

1 **Carbon dioxide migration along faults at the Illinois Basin – Decatur Project**  
2 **revealed using time shift analysis of seismic monitoring data**

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9 **Key Points:**

- 10 • 4D seismic time shift attributes reveal previously unidentified CO<sub>2</sub>  
11 migration behaviour where traditional amplitude attributes could not.  
12  
13 • The CO<sub>2</sub> migrates from the injection interval, upwards along a  
14 permeable fault and re-emerges in overlying permeable reservoir units.  
15  
16  
17 • This behavior has been previously theorized but not yet directly  
18 observed from a CO<sub>2</sub> storage site.  
19

20 **Abstract**

21 Large scale geological storage of CO<sub>2</sub> is being deployed worldwide to reduce  
22 greenhouse gas emissions to the atmosphere. Previous modelling studies have  
23 investigated the potential for CO<sub>2</sub> migration along faults. We observe such migration  
24 at a commercial-scale, demonstration CO<sub>2</sub> storage project, including subsequent  
25 emergence of the CO<sub>2</sub> into overlying permeable layers. Previous attempts at  
26 interpreting the time-lapse seismic data using amplitude attributes were hindered by  
27 noise from the limited survey repeatability combined with a weak signal due to the  
28 stiffness of the rock. Here we apply an alternative interpretation of the seismic data  
29 using time shift attributes, resulting in clear plume anomalies. In addition to migrating  
30 up the fault, we observe the plume diverted by the start of injection at a neighboring  
31 project. This work provides field observations of theorized plume behaviors and  
32 demonstrates an approach to overcome challenges in interpreting seismic monitoring  
33 data for geological CO<sub>2</sub> storage.

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## 36 **1 Introduction**

37 Carbon capture and geological storage is being scaled up worldwide to achieve net  
38 zero carbon emissions by 2050 (Krevor et al., 2023; Pörtner et al., 2022). Monitoring CO<sub>2</sub>  
39 storage through time-lapse seismic techniques has provided observations of the flow  
40 and trapping behavior of the injected CO<sub>2</sub> at storage projects around the world (Furre  
41 et al., 2017; Hansen et al., 2013; Ivandic et al., 2015; Roach & White, 2018). The  
42 observations have revealed fluid dynamics which are more complex and dynamic than  
43 analogous subsurface fluids systems due to the properties of CO<sub>2</sub> as a supercritical  
44 fluid at reservoir conditions (Cavanagh & Haszeldine, 2014; Ringrose et al., 2022).

45 Of particular interest is the potential for CO<sub>2</sub> to move buoyantly upwards from a  
46 target reservoir through leakage pathways such as a fault or wellbore. This has been  
47 investigated using geological analogues, and theoretical and numerical modelling  
48 (Gasda et al., 2004; Gilmore et al., 2022; Miocic et al., 2016; Nordbotten et al., 2009,  
49 Flemisch et al., 2024). Models show that complex dynamics emerge depending on the  
50 permeabilities of fault zones relative to reservoir units, and CO<sub>2</sub> migration up leakage  
51 pathways can in some instances be entirely mitigated by trapping as the plume emerges  
52 in overlying permeable strata.

53 Despite their importance, there are no engineered settings in which the movement  
54 of CO<sub>2</sub> along faults has been observed. CO<sub>2</sub> escape from natural subsurface  
55 accumulations has been inferred to occur through faults based on geochemical and  
56 isotope measurements of carbonate deposits and travertine veins (Shipton et al., 2004;  
57 Dockrill and Shipton; 2010; Kampman et al., 2012; Jung et al., 2014; Miocic et al.,  
58 2018). Natural hydrocarbon gas leakage has also been inferred from seismic  
59 observations of gas chimneys and associated pockmark clusters on the seafloor (e.g.  
60 Gay et al., 2007; Roelofse et al., 2020).

61 Time-lapse seismic surveys are the industry standard for monitoring the plume  
62 dynamics, however, their acquisition and processing must be performed in a way that  
63 maximizes repeatability, which can be affected by factors such as seasonal variations and  
64 differences in acquisition geometry (Landro, 1999; Lumley, 2001; Johnston, 2013;  
65 Meunier et al., 2001; Bakulin et al., 2007). In addition, in general, land seismic surveys  
66 can suffer from significantly more noise than marine seismic surveys due to scattering  
67 by the near surface layer (Pevzner et al., 2011; Stork, 2020). In this paper, we find  
68 evidence of CO<sub>2</sub> migration up faults during injection at the onshore Illinois Basin –  
69 Decatur Project CO<sub>2</sub> storage site using time shift analysis of time-lapse 3D (i.e. 4D)  
70 vertical seismic profile (VSP) surveys. The initial interpretation approach for the 4D  
71 data was based on amplitude difference (Coueslan et al., 2014) and normalized RMS  
72 attributes (Bauer et al., 2019), but observations of the CO<sub>2</sub> plume were ambiguous due  
73 to weak time-lapse signals (Coueslan et al., 2013). During the post-injection phase,  
74 well logs detected an isolated finger of CO<sub>2</sub> in the injection well in a shallower zone  
75 than the injection interval (Zaluski & Lee, 2021) but the lack of seismic monitoring  
76 during that period meant the origins of the CO<sub>2</sub> could not be ascertained. The  
77 application of an amplitude agnostic, time shift analysis, reported here, reveals clear,  
78 qualitative images of a growing CO<sub>2</sub> plume in this interval that has arrived by migration  
79 up a previously identified fault.

## 80 **2 Methods**

### 81 **2.1 The Illinois Basin - Decatur Project**

82 The Illinois Basin - Decatur Project (IBDP) was a commercial-scale  
83 demonstration CO<sub>2</sub> sequestration project in Decatur, Illinois, USA, which stored 1 Mt  
84 of CO<sub>2</sub> over three years from 2011 to 2014. The project injected the CO<sub>2</sub> into the  
85 Mt. Simon Sandstone at a depth of about 2100 m. The project has an injection well

86 (CCS1) and a monitoring well (VW1). Wells CCS2, VW2 are the injection and  
87 monitoring wells for a nearby secondary commercial project, the Illinois Industrial  
88 Carbon Capture and Storage (IL-ICCS) project. The monitoring and site  
89 characterization data from both projects have been made publicly available and  
90 provide a comprehensive dataset suitable for studying the complex behavior of CO<sub>2</sub>  
91 plumes in the field.

## 92 **2.2 Geologic setting**

93 The Mt. Simon sandstone is a Cambrian-age saline aquifer and is one of the major  
94 CO<sub>2</sub> sequestration resources in the United States. It is over 450 m thick at the Decatur  
95 site. Leetaru and Freiburg (2014) and Freiburg et al. (2014) provide a detailed  
96 depositional and diagenetic characterization of the Mt. Simon sandstone at Decatur. It  
97 is unconformably overlain by the Eau Claire Formation, which is a predominantly shale  
98 formation over 90 m thick at the Decatur site and serves as the primary caprock for  
99 the storage unit. The Mt. Simon Sandstone is subdivided into Upper, Middle and  
100 Lower units.

101 The most significant controls on reservoir quality in the Mt. Simon sandstone are  
102 diagenetic, with quartz cementation the most common feature. The Middle Mt. Simon  
103 is commonly referred to as the tight zone, comprising Mt. Simon C and D, with unit  
104 D having the most quartz cement in the entire Mt. Simon sandstone. The best reservoir  
105 quality occurs in the lower Mt. Simon formation, comprising units A and B, with  
106 porosities of up to 28% and permeabilities of up to 1000 mD in Unit A, and an average  
107 porosity and permeability of 22% and 200 mD. Within this unit, there is significant  
108 variation in reservoir quality as shown by the well logs. Unit A is the injection interval  
109 for the project. Several faults were interpreted by Williams-Stroud et al. (2020) to  
110 transect the middle and lower units of the Mt. Simon sandstone with some of them

111 extending down into the Precambrian basement. Williams-Stroud et al. (2020)  
112 interpret the fault lengths to range from approximately 250 m to 1000 m, and that some  
113 of them may comprise multiple intersecting fault planes or smaller faults.

