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# Global assessment of directional effects in the inter-calibration of optical satellite instruments with the TRUTHS mission

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## Abstract

Upcoming SI-Traceable Satellite (SITSat) missions such as TRUTHS aim to achieve an unprecedented accuracy for SI-traceable measurements of the Earth-reflected radiation. These measurements will support the generation of low uncertainty climate records and significantly improve the calibration of other sensors. In such a context, the uncertainty will be limited by the calibration transfer process rather than the reference sensor. This study presents an end-to-end global inter-calibration simulator capable of assessing the potential uncertainty for multiple scenarios that considers the interrelation of different error sources and match-ups. We first define the sensor-to-sensor match-ups through an orbital analysis that is followed by a top-of-atmosphere (TOA) radiance modelling of each match-up. Finally, we calculate the radiometric uncertainty based on different error sources combined globally. In this first implementation we have calculated the match-ups of TRUTHS against observations by the Copernicus Sentinel-2A satellite over land areas throughout a year. We calculate the angular mismatch for both viewing differences and solar changes from different overpass time. We define multiple inter-calibration scenarios based on temporal, angular or cloud constraints. These first results show that considering overpasses up to 15 minute difference, low cloud probability and matching field-of-view (FoV), within  $5^\circ$ , we sample most land areas with a mean error  $<0.1\%$  and bias regression  $<0.5\%$ . We have also restricted the sun zenith angle (SZA) to  $60^\circ$  to minimise solar angle and viewing azimuthal dispersion over the poles. This also results in data-gaps of several months that might be complemented with dedicated manoeuvres or a dedicated processing of these polar-region match-ups.

## I. INTRODUCTION

The last decade has seen the development of missions such as TRUTHS (Traceable Radiometry Underpinning Terrestrial and Helio-Studies [1]) and CLARREO (Climate Absolute Radiance and Refractivity Observatory [2]), now implemented as a NASA pathfinder mission [3], designed explicitly to provide highly accurate and trusted SI(Système international)-traceable climate records. These missions were also designed with the specific intent to provide ‘in-space’ reference calibration to other optical satellite sensors to improve their performance and interoperability. In recognition of this new class of sensor the Committee on Earth Observation Satellites (CEOS) and World Meteorological Organisation Global Space Inter-calibration System (WMO-GSICS) have created the name SITSat (SI-Traceable Satellite) together with an associated formal definition [4].

The TRUTHS mission achieves and evidences its low SI-traceable uncertainty through regular re-calibration of its hyperspectral Imaging Spectrometer (HIS), on-board, directly linked to a space-borne primary reference standard, a Cryogenic Solar Absoluter Radiometer (CSAR). The On-Board Calibration System (OBCS) provides tunable spectrally-resolved radiation that can be distributed between the CSAR, where its power is measured, and the HIS where the now known power is transformed to radiance illuminating and calibrating the HIS. The process can be considered a space adapted mimic of a terrestrial calibration in a national metrology institute. The CSAR is a space adaptation of the terrestrial cryogenic radiometer which has served as the primary SI standard of choice for nearly 40 years [5]. TRUTHS is

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41 currently in the Phase B2 implementation phase as an ESA Earthwatch mission funded by a consortium  
42 of member states led by UK in partnership with Switzerland, Greece, Romania, Czech Republic and  
43 Spain with a target launch date in 2030. The mission has a design goal to globally and continuously  
44 measure Earth reflected spectral radiance from 320 to 2400 nm with a spectral resolution of 4-8 nm,  
45 ground sampling distance of 50 m and uncertainty goal of 0.3% ( $k=2$ ). In practice due to data volume  
46 constraints the full spatial resolution is likely to be limited to specific targets, in particular those used for  
47 calibration of other sensors, such as the CEOS reference sites [6].

48 The upcoming SITSat missions such as TRUTHS, will constitute a system that not only enables  
49 harmonization but the establishment of SI-traceability and performance enhancement. In preparation for  
50 such a scenario where the reference sensor does not limit the uncertainty of an inter-calibration process,  
51 the study and correction of sources of errors related to the calibration transfer process e.g. spatial and  
52 temporal mismatch, becomes highly relevant.

53 One of the first broad studies of the error sources associated with satellite inter-calibration identified  
54 eight dimensions when matching two spacecraft in orbit and studied several of these and their impact  
55 on a calibration against the proposed CLARREO mission [7]. Similarly, the work in [8] studied the  
56 effect of spectral responses, spectral resolution, spectral filter shift, geometric misregistrations, and spatial  
57 resolutions. This work also introduced a combined uncertainty of the different effects with final figures that  
58 represent overall bounds on the achievable uncertainty estimate. Later work in [9] studies the uncertainty  
59 in the spectral, spatial and temporal dimensions associated with an inter-calibration with TRUTHS mission  
60 as a reference sensor. The study effectively describes the contributions as an error distribution rather than  
61 bounds of uncertainty. However, the combination of them does not include all the potential dimensions  
62 in the inter-calibration. Further work has been carried out in different studies but exploring each of the  
63 dimensions independently [10], [11], [12], [13], [14].

64 The orbit definition for the TRUTHS mission is another critical step since it defines the number of  
65 match-ups with the target sensor, their locations and angular configuration among others. A conventional  
66 sun-synchronous orbit flying in close time tandem to another specific satellite could clearly have near  
67 continuous match-up opportunities within the tandem time delay window. However, satellites outside of  
68 this window, other than Geo-stationary satellites, would rarely if ever have time optimized match-ups.  
69 An orbital model that identifies the match-ups between CLARREO and sun-synchronous polar orbital  
70 sensors such as CERES (Clouds and the Earth's Radiant Energy System) or VIIRS (Visible Infrared  
71 Imaging Radiometer Suite) is presented in [15]. The work not only identifies the valid match ups between  
72 the sensors but it also discusses the number of potential samples required to achieve the climate quality  
73 uncertainty in the inter calibration, considering the relatively low instantaneous signal-to-noise ratio (SNR)  
74 of CLARREO (nb, observations are intended to be spatially and temporally averaged reducing sensitivity  
75 to single pixel SNR). However, the study does not consider all the potential uncertainty sources and the  
76 correlation among them in a global context.

77 The interrelation between different errors (i.e. error correlation) is a factor in deriving an appropriate  
78 combined estimate of the potential radiometric uncertainty that could be attributed to the inter-calibration  
79 process. The general assumption of an uncorrelated scenario (i.e. quadratic summation of different un-  
80 certainty contributions) is not necessarily correct and a case by case scenario must be carefully assessed.  
81 Furthermore, the inter-calibration methods generally require the accumulation of different sensor-to-sensor  
82 match-ups. This requires the development of a methodology that is capable of defining the achievable  
83 accuracy based on an error distribution from which an uncertainty estimate can be derived.

84 This study defines and implements an end-to-end inter-calibration simulator that is capable of assessing  
85 the potential uncertainty on a case by case basis for multiple inter-calibration scenarios. Here we aim  
86 to connect the orbit sampling, the specific scene modelling of each sensor-to-sensor match-up and the  
87 combination of different error sources at a global level. In a way, we are aiming to generate a digital twin  
88 prototype for inter-calibration studies. For this first study, we present the uncertainty introduced due to  
89 angular mismatch between the TRUTHS mission and the target reference over land areas. These angular  
90 differences can be introduced by differences in satellite viewing angles but also in different solar illumi-

91 nation angles introduced by the delay between satellite overpasses. Furthermore, these angular differences  
 92 can result in top-of-atmosphere (TOA) radiance errors coming from both surface and atmospheric angular  
 93 sensitivity.

94 The general inter-calibration methodology aims at measuring ideally identical targets by two sensors  
 95 with the same view at the same time and possessing similar spatial and spectral responses (e.g. GSICS  
 96 [16], [17] or CLARREO [2]). For polar orbiting satellites, this is generally possible through satellite  
 97 manoeuvres that align the angular configuration of the TRUTHS sensor to the target satellite if they differ  
 98 from a nominal nadir view.

99 These satellite manoeuvres can reduce directionality errors to a negligible level. However, they require  
 100 a complex tasking, consume the satellite energy resources and have an impact on the main TRUTHS  
 101 mission goal (i.e. provide benchmark measurements of both incoming solar radiation and outgoing reflected  
 102 radiation). Therefore, this study explores a complementary approach that considers near-simultaneous over-  
 103 passes of both nadir and view angle mismatched observations but does not include satellite manoeuvres.  
 104 This implies potentially larger instantaneous errors but ones that are expected to reduce with accumulation  
 105 of different crossings (angles and scenes) over the year.

