

1 **High-resolution geophysical monitoring of moisture accumulation preceding**  
2 **slope movement – a path to improved early warning**

3 **A. Watlet<sup>1,2</sup>, P. Wilkinson<sup>1</sup>, J. Whiteley<sup>3,1</sup>, A. White<sup>1</sup>, S. Uhlemann<sup>4,1</sup>, R. Swift<sup>1</sup>, S. Ouellet<sup>5</sup>,**  
4 **C. Minto<sup>6</sup>, P. Meldrum<sup>1</sup>, L. Jones<sup>1</sup>, D. Gunn<sup>1</sup>, A. Godfrey<sup>6</sup>, B. Dashwood<sup>1</sup>, R. Crickmore<sup>7</sup>,**  
5 **P. Clarkson<sup>6</sup>, J. Boyd<sup>1</sup>, J. Chambers<sup>1</sup>**

6 <sup>1</sup>British Geological Survey, Nottingham, UK

7 <sup>2</sup>Geology and Applied Geology, University of Mons, Belgium

8 <sup>3</sup>AtkinsRéalis, Bristol, UK

9 <sup>4</sup>Lawrence Berkeley National Laboratory, Berkeley, USA

10 <sup>5</sup>University of Calgary, Canada

11 <sup>6</sup>Indeximate, Hinckley, Leicestershire, LE10 1AQA

12 <sup>7</sup>Luna OptaSense

13 Corresponding author: Arnaud Watlet (arnw@bgs.ac.uk)

14 **Peer-review status:**

15 **This is a non peer-reviewed preprint (v1), submitted to *EarthArXiv*.**

16 **The manuscript has been submitted for consideration in**

17 ***Environmental Research Letters*.**

## 18 **Abstract**

19 Slope failures are an ongoing global threat leading to significant numbers of fatalities and  
20 infrastructure damage. Landslide impact on communities can be reduced using efficient early  
21 warning systems to plan mitigation measures and protect elements at risk. This manuscript  
22 presents an innovative geophysical approach to monitoring landslide dynamics, which combines  
23 Electrical Resistivity Tomography (ERT) and low-frequency Distributed Acoustic Sensing  
24 (DAS), and was deployed on a slope representative of many landslides in clay rich lowland  
25 slopes. ERT is used to create detailed, dynamic moisture maps that highlight zones of moisture  
26 accumulation leading to slope instability. The link between ERT derived soil moisture and the  
27 subsequent initiation of slope deformation is confirmed by low-frequency DAS measurements,  
28 which were collocated with the ERT measurements and provide changes in strain at  
29 unprecedented spatiotemporal resolution. Auxiliary hydrological and slope displacement data  
30 support the geophysical interpretation. By revealing critical zones prone to failure, this combined  
31 ERT and DAS monitoring approach sheds new light on landslide mechanisms. This study  
32 demonstrates the advantage of including subsurface geophysical monitoring techniques to  
33 improve landslide early warning approaches, and highlights the importance of relying on  
34 observations from different sources to build effective landslide risk management strategies.

## 35 **1 Introduction**

36 Slope failures are a threat to communities around the globe. They cause significant  
37 damage to critical infrastructure and individual properties and in some cases may lead to loss of  
38 life. In recent history, landslides led to >4500 recorded fatalities per year (Froude & Petley,  
39 2018), and billions of dollars of economic losses (Dilley, 2005; Kirschbaum et al., 2015). Even  
40 non-fatal, minor landslides may have large economic impacts as they affect critical infrastructure  
41 (Emberson et al., 2020). These numbers are set to increase due to climate change and associated  
42 global rise in rainfall intensity, which is a major trigger of landslides (Gariano & Guzzetti, 2016).  
43 While preventing landslides from occurring is impractical due to costs, the associated risks can  
44 be mitigated both at local and regional scales to reduce landslide impacts on society (Lacasse et  
45 al., 2009). A better understanding of the morphology of unstable slopes, and the associated slope  
46 failure mechanisms is key to developing more informed risk management strategies. Monitoring  
47 of unstable slopes, in particular, is an essential component of local landslide Early Warning  
48 Systems (Lo-LEWS) (Maskrey, 2011), which main purpose is to identify precursors of landslide  
49 events (Intrieri et al., 2013) and locate zones that may become unstable due to changes in the  
50 subsurface conditions.

51 Moisture-induced landslides are those triggered by increased soil moisture or  
52 groundwater levels, which raise pore water pressures and hence reduces effective stresses. Basic  
53 Lo-LEWS monitoring approaches mainly integrate surface displacement observations, indicating  
54 ongoing deformation but not detecting the underlying cause. Therefore, Lo-LEWS can benefit  
55 from monitoring subsurface parameters related to the driving factors of slope failure to extend  
56 the effective warning period (Lacroix et al. 2020). Geophysics-based monitoring systems have  
57 emerged as powerful tools to track subsurface conditions of slopes prone to moisture-induced  
58 landslides (Whiteley et al., 2019), increasing the predictive capacity of slope failure (Uhlemann  
59 et al., 2021). Designed to non-invasively image the subsurface, and providing proxies to critical  
60 slope stability properties (e.g. moisture, suction, shear strength), geophysical methods are ideally  
61 equipped to assess the integrity of unstable slopes at various scales (Whiteley et al., 2021).