### 114 **2.3 Monitoring data**

115 The monitoring dataset at the IBDP site comprises in-well and geophysical  
116 monitoring data including time-lapse 3D VSP surveys. Repeat saturation logs recorded  
117 CO<sub>2</sub> saturation profiles periodically in wells CCS1 and VW1. Time-lapse 3D VSP  
118 surveying was chosen as the main geophysical monitoring technique to observe the  
119 CO<sub>2</sub> plume development over time. The surveys were acquired using surface vibrator  
120 sources with 3-component geophones permanently installed in a shallow geophysical  
121 monitoring well GM1 located 60 m northwest of the injection well. A monitor survey  
122 was acquired each year from 2012 to 2015 (M1-M4), with a baseline survey acquired  
123 in 2011 (B2) being the reference pre-injection survey. At the time of M1, M2, M3 and  
124 M4 surveys, 74 kt, 433 kt, 730 kt and 1 Mt of CO<sub>2</sub> had been injected, respectively.  
125 Analysis of the time-lapse vertical seismic profile data is the main focus of this work.  
126 The survey dates, near-surface conditions during acquisition and injected CO<sub>2</sub> mass are  
127 reported by Coueslan et al. (2013) and provided in the Supplementary Information.

128 The main processing steps performed for the 4D VSP data prior to its public release  
129 include de-noise and amplitude scaling, wavefield separation, deconvolution and pre-  
130 stack depth migration. These processing steps were carried out for each monitor  
131 alongside the baseline (B2), ensuring the extraction of co-located sources (given  
132 differences in source locations for the different surveys) and matching geometries.  
133 Details of the time-lapse co-processing are provided in the time-lapse 3D VSP  
134 processing reports (Schlumberger, 2015). We use the migrated stacks as inputs to our  
135 analysis.

## 2.4 Time shift attribute extraction

136  
137 Previous investigations at the IBDP used amplitude attributes including NRMS  
138 and amplitude difference. Coueslan et al. (2013) presented NRMS over a zone  
139 containing the injection interval (1980 m – 2195 m) and a shallow zone (1524 m –  
140 1980 m) covering the Middle and Upper Mt. Simon and the Eau Claire Shale primary  
141 seal. While the strongest NRMS anomalies are in the deeper zone, there are still  
142 anomalies in the shallow zone. They also show an amplitude difference section where  
143 differences can be observed outside the injection interval window (Figure 6 in  
144 Coueslan et al. (2013)). This leaves questions particularly about the finer-scale fluid  
145 movement within the entire Mt. Simon sandstone. An amplitude-based interpretation  
146 is insufficient to answer these questions. We performed an analysis of time shifts in  
147 an attempt to overcome these difficulties in interpretation.

148 Time shift attributes of 4D seismic data have been used successfully to monitor  
149 fluid movement in oil and gas reservoirs (Benguigui et al., 2012; Falahat et al., 2011;  
150 Santos et al., 2016) and to support amplitude interpretation at CO<sub>2</sub> storage sites (Arts  
151 et al., 2004; Chadwick et al., 2004, 2005; Furre et al., 2015; Grude et al., 2013). Time  
152 shifts are induced as a result of changes in fluid content or stress leading to  
153 compaction or extension in the reservoir or the overburden. Landrø and Stammeijer  
154 (2004) define the relative change in elastic wave travel time due to changes in  
155 subsurface layer thicknesses (physical strain) and velocity as  $\frac{\Delta t}{t} = \frac{\Delta z}{z} - \frac{\Delta v}{v}$ , where  $\frac{\Delta t}{t}$  is  
156 the relative time shift or time strain,  $\frac{\Delta z}{z}$  is the vertical physical strain, and  $\frac{\Delta v}{v}$  is the  
157 relative velocity change, which is a function of the rock physics properties of the rock  
158 and the magnitude of the saturation change. MacBeth et al. (2020) provide a review  
159 of various time shift estimation algorithms, from the commonly used and simpler  
160 cross-correlation based methods to sophisticated waveform inversion approaches.

161 We implement a time shift algorithm based on the Dynamic Time Warping  
 162 (DTW) algorithm of Hale (2013), modified to avoid dependency on amplitudes. Our  
 163 implementation is based on matching features – peaks and troughs – between seismic  
 164 traces from the baseline and monitor surveys. DTW instead attempts to match  
 165 amplitudes between seismic traces, which in our case we expect to change between  
 166 baseline and monitor even where there is no CO<sub>2</sub> present, due to the fluid effect being  
 167 so subtle. The application of DTW under these circumstances therefore leads to noise.  
 168 We tested this approach through synthetic modelling; we produced 1D (pseudo-2D)  
 169 synthetic models based on well logs in well CCS1 (see the Supplementary  
 170 Information) and used the repeat saturation logs to produce monitor synthetics under  
 171 fully patchy and fully uniform mixing conditions.

172 The feature-based warping approach operates in a similar way to the standard  
 173 DTW algorithm which is based on the minimizing the dissimilarity error between two  
 174 traces:

$$175 \quad e[i, q] = (f[i] - g[i + l]), \quad (1)$$

176 where  $i$  is the sample index,  $l$  is the integer lag or time shift between seismic traces,  
 177 and  $f$  and  $g$  are the seismic amplitudes of the baseline and monitor traces, respectively.

178 However, in our feature-based implementation, the objective is to align features  
 179 (peaks and troughs) between two seismic traces by minimizing the geometric  
 180 dissimilarity between these features. The dissimilarity error is defined as:

$$181 \quad e_{feature}[i, q] = d(f_{feature}[i], g_{feature}[i + l]) \quad (2)$$

182 where  $f_{feature}[i]$  and  $g_{feature}[i + l]$  are the positions of key features in the baseline  
 183 and monitor traces, respectively, and  $d(f_{feature}[i], g_{feature}[i + l])$  is a measure of  
 184 the distance between the features in the two traces, in this case the L1 or Manhattan

185 distance. The cost matrix is filled in using the distances between the corresponding  
186 features in the baseline and monitor traces. The warping path is then optimized to  
187 minimize the cumulative feature distance along the path. Therefore, the warping is  
188 guided entirely by the spatial relationships between key features in the traces, without  
189 any consideration of the amplitudes of these features. Our synthetic modelling shows  
190 that we can detect CO<sub>2</sub> through feature-based warping for a 5 m thick layer at CO<sub>2</sub>  
191 saturation as low as 10% under uniform saturation, and for thicker layers under fully  
192 patchy saturation (see Supplementary Information). Our synthetic modelling also,  
193 however, reveals that the apparent thickness of CO<sub>2</sub> one would recover from seismic  
194 data is much thicker than the true thickness. This is expected given the low-frequency  
195 nature of seismic data.

