The Community Code Verification Exercise for Simulating Sequences of Earthquakes and Aseismic Slip (SEAS)

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Abstract

Numerical simulations of Sequences of Earthquakes and Aseismic Slip (SEAS) have made great progress over the past decades to address important questions in earthquake physics and fault mechanics. However, significant challenges in SEAS modeling remain in resolving multiscale interactions between aseismic fault slip, earthquake nucleation, and dynamic rupture; and understanding physical factors controlling observables such as seismicity and ground deformation. The increasing capability and complexity of SEAS modeling calls for extensive efforts to verify codes and advance these simulations with rigor, reproducibility, and broadened impact. In 2018, we initiated a community code-verification exercise for SEAS simulations, supported by the Southern California Earthquake Center (SCEC). Here we report the findings from our first two benchmark problems (BP1 and BP2), designed to test the capabilities of different computational methods in correctly solving a mathematically well-defined, basic problem in crustal faulting. These benchmarks are for a 2D antiplane problem, with a 1D planar vertical strike-slip fault obeying rate-and-state friction, embedded in a 2D homogeneous, linear elastic half-space. Sequences of quasi-dynamic earthquakes with periodic occurrences (BP1) or bimodal sizes (BP2) and their interactions with aseismic slip are simulated. The comparison of >70 simulation results from 11 groups using different numerical methods, uploaded to our online platform, show excellent agreements in long-term and coseismic evolution of fault properties. In BP1, we found that the truncated domain boundaries influence interseismic fault stressing, earthquake recurrence, and coseismic rupture process, and that agreement between models is only achieved with sufficiently large domain sizes. In BP2, we found that complexity of long-term fault behavior depends on how well important physical length scales related to spontaneous nucleation and rupture propagation are resolved. Poor numerical resolution can result in the generation of artificial complexity, impacting simulation results that are of potential interest for characterizing seismic hazard, such as earthquake size distributions, moment release, and earthquake recurrence times. These results inform the development of more advanced SEAS models, contributing to our further understanding of earthquake system

dynamics.

Introduction and Motivation

When we develop models of physical systems, credible and reproducible results are essential to scientific progress. Robust predictive models of earthquake source processes have become important means for studying fundamental questions in earthquake science. Models of single earthquakes (known as *dynamic rupture simulations*) have emerged as powerful tools for understanding the influence of fault geometry, friction and prestress on rupture propagation, and for explaining observations of high-frequency ground motions and damage zones (*Day*, 1982; *Olsen et al.*, 1997; *Nielsen et al.*, 2000; *Duan and Oglesby*, 2006; *Ripperger et al.*, 2007; *Bhat et al.*, 2007; *Dunham et al.*, 2011a,b; *Lozos et al.*, 2011; *Gabriel et al.*, 2012; *Shi and Day*, 2013; *Kozdon and Dunham*, 2013; *Xu et al.*, 2015; *Wollherr et al.*, 2018; *Ma and Elbanna*, 2019). Many of the codes used for these studies incorporate advanced features such as 3D domains and complex fault geometries, leading to very large problems for which rigorous convergence tests can be too computationally expensive. An alternative means for verifying model results are code comparisons made across the different modeling groups, using cell sizes at the limit of computational feasibility. Over the past decade, the SCEC/USGS Spontaneous Rupture Code Verification Project has made significant progress in using code comparison studies to provide confidence in model outcomes (*Harris et al.*, 2009; *Barall and Harris*, 2015; *Harris et al.*, 2018).

Although these dynamic rupture simulations have contributed greatly to our understanding of the physical factors that govern ground motion, they are limited to single-event scenarios with imposed artificial prestress conditions and *ad hoc* nucleation procedures. In order to understand earthquake source processes and how fault slip history influences subsequent events, it has been widely recognized that we need models that simulate behavior over multiple seismic events and the intervening periods of aseismic deformation. To address this need, models of Sequences of Earthquakes and Aseismic Slip (SEAS) have emerged that consider all phases of earthquake faulting, from slow tectonic loading to earthquake nucleation (under self-consistent prestress conditions), propagation and termination. However, so far codes for SEAS simulations remain untested. Inspired by the success of the SCEC/USGS Spontaneous Rupture Code Verification Project, this paper describes the efforts of the SEAS initiative – a SCEC (Southern California Earthquake Center) funded working group who has initiated the first code-verification study for earthquake sequence simulations. In this paper, we present the initial benchmark problems and results from the code comparisons submitted to our online platform (`http://scecdata.usc.edu/cvws/seas/`). Through these exercises, we aim to provide confidence in SEAS model outcomes, determine best practices for improvement of accuracy and efficiency of SEAS simulations, and provide other scientists strategies for verification during code development.

In SEAS models the goal is to capture the interplay of interseismic periods and the associated aseismic fault slip that ultimately lead to earthquake nucleation and earthquakes (dynamic rupture events) themselves, in an effort to understand which physical factors control the full range of observables such as aseismic deformation, nucleation locations of earthquakes, ground shaking during dynamic rupture, recurrence times and magnitudes of major earthquakes, see Figure 1. These features distinguish SEAS models from both dynamic rupture models which only consider single events, and the so-called earthquake simulators (*Tullis et al.*, 2012). Earthquake simulators are capable of simulating seismicity patterns over millennium time scales in complex fault network systems (*Richards-Dinger and Dieterich*, 2012) but are missing key physical features that could potentially dominate earthquake and fault interaction, such as stress transfer generated by dynamic waves, aseismic slip within fault segments, and inelastic responses.

SEAS modeling is not without significant challenges, due to the varying temporal and spatial scales that characterize earthquake source behavior. For computational efficiency the vast majority of SEAS models do not consider full dynamics during earthquake rupture, but rather take a "quasi-dynamic" approach, where inertia is only approximated (see section for further details). Computations are further complicated when material heterogeneities, bulk inelastic responses and fault nonplanarity are included. However, accounting for such complexity is widely recognized as crucial for understanding the real Earth and predicting seismic hazards. Significant developments in SEAS models over the past decade have incorporated some of these complexities and connected model outcomes to geophysical observations. For example, seismological and geodetic observations have been combined with modeling of coseismic and quasi-static (aseismic) deformation to infer the spatial distribution of fault frictional properties (*Johnson et al.*, 2006; *Barbot et al.*, 2009; *Mitsui and Hirahara*, 2011; *Dublanchet et al.*, 2013; *Floyd et al.*, 2016; *Jiang and Fialko*, 2016), the decay rate of aftershocks (*Perfettini and Avouac*, 2004, 2007), the role of tremor and slow slip (*Mele Veedu and Barbot*, 2016; *Dublanchet*, 2017; *Luo and Ampuero*, 2017), and long-term models have been used to reproduce characteristics of multiple and/or repeating events (*Chen and Lapusta*, 2009; *Barbot et al.*, 2012). The framework of earthquake cycle modeling is also adopted to explain geodetic and geologic data (*Meade et al.*, 2013; *Kaneko et al.*, 2011; *Wei et al.*, 2013, 2018), study subduction zones (*Hori et al.*, 2004; *van Dinther et al.*, 2013; *Noda and Lapusta*, 2013; *Liu and Rice*, 2005, 2007; *Li and Liu*, 2016, 2017), collision zones (*Qiu et al.*, 2016; *Michel et al.*, 2017), and explore induced seismicity phenomena (*McClure and Horne*, 2011; *Dieterich et al.*, 2015), among many applications.