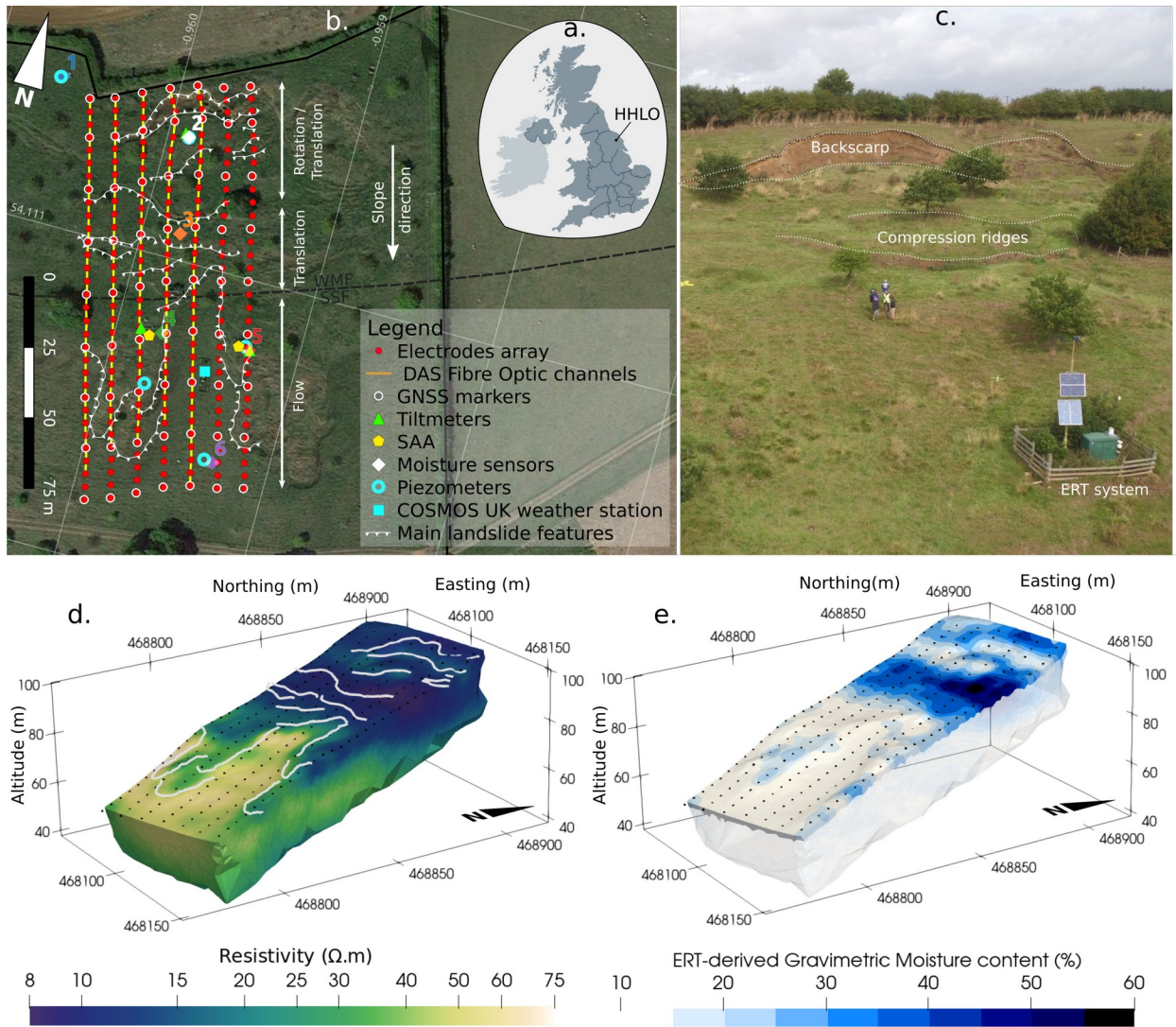
62 Electrical Resistivity Tomography (ERT) has long been used to investigate landslides in  
63 2D or 3D (Jongmans & Garambois, 2007), providing electrical resistivity models linked to the  
64 geology, hydrology and morphology of the landslide. More recently, time-lapse ERT (i.e. in 4D)  
65 has increasingly been applied to monitor landslides (Bièvre et al., 2012; Gance et al., 2016; Hojat  
66 et al., 2019; Lapenna & Perrone, 2022; Lehmann et al., 2013; Perrone et al., 2014; Supper, 2014;  
67 Tsai et al., 2021; Watlet et al., 2023; Whiteley et al., 2023). The main benefits of geoelectrical  
68 monitoring lie in the possibility to link changes in electrical resistivity to changes in subsurface  
69 conditions, mainly moisture (Holmes et al., 2022; Slater & Binley, 2021), coupled with the  
70 maturity of remote monitoring equipment specifically designed for autonomous monitoring of  
71 slope processes (Chambers *et al.* 2022). At the other end of the near-surface geophysics  
72 spectrum, Distributed Acoustic Sensing (DAS) systems have rapidly emerged as novel tools  
73 capable of detecting seismic signals (Dou et al., 2017). More recently, DAS has shown great  
74 potential in the low-frequency domain (<1Hz) to monitor dynamic changes in strain (Crickmore  
75 et al., 2020; Karrenbach et al., 2019).

76 We present, to the best of our knowledge, the first 4D ERT imaging of slope movement  
77 supported by strain measurements from low-frequency DAS, and hydrological and geotechnical  
78 datasets. With this study, we aim to demonstrate the advanced capability to detect precursory  
79 conditions to slope displacement. Incorporating 4D soil moisture data in the feed of information  
80 used to assess slope stability has the potential to improve landslide early warning strategies,  
81 thereby enhancing landslide risk mitigation.

## 82 **2 Site description and methodology**

### 83 **2.1 The Hollin Hill Landslide Observatory (HHLO)**

84 The HHLO (Fig. 1, Chambers et al. 2011; Gunn et al. 2013) in North Yorkshire, UK, was  
85 designed in the mid-2000s as a test site for developing novel geophysical monitoring of unstable  
86 slopes. The site features a moisture-induced, slow-moving landslide, representative of many  
87 clay-rich lowland landslides worldwide. It has a well-documented history of seasonal  
88 reactivation with peaks in movement generally occurring during winter, between December and  
89 March (see Fig. S1 in the Supplementary material). The landslide's morphology largely depends  
90 on the underlying geological structure. The south-facing slope comprises two main geological  
91 units (Lower to Late Jurassic) gently dipping to the North: the Whitby Mudstone Formation  
92 (WMF) and the Staithes Sandstone Formation (SSF). Due to lower permeability and high  
93 plasticity, the WMF slowly creeps over the SSF when reaching elevated moisture contents. This  
94 translational movement mostly occurs in the central part of the slope. In the top part, a complex  
95 rotational failure within the WMF is observed, linked to the mass wasting generated by creeping  
96 downslope (Uhlemann et al. 2017; Boyd et al. 2021). The hydrogeological context of the HHLO  
97 includes the occurrence of perched water tables at shallow depth (Gunn *et al.* 2013) overlying a  
98 deeper regional groundwater table.



99 **Figure 1:** a) Location of Hollin Hill on UK map, b) Map of the HHLO displaying the location of  
 100 the ERT array, fibre optic cable, point sensors (and location number), GNSS markers and main  
 101 landslide features; c) Drone photo highlighting the backscarp and compression ridges of the  
 102 HHLO. d) Resistivity model and e) ERT-derived GMC model for the monitoring baseline (22  
 103 November 2020).

104 Since first deployed in 2008, 4D geoelectrical imaging revealed complex, seasonal  
 105 moisture dynamics in the slope (Uhlemann et al. 2017; Merritt et al. 2018). Preferential  
 106 infiltration and moisture build-up have also been linked with periods of increased movements,  
 107 and evidence of superficial drying processes are associated with surface shrinking and cracking.  
 108 However, properly demonstrating that local zones of elevated moisture content were leading to  
 109 co-located displacement or slope failure has been challenging. One main reason has been the  
 110 challenge of monitoring slope deformation at a spatial and temporal scale comparable to that of  
 111 time-lapse ERT measurements (Kelevitz et al. 2021). Deriving electrode movements from time-  
 112 lapse ERT measurements was successfully developed (Wilkinson et al. 2015, 2016), providing a  
 113 means of tracking large displacements greater than 10% of the electrode spacing. But other

114 techniques providing independent measurement of surface deformation at higher resolution, such  
 115 as strain from low-frequency DAS, ideally complement the toolbox of monitoring techniques  
 116 able to detect minor movements precursory to larger slope failure.

