierarchical geometric fan model with ten progressively more randomised realisations, shows that the combined metrics can clearly distinguish between hierarchical and non-hierarchical realisations.

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4. The combined metrics also show that there is no hierarchy present in the four Lobyte3D realisations, suggesting that either Lobyte3D is missing key as yet unidentified processes responsible for producing hierarchy, or that hierarchal interpretations of outcrop and subsurface data are more complicated and less realistic than typically assumed.

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486 **Figure captions**

487 Figure 1: An idealised model of hierarchical stacking patterns with three primary clusters each defining
488 a lobe, and each further subdivided into four lobe-element sub-clusters, each of which is composed
489 of a series of individual turbidite beds.

490 Figure 2: Centroid plot of synthetic fan models, with a normalised 0-to-1 xy coordinate range, and
491 varying degrees of randomness in the bed centroid xy coordinates A. Totally deterministic and
492 hierarchical, without random offset, B. moderate randomness with a random element of 0.1, C.
493 significant randomness with a random element of 0.5. D. Totally random model with a random
494 element of 1.0. As randomness increases from 0 to 1, the distinction between clusters diminishes,
495 reflecting a transition from well-defined, hierarchical patterns, to a random arrangement of beds.

496 Figure 3. Dendograms calculated from a selection of synthetic fan scenarios. A. Totally deterministic
497 and hierarchical model. B. Synthetic model with a random offset of 0.2. C. Synthetic model with a
498 random offset of 0.5. D. Totally stochastic model with a random offset

499 Figure 4. Measurements of clustering and hierarchy in the synthetic fan models. A. Cluster strength
500 plotted against the maximum random point separation shows that cluster strength decreases sharply
501 from a maximum with no random element in the synthetic fan model, to much lower values for a
502 maximum random offset of 0.1 and greater. B. The hierarchy step metric shows 3 hierarchical levels
503 for maximum random offsets less than 0.1, and only one level, so no evidence of hierarchy, for greater
504 levels of randomness in the synthetic fan models.

505 Figure 5. Topography from the no noise model showing the lobe (yellow), channel, and sediment flow
506 paths (blue) for pre-avulsion flow 189 (a) and post-avulsion flow 190 (b) at the avulsion node location.
507 Yellow cells indicate the location of deposition of the previous flow. Flow 189 deposits a small part of
508 its sediment load at the channel mouth, diverts and climbs over previously-deposited topography, and
509 decelerates and deposits. Flow 190, in contrast, deposits, ascends, but retains enough velocity to
510 divert, accelerate, and start cutting a new channel, defining a new route to begin to deposit a new
511 lobe.

512 Figure 6. Plot of the no-noise model topography (solid lines) and flow velocity (dashed lines) versus
513 flow distance along the route of flows 189 (red lines) and 190 (blue lines). Prior to avulsion, flow 189
514 velocity first reverses sign as it hits an opposite-facing slope on previous depositional mound
515 topography, deposits some sediment in the channel mouth that accretes to the back of the previous
516 depositional mound, then decelerates to near zero velocity climbing the prior topography, below the
517 threshold velocity for continued transport, at which point full flow deposition commences. In contrast,
518 flow 190 has sufficient velocity on the slightly steeper slope such that flow deceleration climbing the
519 mound is insufficient to trigger deposition, leaving sufficient remaining velocity to flow over the
520 mound crest, accelerate down the mound lee slope, and start cutting a new channel that defines a
521 new avulsed route further into the basin.

522 Figure 7. 3D views for each of the different initial topographies, showing how successive flows in
523 different colours backstep up-slope to form lobes, and then avulse as flows divert around the
524 depositional topography created by previous flows using different initial topography. A. no noise
525 topography, B. very smooth noise, C. smooth noise, and D. raw noise topography. Blue circles show
526 the apex position of each turbidite bed, so show stacking pattern of beds, which is mostly
527 aggradational with a slight retrogradational element.

528 Figure 8. Strike-oriented cross-section and chronostratigraphic plot a y = 15km, for each of the four
529 initial topographies, showing distinct packages of flow deposits each separated by a hemipelagic unit.
530 A. no noise topography, B. very smooth noise, C. smooth noise, and D. raw noise. Clustering of beds is

531 evident in all four model runs, but becomes more complex as the degree of smoothing of the noise in
532 the initial topography is reduced. Note different colours in the cross section delineate turbidite beds,
533 and triangle geometries are backfilled channels, and in the chronostratigraphic diagram light blue
534 indicates lobe deposition while pale pink indicates channel erosion.

535 Figure 9. Plot of centroids of stacked beds obtained from Lobyte3D with different initial topographies.
536 A: No noise, 3 lobes. b: very smooth noise, 4 lobes. c: smooth noise, 4 – 5 lobes. d: raw noise, 6 lobes.
537 This figure illustrates the impact of four different initial topographies. The plot unveils a distinct
538 pattern in the flow behaviour, characterized by backstepping of flows followed by avulsion events,
539 leading to the deposition of sediment in new locations. Each bar on the plot represents the
540 chronological order of flow deposits, ranging from the earliest to the latest. The visualization provides
541 valuable insights into the dynamic nature of sedimentation processes and the influence of different
542 initial topographies on the stacking patterns of beds.

543 Figure 10. Measurements of clustering and hierarchy in the four Lobyte3D models, plotted on top of
544 the synthetic fan model values. Note that Lobyte3D data points are plotted at the point on the x-axis
545 where, according to simple linear interpolation, the synthetic fan model would have the same cluster
546 strength value, assuming that the cluster strength is a reasonable measure of the degree of
547 randomness present in the bed centroid xy distribution. See text for discussion.

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