106 In this manuscript, the selected target mission is the Copernicus Sentinel 2 (S2). The Copernicus S2  
 107 satellite mission currently consists of two satellites (S2A and S2B) that together sample the Earth with  
 108 better than a 5-day revisit. Its main payload instrument measures in 13 spectral bands spanning the visible,  
 109 near-infrared (VNIR) and the shortwave infrared (SWIR) at spatial resolutions of 10, 20 or 60 m [18].

110 The specific study of the angular mismatch supports both the definition of an orbit and pointing strategy  
 111 for the TRUTHS mission that optimises the inter-calibration accuracy with minimum impact on the global  
 112 benchmark accuracy. The continuous development of this simulator is expected to become the basis for  
 113 the definition of an inter-calibration strategy for the TRUTHS mission and/or similar optical instruments.

114 The manuscript is structured in two sections consisting of methodology (Section II) and results (Section  
 115 III). Section II is subdivided into a definition of the end-to-end general framework (subsection II-A), the  
 116 orbit definition and match-up data (subsection II-B) and the modelling of TOA radiance including both  
 117 the scene surface and atmosphere (subsection II-C). Section III first describes the distribution of sensor-  
 118 to-sensor match-ups based on parameters such as time differences, latitude or angular distribution. It then  
 119 provides the results of the inter-calibration uncertainty assessment for each considered scenario.

## 120 II. METHODOLOGY

### 121 A. General framework

122 The general idea of the proposed methodology is that of simulating the end-to-end process of the inter-  
 123 calibration at a global scale. That is, we aim to use the orbital projections to generate all the resultant  
 124 match-ups between two sensors and the associated characteristics of their observations that impact the  
 125 match-up uncertainty. We could refer to this as an observational digital-twin for inter-calibration studies.

126 The logic of this concept is represented in Figure 1.

127 [Fig. 1 about here.]

128 The left end of the schema includes the *orbit match-up generator* and the *match-up products database*.  
 129 The former provides location and angular information at the event (detailed discussion in subsection  
 130 II-B) whereas the second ingests the relevant information to model the surface bidirectional reflectance  
 131 factor (BRDF) and the atmosphere. These two are fundamental information for the module *TOA radiance*  
 132 *modelling* used to generate a realistic TOA radiance scene at each sensor-to-sensor match-up (detailed  
 133 discussion in subsection II-C). The following module, *error match-up generator* aims to assess the effect  
 134 of spectral response mismatch, spatial response mismatch, scene/cloud dynamics, polarisation or angular  
 135 mismatch. In this study, we have implemented the angular mismatch which is assessed by managing the  
 136 call to the *TOA radiance modelling*. Specifically, we call the module for each sensor-to-sensor match-up  
 137 with specific viewing angular information and timestamp for TRUTHS and S2A overpasses respectively.

138 The result of this process is an error that is iteratively produced at each sensor-to-sensor match-up and  
 139 managed by the *global post-processing assessment*. In this first implementation, the global assessment is  
 140 based on an analysis of the error distribution and the fitting of the radiance curve that are discussed in  
 141 Section III. The implementation has been applied to three different scenarios defined as:

- 142 • *Relaxed scenario* (Subsection III-B). This scenario only discards sensor-to-sensor match-ups with a  
 143 sun zenith angle (SZA) higher than  $60^\circ$  or a time difference between sensors larger than 15 minutes.
- 144 • *Intermediate scenario* (Subsection III-C). This scenario further filters out the previous match-ups by  
 145 constraining S2A field-of-view (FoV) (here simplified to  $5^\circ$  viewing zenith angle (VZA)) matching  
 146 the TRUTHS FoV. It also filters out the matches by considering low probability cloud events (further  
 147 info in subsection II-C).
- 148 • *Restrictive scenario* (Subsection III-D). This latter scenario restricts the matches from the previous  
 149 case by decreasing the maximum delay between sensors to just 5 minutes and only considers angle  
 150 matching below 2 degrees.

151 The tighter criteria for ray-tacing in the third scenario are tending towards GSICS collocation  
 152 practices, where so far larger experience with low Earth orbit (LEO) sensors [17] has been made in  
 153 the thermal infrared.

## 154 B. Orbit analysis

155 TRUTHS satellite mission will be launched into a non-sun-synchronous orbit with an inclination of 90  
 156 degrees and an average geodetic altitude of 611 km. Sentinel-2 orbit is sun-synchronous with 10:30 Local  
 157 Time at Descending Node, an average geodetic altitude of 800.9 km and an inclination of 98.6 deg.

158 Due to the difference in altitude between both satellites, TRUTHS and Sentinel-2 will overtake each  
 159 other frequently, with a period of about 1.8 days. The TRUTHS orbital plane will rotate with respect to the  
 160 Sun and will complete a full revolution after 1 year. During the periods of the year when the orbital plane  
 161 is close to the orbital plane of sensors in sun-synchronous orbits, co-observations (without manoeuvres)  
 162 may be possible at latitudes other than polar regions. The TRUTHS Mean Local Solar Time at Ascending  
 163 Node Crossing on the 1<sup>st</sup> of January has been set to 17:00h, which corresponds to approximately RAAN  
 164  $356^\circ$ .

165 The methodology to identify collocated observations between TRUTHS sensor with 100km-wide swath  
 166 and Sentinel-2 MSI instrument is outlined below and illustrated in Figure 2:

- 167 • Sentinel-2 swath contour is split with a step of 5 seconds (green rectangles)
- 168 • TRUTHS swath is split in across-track direction with a granularity of 10 km (blue lines)
- 169 • the intersection of each intermediate TRUTHS swath line with the rectangular portions of Sentinel-2  
 170 swath will result in 2 points
- 171 • from those 2 resulting points, the viewing geometry angles (SAA, SZA, VAA, OZA) and timestamp  
 172 to TRUTHS and Sentinel-2 are calculated and used for further analysis.

173 [Fig. 2 about here.]

## 174 C. Top-of-atmosphere radiance modelling

175 The TOA radiance modelling is generated with the Library for Radiative Transfer (LibRadtran) [19],  
 176 [20]. We parameterise the scene (surface, atmosphere and geometry) and obtain an output result that  
 177 represents the convolved radiance into a spectral response function (SRF). In this implementation, we  
 178 have selected the SRF of the Moderate Resolution Imaging Spectroradiometer (MODIS) bands 2 (approx  
 179 841-876 nm spectral interval), 3 (approx 459-479 nm spectral interval) and 6 (approx 1628-1652 nm  
 180 spectral interval) to keep consistency with the selected BRDF surface products [21].

181 As mentioned in the previous paragraph, we have selected the MCD43 products [22]. The product  
 182 describes the BRDF using the RossThick-LiSparseReciprocal kernels obtained from an inversion of a  
 183 semiempirical model over 16 days of MODIS directional surface reflectance data. The three kernel

184 values (fiso , fvol , fgeo) can be used in Libradtran to estimate the surface anisotropic effects [23],  
 185 [24]. Specifically, we have used daily L3 Global 30ArcSec CMG V006 products for MODIS bands 2, 3  
 186 and 6 [25] from year 2021. These BRDF kernels are then introduced as part of the input parameterisation  
 187 of the Libradtran radiative transfer software. If the product does not contain a retrieval value, we search  
 188 for and iterate at 5-day intervals from the acquisition day up to a maximum of 20 days difference. In case  
 189 there is no valid result at any of these days, we use the default BRDF associated to an IGBP landclass in  
 190 Libradtran. The IGBP landclass is obtained at each sensor-to-sensor match-up from MCD12C products  
 191 [26] hosted in Google Earth Engine (GEE) [27].

192 The geometry configuration is based on the angular configuration for each satellite overpass at the  
 193 match-up points given by the orbital simulation (see subsection II-B). This information is complemented  
 194 by the altitude given by a digital elevation model at  $0.1^\circ$  spatial resolution [28].

195 The aerosol optical thickness (AOT) is modelled from the Copernicus Atmosphere Monitoring Service  
 196 (CAMS) Global Near-Real-Time [29], [30] from the European Centre for Medium-Range Weather Fore-  
 197 casts (ECMWF) and hosted in GEE. The forecast value for the closest hour, day, and location, is selected.  
 198 In case no valid value is found or the connection with the server is lost, the value will be retrieved from  
 199 an AOT with the monthly average from March 2019 to March 2020 at a  $0.1^\circ$  spatial resolution[31]. In  
 200 the unlikely scenario that both approaches fail, a default value of 0.2 will be allocated. Other properties  
 201 of the AOT are modelled with the default values: rural type aerosol in the boundary layer, background  
 202 aerosol above 2 km and spring-summer conditions [19], [20].