While SEAS models are being used to explain, reproduce, and predict earthquake behavior and other geophysical phenomena, a critical step must be to ensure that these methodologies are accurate. The SEAS initiative is also taking the step to improve and promote a new generation of verified numerical SEAS models that can simulate much longer periods of earthquake activity than single-event dynamic rupture simulations but with the same level of computational rigor, while incorporating qualitatively different features such as (a) pre-, inter-, and post-seismic slip and the resulting stress redistribution, (b) spontaneous earthquake nucleation, and (c) physical processes relevant to long-term slip such as interseismic healing of the fault zone, viscoelasticity, and fluid flow. Such SEAS models can provide physics-based approximations for larger-scale and longer-term earthquake simulators. In addition they can inform the initial conditions and nucleation procedures for dynamic rupture simulations, however our vision for SEAS models is to develop them all to include full dynamic ruptures, capturing the range of processes and heterogeneities known to be essential for realistic ground motion modeling.

SEAS Modeling Challenges and Initial Benchmark Problems

Although the ultimate SEAS modeling framework would naturally include dynamic rupture modeling, current methods for simulating SEAS problems require computational codes that are fundamentally different from those used in single-event dynamic rupture simulations. The use of variable time stepping and possible switching between different computational schemes is required in order to resolve sub-seconds to year-long changes. The interaction between the highly nonlinear nature of the problems and round-off errors can lead to model divergence. The need to distinguish between legitimate solution differences due and improper choices of algorithm and modeling procedures necessitates new and more suitable comparison metrics.

SEAS models are unique in that they cover a wide range of numerical methodologies and applications in earthquake science. Methods based on spectral boundary integral formulations (BIEM) are efficient in solving for earthquake ruptures with quasi-dynamic or full inertial effects (*Lapusta and Rice*, 2003; *Lapusta and Liu*, 2009; *Jiang and Lapusta*, 2016). Methods based on the finite difference method (FDM) or a hybrid finite element/spectral BIEM have been used to simulate quasi-dynamic ruptures on faults with more complex bulk rheologies (*Erickson and Dunham*, 2014; *Erickson et al.*, 2017; *Allison and Dunham*, 2018; *Mckay et al.*, 2019; *Abdelmeguid et al.*, 2019). Other SEAS modeling approaches include boundary element methods (BEM) for simulating slow slip and tremor (e.g., *Tse and Rice*, 1986; *Rice and Tse*, 1986; *Ong et al.*, 2019; *Goswami and Barbot*, 2018; *Luo and Ampuero*, 2011; *Nakata et al.*, 2012; *Liu*, 2013; *Wei et al.*, 2013), coupling faulting with fluid/heat transport and inelastic dilatancy (*Segall and Bradley*, 2012a), effects of surface topography (*Ohtani and Hirahara*, 2015), frictional heterogeneities (*Kato*, 2016) and viscoelastic response (*Kato*, 2002; *Lambert and Barbot*, 2016; *Barbot*, 2018). A spectral element method (SEM) has also been developed for simulating fully dynamic earthquakes in a heterogeneous bulk (*Kaneko et al.*, 2010).

To verify the accuracy of SEAS models based on these different computational methods, the SEAS group developed our first benchmark problem, BP1, to test the capabilities of different computational methods in correctly solving a mathematically well-defined problem in crustal faulting. The overall strategy of our benchmark exercises is to produce robust results and maximize participation, with the goal of obtaining agreements in resolving detailed fault slip history over a range of time scales. These efforts required us to better understand the dependence of fault slip history on initial conditions, model spin-up, fault properties, and friction laws. Given the complexity of this task, it was important to start from the most basic problem and gradually add model complexity. BP1 is a 2D antiplane problem, with a 1D planar vertical strike-slip fault embedded in a 2D homogeneous, linear elastic half-space with a free surface, see Figure 2. Full details of this benchmark (and subsequent benchmarks), including governing equations and initial and fault interface conditions, are available online on the SEAS platform (`http://scecdata.usc.edu/cvws/seas/index.html`). We include some of the details on the friction law here, for clarity of important concepts.

The fault is governed by rate- and state-dependent friction (*Dieterich*, 1979; *Ruina*, 1983; *Marone*, 1998) where shear stress on the fault τ is set equal to fault strength F, namely

$$\tau = F(V, \theta), \tag{1}$$

where $\tau = \tau^0 + \tau^{\mathrm{qs}} - \eta V$ is the sum of the prestress τ^0, the shear stress due to quasi-static deformation τ^{qs}, and the radiation damping term $-\eta V$ as approximation to inertia (*Rice*, 1993). $\eta = \mu/2c_{\mathrm{s}}$ is half the shear-wave impedance for shear wave speed $c_{\mathrm{s}} = \sqrt{\mu/\rho}$, where μ is the elastic shear modulus and ρ is the material density. The fault strength $F = \sigma_\mathrm{n} f(V,\theta)$, where V is the slip rate and θ is a state variable. σ_n is the effective normal stress on the fault. For this first benchmark problem we assume θ evolves according to the aging law

$$\frac{d\theta}{dt} = 1 - \frac{V\theta}{L}, \tag{2}$$

where L is the critical slip distance. The friction coefficient f is given by a regularized formulation (*Lapusta et al.*, 2000)

$$f(V,\theta) = a \sinh^{-1}\left[\frac{V}{2V_0}\exp\left(\frac{f_0 + b\ln(V_0\theta/L)}{a}\right)\right] \tag{3}$$

for reference friction coefficient f_0 and reference slip rate V_0. Depth-dependent frictional parameters a and b define a shallow seismogenic region with velocity-weakening (VW) friction and a deeper velocity-strengthening (VS) region, below which a relative plate motion rate is imposed. A periodic sequence of spontaneous, quasi-dynamic earthquakes and slow slip are simulated in the model, see Figure 3a, where results from the BICyclE code (*Lapusta et al.*, 2000; *Lapusta and Liu*, 2009) show slip contours plotted against fault depth in blue every 5 yr during interseismic loading and in red every 1 s during the coseismic phase. Over a 1200 year simulation period, approximately 13 events take place, nucleating at a depth of ~12 km, rupturing to a depth of ~18 km, and accumulating ~3 m of slip at the Earth's surface. Model parameters used for the benchmark are given in Table 1.

A critical physical length scale present in this first benchmark problem, often referred to as the process zone or cohesive zone Λ, describes the spatial region near the rupture front under which breakdown of fault resistance occurs, and shrinks as ruptures propagate faster (*Palmer and Rice*, 1973). For fault models governed by rate-and-state friction, the quasi-static process zone at a rupture speed of 0^+, Λ_0, can be estimated (*Day et al.*, 2005; *Ampuero and Rubin*, 2008; *Perfettini and Ampuero*, 2008) as

$$\Lambda_0 = C\frac{\mu L}{b\sigma_\mathrm{n}}, \tag{4}$$

where C is a constant of order 1. Another characteristic length scale which has been shown to control model behavior is the critical nucleation size h^*, which governs the minimum extent of the rate-weakening region under which spontaneous nucleation may occur, (see *Andrews*, 1976a,b; *Rubin and Ampuero*, 2005; *Ampuero and Rubin*, 2008). For 2D problems, the critical nucleation size can be estimated for the aging law (with $0.5 < a/b < 1$) as

$$h^* = \frac{2}{\pi} \frac{\mu b L}{(b-a)^2 \sigma_{\mathrm{n}}}. \tag{5}$$

A cell size of 50 m was used for BP1, resolving Λ_0 with approximately 6 grid points and h^* with approximately 40 grid points.