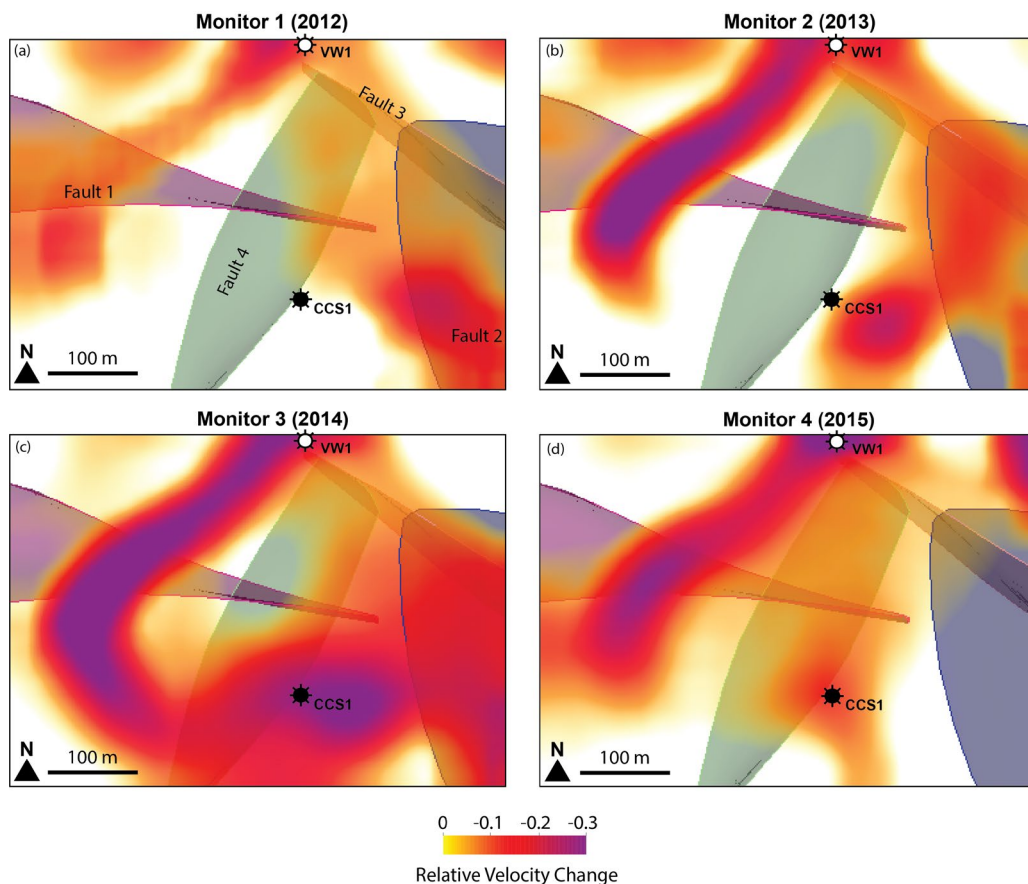
196 Time shifts were extracted from full stacks of each of the four 3D monitor surveys  
197 relative to the B2 baseline survey. We extract time shifts starting from 870 ms (or  
198 about 1500 m), because data folds are minimum in the shallow interval due to VSP  
199 geometry constraints. The time-lapse 3D VSP processing report notes that data  
200 shallower than 1500 m was not used to compute time-lapse attributes for the same  
201 reason (Schlumberger, 2015). We obtain time strain by taking the first derivative of  
202 the time shift volumes.



203 **3 Results and Discussion**

204 **3.1 CO<sub>2</sub> plume interpretation from relative velocity change**

205 We interpret CO<sub>2</sub> plumes qualitatively from the results of time strain, identifying  
206 multiple plume layers, with the feature having the greatest areal extent being in the  
207 deepest in the injection interval (the lower unit of the Mt. Simon A formation). Figure  
208 1 shows views of the plume features in the shallowest interval for all four monitors.  
209 These features are generally consistent across time from 2012 to 2015. We interpret  
210 the regions of relative velocity change  $< -0.02$  to be areas of CO<sub>2</sub> accumulation. Also  
211 shown are four out of several faults interpreted by Williams-Stroud et al. (2020). These  
212 faults were interpreted prior to injection, from 3D surface seismic data acquired during  
213 site characterization. Some of the interpreted plume anomalies exceed the lateral  
214 coverage of the 3D VSP cubes.



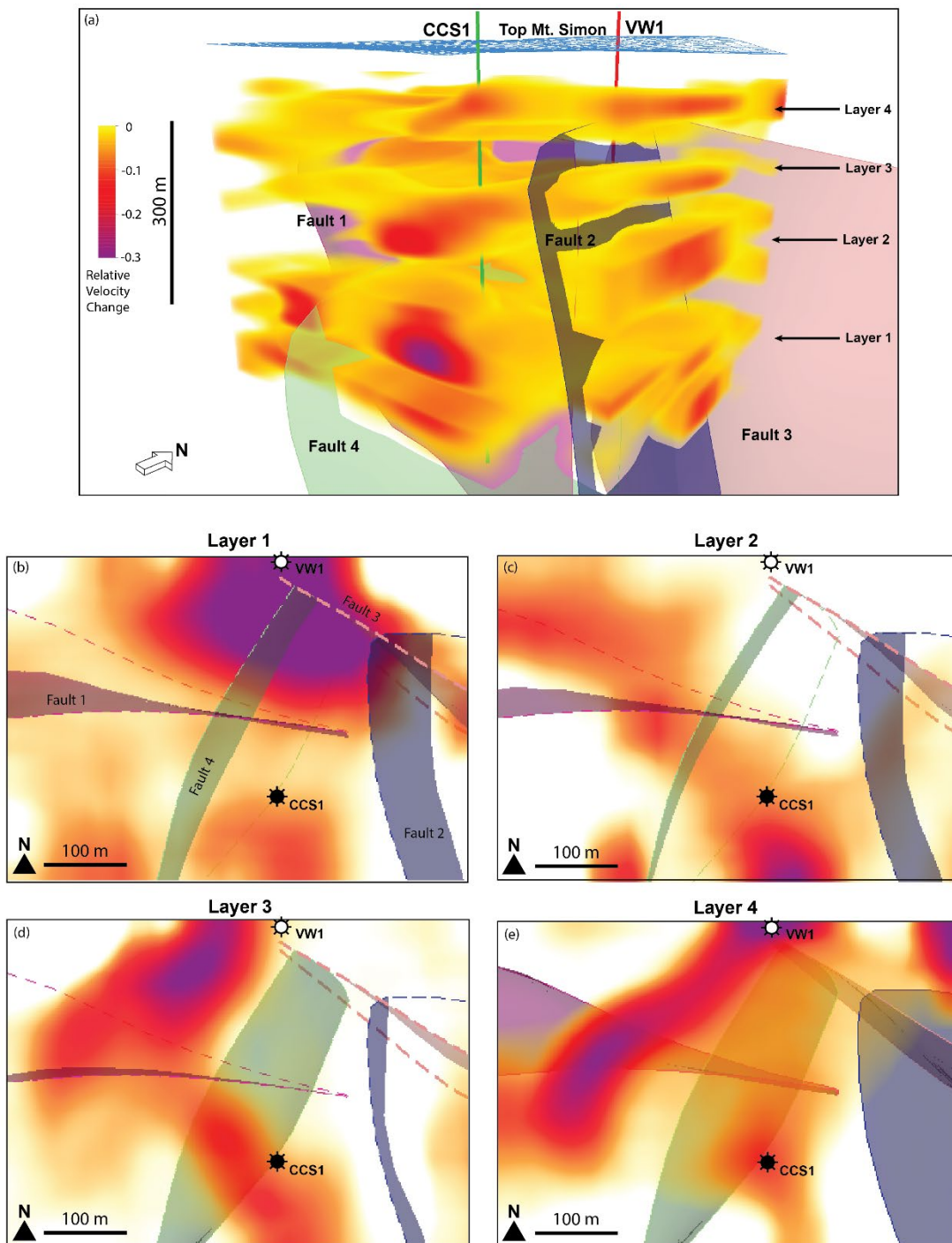
215 **Figure 1.** Map views of relative velocity change showing the shallowest layer (at about 1550 m)  
216 from all four monitors (M1-M4) relative to the baseline (B2). Note the excellent consistency in the  
217 features.  
218

219 The similarity and consistency in the geometry of the plume features across the  
220 monitors suggests that the vertical distribution behavior developed quite early, within  
221 four months of injection (the time of the first monitor). Therefore, with increasing mass  
222 of injected CO<sub>2</sub> over time, we expect any major growth of the plumes to be lateral,  
223 which the narrow seismic cubes make impossible to fully observe.