203 The water vapour (WV) is obtained from Global Forecast System (GFS) 384-Hour Predicted Atmosphere  
 204 Data produced by National Oceanic and Atmospheric Administration (NOAA) and hosted in GEE.  
 205 Similarly to the AOT, the closest value for the closest 6-hour forecast sample is selected. In the absence  
 206 of a value or invalid retrieval, WV maps with monthly average values from March 2019 to March 2020 at  
 207 a  $0.1^\circ$  spatial resolution will be accessed [32]. If both the two previous methods report an unsuccessful  
 208 result, we allocate a value of 1 cm. From the same GFS product, we also extract a forecast value of cloud  
 209 probability in the pixel area defined as  $27830 \times 27830$  meters.

210 The atmospheric profile is set to mid-latitude summer with a representative wavelength absorption  
 211 parameterization (REPTRAN model [33]) customised for MODIS bands to be consistent with the BRDF  
 212 products. The radiative transfer runs with 16 streams and the DISORT solver.

213 Figure 3 represents the viewing error modelled for inclinations up to 20 degrees for the considered  
 214 MODIS bands. It also describes the temporal error as a consequence of the sun's movement with delays  
 215 of  $\pm 30$  minutes from the overpass time. The overpass represents a typical S2A overpass at latitude -  
 216 23.6002 and longitude 15.11956 that coincides with the CEOS RadCalNet Gobabeb site [34]. The specific  
 217 overpass time is 09h:17m:02s for the 25th of November 2021. The atmosphere has been modelled with  
 218 an AOT 0.14, WV of 1.694 cm and altitude of 510 m.

219 [Fig. 3 about here.]

220 This example indicates the relatively significant level of error, exceeding the 1% value, that occur for  
 221 viewing angle differences larger than TRUTHS FoV ( $5^\circ$ ). This viewing error also varies as function of  
 222 spectral band. The directionality of MODIS B3 is dominated by the Rayleigh scattering whereas MODIS  
 223 B6 shows a nearly symmetric result from nadir with a visible anisotropy due to the hotspot right at the  
 224 edge of the polar plot. It also shows that these B6 errors have an important azimuthal dependence mostly  
 225 separated by the backward and forward scattering properties of the surface.

226 Similarly, Figure 4 illustrates the temporal variations for the same example as in Figure 3.

227 [Fig. 4 about here.]

228 The temporal variations show important variations but to a lesser extent than the viewing impact. The  
 229 temporal error tends to be highly linear for time delays below 30 minutes. Again, there is an important  
 230 difference depending on the spectral band that for the 15 minute threshold can range from 0.5% in MODIS

231 B6 to over 1% in MODIS B3. Thus, the coupling of both surface and atmosphere proves very critical in  
 232 order to simulate a correct balance between the two effects.

### 233 III. RESULTS

#### 234 A. Orbit match-ups and parameters

235 The orbit analysis described in Section II-B results in a set of timestamp, location and angular infor-  
 236 mation for both the S2A and TRUTHS mission over a year. The analysis is only restricted to 15 minutes  
 237 so that further filtering and analysis can select the optimum sensor-to-sensor matches for each scenario.

238 In general, the time difference between the two missions shows a nearly uniform and symmetric  
 239 distribution (mean value below 20 seconds for all cases). The long repeat cycle of the TRUTHS mission  
 240 (61 days; see subsection II-B) as compared to the 10 days repeat cycle of S2A results in a diverse number  
 241 of opportunities with different angular and temporal conditions. This potentially leads towards a more  
 242 symmetric distribution of the time delays between the two sensors in a match-up area. The *intermediate*  
 243 *scenario* produces the most symmetric distribution (mean value below 5 seconds) likely explained by the  
 244 constraining of the S2A FoV to  $5^\circ$ , matching that of TRUTHS FoV.

245 Figure 5 includes the polar distribution of solar and viewing angles for different scenarios. The location  
 246 of the sensor-to-sensor match-ups is displayed in subsections 7, 9 and 11. The considered scenarios are:  
 247 *all*, *relaxed intermediate*. The former refers to all the sensor-to-sensor match-ups over sunlit land areas  
 248 whereas the latter two scenarios were defined at the end of Section I.

249 [Fig. 5 about here.]

250 The polar plot of the angle distribution indicates that without a general restriction on the SZA, a large  
 251 fraction of crossings would occur at very high SZA over the poles. In that case, not only the large  
 252 SZA would be challenging but also the viewing azimuthal differences between TRUTHS and S2A. The  
 253 TRUTHS orbit is designed as a true  $90^\circ$  polar orbit whereas the S2A orbit has a slight inclination of  
 254  $98.62^\circ$ . Thus, the restriction to a SZA lower than  $60^\circ$  in the *relaxed scenario* significantly reduces both  
 255 the solar angle and the viewing azimuthal dispersion. The *intermediate scenario* shows that a 15-minute  
 256 threshold between mission overpasses still results in important solar angle differences between TRUTHS  
 257 and S2A. However, this is partially compensated because these angular differences do not visually indicate  
 258 a correlated nature.

259 The temporal distribution of these opportunities over the year is also an important criterion since any  
 260 calibration effort ideally requires a continuous effort assessment, dependent on drift of the target sensor  
 261 and any sub-orbital variations. Figure 6 depicts the same sensor-to-sensor match-ups as a function of day  
 262 of the year and the latitude.

263 [Fig. 6 about here.]

264 As explained in subsection II-B, the rotation of the TRUTHS orbital plane with respect to the Sun  
 265 results in a yearly pattern. Combined with a general criterion of a SZA threshold of  $60^\circ$  to avoid large  
 266 angular effects in polar regions, results in an approximate two-month period of match-ups followed by a  
 267 four-month of no valid opportunities.

#### 268 B. Results for a relaxed scenario: $SZA < 60^\circ$ and $\Delta t < 15'$

269 As explained in Section I, this scenario considers all match-ups with the only conditions being that the  
 270 SZA is lower than  $60^\circ$  and the time difference is lower than 15 minutes. Figure 7 presents the match-ups  
 271 across the globe with a colour bar indicating the level of error for each sample. These same errors are  
 272 presented as an error distribution and radiance linear regression in Figure 8.

273 [Fig. 7 about here.]

274 [Fig. 8 about here.]

275 The maps show a good distribution of coincidences that cover a range of biomes, latitudes and  
 276 longitudes. However, there are specific areas like the Sahara desert or the Amazon forest that are not  
 277 covered due to the orbit configuration selected for this analysis. Using other orbit RAAN assumption or  
 278 performing the simulation over other years (due to the relative phasing between S2 and TRUTHS) would  
 279 have yielded match-ups over Sahara/Amazon areas. Several of the stripes are long enough to infer an  
 280 evolution of the viewing angles through the orbit that is illustrated through a gradient of colour at each  
 281 stripe.

282 Most of the errors are contained within 5% and the error standard deviation is between 2-3%. However,  
 283 the distribution in all cases presents a slight asymmetric distribution that is translated in mean error values  
 284 of 0.5-1%. The fitted radiance curve for B2 and B6 shows a slight overestimation that in the case of B6  
 285 represents a significant bias. This bias for B6 can be explained by the error resulting from high radiance  
 286 values of S2A. High radiance values tend to be close to the swath edge of S2A and the hot-spot area  
 287 of the surface reflectance (see Figure 3c). These higher radiance values create an imbalance in the curve  
 288 fitting that could explain the higher bias. B3 results in a lower bias but higher offset both in absolute and  
 289 relative terms. Conversely, this might indicate that the relative angular error is nearly constant through  
 290 the radiance range likely explained by the more symmetric nature of the B3 surface error (see Figure 3b)

### 291 C. Results for an intermediate scenario: matching FoV and cloud screening

292 This *intermediate scenario* narrows down the number of sensor-to-sensor matches by matching both  
 293 S2A and TRUTHS FoV and only considering those opportunities that are likely to be cloud-free.

294 Figure 9 presents the matches for this scenario.

295 [Fig. 9 about here.]

296 It is clearly visible that the number of opportunities has significantly decreased. However, it still covers  
 297 a large number of areas across the globe. It is interesting to note how most of the crossings over tropical  
 298 regions are mostly not present due to their high cloud probability (e.g. central Africa or Borneo island).

299 Figure 10 reports the error distribution and radiance linear regression for this scenario.

300 [Fig. 10 about here.]

301 The standard deviation of the angular errors has been reduced to the range 1-2%. More importantly,  
 302 the error distribution is now almost symmetric with just a small mean error of 0.1% for B3. This can  
 303 be explained because we are now matching TRUTHS and S2 FoV results in a symmetric and reciprocal  
 304 angular sampling. Together with a nearly uniform delay distribution, constrains the error propagation and  
 305 results to a symmetric error distribution of TOA radiance biases.

306 This has been directly translated in a better fitting for B2 and B6 but not so for B3 (see Figures 10d,  
 307 10e and 10f). In the latter case, the spectral band is highly influenced by atmospheric directionality and  
 308 matching FoVs does not represent a significant improvement.