We developed the second benchmark BP2 that is similar to BP1 to explore the model resolution issues, which will be important in future benchmarks in 3D when computational efficiency demands a larger cell size. Complexity of event sizes and recurrence times is known to emerge through a reduction in the characteristic slip distance L (*Lapusta and Rice*, 2003; *Mitsui and Hirahara*, 2011; *Wu and Chen*, 2014; *Kato*, 2014; *Barbot*, 2019; *Viesca*, 2016a,b; *Cattania*, 2019). Thus BP2 is exactly the same as BP1 except that L is halved, resulting in bimodal sequences of full and partial ruptures of the velocity-weakening region (every large event is accompanied by a smaller event and the sequence repeats periodically). Besides aiming for agreements between different models, one main objective is to understand complexity in simulated events and how to deal with numerical resolution issues. A reduction in L corresponds to a reduction in the quasi-static process zone size Λ_0. BP2 requests model outputs using a cell size of 25 m, 50 m, 100 m, 200 m, 300 m, 400 m and 800 m. The first three cases resolve Λ_0 with approximately 6, 3, and 1.7 grid points, and the other four cases do not resolve Λ_0. Figures 3b-d show results from the BICycle code using a cell size of 25 m, 100 m and 200 m respectively. Small cell sizes of 25 m and 50 m (the latter is not shown) show nearly indistinguishable, bimodal patterns of events nucleating at $\sim$15 km depth, suggesting model convergence. A cell size of 100 m leads to a resolution issue where periodic behavior is observed, but the bimodal sequence of events is replaced by an alternating sequence of large, small and medium sized events. A cell size of 200 m, which does not resolve the process zone, reveals a loss of periodic behavior altogether in favor of a broad range of event sizes and nucleation locations.

Modeling Groups and Working Platforms

For these benchmark exercises, we have used two SCEC-funded workshops (hosted in April and November 2018, `http://scecdata.usc.edu/cvws/seas/workshop_presentations.html`) as open platforms for modelers to share and follow recent scientific progress in the field, discuss details in benchmark design/results, and collectively decide the directions of our future efforts, with considerable inputs from students and early career scientists. Over 10 modeling groups participated in these first two benchmarks; the details of the group members and different computational methods are summarized in Table . Note that the modeler name refers to the member of the modeling group who uploaded the data to the platform for simulations done by the group. It does not necessarily refer to the code author(s) - see the references in Table for authorship and code availability. For time-stepping schemes, the majority of groups used adaptive Runge-Kutta methods for both benchmark problems (the details of which can be found in the references listed in Table), with the exception of QDYN, which applies a Bulirsch-Stoer method for BP1, and BICyclE, which incorporates adaptive time-stepping based on stability conditions derived from the choice of constitutive relationship.

To facilitate the submission and comparison of simulation results, we established an online platform that provides access to community resources and supports the submission, storage, visualization, and comparison of benchmark results, see Figure 4. For our first benchmarks, we adopted a platform with similar functionality developed for the SCEC dynamic rupture simulation group (`http://scecdata.usc.edu/cvws/seas/`). All modelers can upload and immediately plot time-series data to quickly assess the overall agreements between models for the time evolution of fault slip, slip rates and shear stress at representative locations on fault. We use the online platform for preliminary model comparisons and analyze more detailed model observables to verify these computational codes.

Model Comparisons and What We Learned

It is important to note that the problem descriptions for BP1 and BP2 consider a semi-infinite half-space. Codes based on a volume discretization (FDM/FEM) therefore had to make their own decisions regarding computational domain truncation and far-field boundary conditions. The figures in the following sections contain labels generated by the platform which state the model group name and correspond to results from a particular model set-up. Some results are followed by the version corresponding to an alternative set-up, e.g. **abrahams.3** corresponds to results from the **abrahams** group with an increased computational domain size of $(L_x, L_z) = (400\,\text{km}, 200\,\text{km})$ and a remote displacement boundary condition, see the lower right of Figure 4. We discuss in the next sections the implications that these choices had on model comparisons.

Results from BP1

For the first benchmark problem, BP1, we found qualitative agreements in nucleation sites, depth extent of rupture, and slip with depth similar to those exemplified by the slip contours in Figure 3a. In Figure 5 we plot time series of local shear stress and slip rates at mid-seismogenic depth ($z = 7.5\,\text{km}$) from BP1 over the first 700 years for different model results. Results from several BEM codes as well as codes with volume discretization (**abrahams** and **kozdon** modeling groups) and varying computational domain sizes are compared in Figure 5a-b. The legends indicate the computational domain size and boundary condition. For BEM codes, HS refers to a half-space, and (L_z, boundary condition) refers to computational domain depth and boundary condition, where BC3 corresponds to a periodic boundary condition. For codes with a volume discretization, (L_x/L_z/boundary condition), provides the computational domain size used and BC1 and BC2 refers to a far-field free surface or a far-field displacement boundary condition, respectively.

Figure 5(a-b) show model results from a BEM simulation (**liu**, in black) along with four model results from volume discretization codes, revealing quantitative differences in interevent times and peak values. Interevent times for different models range from approximately 78.3 to 78.8 years over the whole 3000 year simulation period, leading to model divergence at a near-constant rate. We found that these discrepancies were caused by choices in domain truncation and boundary conditions. We were surprised to find that far-field boundary condition type leads to quantitative differences in long-term fault behavior for relatively small domains (revealed by the blue and orange curves). This in part is due to small differences in the physical problem being solved by implementations that use periodic or finite domain boundary conditions compared to the spatial domain BEM methods which represent a truly infinite domain, and therefore larger loading regions. The green and red curves show how the discrepancy in long-term behavior among computational methodologies decreases as the physical domain size is increased, suggesting convergence of results across the modeling groups. Figure 5(c-d) shows comparisons of all models with $L_z > 160\,\text{km}$, further illustrating that excellent agreements between model results can be achieved with sufficiently large domain sizes.

While computational domain size and boundary conditions can lead to model divergence over the long term, the coseismic behavior of individual earthquake are qualitatively well reproduced by all models. In Figure 6 we show the time series of shear stress evolution near the nucleation depth (12.5 km) and slip rate (at a mid-seismogenic depth of 7.5 km) during the coseismic phase for the 8th event in the sequence from Figure 5. We chose these plotting depths as they best illustrate model discrepancies, with time series aligned relative to the rupture initiation time at the depth of 12.5 km. Peak values in slip rates at 7.5 km depth occur approximately 10 s later, and co-seismic surface reflection phases are marked for all four plots with black arrows. Figures 6(a-b) show results from models on relatively small computational domains, revealing discrepancies in pre-rupture stress levels near the locked-creeping transition due to differences in interseismic loading, and resultant coseismic rupture behavior, including peak shear stress and rupture speeds as evidenced by rupture initiation times of the direct and surface-reflection phases at depth of 7.5 km. Figures 6(c-d) illustrate excellent agreements for model results on larger domains. The discrepancy of <1 MPa in prestress levels at transitional depths does not result in pronounced difference in fault slip rate evolution.

Results from BP2

For BP2 we suggested submissions of multiple models with different spatial resolutions from each group, see Table . By design, models with a cell size/node spacing that does not resolve critical length scales – process zone size and nucleation zone size defined in (4) and (5) – would produce increased complexity in earthquake sequences, observed previously (*Rice*, 1993; *Ben-Zion and Rice*, 1997; *Day et al.*, 2005; *Lapusta and Liu*, 2009), and illustrated in the cumulative slip profiles in Figure 3(b-d).