224 Although we do not attempt to invert for CO<sub>2</sub> saturation given uncertainty in the  
225 fluid mixing type, we note that our ranges of relative velocity change can be higher in  
226 terms of absolute values than the maximum expected from fluid substitution  
227 modelling. This is attributed to data quality leading to errors in the time shift  
228 estimation. Because time strain and therefore relative velocity change is a derivative  
229 of time shift, even a small error in time shift will magnify when converted to relative  
230 velocity change (Macbeth and Izadian, 2023).

### 231 **3.2 Capillary barriers and fault zone migration of CO<sub>2</sub> within the Mt. Simon**

232 We interpret fault zone migration of CO<sub>2</sub> in the Mt. Simon sandstone. We infer  
233 such migration from areas of multiple plume features separated by low reservoir  
234 quality zones, with the plume features intersected by a fault. Figure 2 (a) shows such  
235 a scenario in the south-eastern corner of the cube. All three shallower layers appear to  
236 have emerged through Fault 2 from the injection interval. We interpret that CO<sub>2</sub> from  
237 the injection interval preferentially flows upwards under buoyancy through the fault  
238 zone and emerges at shallower intervals.

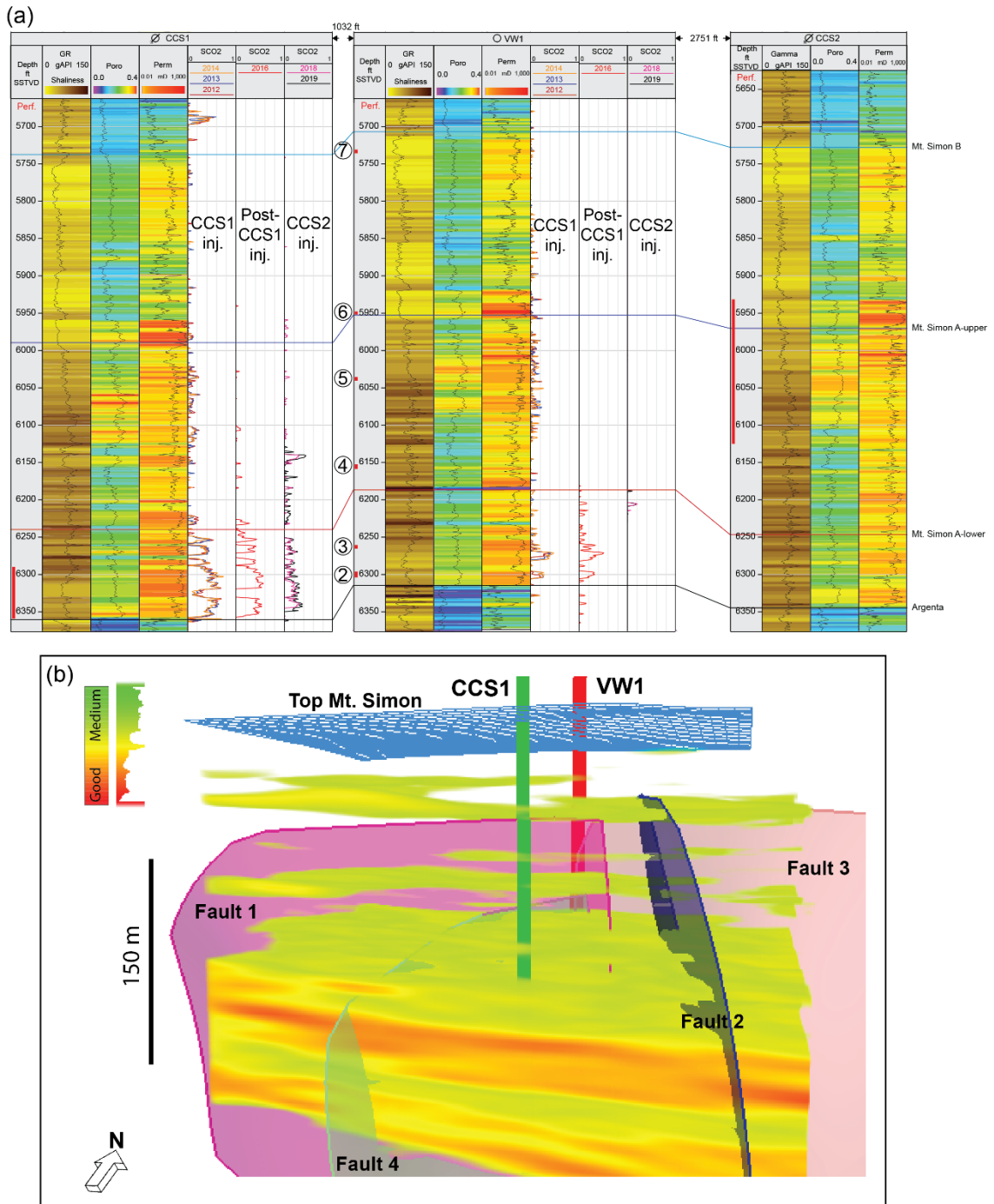


239

240 **Figure 2.** (a) A 3D view of relative velocity change for M4 relative to B2. Our interpretation is that  
 241 regions where the relative change in velocity is  $< -0.02$  are regions of CO<sub>2</sub> saturation. Also shown  
 242 are three out of several faults interpreted by Williams-Stroud et al. (2020). Here we identify four  
 243 layers or zones with CO<sub>2</sub> accumulations. (b) Map views of the four identified layers of CO<sub>2</sub> from  
 244 Layer 1 to 4.

245 The vertical and lateral distributions of the plumes appear to be controlled by  
246 reservoir quality. We validate this by comparing observations of saturation  
247 distribution and reservoir quality in the wells and in seismic data. As shown in Figure  
248 3, well log panels for the injection and monitoring wells show the variation in reservoir  
249 quality across the Mt. Simon. Repeat saturation logging measurements are shown from  
250 each year across the CCS1 injection period through to post-injection and to the CCS2  
251 injection period. From observation of the time-lapse saturation logs, it can be interpreted  
252 that the injected CO<sub>2</sub> preferentially fills the high-quality reservoir sandstones and avoids  
253 poorer quality or tight sandstones (Figure 3 (a)). We define tight sandstones as those  
254 with low porosity, low permeability and high capillary entry pressure.

255 Early modelling attempts at the Decatur site evaluated the risk of extensive lateral  
256 migration as low and expected a more vertical filling of the lower Mt. Simon  
257 sandstone by the injected CO<sub>2</sub> (Finley et al., 2013). This informed the design of the time-  
258 lapse VSP surveys used for studying the plume development (Coueslan et al., 2009).  
259 Strandli and Benson (2013) and Strandli et al. (2014) show that there is excellent  
260 pressure communication between the two zones where the fingers of the plume are  
261 detected in VW1 (zones 2 and 3 in Figure 3 (a)), with both bottomhole pressure gauges  
262 showing identical behaviors and near-instantaneous responses to varying injection rates.  
263 Nonetheless, the lower finger does not at any point buoyantly rise and coalesce with the  
264 upper finger, even after injection had ceased, as it is held back by a tight zone at 1920  
265 m (Figure 3 (a)). The upper finger is also contained by another tight zone at 1905 m.  
266 These tight zones clearly have sufficient permeability to allow good pressure  
267 communication across and even allow the flow of displaced brine as shown by Strandli  
268 et al. (2014). This suggests that these tight zones are capillary barriers rather than  
269 permeability barriers.



270

271 **Figure 3.** (a) Well log panels for the injection and monitoring wells showing the variation in  
 272 reservoir quality across the Mt. Simon in terms of shaliness, porosity and permeability. Repeat  
 273 saturation logging measurements are shown form each year across the CCS1 injection period through to  
 274 post-injection and to the CCS2 injection period. Perforated zones are shown in red. Pressure  
 275 monitoring zones are numbered. (b) Reservoir quality represented by acoustic impedance in 3D,  
 276 with low quality zones rendered transparent.