117 Over the years, state-of-the-art sensors have also been deployed at the HHLO to provide  
 118 independent measurements for comparison and interpretation alongside geophysics-based  
 119 monitoring. Clusters of point sensors including shallow soil moisture (at 20 cm and 50 cm bgl),  
 120 matric potential (at 50 cm bgl) and piezometers monitoring water level in shallow and deep  
 121 boreholes are distributed over 6 locations (1-6 in Fig. 1). Ground deformation associated with the  
 122 landslide activity is also tracked via four independent approaches at the HHLO, including  
 123 tiltmeters (at location 2, 4 and 5), Shape Accelerometers Arrays (SAA; Abdoun *et al.* 2013) (at  
 124 location 4 and 5), GNSS marker pegs and repeated LiDAR scans (see Table S1 and Text S3 in  
 125 the Supplementary material for more details; Lague *et al.*, 2013)

## 126 **2.2 Gravimetric Water Content from Electrical Resistivity Tomography**

127 The PRIME system installed since November 2020 at the HHLO is a low-cost and low-  
 128 power ERT instrument designed for remotely monitoring slope condition (Holmes *et al.* 2020).  
 129 ERT measurements are acquired on a scheduled, daily basis and telemetered to remote servers  
 130 through 4G internet. The ERT array comprises seven lines oriented in the slope direction, each  
 131 with 32 electrodes, forming a grid of 224 electrodes with a separation of 9.5 m across the slope  
 132 and 4.75 m along the slope (see Fig. 1). A comparable ERT array layout was installed for a  
 133 decade (2008 – 2019) at the HHLO (Kuras *et al.* 2009), and proved to capture shallow  
 134 hydrological processes throughout the hillslope (Uhlemann *et al.* 2017; Merritt *et al.* 2018). ERT  
 135 time-lapse inversion follows a hybrid inversion scheme mimicking a time-lapse inversion but  
 136 incorporating potential electrode movements as monitored by repeated GNSS surveys of a  
 137 network of ground control points (Uhlemann *et al.* 2016; Boyd *et al.* 2021). Since only one large  
 138 slope displacement event occurred within the time window presented in this manuscript (22  
 139 November 2020 to 30 March 2022), electrode locations have been adapted only once following  
 140 this event. Adjusted electrode locations are derived from inverting the ERT data for electrode  
 141 movements, following a methodology developed in (Wilkinson *et al.* 2015, 2016).

142 In this study, we present ERT monitoring results as soil moisture models. Resistivity  
 143 models are translated into Gravimetric Moisture Content (GMC) models after inversion and  
 144 temperature correction, following the approach by Uhlemann *et al.* (2017), calibrated for the  
 145 HHLO by Merritt *et al.* (2016) using Waxman & Smits (1968) relationships (Fig 1. d-e). The  
 146 calibration was performed on soil and shallow borehole core samples from the SSF and WMF.  
 147 We use separate parameter sets for the WMF and the SSF as in Uhlemann *et al.* (2017). Boyd  
 148 *et al.* (2024) has highlighted that this relationship is likely to be valid only at shallow depths, given  
 149 that Waxman-Smits equation parameters change for deeper, more consolidated rocks. Therefore,  
 150 the GMC models are generated using the relationship developed by Uhlemann *et al.* (2017)  
 151 applied to the first 2 m below the ground surface, which represents the layer above mapped shear  
 152 zones. However, due to the presence of perched water levels at ~2m below ground level (bgl),  
 153 especially in the WMF, most temporal changes in resistivity, and therefore GMC, are expected to  
 154 occur at shallow depth. More detailed on the acquisition and processing of the ERT data is  
 155 available in Text S1 (Brunet *et al.*, 2010; Keller & Frischknecht, 1966; Mwakanyamale *et al.*,  
 156 2012)

## 157 **2.3 Strain from low-frequency Distributed Acoustic Sensing**

158 We rely on strain measurements acquired by a DAS system along a fibre optic cable  
159 deployed at the HHLO (Clarkson *et al.* 2021). The DAS system consists of a Luna Optasense  
160 ODH-F interrogator unit which transmits coherent laser pulses within the fibre, and acts as a  
161 distributed interferometer. Any strain disturbance to the fibre changes the optical phase of the  
162 backscattered light (Bao & Chen, 2012; Bao & Wang, 2021) and can be recorded. A low-pass  
163 filter at 1 Hz is applied to the DAS data and optical phase data are converted to units of strain.  
164 The fibre was buried at ~10 cm bgl within narrow trenches along the slope direction to form six  
165 lines, five of which are co-located with the easternmost five lines of the ERT array. The strain  
166 measurements derived from low-frequency DAS are sampled with a 1 m spatial interval over a  
167 gauge length of 4 m, which defines the spatial resolution (detailed processing in Text S2 of the  
168 Supplementary material). In this study, we investigate change in strain averaged at daily time  
169 intervals on two periods overlapping the ERT dataset from 22 November 2020 to 30 January  
170 2021 (70 days), and then from 22 November 2021 to 28 February 2022 (100 days), each focusing  
171 on the wettest part of the season. Data are expressed as cumulative change in microstrain ( $\mu\epsilon$ )  
172 with respect to a baseline set at the beginning of each period.