While drastic differences in small event patterns arise for large cell sizes, we found that with increasing resolution results converge to an alternating sequence of large and small events among most models. Figure 7a shows the long term evolution of slip rates at 9.6 km (near the bottom of the seismogenic zone and above the earthquake initiation depth) for the best model results (with a cell size of 25 m and large computational domain sizes). We found that even models with similar cell/domain sizes tend to produce results that are initially closely matching, but diverge over time, likely due to accumulation of numerical round-off errors and differences in computational techniques. However, if we zoom in on the tenth event in the sequence (gray bar in Figure 7a), the time series of fault slip rates, aligned with respect to the start time of seismic slip at the depth of 12 km within each model, show good agreements (Figure 7b). While small discrepancies exist in peak slip rates and early source complexity, partly due to differences in interevent times, the models with the highest resolution exhibit good agreements in their overall coseismic behavior despite their divergence in the long term.

Figure 8 illustrates how model agreement is gradually lost with decreased model resolution. For cell sizes of 25 m and 50 m, long-term stress evolution near the locked-creeping transition is qualitatively similar for the three models shown and the offset in the timing of earthquakes does not significantly affect coseismic behavior of major events, as indicated by comparable coseismic stress drops. For large cell sizes of 100 m and 200 m, not only is the time offset more random, but also coseismic stress drops and event patterns vary between models. Numerical artifacts and different computational techniques likely contribute to the divergence of simulation results.

In Figure 9 we plot the distribution of earthquake sizes, seismic moment release and frequency-size relation for two groups of models (**jiang** and **cattania**) with increasing cell sizes. For the 2D problem, we define earthquake size as moment release per length for each event, $M = \int \mu\, s\, \mathrm{d}z$, where shear modulus $\mu = c_s^2 \rho \approx 32\,\mathrm{GPa}$ and s is total coseismic slip over the cell. While better resolved models (cell sizes of 25 m and 50 m) show excellent agreements between the two groups, models produce dramatically different earthquake statistics when cell size increases to 400 m, with the most significant discrepancies in smaller earthquakes between the two models (Figure 9a). The distribution of total seismic moment release, M_t, calculated as the sum of moment release during all earthquakes within a certain magnitude range, also changes with cell sizes, though in a similar manner for the two model groups (Figure 9b). Overall, models with larger cell sizes tend to produce large earthquakes with reduced total moment; part of the moment deficit is accommodated through many more smaller earthquakes and the rest through additional aseismic slip. For example, the total moment release through largest earthquakes in 400-m models is only half of that in 25-m models. These results demonstrate that simulated small earthquakes are especially sensitive to model resolution and large earthquake behavior can also be affected. In addition, Figure 9c reveals how different simulations with poor resolution can produce similar power-law features in frequency-size distributions over certain ranges of earthquake sizes, as a result of numerical artifacts rather than well-resolved physics.

In Figure 10 we illustrate the effect of model resolution on the partition between seismic and aseismic slip. Normalized seismic moment release R_s is plotted against depth for several modeling groups, in solid lines for total seismic moment release and dashed lines for seismic moment due to surface-breaching events. $R_s = 0$ implies that all plate motion is accommodated by aseismic slip on the fault, while $R_s = 1$ means that all moment is released through earthquakes. A transitional zone in this partitioning around $z = H$ and down to $z = H + h$ ($H = 15$ and $h = 3$ in this exercise) is evidenced in the well-resolved models ($\Delta_z = 25$, 50, 100 m). The poorly resolved models, however, illustrate model discrepancies in the seismic/aseismic partitioning, with the near-surface slip budget being increasingly accommodated by small earthquakes and aseismic slip with increased cell sizes.

In Figure 11 we show interevent times for large surface-breaching events for all models and cell sizes, showing a strong agreement of ∼110 years for a cell size of 25 m, with an increasing variability and discrepancies among models with increased cell size. Although the range of earthquake recurrence intervals are highly dependent on cell sizes, the median values across models with larger cell sizes do not significantly deviate from the uniform recurrence intervals in well-resolved models. This suggests that at least some observables in these models retain information of the true behavior of physical models and the larger cell sizes can be viewed as a factor that leads to increased modeling errors.

Conclusions and Perspectives

For the first two SEAS benchmarks we found that discrepancies among well-resolved models were significantly influenced by computational domain size, with larger domains yielding improvements in agreements, regardless of domain boundary conditions. Spin-up periods (time required for system to be independent of initial conditions) for well-resolved models was relatively short - approximately 2-3 events. Results on large domains agree well initially but still diverge over time, which was not unexpected due to accumulation of round-off errors and differences in computational techniques. For BP2 we investigated model resolution and observed qualitative similarities of bimodal events when the process zone was resolved by approximately 3 and 6 grid points, suggesting model convergence. A failure to resolve this length scale however, can lead to substantial differences in long-term fault behavior as well as earthquake statistics relevant to seismic hazard, such as frequency-size distributions and interevent times.

Although our initial benchmarks have a simple setup, comparison of results for tens of models have yielded some unexpected and important insights, affirming the importance of starting simple in a community code verification exercise. The results and lessons from our initial benchmarks prepare us for future benchmark problems that incrementally incorporate additional, potentially dominating physical factors, including fully dynamic ruptures, coupling with fluids, multiple fault segments, nonplanar fault geometries, and inelastic bulk constitutive behavior (e.g., *Segall and Rice*, 1995; *Noda and Lapusta*, 2010; *Segall and Rice*, 2006; *Segall et al.*, 2010; *Erickson et al.*, 2017; *Lambert and Barbot*, 2016; *Qiu et al.*, 2016; *Barbot*, 2018; *Ong et al.*, 2019). For future verification exercises, we plan to address important issues in SEAS simulations, such as 3D effects, heterogeneous fault frictional properties, and full dynamics, which should advance the state-of-the-art computational capabilities in our field.

The goal of the SEAS initiative is to promote advanced models with robust physical features—a large spectrum of rupture styles and patterns, including slow-slip events, complex earthquake sequences, fluid effects, dynamic stress changes, and inelastic deformation—that are currently missing in the large-scale, long-term earthquake simulator frameworks such as ViscoSim, RSQSIM, Virtual California, and ALLCAL (*Pollitz*, 2012; *Richards-Dinger and Dieterich*, 2012; *Sachs et al.*, 2012; *Ward*, 2012). This new generation of verified SEAS models will help determine the controlling physical mechanisms of earthquake nucleation, propagation, and arrest. The community-wide initiative would also provide incentives and new ideas to characterize modeling uncertainty for the increasingly complex earthquake source models, an important step in using physics-based models for the assessment of seismic hazard. Future validation efforts comparing physics-based models with geophysical observations will bridge studies in paleoseismology, geodesy, and seismology to understand fault behavior over multiple temporal and spatial scales.

Data and Resources: Our online platform (`http://scecdata.usc.edu/cvws/seas/`) is being developed and maintained by M.B. The data for local fault properties are stored on the platform.

Author Contributions: B.A.E. and J.J. designed the benchmark problems, analyzed model results, co-organized the workshops and co-wrote this article. M.B. developed and maintains the online platform. M.B., N.L., E.M.D. and R.H. provided major support and advice in forming the working group, obtaining funding, and manuscript writing. Remaining co-authors provided feedback on benchmark design, participated in the benchmark exercises, helped revise the manuscript, and are listed alphabetically.