277 Away from the wells, we use a 3D volume of acoustic impedance, a product of  
 278 rock bulk density and P-wave velocity, to represent reservoir quality. The acoustic  
 279 impedance 3D volume was released as part of the IBDP dataset. Zones of high

280 acoustic impedance represent low quality or tight zones and vice-versa. The acoustic  
281 impedance volume was derived from inversion of 3D seismic data acquired for site  
282 characterization. Acoustic impedance is a good proxy for reservoir quality in this case  
283 because the primary cause of poor reservoir quality in the Mt. Simon is quartz  
284 cementation (Freiburg et al., 2014), which typically results in higher P-wave velocities  
285 by stiffening the rock frame. Cementation also means porosity destruction, which raises  
286 rock bulk densities. The acoustic impedance volume shown in Figure 3 (b) shows the  
287 absence of high-quality pathways through the rock matrix for CO<sub>2</sub> to migrate upwards  
288 from the injection interval.

289 The behavior of CO<sub>2</sub> emergence in a high-quality zone could mitigate leakage up  
290 conductive faults as the amount of CO<sub>2</sub> that continues to migrate up a fault is  
291 progressively reduced with each encountered high-quality zone. Where the  
292 conductive faults are intra-reservoir and do not traverse the seal, they would merely  
293 serve to provide access to other good quality zones of the reservoir, distributing the  
294 CO<sub>2</sub> among them, as has been shown through modelling (Yang et al., 2018; Zhang et  
295 al., 2024). Such is the case at Decatur; the fault provides flow pathways to overlying  
296 good quality zone and stringers in the Mt. Simon formation, which the injected CO<sub>2</sub> is  
297 unable to access normally due to capillary barriers.

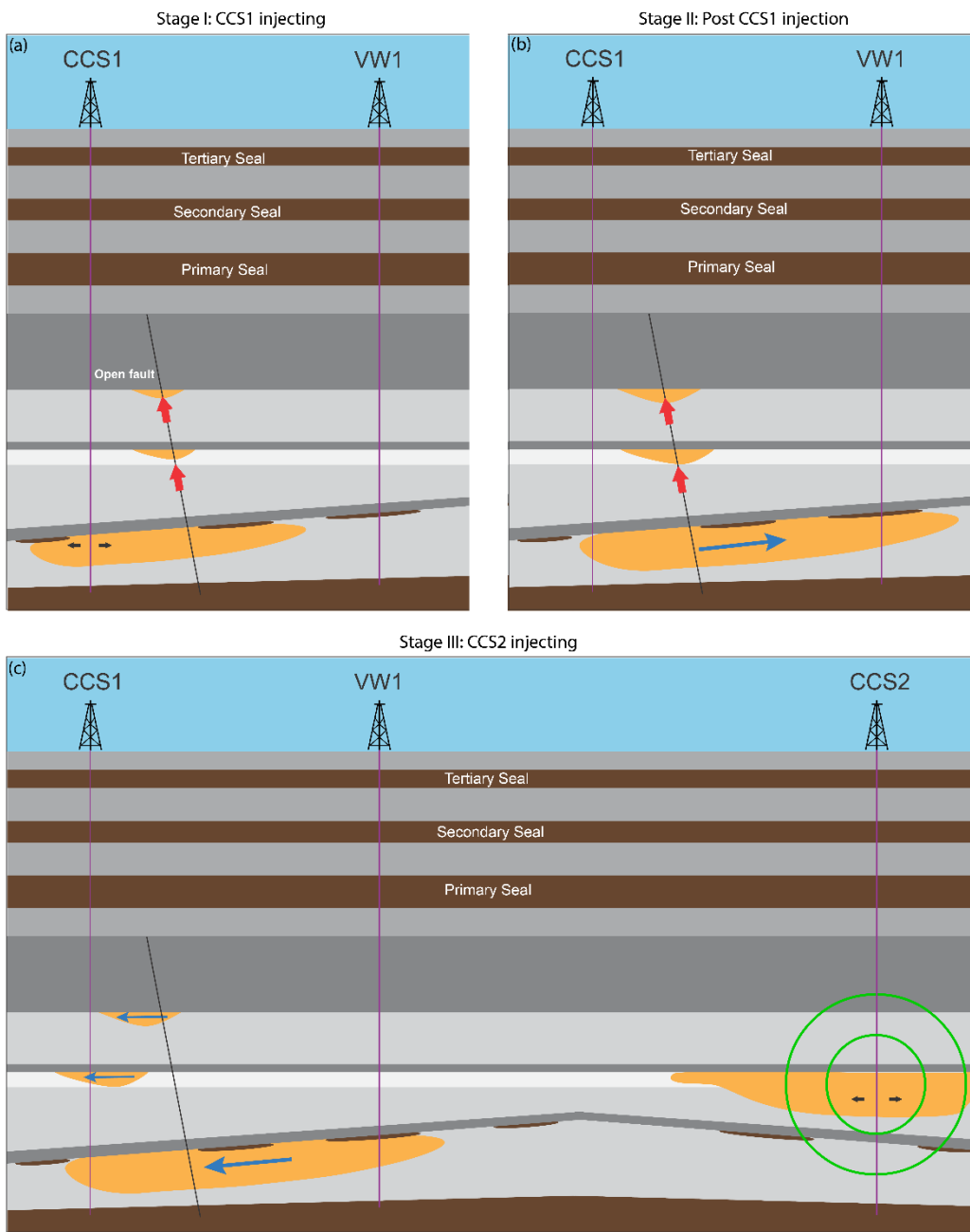
### 298 **3.3 Origins of late CO<sub>2</sub> arrival at injection well post-injection**

299 An isolated finger of CO<sub>2</sub> was detected in the injection well during the post-  
300 injection period of the project in May 2018. This CO<sub>2</sub> was detected in the upper unit  
301 of the Mt. Simon A formation, and it increased in saturation in the March 2019 survey  
302 (Figure 3(a)). The saturation logging report (Swager, 2019) suggested the origins of  
303 the CO<sub>2</sub> to be the Illinois Industrial Carbon Capture and Storage (IL-ICCS) project  
304 located about 1100 m north of well CCS1. The injection well at this secondary project,

305 well CCS2, had been injecting into the upper unit of the Mt. Simon A formation for  
306 13 months at the time of detection. A simplified mass and volume balance analysis  
307 shows it is unlikely that enough CO<sub>2</sub> had been injected in well CCS2 to have reached  
308 well CCS1 at the time of detection. In addition, the uppermost part of the A-Upper  
309 unit (c. 1814 m in well CCS2) has the highest reservoir quality throughout the entire  
310 Mt. Simon sandstone, with permeabilities up to 1000 mD. Given the excellent  
311 correlation of this interval across the three wells, it is the most likely pathway for any  
312 rapid migration of CO<sub>2</sub>. However, the late-arriving CO<sub>2</sub> was detected instead in an  
313 interval in the lower half of the unit at a depth of 1875 m. This interval is deeper than  
314 the injection zone in CCS2, which would require the CO<sub>2</sub> to flow downdip. This is  
315 unlikely outside the viscous region due to buoyancy forces. Moreover, no CO<sub>2</sub> was  
316 detected in the corresponding interval of well VW1, which is located between wells  
317 CCS2 and CCS1. Figure S.4 in the Supplementary Information summarizes this  
318 analysis.