### 173 **3 Results and discussion**

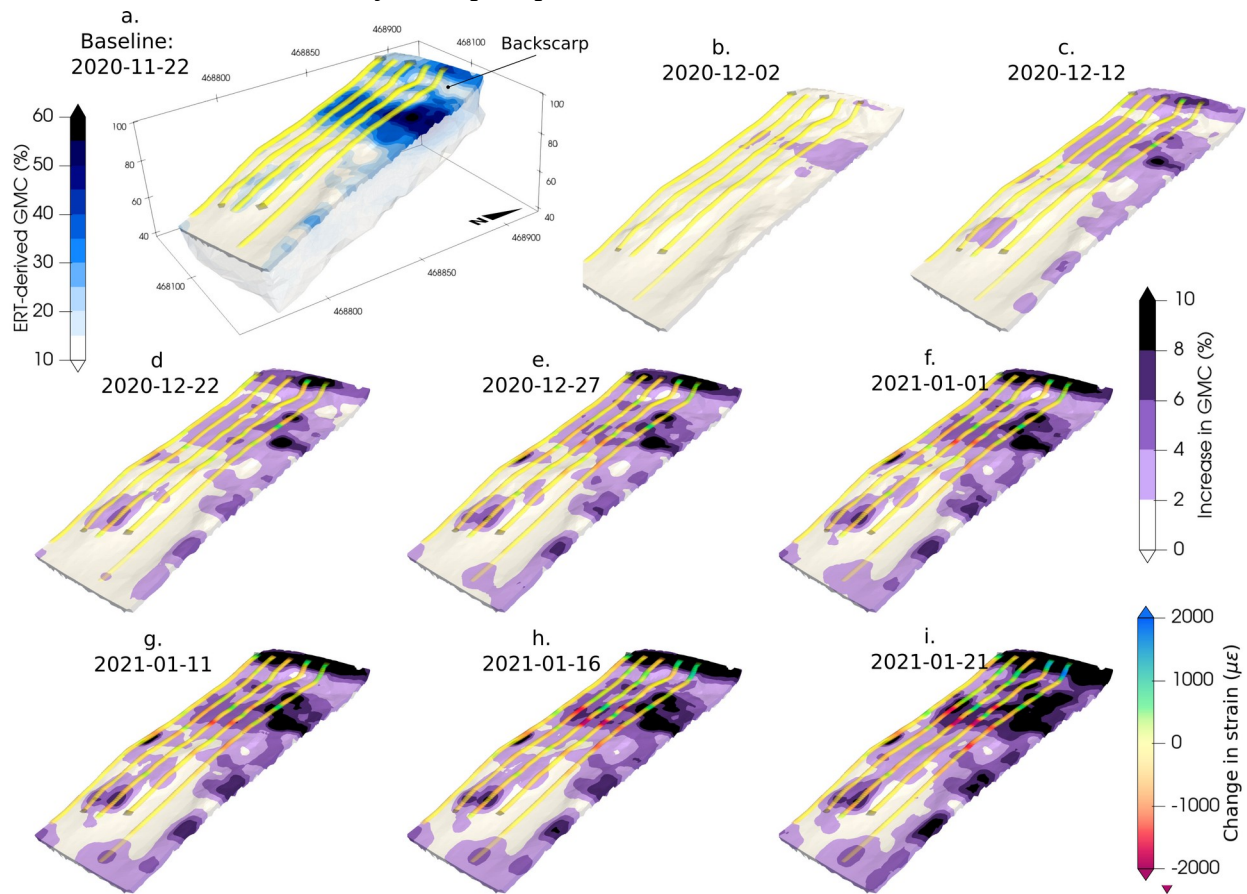
#### 174 **3.1 Moisture accumulation preceding landslide reactivation**

175 The ERT-derived soil moisture dataset of this study starts on 22 November 2020.  
176 Increase in GMC is displayed at regular intervals before the main slope displacement event on  
177 20-21 January 2021 (Fig. 2). This increase is most pronounced in the WMF formation, especially  
178 above the backscarp and in the area of the rotational slip, with localised increases higher than  
179 10% GMC. This general moisture trend is corroborated by the network of soil moisture sensors.  
180 The backscarp itself stays relatively dry, contrasting with the zone directly above and below. The  
181 steepness of the scarp combined with locally lower permeability near the slip plane favors  
182 surface run-off processes, hindering in-situ water infiltration. The resistivity models in the  
183 backscarp region also show preferential flow between the zone above the scarp and the flatter  
184 region at the toe of the scarp, favoring moisture accumulation (see Fig S2 in the Supplementary  
185 material).

186 Deformation data show that the 2021 reactivation started with two minor precursory  
187 displacement events (in the order of 1 mm recorded by the shallowest SAA at 10 cm bgl)  
188 following rainfall events, on 27 December 2020 and 14 January 2021 (Fig. 3). The first precursor  
189 event seems to have predominantly affected the middle part of the slope, where change in  
190 microstrain indicates compression in the mid-slope ridges (Fig. 4). The second precursory event  
191 followed snowfall and is documented using strain data from the low-frequency DAS at 1 minute  
192 sampling frequency in Ouellet *et al.* (2024). It started with mid-slope deformation, then  
193 propagated upslope to the backscarp. The main deformation occurred on 20-21 January 2021, as  
194 Storm Christophe hit the UK. Deformation was mainly confined to the top part of the slope  
195 underneath the backscarp, as corroborated by the microstrain data (Fig. 3c), with two main  
196 transverse zones of compressions on existing ridges, and extension in the backscarp. The top-  
197 slope tiltmeter recorded a tilt step of  $0.3^\circ$  in the slope direction, indicating rotational processes.  
198 The mid-slope tiltmeters showed no change, although the western SAA recorded ~12 mm  
199 horizontal displacement, indicating minor translational movement mid-slope (Fig. 3b). Following  
200 this main event, two minor events were visible in the tiltmeters and SAA data on 29 January



201 2021 and 19 February 2021, with respectively 2 mm and 1 mm as recorded by the SAA, as well  
 202 as 0.04° and 0.02° recorded by the top-slope tiltmeter.



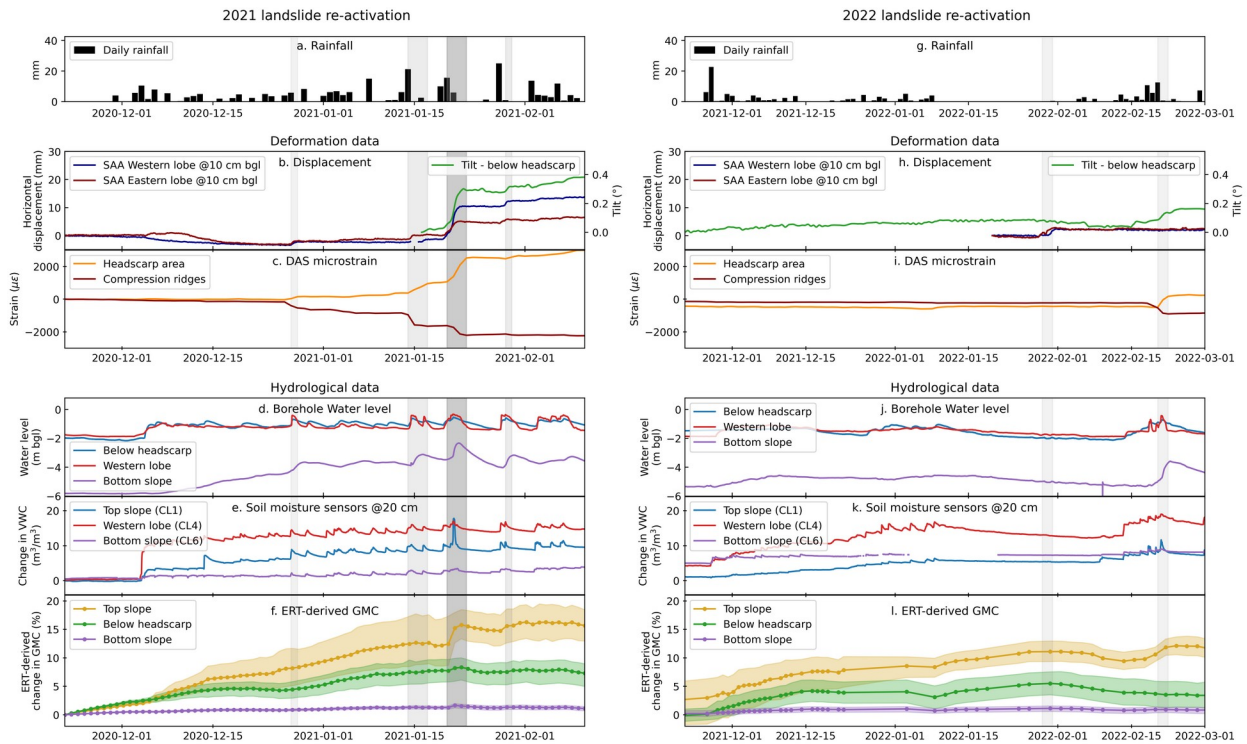
203 **Figure 2:** ERT-derived Gravimetric Moisture Content (GMC) model for the baseline on 22  
 204 November 2020 (a), and models of relative increase in GMC with respect to the baseline  
 205 displayed on a selection of time-steps (b-i). Recorded changes in microstrain are also shown.