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Table 1: Parameter values used in the benchmark problem

Parameter	Definition	Value, Units
ρ	density	$2670\,\mathrm{kg/m^3}$
c_s	shear wave speed	$3.464\,\mathrm{km/s}$
σ_n	effective normal stress on fault	$50\,\mathrm{MPa}$
a	rate-and-state parameter	variable (see Fig. 1)
b	rate-and-state parameter	variable (see Fig. 1)
L	critical slip distance	BP1: $0.008\,\mathrm{m}$
		BP2: $0.004\,\mathrm{m}$
V_p	plate rate	$10^{-9}\,\mathrm{m/s}$
V_init	initial slip rate	$10^{-9}\,\mathrm{m/s}$
V_0	reference slip rate	$10^{-6}\,\mathrm{m/s}$
f_0	reference friction coefficient	0.6
H	depth extent of uniform VW region	$15\,\mathrm{km}$
h	width of VW-VS transition zone	$3\,\mathrm{km}$
W_f	width of rate-and-state fault	$40\,\mathrm{km}$
Δz	suggested cell sizes	BP1: $25\,\mathrm{m}$
		BP2: $25\,\mathrm{m}$, $50\,\mathrm{m}$, $100\,\mathrm{m}$, $200\,\mathrm{m}$,
		$300\,\mathrm{m}$, $400\,\mathrm{m}$, $800\,\mathrm{m}$
t_f	final simulation time	BP1: 3000 years
		BP2: 1200 years
L_z	depth of computational domain	*not specified*
L_x	off-fault distance of computational domain	*not specified*

Table 2: Details of participating SEAS codes and modeling groups.

Code Name	**Type**	**Modeler Name** & Group Members	**References**
SCycle	FDM	**abrahams** (Abrahams/ Allison/Dunham)	*Erickson and Dunham* (2014) *Allison and Dunham* (2018) `https://github.com/kali-allison/SCycle`
FDCycle	FDM	**erickson** (Erickson/Mckay)	*Erickson and Dunham* (2014) `https://github.com/brittany-erickson/FDCycle`
QDESDG	DG-FEM	**kozdon** (Kozdon)	`https://github.com/jkozdon/QDESDG`
Unicycle	BEM	**barbot** (Barbot)	*Barbot* (2019) `http://bitbucket.org/sbarbot`
FDRA	BEM	**cattania** (Cattania/Segall)	*Segall and Bradley* (2012b); *Bradley* (2014)
BICyclE	BEM	**jiang** (Jiang) **lambert** (Lambert/Lapusta) **xma** (Ma/Elbanna)	*Lapusta et al.* (2000); *Lapusta and Liu* (2009)
QDYN	BEM	**luo** (Luo/Idini/ van den Ende/Ampuero)	*Luo and Ampuero* (2017) `https://github.com/ydluo/qdyn`
ESAM	BEM	**liu** (Liu) **wei** (Wei/Shi)	*Liu and Rice* (2007)

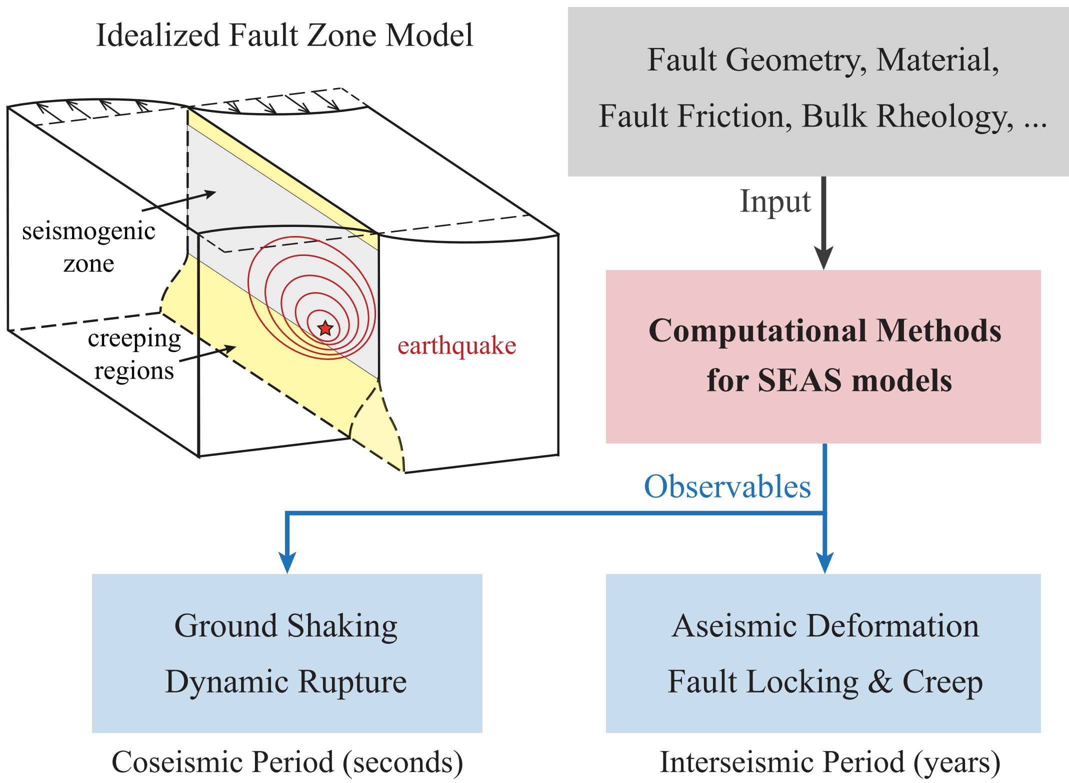

Figure 1: Ingredients and observables for SEAS (sequences of earthquakes and aseismic slip) models. In a conceptual fault-zone model, earthquakes initiate at seismogenic depths (red star) and rupture through the interseismically locked regions (gray), while aseismic slip occurs in deeper and sometimes shallower regions (yellow). For numerical models, given fault zone properties, computational simulations can reproduce long-term fault locking and creep over years to decades, punctuated by dynamic earthquake ruptures over seconds to minutes. Seismic shaking and aseismic deformation are typical observables from the surface.

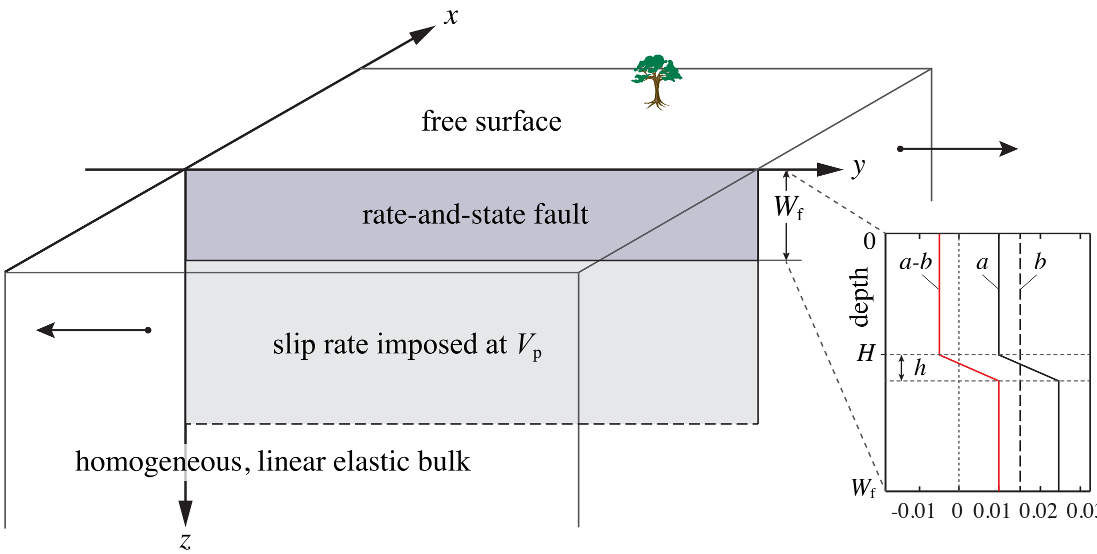

Figure 2: Our first SEAS benchmark is based on the model in *Rice* (1993), where a planar fault is embedded in a homogeneous, linear elastic half-space with a free surface. A vertical cross-section of the 3D setting is taken so that slip varies only with depth and deformation is 2D antiplane strain. The fault is governed by rate-and-state friction with depth-dependent frictional parameters a and b above the depth W_f, below which a steady slow loading rate V_p is assumed. The friction-controlled fault is seismogenic due to velocity-weakening properties ($(a-b) < 0$) down to depth H and accommodates aseismic creep at greater depths due to velocity-strengthening properties ($(a-b) > 0$). Earthquakes nucleate spontaneously, with inertia approximated with radiation damping.