### 309 D. Results for a restrictive scenario: matching angles and Delta $t < 5'$

310 This scenario sets up highly restrictive conditions in order to select the "best" sensor-to-sensor matches  
 311 in terms of angular match.

312 Following on from the previous *intermediate scenario*, we have further reduced the maximum time  
 313 delay between missions to five minutes and selected matching angles with less than 2°. This matching  
 314 angle is defined as:

$$\begin{aligned}
 & \arccos(\cos(VZA_{TRUTHS}) \cdot \cos(VZA_{S2A}) \\
 & \cdot \cos(VAA_{TRUTHS} - VAA_{S2A}) + \sin(VZA_{TRUTHS}) \\
 & \cdot \sin(VZA_{S2A})) \leq 2^\circ
 \end{aligned} \tag{1}$$

315 where VAA represents the viewing azimuth angle.

316 Figure 11 represents the global matches with the associated error to each of them. Note that due to  
 317 the low number of opportunities and low error value, the scales have been significantly increased and the  
 318 colour bar has been reduced to a range of  $\pm 1\%$ .

319 [Fig. 11 about here.]

320 The map indicates that most of sensor-to-sensor matches have been lost with matches concentrated in 9  
 321 cluster areas. For example, there are no matches in the entire continents of Africa and Oceania. It should  
 322 of course be noted that small changes in selected orbit configurations of both TRUTHS and indeed S2  
 323 (reflecting small anular changes) can have a significant impact on the locations of match-ups and so the  
 324 above should be seen as illustrative.

325 Figure 12 displays the error distribution and radiance curve fitting for this scenario.

326 [Fig. 12 about here.]

327 The error distribution shows again a very small mean error (below the 0.1%) but significantly decreases  
 328 the error dispersion with a standard deviation of 0.3%. On the contrary, the lower radiance dynamic range  
 329 and small number of samples does not improve (or even worsens) the curve radiance fitting. Thus, this  
 330 scenario indicates these samples can be used as "golden points" in order to constrain an inter-comparison  
 331 but are not sufficient for a more detailed characterisation e.g. large radiance range or location dependence.

## 332 IV. DISCUSSION

### 333 A. General comments

334 We have presented a novel study that seeks to define an optimum inter-calibration strategy for the  
 335 TRUTHS mission based on an end-to-end global simulation (or "inter-calibration digital twin"). The  
 336 general methodology described in subsection II-A defines an orbit match-up analysis that is the input to  
 337 a TOA radiance modelling of the event where the combination of different error sources at a global level  
 338 results in an integrated performance assessment of the intercalibration.

339 For this first study, we present the error introduced due to angular mismatch (both satellite viewing  
 340 angles and solar angles) between the TRUTHS mission and the S2A satellite over land. We have defined a  
 341 general scenario (*all*) and three different scenarios (named *relaxed intermediate* and *restrictive*) that refer  
 342 to different temporal, angular or cloud constraints.

343 Subsection III-A indicates that the restriction to a SZA lower than  $60^\circ$  significantly reduces both the  
 344 solar angle and the viewing azimuthal dispersion. However, Figure 6 suggests that it will also lead to  
 345 significant periods with no sensor-to-sensor match-ups for the three proposed scenarios.

346 The results for the *relaxed scenario* report a high number of opportunities but results in a mean error  
 347 distribution at the 0.5-1%. The fitted radiance also presents a significant bias that for surface effects as  
 348 in B6 can be explained by the impact of anisotropic high radiance values of S2A.

349 The results for the *intermediate scenario* report a lower number of opportunities but still a good  
 350 coverage of different areas across the globe. However, the introduction of cloud probability generates a  
 351 more realistic simulation of potential match-ups and indicate how crossings over tropical regions mostly  
 352 disappear. Thus, it suggest that the definition of an orbit (e.g. RAAN  $0\pm 5^\circ$ ) might result in a majority  
 353 of crossings over desert areas or tropical forests with a direct consequence on the number of cloud-free  
 354 opportunities. This scenario clearly improves the mean error distribution to a value below 0.1% that is  
 355 translated into an improvement of the curve fitting for bands dominated by surface effects (MODIS B2  
 356 and B6).

357 Finally, the results for the *restrictive scenario* result in the lowest angular match-up error (standard  
 358 deviation below 0.3%) but at the cost of a very small number of opportunities. This is sufficient to broadly  
 359 check the inter-calibration at every event but does not allow a characterisation in terms of radiance range,  
 360 location dependency or focal plane variations. However, for some sensors which contain their own on-board

361 calibration/monitoring systems this may still be adequate, particularly if they can also be supplemented  
 362 by other targets and/or sensors that may also have been calibrated by TRUTHS independently.

363 Based on these preliminary findings, a potential optimum global strategy utilising only this methodology  
 364 could be that of selecting an *intermediate scenario* as a baseline approach due to its large number of  
 365 sensor-to-sensor match-ups, large radiance dynamic range and a negligible bias due to angular effects (see  
 366 Figures 9 and 10). This can be complemented with a *restrictive scenario* (here they are a subset of an  
 367 *intermediate scenario*) that could be used as an anchor point. Nonetheless, this approach would result in  
 368 significant temporal gaps of approximately four months as presented in Figure 6. In order to complement  
 369 these time gaps, dedicated manoeuvres could be scheduled during these periods depending on the mission  
 370 needs. Alternatively, the sensor-to-sensor match-ups over these polar regions could be considered at the  
 371 cost of larger directional errors and/or specific angular corrections.

372 As indicated above for the full TRUTHS calibration system we will likely have an integrated calibration  
 373 system of systems, utilizing a range of methods to cover the range of observational conditions, including  
 374 all those currently in use, summarized on the CEOS CalVal portal [35] but enhanced by a TRUTHS  
 375 reference calibration from space.

### 376 *B. Adapting to other scenarios*

377 The same code can be adapted to model different scenarios that are not either global or an inter-  
 378 calibration between two sensors in space.

379 For example, this code has been adapted to model in-situ targets such as RadCalNet [34] where TRUTHS  
 380 will be used to transfer its high accuracy calibration to anchor the network which in turn will then provide  
 381 on-going calibrations to other sensors. The example presented in Figure 3 has been modelled based on the  
 382 RadCalNet Gobabeb typical site conditions. Similarly, as for the scenarios presented here, the opportunities  
 383 throughout the year have been identified and translated into angular mismatch error. In this specific case,  
 384 these angular errors might be partially compensated by including a BRDF correction due to its in-situ  
 385 calculation. In the future we will extend the analysis to consider geo-stationary satellites and of course  
 386 aircraft sensors or an ad-hoc validation campaign. However, in all cases it is important that we test the  
 387 validity of these simulations against real data. At the time of writing, there are no hyperspectral sensors  
 388 with global coverage and full polar orbit. In the absence of a perfectly matching data, alternatives such  
 389 as S2 vs. EnMAP or similar combinations could be explored.

390 This study has only been based on land areas with no consideration of ocean sensor-to-sensor match-  
 391 ups. By including ocean opportunities we would be distorting the results since most of the sensor-to-sensor  
 392 match-ups are at extremely low radiance values where effects such as noise, polarisation or straylight will  
 393 be most relevant. Thus, we consider it best to pursue the ocean case as a separate analysis for specific  
 394 ocean focused missions e.g. those used for Ocean colour.

395 Similarly to the ocean case, cloudy scenes have not been considered but filtered out assuming a cloud  
 396 cover criterion. In order to consider them for the inter-calibration, a specific criterion must be set that is  
 397 based on the cloud dynamics and scene uniformity. Future studies should look into this specific match-  
 398 ups which could enlarge the number of opportunities and the dynamic range of the sensor-to-sensor  
 399 inter-calibration (particularly in the case of a *restrictive scenario* subsection III-D).

400 Finally, we have made the comparison in terms of radiance for the scenarios here presented here. This  
 401 is useful if we are directly comparing the radiance calibration between TRUTHS and a target sensor  
 402 over a large radiance dynamic range. However, there is the option to compare these results in terms of  
 403 reflectance which is straightforward with the code presented here.

### 404 *C. Further work*

405 The approach presented here is under continuous evolution and is expected to include several new  
 406 features and refinements as the mission moves into an operational phase. The obvious next step is to  
 407 include the other sources of error such as spectral and spatial mismatch but also polarization.



408 Current modelling of the BRDF relies on the use of MODIS MCD43D products. They are sufficiently  
 409 realistic to model patterns of surface directionality but improvements will be considered as a trade-off  
 410 with memory and processing requirements. For example, the use of quality flags in separate products  
 411 MCD43D31-MCD43D41 would select the best products and also allow alternative BRDF products to be  
 412 considered if necessary. The atmospheric modelling is mostly based on AOT and WV products. However  
 413 other type of information such as type of aerosol can also be envisaged.