319 We present an alternative hypothesis based on plume interpretations from 4D  
320 seismic time shift analysis and pressure and saturation logging data. We propose that  
321 the CO<sub>2</sub> instead originated from the CCS1 well – the same well it was detected in –  
322 but from layer 1 in the underlying injection interval. The evidence supports that the  
323 CO<sub>2</sub> travelled vertically through Fault 2, forming layer 2 (Figure 2 (c)). Over time,  
324 layer 2 got larger as more CO<sub>2</sub> pooled. Once injection began at the nearby IL-ICCS  
325 project, the pressure gradient induced as a result of active CO<sub>2</sub> injection in well CCS2  
326 then forces layer 2 to flow across the face of CCS1, resulting in this new detection.  
327 We argue this given that bottomhole pressure data shows good pressure  
328 communication between wells CCS1 and CCS2. Our interpretation of the overall CO<sub>2</sub>  
329 migration behavior during the three stages of CCS1 injection, post CCS1 injection and

330 CCS2 injection is summarized in Figure 4.



331

332 **Figure 4.** A conceptual schematic summarizing the overall plume behavior during (a) CCS injection,  
333 (b) post CCS1 injection, and (c) CCS2 injection. Reservoir quality is indicated in grayscale with darker  
334 tones representing tight zones.



335        **4 Conclusion**

336        We have re-interpreted data from time-lapse seismic surveys at the Illinois Basin -  
337        Decatur Project and shown that the CO<sub>2</sub> plume had been migrating along major faults  
338        between high quality units of the reservoir and moving laterally in response to  
339        injection at a neighboring site. The analysis provides an important dataset of  
340        previously theorized plume migration behavior between fault zones and reservoir  
341        units. This interpretation was otherwise not possible using a conventional analysis of  
342        amplitude attributes. The factors which hindered a more straightforward amplitude-  
343        based analysis may occur commonly in projects, especially in onshore settings. The  
344        much clearer picture of CO<sub>2</sub> plume anomalies provided by time shifts allowed a  
345        meaningful integration of multiple independent measurements to produce a coherent  
346        interpretation of the migration behavior of injected CO<sub>2</sub> at the Decatur site. We were  
347        able to identify an interplay of capillary heterogeneity and upward flow of CO<sub>2</sub> along  
348        permeable faults under buoyancy forces. In addition, we identify the role of pressure  
349        gradients resulting from CO<sub>2</sub> injection at a neighboring project in causing the re-  
350        mobilization and flow of CO<sub>2</sub> at the Decatur project post-injection. These behaviors  
351        and their impacts have been previously theorized, and the observations provided from  
352        an industry scale geological CO<sub>2</sub> storage site provides important validation of these  
353        theories and data from which future projects may be designed.

354        **Acknowledgments**

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357        Development Fund for providing the funding for this research.

358       **Open Research**

359       The original dataset and reports used in this study were made publicly available  
360 by the National Energy Technology Laboratory through the Energy Data eXchange  
361 (ISGS, 2021a, 2021b). Bukar, 2024 provides the processed data and code used in this  
362 study. The codes are also accessible at [https://github.com/ImperialCollegeLondon/4d-](https://github.com/ImperialCollegeLondon/4d-seismic-co2)  
363 [seismic-co2](https://github.com/ImperialCollegeLondon/4d-seismic-co2)

364

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# Supporting information for "Carbon dioxide migration along faults at the Illinois Basin – Decatur Project revealed using time shift analysis of seismic monitoring data"

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## Contents

1. S1 Feature-based Warping Approach to Time Shift Analysis
  - S1.1 Synthetic modelling
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2. S2 Evaluating the possibility of CCS2 as the source of the late CO<sub>2</sub> arrival at injection well post-injection
3. Table S1:

## S1 Feature-based Warping Approach to Time Shift Analysis

We introduce *Feature-based Warping (FW)*, a modification to Dynamic Time Warping (DTW), which seeks to align matching features (peaks and troughs) in two seismic traces. The dissimilarity error is defined as:

$$e_{feature}[i, q] = d(f_{feature}[i], g_{feature}[i + l])$$

where  $f_{feature}[i]$  and  $g_{feature}[i + l]$  are the positions of key features in the baseline and monitor traces, respectively, and  $d(f_{feature}[i], g_{feature}[i + l])$  is a measure of the distance between the features in the two traces, in this case the L1 or Manhattan distance.

### S1.1 Synthetic Modelling

We use well log data from well CCS1 to generate a 1D (pseudo-2D) synthetic model. The well logs are displayed in Figure S1. We select three zones from the RST logs for March 2012 (equivalent to M1) to substitute CO<sub>2</sub>; the main injection interval (Mt. Simon A – Lower), a 30-meter interval in Mt. Simon A – Upper, and a 5-meter interval in Mt. Simon C where there is a detection of CO<sub>2</sub> from the RST logs.