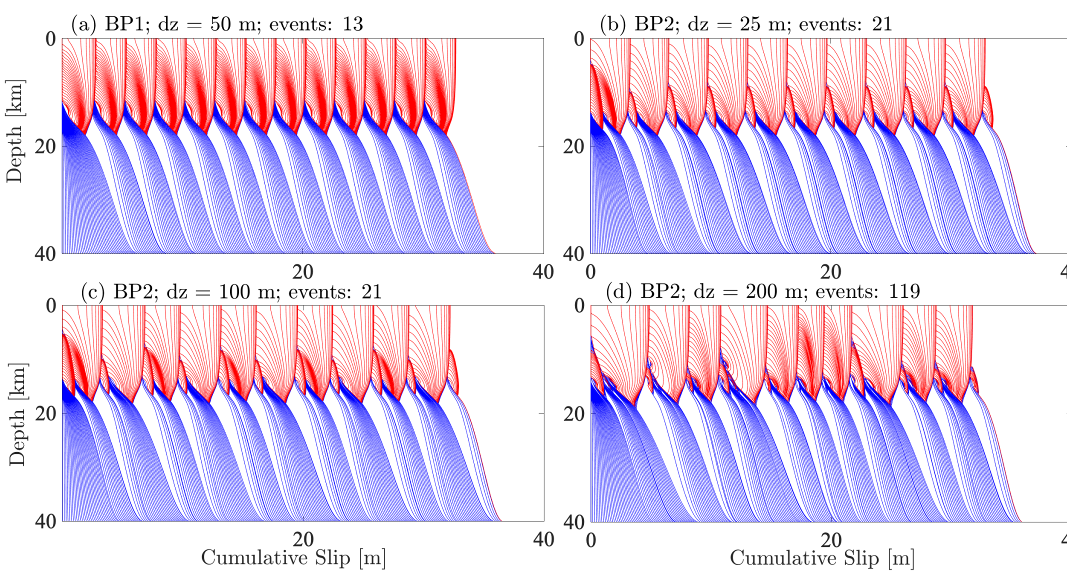

Figure 3: Cumulative slip profiles plotted over a 1,200 year period in blue every 5 years during interseismic loading and in red every second during quasi-dynamic rupture. Results were obtained using the BICyclE code for (a) BP1 with a cell size of 50 m, (b) BP2 with a cell size of 25 m, (c) BP2 with a cell size of 100 m and (d) BP2 with a cell size of 200 m. Number of events also listed, where we define a seismic event to be one with a local slip rate > 0.01 m/s separated by aseismic periods of at least 15 s.

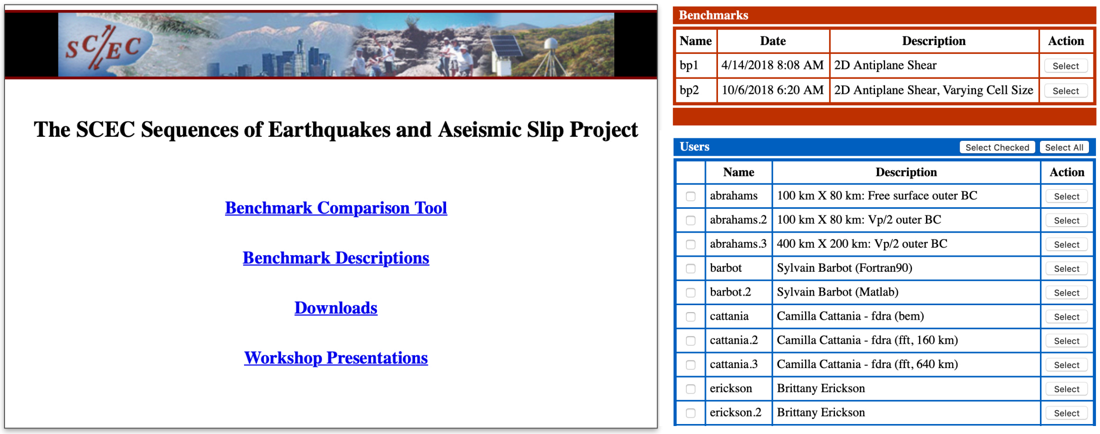

Figure 4: Online platform for the SEAS working group. (Left) Home page for our website. (Top right) Currently available benchmarks. (Bottom right) Examples of BP1 model submissions.

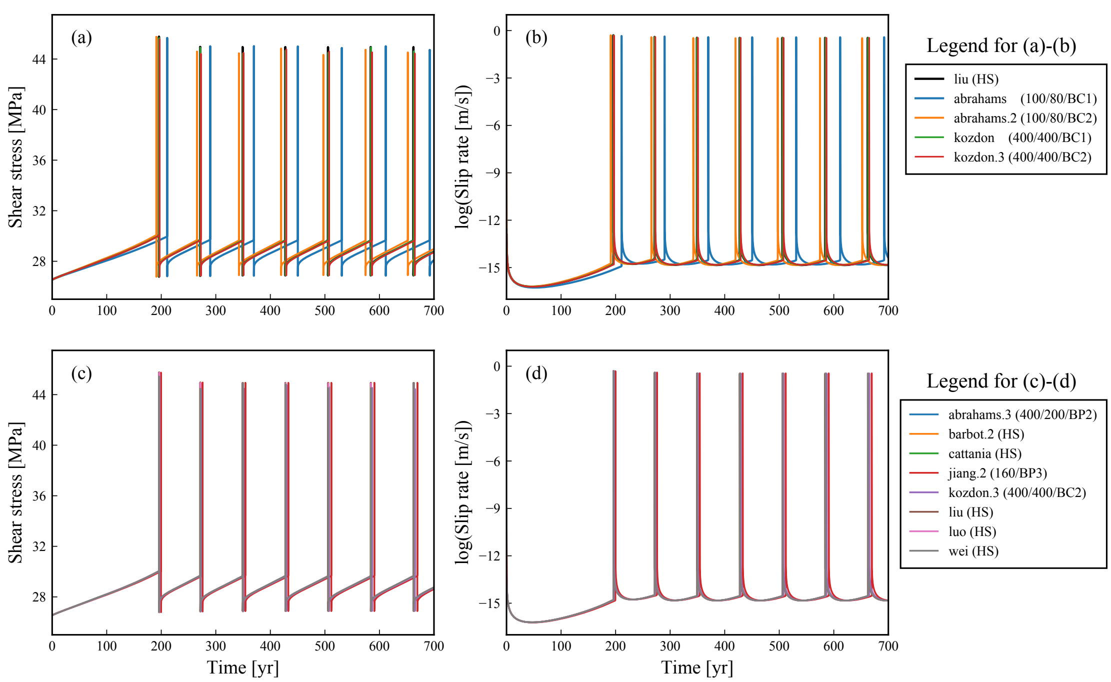

Figure 5: Long-term behavior of BP1 models. (a) Shear stress and (b) slip rates at the depth of 7.5 km in models with different outer boundary conditions (BC) and computational domain sizes. (c) Shear stress and (d) slip rates at depth of 7.5 km in models with sufficiently large computational domain sizes. Legend labels indicate model names followed by information on BC and domain size, namely, (L_x/L_z/BC) for FDM/FEM, and (L_z/BC) or (HS, half-space) for BEM. BC1 and BC2 refer to the far-field free surface or displacement BC and BC3 refers to the peridic BC.