414 The current band modelling in terms of REPTRAN MODIS bands significantly reduces the computing  
 415 requirements. It could be possible to consider a hyperspectral implementation that would imply the parsing  
 416 of several more BRDF bands and the execution of the radiative transfer with a smaller band resolution.  
 417 This would not only allow a hyperspectral assessment of the angular effect but would also allow the blend  
 418 of this effect with the spectral response one [9].

419 This study has successfully considered the cloud cover by setting a 20% cloud probability threshold  
 420 based on forecast values in a pixel area of  $27830 \times 27830$  meters. An alternative would be that of modelling  
 421 the cloud probability based on the closest overpass of Sentinel 2 or Landsat missions. This approach would  
 422 provide a high-spatial resolution (20-30m as compared to 50-100 m of TRUTHS spatial resolution) but  
 423 other effects might arise such as the quality of the cloud detection algorithm or the constant local time  
 424 overpass. Even more important is the consideration of clouds dynamics and general scene changes for  
 425 example by including a simple transport model of the high-spatial resolution cloud.

426 The current prototype runs on a HP DL380P G9 server with 2 x Intel Xeon E5-2690 V4 (14 cores)  
 427 and 128GB RAM. This is sufficient to run each MODIS band in approximately 2 hours. However, all the  
 428 potential improvements mentioned here will require an improvement of the processing resources as well  
 429 as software optimisation so as not to exponentially increase the running time.

#### 430 *D. Conclusion*

431 In conclusion, we have illustrated here through our simulator how the new SITSat class of sensor like  
 432 TRUTHS will provide the means to revolutionise future decades of satellite earth observation. Providing, as  
 433 a free and open service, the capability to improve the performance and interoperability of optical satellite  
 434 imager data products through in-orbit reference calibration directly traceable to a certifiable SI-Traceable  
 435 reference.

436 The new system of systems enabled by such calibrations will enhance climate and other science and  
 437 commercial applications facilitating increased trust in their derived information. The implementation of  
 438 calibration methodologies illustrated in this paper will benefit not only public sector space agencies  
 439 but also most importantly the ‘new space’ providers where the ability to have their own on-board  
 440 calibration/monitoring systems is rarely possible.

#### 441 ACKNOWLEDGMENTS

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#### 443 V. REFERENCES SECTION

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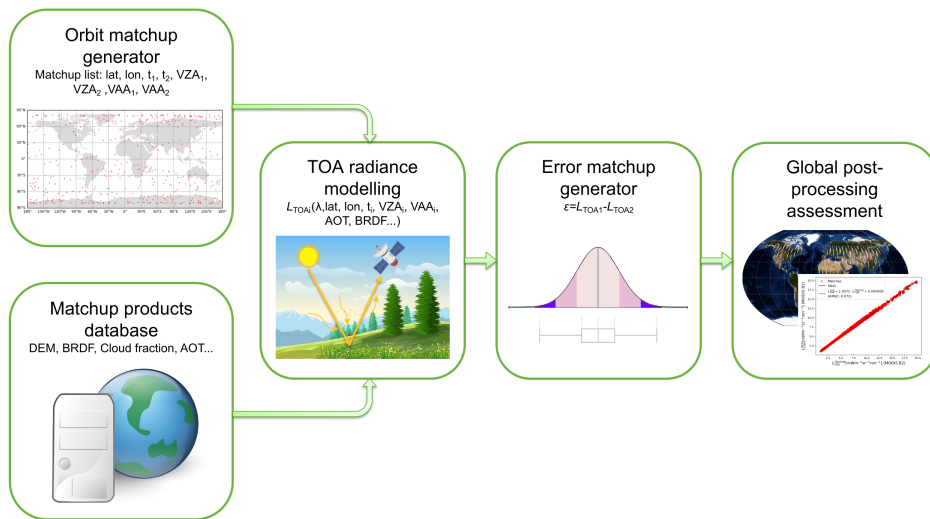


Fig. 1. Workflow schema of the TRUTHS inter-calibration assessment based on global realistic simulations.

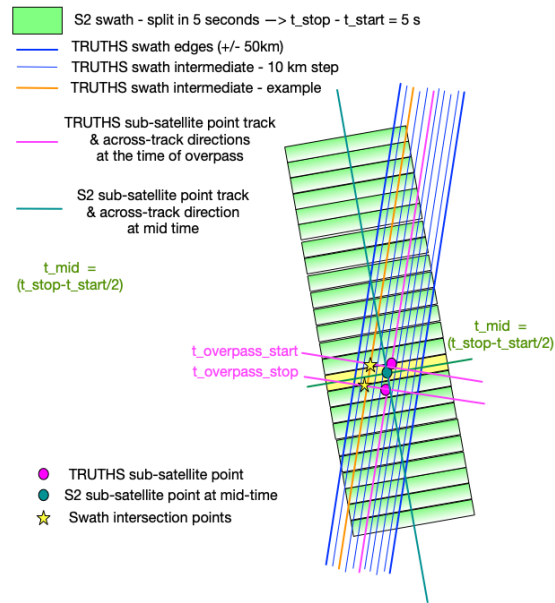


Fig. 2. Schematic representation of the orbit modelling to generate the TRUTHS vs. S2A matches across the globe.

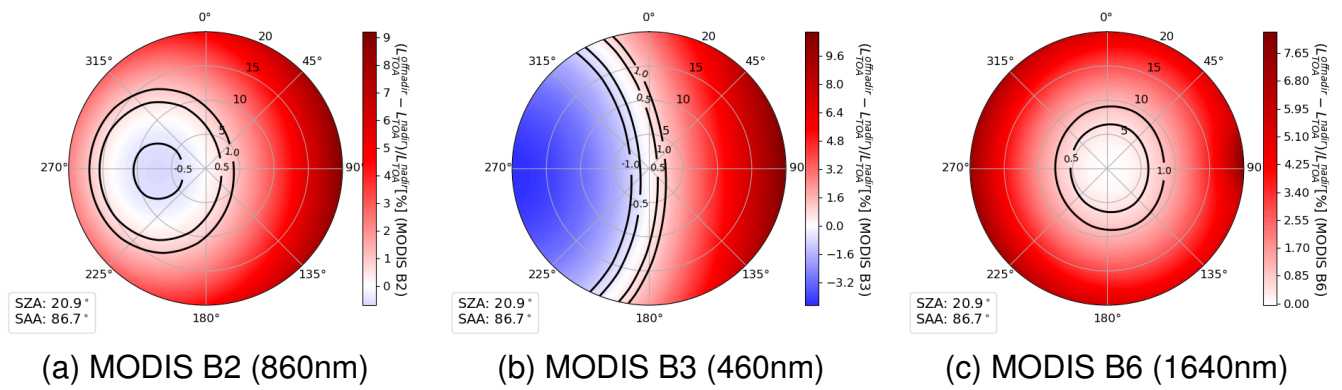


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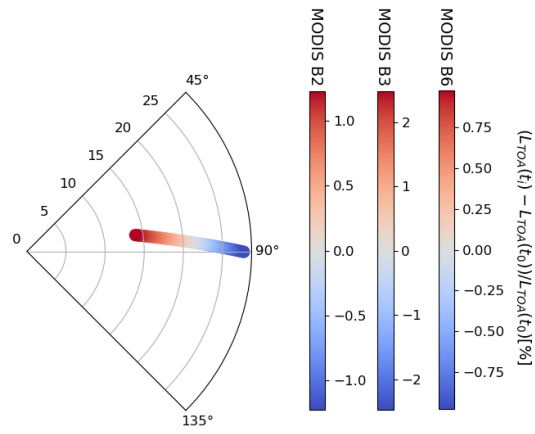


Fig. 4. TRUTHS solar angle evolution and radiometric error modeled for temporal delays up to  $\pm 30$  minutes from the overpass time and MODIS bands B2, B3 and B6.