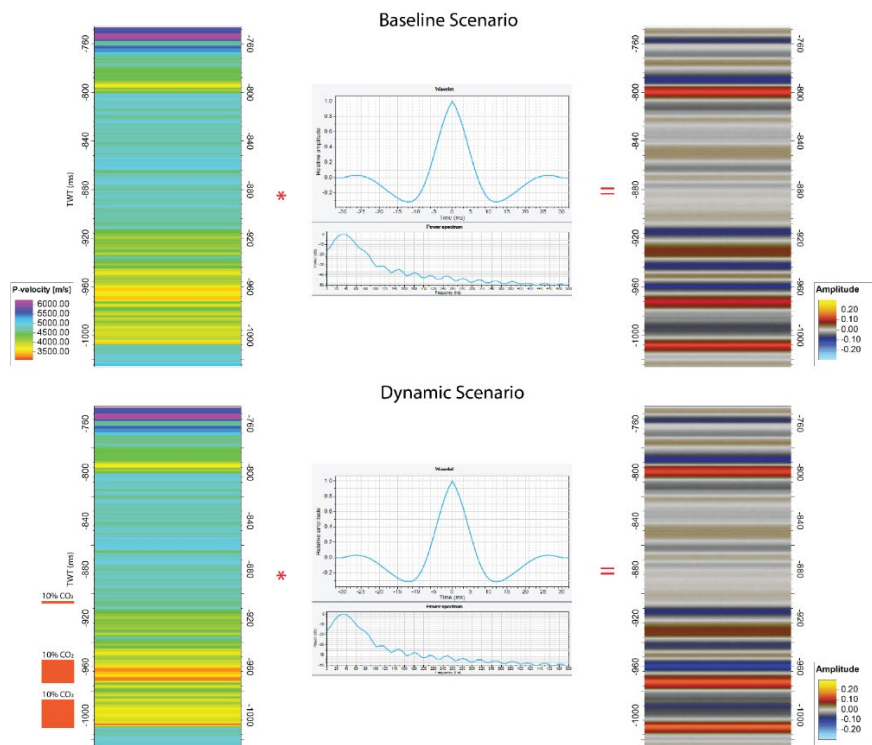


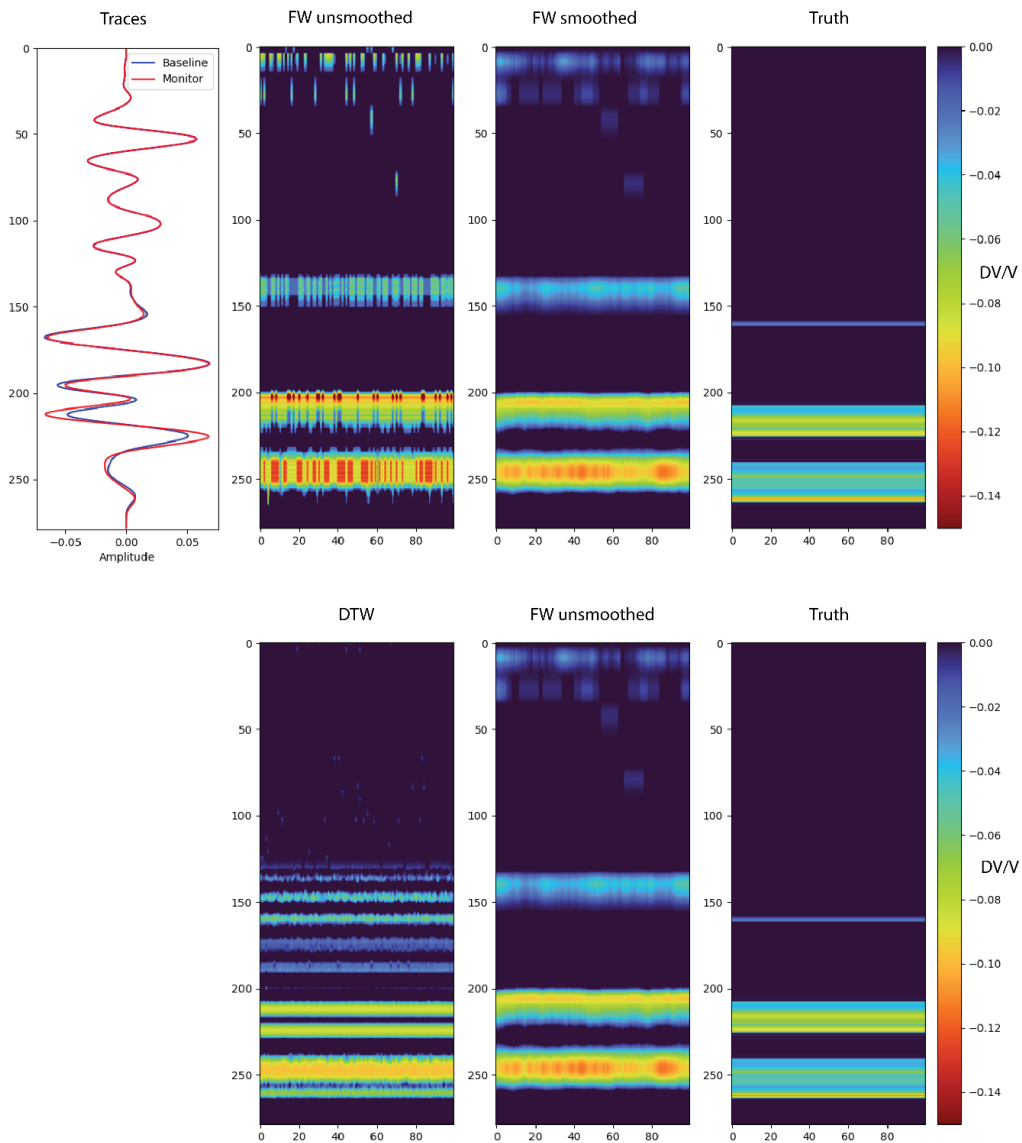
Figure S1: Synthetic modelling based on well log data from CCS1. Baseline and monitor scenarios are produced.

For these zones we choose a 10% CO<sub>2</sub> saturation. Fluid replacement was performed using Gassmann fluid substitution with both fully uniform and patchy mixing to create dynamic or monitor scenarios. The model of acoustic impedance is then convolved with a statistical wavelet extracted from the VSP baseline (B2) so it represents the frequency characteristics in the reservoir region. The same wavelet is used to produce a synthetic seismic for the monitor scenarios. Random noise of 60 dB S/N is added to the outputs. This is shown in Figure S1.

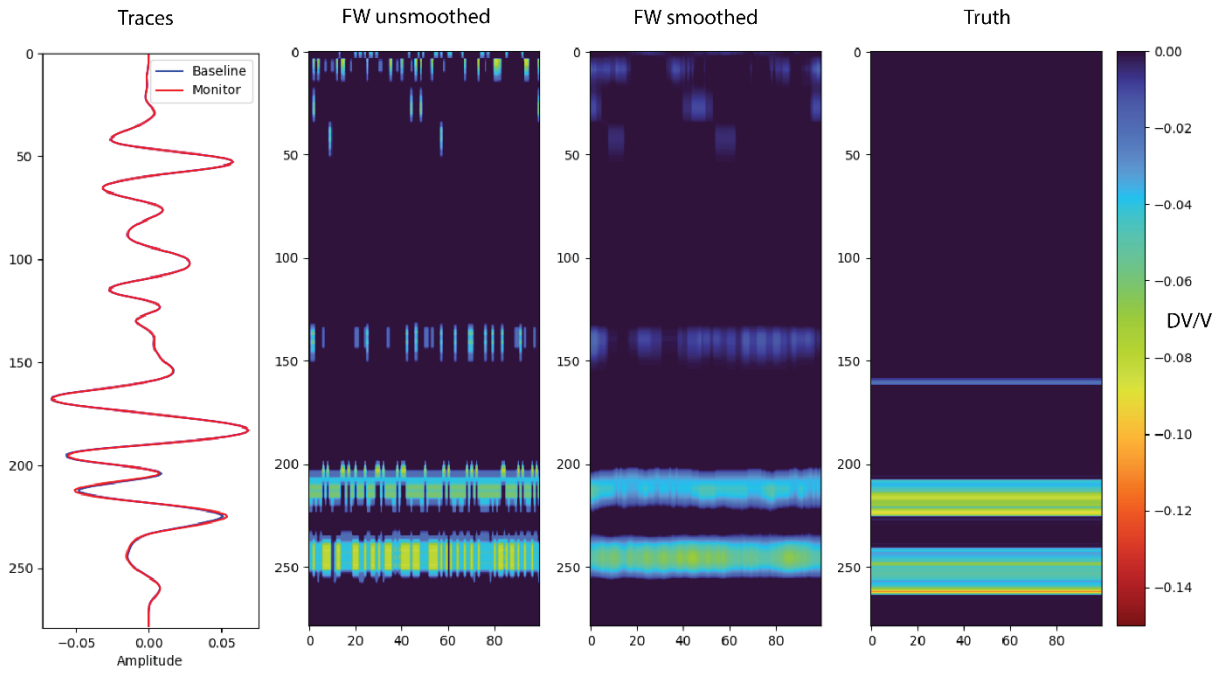
### S1.2 Feature-based warping execution

Features (peaks and troughs) are found through a sequential search for local maxima through the traces. Corresponding features are then matched. To avoid cycle skipping challenges caused by spurious features present in one trace but not the other, band pass or low pass filtering may be applied. The features are used to construct a cost matrix where the cost increases with the distance between matched features. The magnitudes of amplitudes of the features are irrelevant. By comparison, the cost matrix for a DTW approach is based on the absolute difference in amplitudes of all pairs of sample points in the traces.

We compare the results of Feature-based Warping (FW), Dynamic Time Warping (DTW), and the true relative velocity change. The feature-based warping approach produces less artefacts and is more efficient as there are less points of comparison. This approach is also able to reliably detect thin layers of CO<sub>2</sub> at low saturations even at lower frequencies, illustrating the robustness of the time shifts detected by this method.