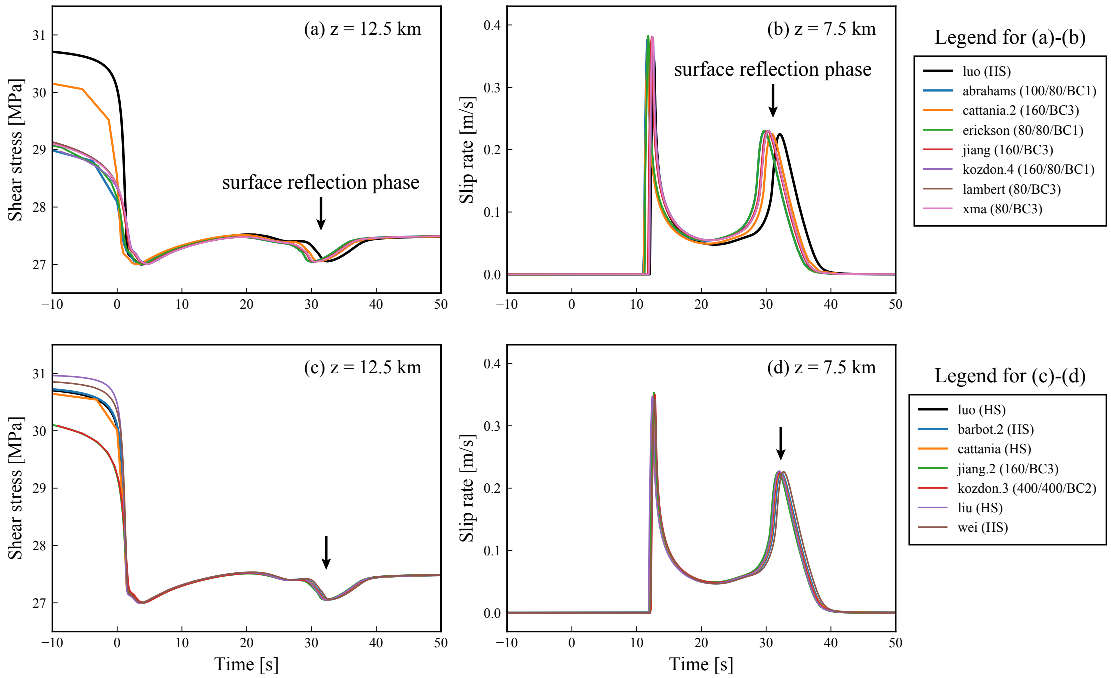

Figure 6: Coseismic behavior of BP1 models. Coseismic phase during the 8th event in Figure 5 is shown. Models with smaller computational domain sizes show discrepancies in (a) shear stresses at 12.5 km depth and (b) slip rates at 7.5 km depth. Models with sufficiently large computational domain sizes are compared for (c) shear stresses at 12.5 km depth and (d) slip rates at 7.5 km depth. Time series are aligned relative to the rupture initiation time at the depth of 12.5 km in each model. Note that the half-space solution **luo** is the same in (b) and (d) and serves as a reference. The surface reflection phase is marked by a black arrow.

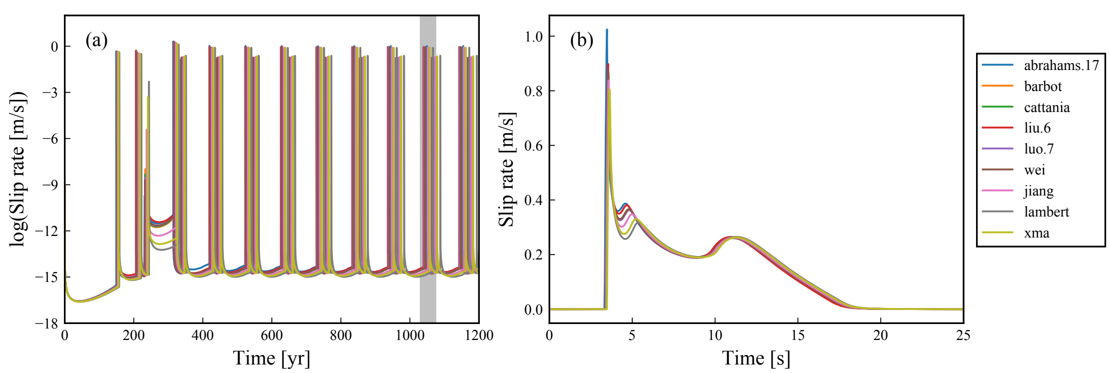

Figure 7: Comparison of best-resolved BP2 models (cell size of ~25 m). (a) Long-term evolution of slip rates at depth of 9.6 km; (b) coseismic evolution of slip rates at the depth of 9.6 km for the 10th large events in the sequence (marked in gray in (a)). Time series are aligned relative to the rupture initiation time at the depth of 12 km in each model.

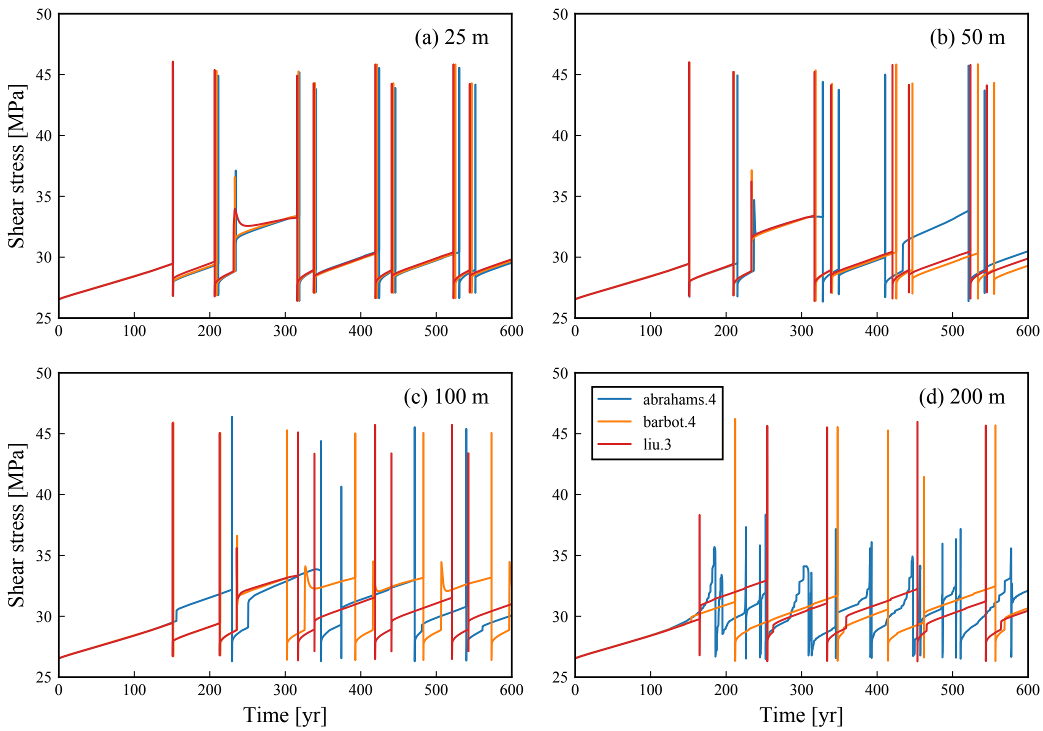

Figure 8: Increasing discrepancy in BP2 models due to an increased cell size of (a) 25 m, (b) 50 m, (c) 100 m, and (d) 200 m. Time evolution of shear stress at the depth of 9.6 km during the first 600 years is shown for models from three groups (**abrahams**, **barbot**, and **liu**).