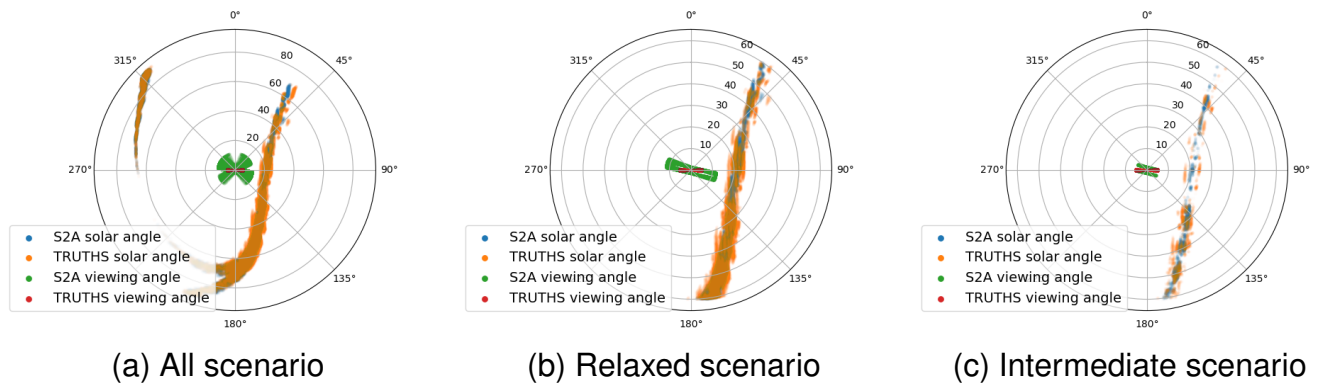


Fig. 5. TRUTHS vs. S2A sensor-to-sensor match-up polar distribution of angles for 3 different scenarios: *all* (Figure 5a), *relaxed* (Figure 5b) and *intermediate* scenarios (Figure 5c).

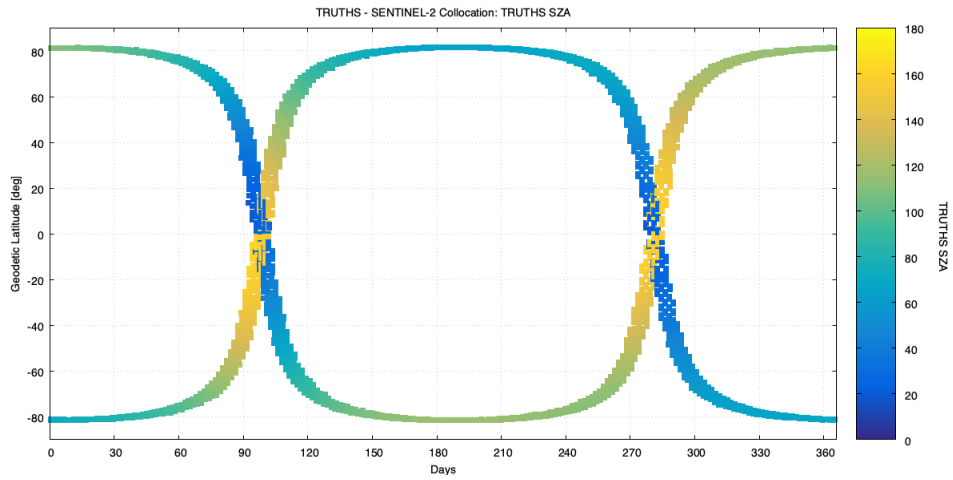


Fig. 6. Collocation opportunities TRUTHS - S2A as a function of the day of the year and considering actual swaths for TRUTHS and S2.

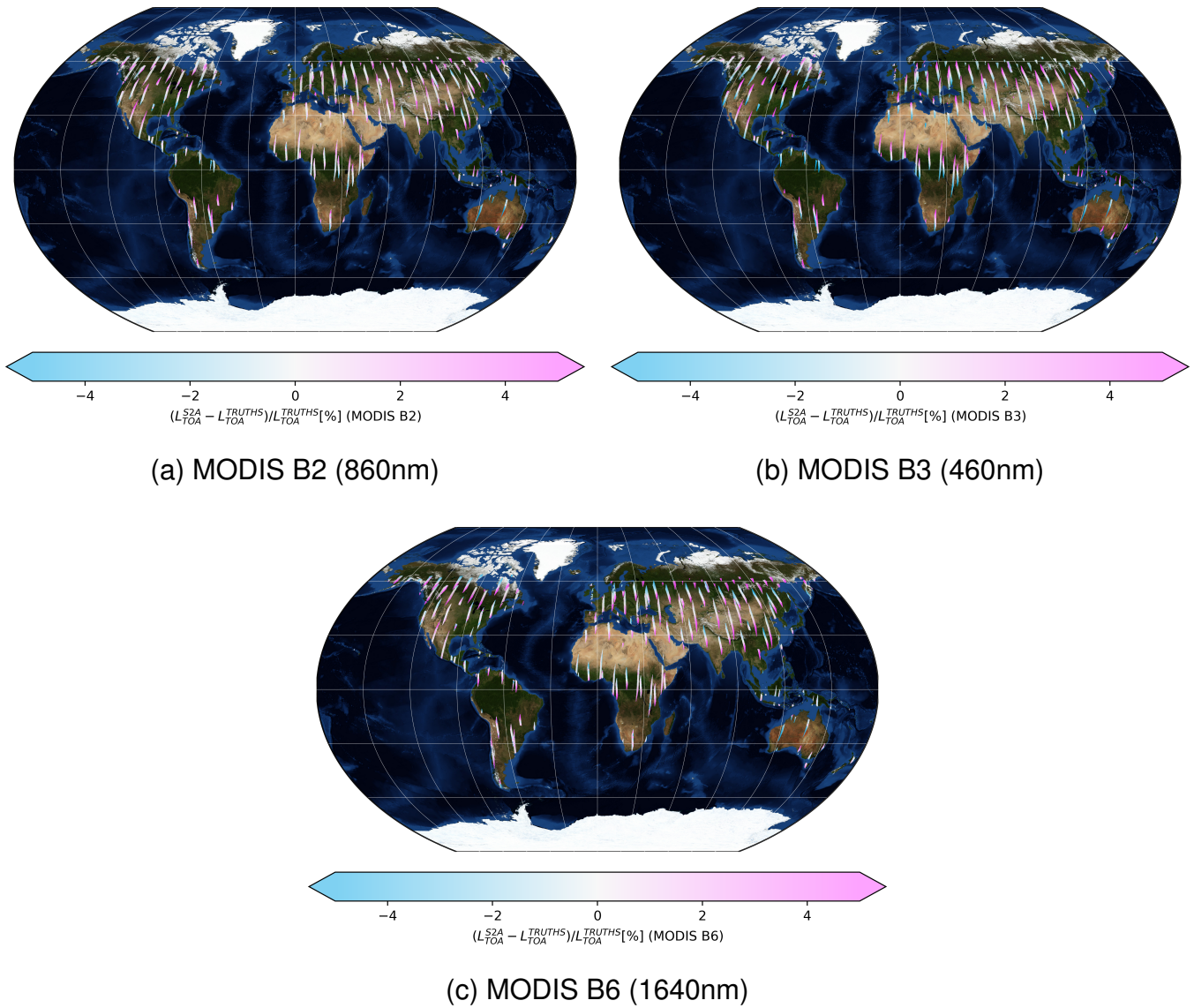


Fig. 7. TRUTHS vs. S2A angular error over the Earth projection considering a *relaxed scenario* for MODIS bands B2 (860nm; Figure 7a), B3 (460nm; Figure 7b) and B6 (1640nm; Figure 7c).