206 In 2022, the landslide remained comparatively stable, with only a few minor deformation  
 207 events. Each observed deformation in 2022 is visible in only one of the datasets from DAS (Fig.  
 208 3i), SAA, or the top-slope tilt-meter (Fig. 3h), indicating much smaller and more localized  
 209 deformation than in 2021. This is confirmed by the GNSS surveys and LIDAR scans which  
 210 detected no noticeable surface topography variation.

### 211 3.2 Landslide mechanism

212 A joint analysis of vertical displacement (from LIDAR surveys), horizontal displacement (from  
 213 GNSS markers), tilt data and downslope strain (from low-frequency DAS) during the 20-21  
 214 January event highlights rotational movement mainly in a small area underneath the backscarp,  
 215 where ground elevation increased below a zone of extension on the fiber. This area coincides  
 216 with the GNSS marker with the highest horizontal displacement, confirming a combination of  
 217 translational and rotational movement, limited to the top half of the slope. Despite a lack of  
 218 temporal resolution in the geophysics-based data, comparing tilt change at the top of the slope  
 219 and displacement data from the central slope SAA suggests similar dynamics as described by  
 220 Ouellet et al. (2024), with central slope destabilization and horizontal displacement propagating

221 and amplifying upslope, including a rotational component when reaching the backscarp zone.  
 222 During the 14 January precursory event, high temporal resolution low-frequency DAS (Ouellet  
 223 et al. 2024) showed that this retrogressional behavior propagated from the central slope to the  
 224 backscarp at  $\sim 1.7$  m/h. Similar retrogressive dynamics were also identified at larger timescales  
 225 by large mobilization of the flow lobes in 2013 followed by the development of the backscarp in  
 226 2016.



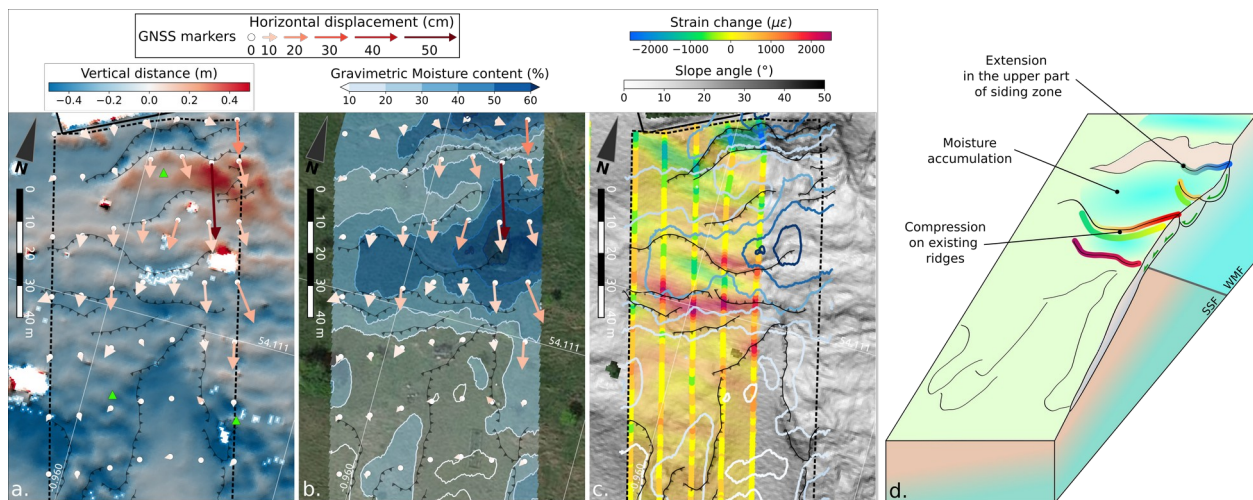
227 **Figure 3:** Summary of the geophysical, hydrological and displacement datasets acquired during the  
 228 2021 (a-f) and 2022 (g-l) landslide reactivation periods (November 2020 to February 2021,  
 229 and November 2021 to March 2022). Figures display rainfall (a, g), surface displacement (b, h),  
 230 DAS microstrain (c, i) using channels highlighted in Fig. S3, borehole water level (d, j), soil  
 231 moisture at 20 cm bgl (e, k), ERT-derived GMC (f, l). Grey boxes indicate periods of minor  
 232 (light grey) and major (dark grey) deformation event.

233 The top-slope tiltmeter showed significant downslope tilt starting on 20 January 2021  
 234 around 20:00 UTC, peaking between 02:00 and 03.00 UTC on 21 January 2021, coinciding with  
 235 a peak in moisture content at the top of the slope. Peak displacement lasted 15 hours, as inferred  
 236 from the tilt data. This event cannot be related to a particularly extreme rainfall event, with only  
 237 10 and 15.6 mm on 19 and 20 January. Rainfall on 20 January was low but sustained, becoming  
 238 more intense towards the evening with 9.59 mm recorded over 4 hours starting from 20:00,  
 239 peaking at 22:00. Despite the daily rainfall being unremarkable, this 4-hour event was the most  
 240 intense since summer 2020 and the second highest over winter 2021, linked to smaller  
 241 movements recorded by the SAA and tiltmeters.