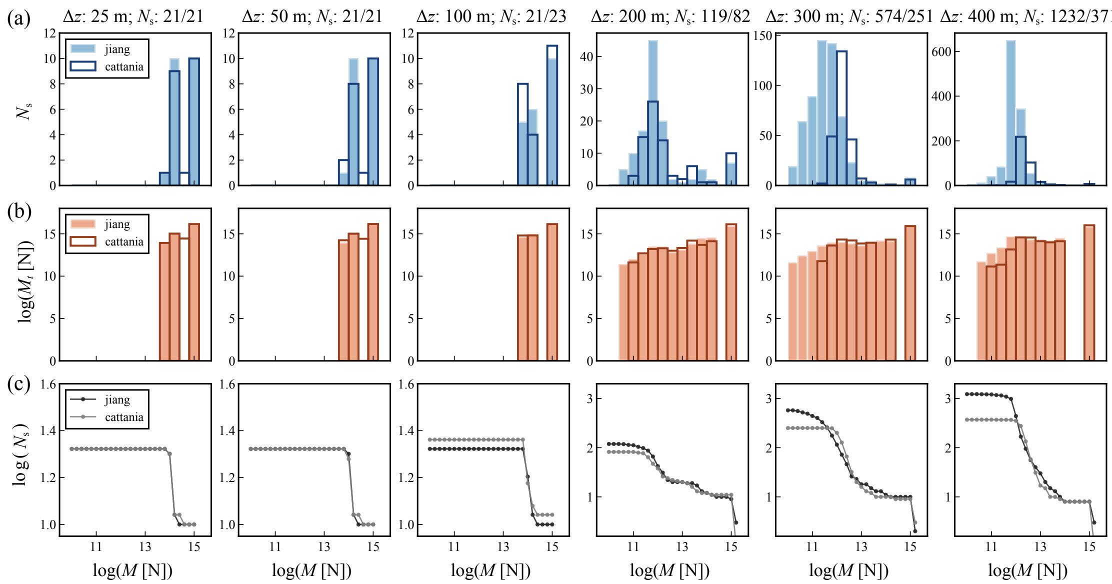

Figure 9: Effect of model resolution on earthquake patterns. Distribution of (a, top row) earthquake sizes and (b, middle row) of total seismic moment release per unit length, M (in unit of N) and (c, bottom row) frequency-size relation. Models from two groups (**jiang** and **cattania**) are compared. The corresponding cell size (Δz) and total seismic event numbers (N_{s}) are marked in the titles. Seismic moment M refers to the seismic moment of each earthquake; total seismic moment M_{t} refers to the sum of moment release for all earthquakes within each magnitude bin. N_{s} in (c) refers to the number of seismic events with moment above the corresponding M.

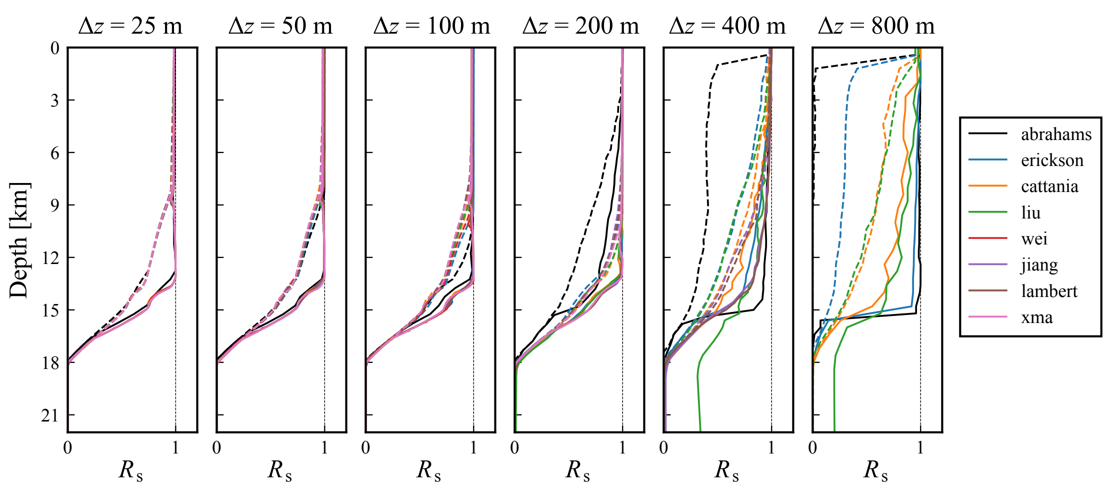

Figure 10: Effect of model resolution on seismic-aseismic slip partitioning over depth. Depth distribution of the ratio of total seismic moment release to total moment release, R_{s}, is shown by solid lines. The ratio between seismic moment due to surface-breaching earthquakes (with surface slip greater than 0.1 m) to total moment release is indicated by dashed lines. Simulations with different resolutions are shown, with the same color for each modeling group. Note that not all groups have simulation results for all resolutions.

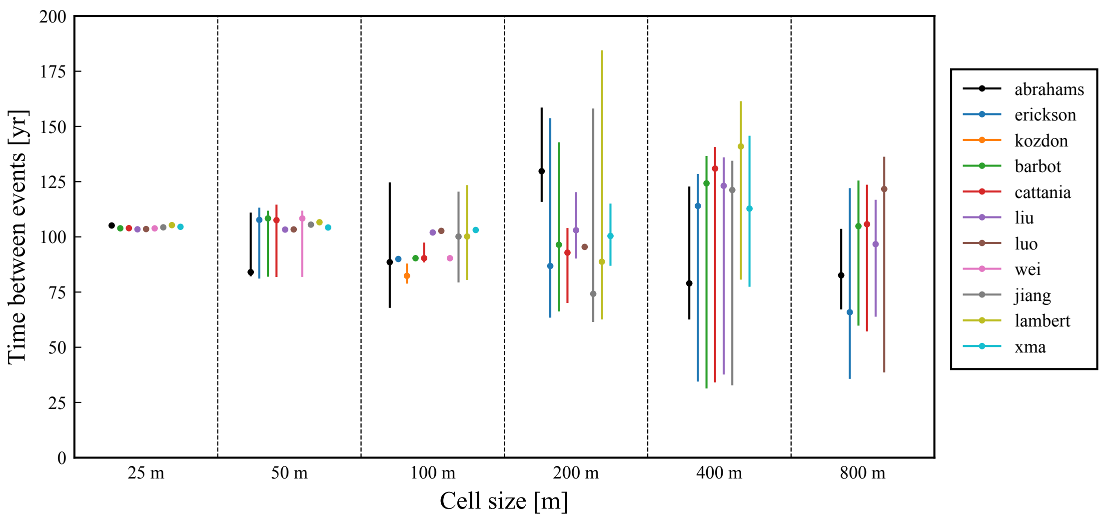

Figure 11: Effect of model resolution on recurrence intervals of large surface-breaching events. The vertical lines indicate the range of recurrence interval values, with the median value marked as dots.