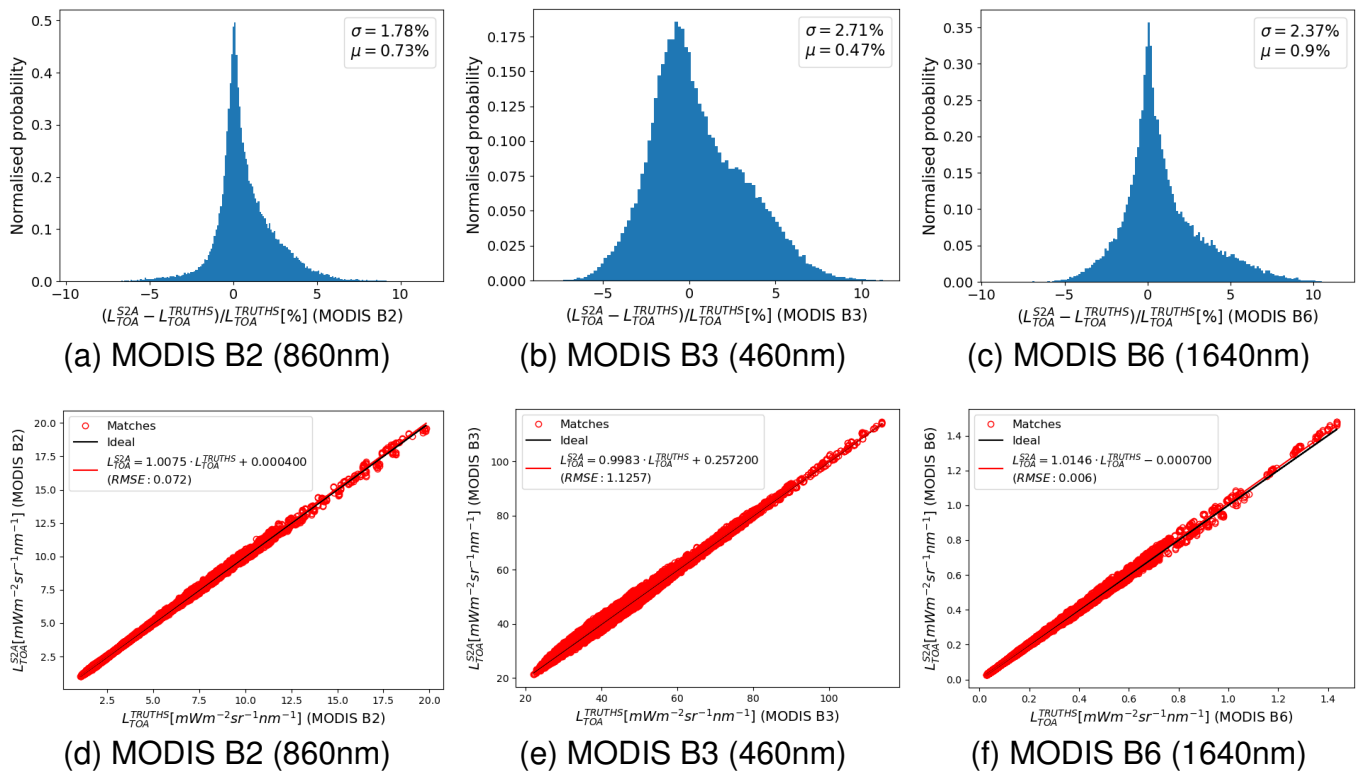


Fig. 8. TRUTHS vs. S2A angular error distribution considering a *relaxed scenario* for MODIS bands B2 (860nm; Figure 8a), B3 (460nm; Figure 8a) and B6 (1640nm; Figure 8a) and radiance regression the same three MODIS bands (Figures 8d, 8e and 8f)

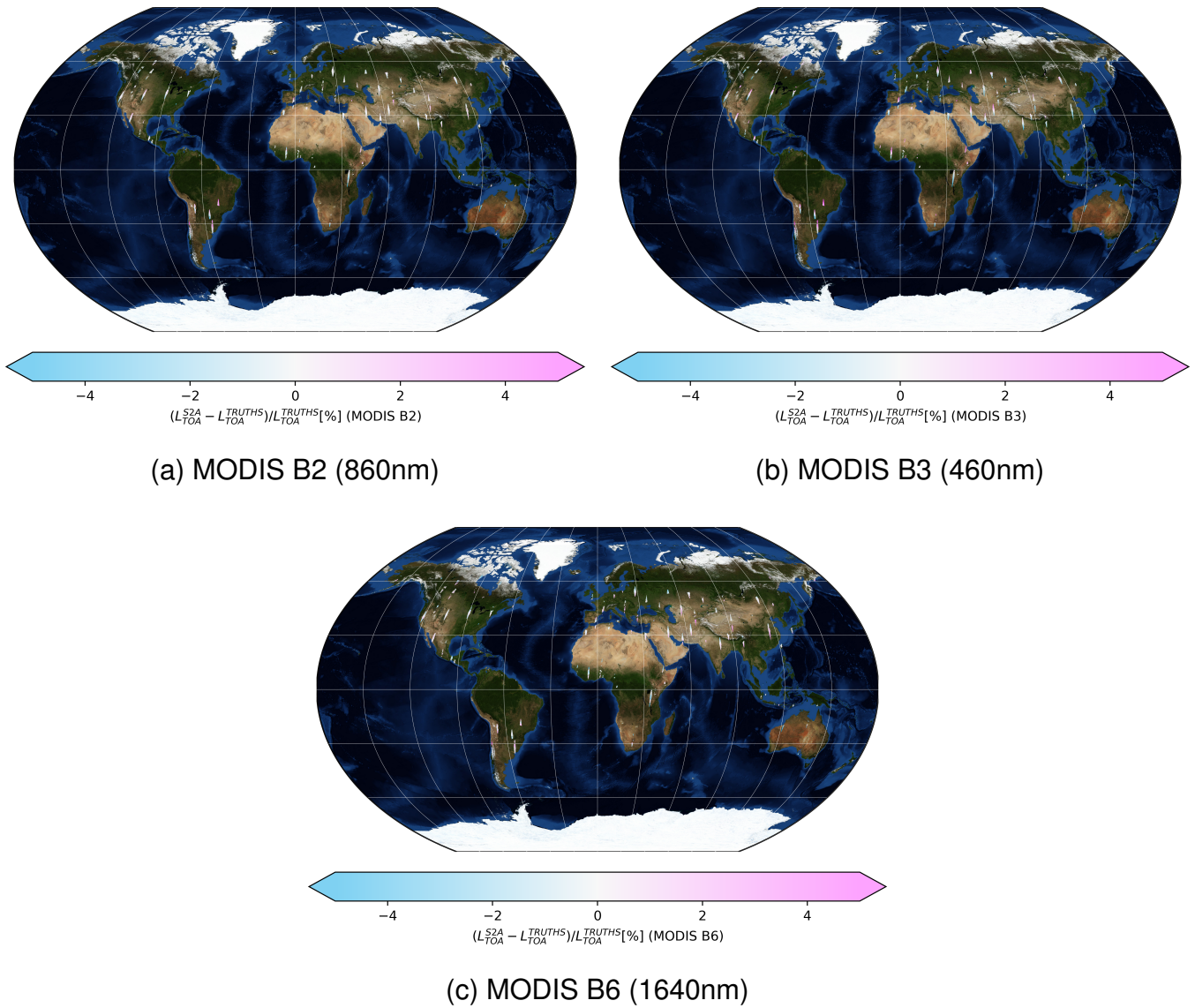


Fig. 9. TRUTHS vs. S2A angular error over the Earth projection considering a *intermediate scenario* for MODIS bands B2 (860nm; Figure 9a), B3 (460nm; Figure 9b) and B6 (1640nm; Figure 9c).

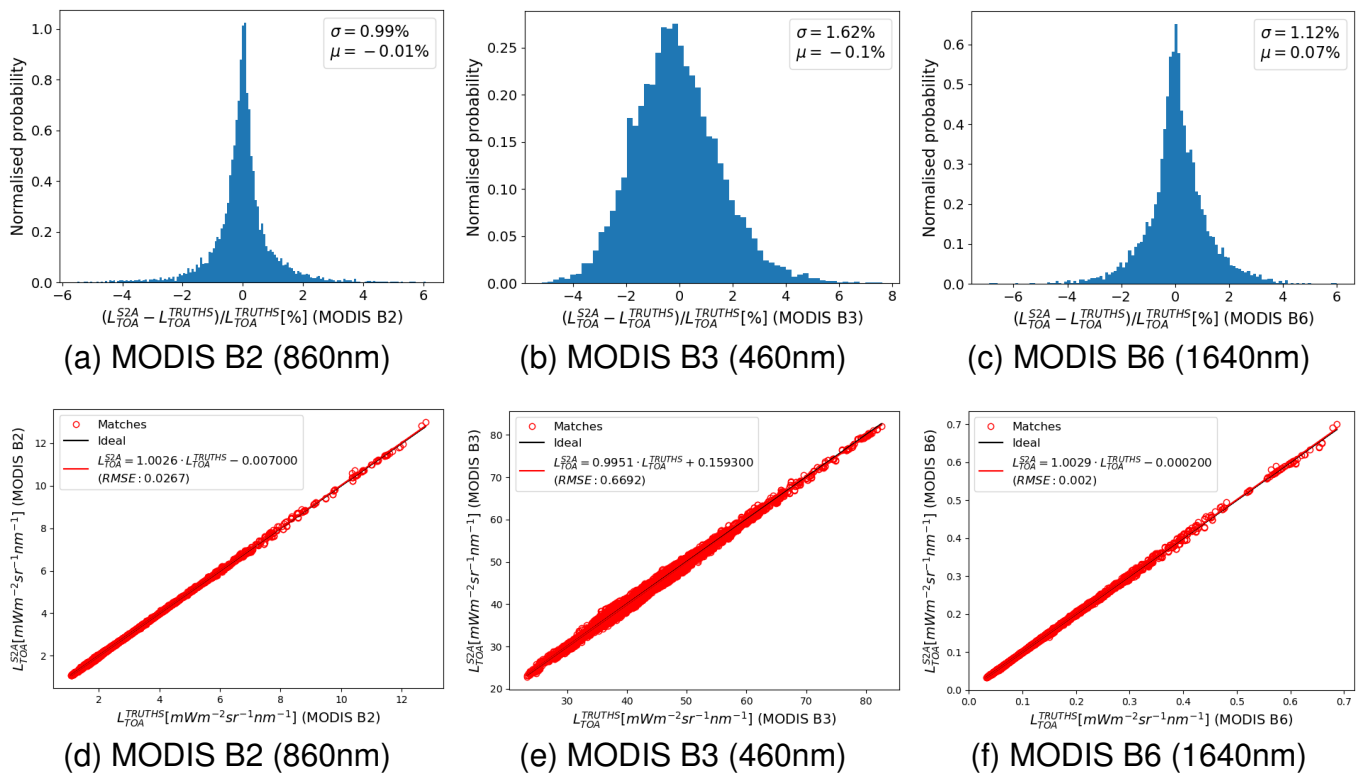


Fig. 10. TRUTHS vs. S2A angular error distribution considering a *intermediate scenario* for MODIS bands B2 (860nm; Figure 10a), B3 (460nm; Figure 10b) and B6 (1640nm; Figure 10c) and radiance regression the same three MODIS bands (Figures 10d, 10e and 10f)