242 However, the main deformation event and precursors occurred in the area with the  
 243 highest moisture content ( $>40\%$  GMC and up to  $55\%$  GMC) as established by the ERT  
 244 monitoring, and the highest increase in moisture with respect to the baseline ( $> 10\%$  GMC, Fig.  
 245 2). This confirms elevated soil moisture as the driving factor for ground displacement, with



246 WMF mudstone material potentially reaching a local liquid limit. GMC higher than 55%  
 247 matches with liquid limits previously measured on WMF soil samples (Merritt et al. 2014) and  
 248 fits well with previously obtained thresholds for landslide activation of 49% (Uhlemann et al.,  
 249 2017). Data from moisture sensors and piezometers show high peaks in moisture and water level  
 250 starting at 22:00, which are hard to explain solely by local rainfall. As a consequence of Storm  
 251 Christophe hitting the UK, heavy rain with spatially varying intensity was recorded in Northern  
 252 England (Met Office, 2021). It is likely that the event was triggered by surface or subsurface run-  
 253 off from that plateau upslope, temporarily saturating parts of the hillslope already at high  
 254 moisture levels. Rain rate data from NIMROD MET-Office rainfall radar (over 1 km<sup>2</sup> cells and 5  
 255 min intervals; (Met Office, 2003)) reveals that more intense rainfall occurred just north of the  
 256 site, on the plateau directly upslope of the hill.



257 **Figure 4:** Maps showing a) vertical displacement computed from LiDAR scans from November  
 258 2020 and September 2021, and horizontal displacement on the network of GNSS markers  
 259 between 15 January 2021 and 20 February 2021; b) ERT-derived GMC following peak  
 260 movement in landslide reactivation 2021 (22 January 2021) as compared to GNSS markers  
 261 displacement; c) Strain change recorded on the fibre and interpolated, and compared to GMC  
 262 contour lines following peak movement (22 January 2021); d) Sketch describing the landslide  
 263 dynamics at the HHLO and the geophysical observations on the ERT and DAS monitoring  
 264 systems.

### 265 3.3 Combining ERT and low-frequency DAS and implications for landslide early 266 warning

267 This study highlights the complementarity of ERT and low-frequency DAS to reveal the  
 268 mechanisms leading to slope deformation with unprecedented detail. The ERT-based moisture  
 269 imaging provides time-lapse snapshots of the subsurface with high spatial resolution, setting the  
 270 moisture condition context throughout the slope. Despite the 3D ERT-based GMC models being  
 271 displayed on a relatively fine mesh, the overall resolution depends on the electrode separation,  
 272 which is relatively sparse at the HHLO (see Sect. 2). This layout has the benefit of sampling a  
 273 large portion of the hillslope, while limiting the capability of the system to image subtle shallow  
 274 resistivity changes but providing spatially continuous images at depths closer to the expected slip  
 275 surface. This is precisely where the complementarity with the low-frequency DAS is most  
 276 powerful. By providing strain data at shallow depth (~10 cm), with high spatial resolution along

277 the FO cable, i.e. in the slope direction, it provides direct and localised information on slope  
278 stability in the near surface where the ERT system has poor sensitivity.

279 The ERT-derived moisture models accurately delineate zones of interest (Fig. 4d) where  
280 moisture slowly builds up, and the WMF clay materials are above the plastic limit, locally  
281 reaching the liquid limit. Slope deformation occurred in an area that showed elevated moisture  
282 contents in the weeks prior to movement. The low-frequency DAS complements these  
283 observations by identifying strain changes at the edge of the zones of elevated moisture, as minor  
284 displacement occurs. This demonstrates that calibrated time-lapse ERT providing spatio-  
285 temporal soil moisture dynamics, effectively validates elevated soil moisture as the cause of  
286 slope movement, and identifies zones where landslide susceptibility increases. DAS strain data  
287 then sheds light on how the elevated moisture translates in terms of slope stability. Crucially, the  
288 co-location of these measurements allows time-lapse imaging of holistic slope processes that  
289 cannot be practicably replicated using point sensors nor rainfall data alone. This makes it  
290 extremely valuable for both sources of geophysical information to jointly feed a new generation  
291 of Lo-LEWS looking at changes in co-related material properties (Bogaard and Greco 2018;  
292 Segoni et al. 2018; Whiteley et al. 2021), with a particular interest in the surveillance of critical  
293 infrastructures, such as long linear assets (e.g. railway cutting, flood embankment, etc.).

294 Datasets acquired at the HHLO prior to the relatively minor slope deformation event in  
295 2021 also help to improve the definition of thresholds that can be used to issue Lo-LEWS alarms  
296 for future, potentially larger events. For instance, no significant movement was recorded in 2022.  
297 Comparing the ERT-derived moisture models from January 2021 and during winter 2022 shows  
298 that moisture was at lower levels throughout the slope, particularly in the top of the slope where  
299 zones with the highest moisture contents remained below the thresholds of the January 2021  
300 event (Figs. 3f, 3l).

#### 301 **4 Summary**

302 This study presents the deployment of a long-term ERT and strain monitoring from low  
303 frequency DAS at the Hollin Hill Landslide Observatory (HHLO), together with a network of  
304 hydrological and geotechnical sensors and techniques. It represents, to the best of our  
305 knowledge, the first combination of ERT and DAS monitoring on an active slow-moving  
306 landslide. Through a robust and already well documented methodology, daily 3D electrical  
307 resistivity models are transformed into shallow soil moisture models at high spatial resolution.  
308 These reveals zones of moisture accumulation in the top part of the slope, which eventually led  
309 to slope movement, with a peak in January 2021, as revealed with an unprecedented spatial  
310 resolution by changes in strain measured by the low-frequency DAS along a fibre optic cable co-  
311 located with the ERT array.

312 Results from this interdisciplinary approach highlight the efficacy of integrating multiple  
313 geophysical methods together to enhance the observability and understanding of landslide  
314 mechanisms. A notable strength of this approach lies in the capability of ERT, via high-spatial  
315 resolution imaging, to delineate zones of elevated moisture content, which can be interpreted as  
316 precursory indicators of slope instability. Unlike point sensors, which do not provide spatially  
317 continuous measurements of subsurface properties, the ERT and DAS monitoring capability  
318 described in this study can provide high-resolution spatiotemporal images that allow a holistic  
319 assessment of subsurface processes at the whole-slope scale. This study offers novel ways to  
320 address the critical need to advance the observational capability in slope stability analysis, which

321 will inevitably lead to improved early warning systems and to better informed risk management  
322 strategies, and therefore enhance the resilience of societies to landslide hazards worldwide.

### 323 **Acknowledgments**

324 BGS authors publish with the permission of the Executive Director, British Geological Survey  
325 (UKRI-NERC). We would like to thank Josie Gibson, Frances Standen and James Standen for  
326 their continued support at Hollin Hill. We also thank Brendon Purnell from Luna Optasense, and  
327 members of Environmental & Engineering Geophysics at BGS, including Mihai Cimpoiasu,  
328 Harry Harrison, Jessica Holmes, Cornelia Inauen, Oliver Kuras and Dave Morgan for their help  
329 and support. Processed data from ERT, low-frequency DAS, soil moisture sensors, tilt-meters,  
330 Shape Accelerometer Arrays, LiDAR scans, GNSS surveys are available at Zenodo via  
331 <https://doi.org/10.5281/zenodo.13118623> with Creative Commons Attribution 4.0 International  
332 license (British Geological Survey, 2024). ERT data were pre-processed using Pandas  
333 (McKinney et al., 2010), and Resipy (Blanchy et al, 2020; <https://resipy.org>), inversions were  
334 performed using E4D (Johnson et al., 2010; <https://www.pnnl.gov/projects/e4d>). Figures were  
335 created using Matplotlib (Hunter et al., 2007); Paraview (Ahrens et al., 2005), Qgis and  
336 InkScape.