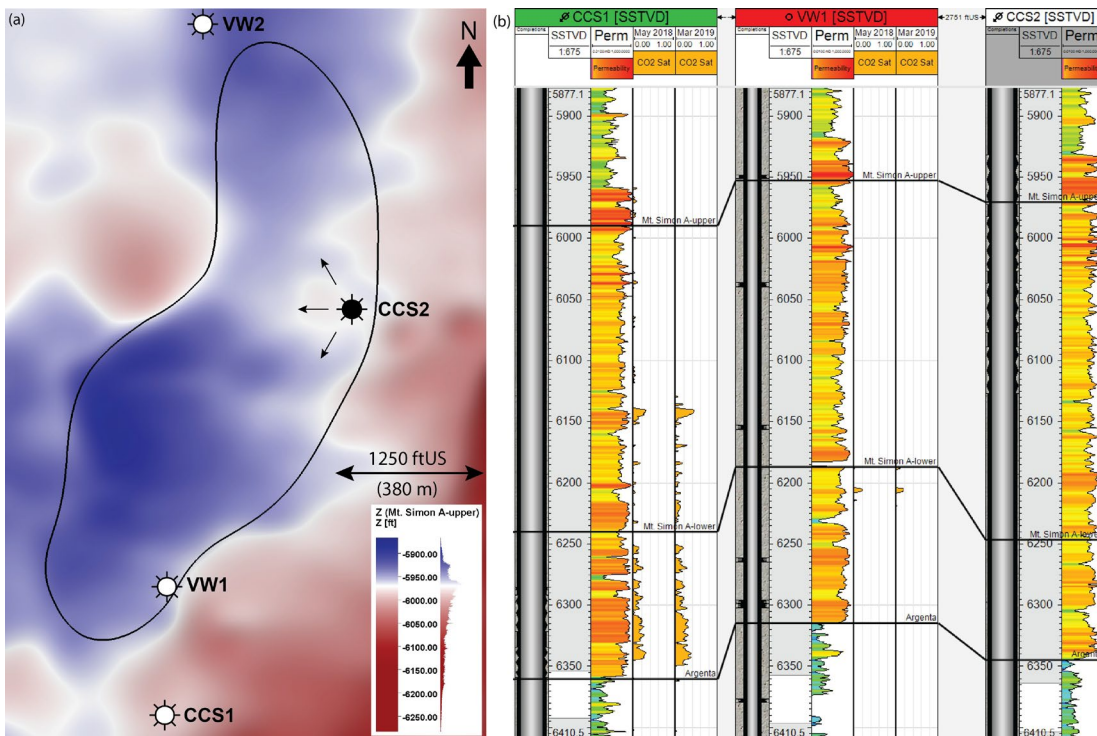


**Figure S2: Uniform mixing** – Comparison of the feature-based approach with DTW and the true relative velocity change for uniform mixing.

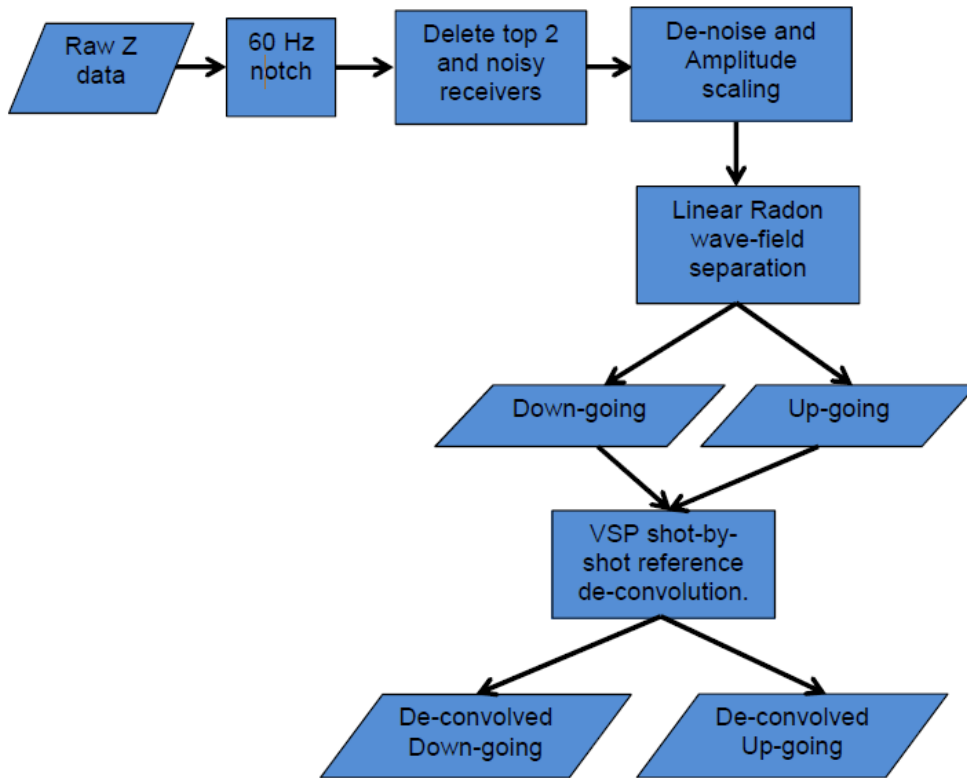


**Figure S3: Patchy mixing** – Comparison of the feature-based approach with DTW and the true relative velocity change for fully patchy mixing.

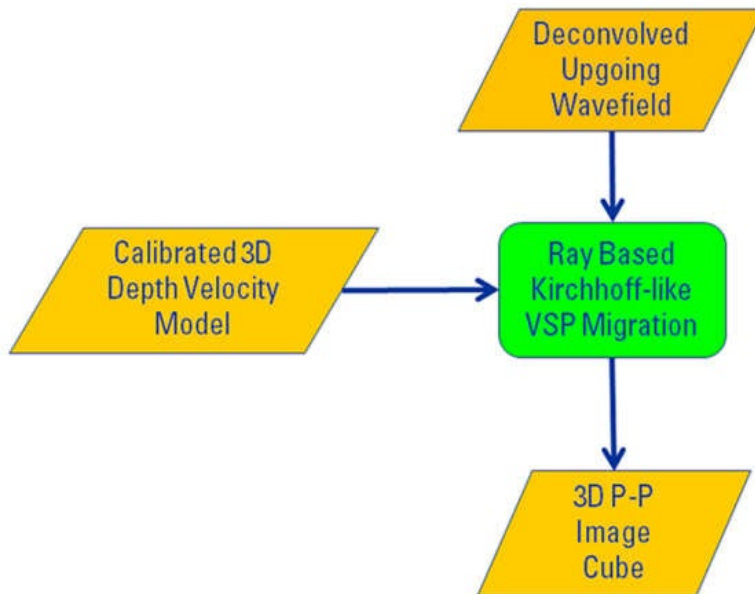
## S2 Evaluating the possibility of CCS2 as the source of the late CO<sub>2</sub> arrival at injection well post-injection



**Figure S4:** (a) Plume footprint equivalent to 687,000 t of CO<sub>2</sub> derived using a simplified mass and volume balance. We consider flow through only the top one-third thickness of the injection zone at a conservative CO<sub>2</sub> saturation of 0.2 and with no dissolution. (b) Well correlation panel showing wells CCS1, CCS2 and VW1 with no CO<sub>2</sub> detection at VW1.



**Figure S5:** Processing block diagram for 4D VSP data from raw to deconvolution (Schlumberger, 2015).



**Figure S6:** Processing block diagram for depth migration performed on the 4D VSP data (Schlumberger, 2015).



**Table S1:** Time-lapse VSP survey dates, ground conditions during acquisition and injected CO<sub>2</sub> quantity. Repeated shots refer to the number of shots in the monitor surveys that were co-located with the Baseline 2 survey (i.e., within 50 feet spatial tolerance in source easting and northing coordinates). Co-location issues were encountered due to permit issues with local landowners and the construction of new electrical and industrial infrastructure at the site.

<b>Survey</b>	<b>Date</b>	<b>Ground conditions</b>	<b>Vibrator sweep (Hz)</b>	<b>Repeated shots (relative to B2)</b>	<b>Amount of CO<sub>2</sub> injected (tonnes)</b>
Baseline 1 (B1)	Jan. 27-30, 2010	Wet	2-100	-	Pre-injection
Baseline 2 (B2)	Apr. 12-14, 2011	Dry	8-120	-	Pre-injection
Monitor 1 (M1)	Feb. 11-12, 2012	Frozen/Dry	8-120	467	74,000
Monitor 2 (M2)	Apr. 4-5, 2013	Damp	8-120	385	433,000
Monitor 3 (M3)	Feb. 3-5, 2014	Frozen	8-120	378	730,000
Monitor 4 (M4)	Jan. 15-17, 2015	Frozen	8-120	458	~1,000,000