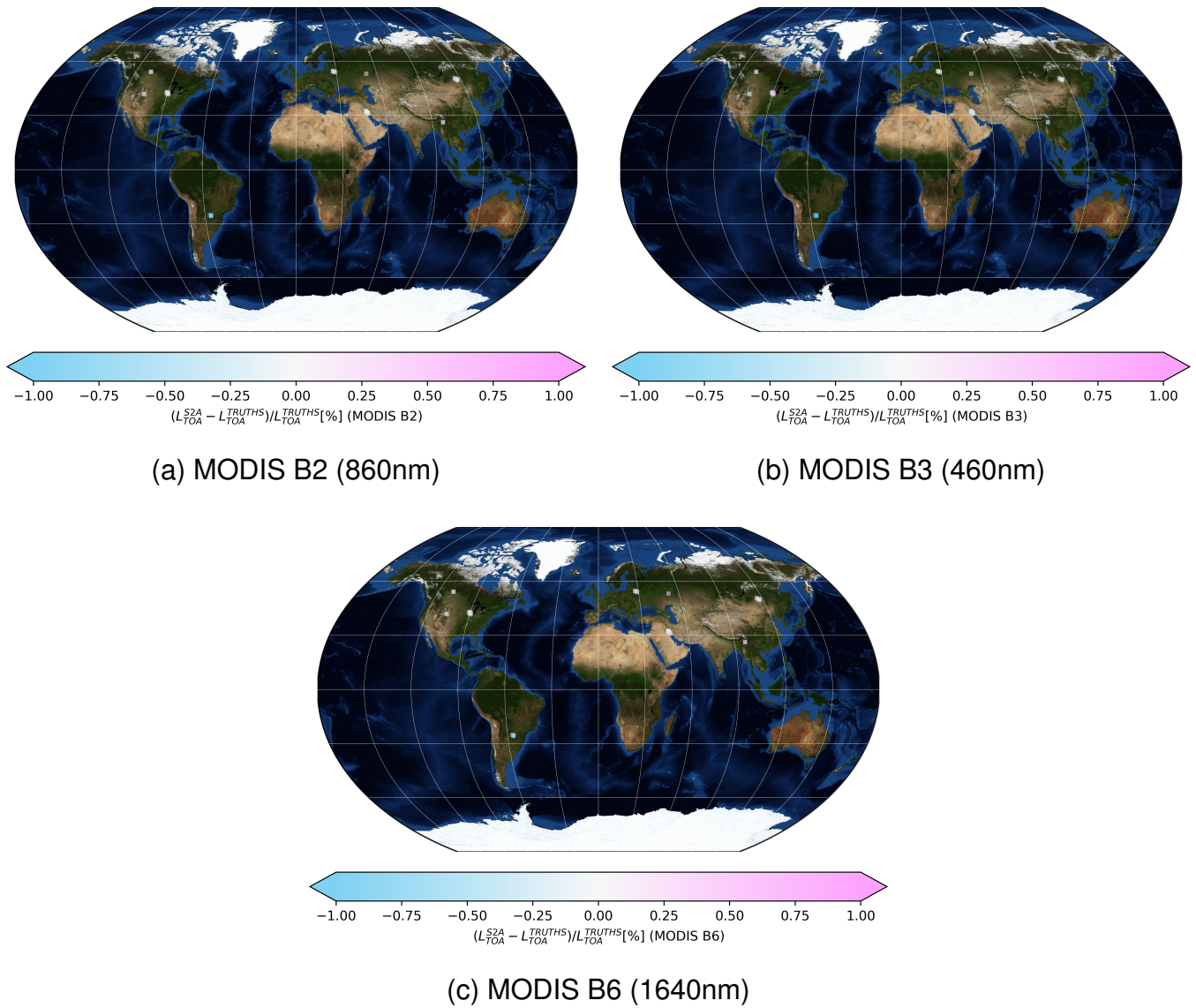


Fig. 11. TRUTHS vs. S2A angular error over the Earth projection considering a *restrictive scenario* for MODIS bands B2 (860nm; Figure 11a), B3 (460nm; Figure 11b) and B6 (1640nm; Figure 11c).

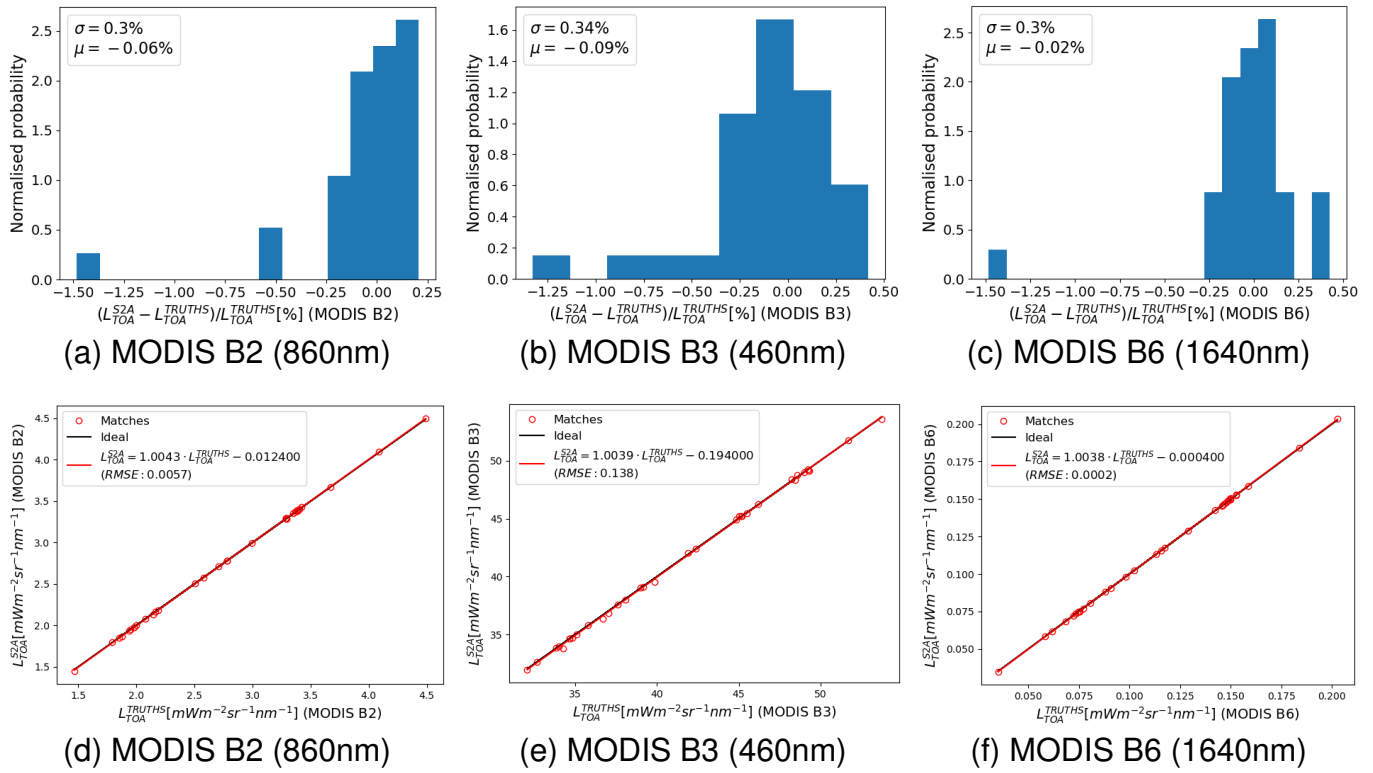


Fig. 12. TRUTHS vs. S2A angular error distribution considering a *restrictive scenario* for MODIS bands B2 (860nm; Figure 12a), B3 (460nm; Figure 12b) and B6 (1640nm; Figure 12c) and radiance regression the same three MODIS bands (Figures 12d, 12e and 12f). The markers in this illustration have been exaggerated for visual purposes as well as a lower colour bar range