337

### 338 **References**

- 339 Abdoun, T., Bennett, V., Desrosiers, T., Simm, J. & Barendse, M., 2013. Asset Management and  
340 Safety Assessment of Levees and Earthen Dams Through Comprehensive Real-Time  
341 Field Monitoring. *Geotech Geol Eng*, **31**, 833–843. doi:10.1007/s10706-012-9569  
342 Ahrens, J., Geveci, B., Law, C., Hansen, C., & Johnson, C. (2005). Paraview: An end-user tool  
343 for large-data visualization. *The visualization handbook*, 717, 50038-1.  
344 Bao, X., & Chen, L. (2012). Recent progress in distributed fiber optic sensors. *Sensors*, *12*(7),  
345 pp.8601-8639.  
346 Bao, X., & Wang, Y. (2021). Recent Advancements in Rayleigh Scattering-Based Distributed  
347 Fiber Sensors. *Advanced Devices & Instrumentation*, 2021, 2021/8696571.  
348 <https://doi.org/10.34133/2021/8696571>  
349 Bièvre, G., Jongmans, D., Winiarski, T., & Zumbo, V. (2012). Application of geophysical  
350 measurements for assessing the role of fissures in water infiltration within a clay  
351 landslide (Trièves area, French Alps). *Hydrological Processes*, *26*(14), 2128-2142.  
352 Blanchy, G., Saneiyani, S., Boyd, J., McLachlan, P. and Binley, A., 2020. ResIPy, an intuitive  
353 open source software for complex geoelectrical inversion/modeling. *Computers &*  
354 *Geosciences*, *137*, p.104423.  
355 Boyd, J., Chambers, J., Wilkinson, P., Peppas, M., Watlet, A., Kirkham, M., Jones, L., *et al.*,  
356 (2021). A linked geomorphological and geophysical modelling methodology applied to  
357 an active landslide. *Landslides*, 1–16, Springer.

- 358 Boyd, J. P., Binley, A., Wilkinson, P., Holmes, J., Bruce, E., & Chambers, J. (2024). Practical  
359 considerations for using petrophysics and geoelectrical methods on clay rich landslides.  
360 *Engineering Geology*, 334, 107506.
- 361 British Geological Survey. (2024). Data used in manuscript "High-resolution geophysical  
362 monitoring of moisture accumulation preceding slope movement – a path to improved  
363 early warning". <https://doi.org/10.5281/zenodo.1311862>
- 364 Brunet, P., Clément, R., & Bouvier, C. (2010). Monitoring soil water content and deficit using  
365 Electrical Resistivity Tomography (ERT) – A case study in the Cevennes area, France.  
366 *Journal of Hydrology*, 380(1–2), 146–153. <https://doi.org/10.1016/j.jhydrol.2009.10.032>
- 367 Chambers, J.E., Wilkinson, P.B., Kuras, O., Ford, J.R., Gunn, D.A., Meldrum, P.I., Pennington,  
368 C.V.L., *et al.*, (2011). Three-dimensional geophysical anatomy of an active landslide in  
369 Lias Group mudrocks, Cleveland Basin, UK. *Geomorphology*, 125, 472–484.  
370 [doi:10.1016/j.geomorph.2010.09.017](https://doi.org/10.1016/j.geomorph.2010.09.017)
- 371 Chambers, J., Holmes, J., Whiteley, J., Boyd, J., Meldrum, P., Wilkinson, P., Kuras, O., Swift,  
372 R., Harrison, H., Glendinning, S., Stirling, R., Huntley, D., Slater, N. & Donohue, S.  
373 (2022). Long-term geoelectrical monitoring of landslides in natural and engineered  
374 slopes. *The Leading Edge*, 41, 768-776. [10.1190/tle41110768.1](https://doi.org/10.1190/tle41110768.1)
- 375 Clarkson, P., Crickmore, R., Godfrey, A., Minto, C., Purnell, B., Gunn, D., Dashwood, B., *et al.*,  
376 (2021). Ground Condition Monitoring of a Landslide using Distributed Rayleigh Sensing.  
377 *EAGE GeoTech 2021 Second EAGE Workshop on Distributed Fibre Optic Sensing*, Vol.  
378 2021, pp. 1–5, European Association of Geoscientists & Engineers.
- 379 Crickmore, R., Godfrey, A. & Minto, C., (2020). Temperature and Strain Separation from a  
380 Distributed Rayleigh System. *EAGE Workshop on Fiber Optic Sensing for Energy*  
381 *Applications in Asia Pacific*, Vol. 2020, pp. 1–4, European Association of Geoscientists  
382 & Engineers.
- 383 Dilley, M. (2005). *Natural disaster hotspots: a global risk analysis* (Vol. 5). World Bank  
384 Publications.
- 385 Dou, S., Lindsey, N., Wagner, A.M., Daley, T.M., Freifeld, B., Robertson, M., Peterson, J., *et*  
386 *al.*, (2017). Distributed acoustic sensing for seismic monitoring of the near surface: A  
387 traffic-noise interferometry case study. *Scientific reports*, 7, 1–12, Nature Publishing  
388 Group.
- 389 Emberson, R., Kirschbaum, D. & Stanley, T., (2020). New global characterization of landslide  
390 exposure. *Natural Hazards and Earth System Sciences Discussions*, 2020, 1–21,  
391 Göttingen, Germany.
- 392 Froude, M.J. & Petley, D.N., (2018). Global fatal landslide occurrence from 2004 to 2016.  
393 *Natural Hazards and Earth System Sciences*, 18, 2161–2181, Copernicus GmbH.
- 394 Gance, J., Malet, J.-P., Supper, R., Saille, P., Ottowitz, D. & Jochum, B., (2016). Permanent  
395 electrical resistivity measurements for monitoring water circulation in clayey landslides.  
396 *Journal of Applied Geophysics*, 126, 98–115. [doi:10.1016/j.jappgeo.2016.01.011](https://doi.org/10.1016/j.jappgeo.2016.01.011)
- 397 Gariano, S.L. & Guzzetti, F., (2016). Landslides in a changing climate. *Earth-Science Reviews*,  
398 162, 227–252, Elsevier.

- 399 Gunn, D.A., Chambers, J.E., Hobbs, P.R.N., Ford, J.R., Wilkinson, P.B., Jenkins, G.O. &  
400 Merritt, A., (2013). Rapid observations to guide the design of systems for long-term  
401 monitoring of a complex landslide in the Upper Lias clays of North Yorkshire, UK.  
402 *Quarterly Journal of Engineering Geology and Hydrogeology*, **46**, 323–336,  
403 GeoScienceWorld.
- 404 Hojat, A., Arosio, D., Ivanov, V.I., Longoni, L., Papini, M., Scaioni, M., Tresoldi, G. and Zanzi,  
405 L., (2019). Geoelectrical characterization and monitoring of slopes on a rainfall-triggered  
406 landslide simulator. *Journal of Applied Geophysics*, *170*, p.103844.
- 407 Holmes, J., Chambers, J., Meldrum, P., Wilkinson, P., Boyd, J., Williamson, P., Huntley, D., *et*  
408 *al.*, (2020). Four-dimensional electrical resistivity tomography for continuous, near-real-  
409 time monitoring of a landslide affecting transport infrastructure in British Columbia,  
410 Canada. *Near Surface Geophysics*, Wiley Online Library.
- 411 Holmes, J., Chambers, J., Wilkinson, P., Meldrum, P., Cimpoiașu, M., Boyd, J., Huntley, D., *et*  
412 *al.*, (2022). Application of petrophysical relationships to electrical resistivity models for  
413 assessing the stability of a landslide in British Columbia, Canada. *Engineering Geology*,  
414 106613, Elsevier.
- 415 Hunter, J. D. (2007). Matplotlib: A 2D graphics environment. *Computing in science &*  
416 *engineering*, *9*(03), 90-95.
- 417 Intrieri, E., Gigli, G., Casagli, N. & Nadim, F., (2013). Brief communication" Landslide Early  
418 Warning System: toolbox and general concepts". *Natural hazards and earth system*  
419 *sciences*, **13**, 85–90, Copernicus GmbH.
- 420 Johnson, T.C., Versteeg, R.J., Ward, A., Day-Lewis, F.D. & Revil, A., (2010). Improved  
421 hydrogeophysical characterization and monitoring through high performance electrical  
422 geophysical modeling and inversion. *Geophysics*, **75**, WA27–WA41.
- 423 Jongmans, D. & Garambois, S., (2007). Geophysical investigation of landslides: a review.  
424 *Bulletin de la Société géologique de France*, **178**, 101–112.
- 425 Karrenbach, M., Cole, S., Ridge, A., Boone, K., Kahn, D., Rich, J., Silver, K., *et al.*, (2019).  
426 Fiber-optic distributed acoustic sensing of microseismicity, strain and temperature during  
427 hydraulic fracturing. *Geophysics*, **84**, D11–D23, Society of Exploration Geophysicists.
- 428 Keller, G. V., & Frischknecht, F. C. (1966). Electrical methods in geophysical prospecting  
429 Kirschbaum, D., Stanley, T. & Zhou, Y., 2015. Spatial and temporal analysis of a global  
430 landslide catalog. *Geomorphology*, **249**, 4–15, Elsevier.
- 431 Kuras, O., Pritchard, J.D., Meldrum, P.I., Chambers, J.E., Wilkinson, P.B., Ogilvy, R.D. &  
432 Wealthall, G.P., (2009). Monitoring hydraulic processes with automated time-lapse  
433 electrical resistivity tomography (ALERT). *Comptes Rendus Geoscience*, **341**, 868–885.
- 434 Lacasse, S., Nadim, F., Lacasse, S. & Nadim, F., (2009). Landslide Risk Assessment and  
435 Mitigation Strategy. in *Landslides – Disaster Risk Reduction*, pp. 31–61, eds. Sassa, K. &  
436 Canuti, P., Springer Berlin Heidelberg. Doi:10.1007/978-3-540-69970-5\_3
- 437 Lacroix, P., Handwerger, A. L., & Bièvre, G. (2020). Life and death of slow-moving landslides.  
438 *Nature Reviews Earth & Environment*, *1*(8), 404-419.



- 439 Lague, D., Brodu, N. & Leroux, J., (2013). Accurate 3D comparison of complex topography  
440 with terrestrial laser scanner: Application to the Rangitikei canyon (N-Z). *ISPRS Journal*  
441 *of Photogrammetry and Remote Sensing*, **82**, 10–26. doi:10.1016/j.isprsjprs.2013.04.009
- 442 Lapenna, V. & Perrone, A., (2022). Time-lapse electrical resistivity tomography (TL-ERT) for  
443 landslide monitoring: Recent advances and future directions. *Applied Sciences*, **12**, 1425,  
444 MDPI.
- 445 Lehmann, P., Gambazzi, F., Suski, B., Baron, L., Askarinejad, A., Springman, S.M., Holliger,  
446 K., *et al.*, (2013). Evolution of soil wetting patterns preceding a hydrologically induced  
447 landslide inferred from electrical resistivity survey and point measurements of volumetric  
448 water content and pore water pressure. *Water Resources Research*, **49**, 7992–8004, Wiley  
449 Online Library.
- 450 Maskrey, A., (2011). Revisiting community-based disaster risk management. *Environmental*  
451 *Hazards*, **10**, 42–52, Taylor & Francis.
- 452 McKinney, W., van der Walt, S., & Millman, J. (2010). Proceedings of the 9th Python in Science  
453 Conference.
- 454 Merritt, A.J., Chambers, J.E., Murphy, W., Wilkinson, P.B., West, L.J., Gunn, D.A., Meldrum,  
455 P.I., *et al.*, (2014). 3D ground model development for an active landslide in Lias  
456 mudrocks using geophysical, remote sensing and geotechnical methods. *Landslides*, **11**,  
457 537–550. doi:10.1007/s10346-013-0409-1
- 458 Merritt, A.J., Chambers, J.E., Murphy, W., Wilkinson, P.B., West, L.J., Uhlemann, S., Meldrum,  
459 P.I., *et al.*, (2018). Landslide activation behaviour illuminated by electrical resistance  
460 monitoring: Landslide Activation Behaviour. *Earth Surface Processes and Landforms*,  
461 **43**, 1321–1334. doi:10.1002/esp.4316
- 462 Merritt, A.J., Chambers, J.E., Wilkinson, P.B., West, L.J., Murphy, W., Gunn, D. & Uhlemann,  
463 S., (2016). Measurement and modelling of moisture—electrical resistivity relationship of  
464 fine-grained unsaturated soils and electrical anisotropy. *Journal of Applied Geophysics*,  
465 **124**, 155–165. doi:10.1016/j.jappgeo.2015.11.005
- 466 Met Office, (2003). 1 km Resolution UK Composite Rainfall Data from the Met Office Nimrod  
467 System. NCAS British Atmospheric Data Centre. Retrieved from  
468 <https://catalogue.ceda.ac.uk/uuid/27dd6ffba67f667a18c62de5c3456350>
- 469 Met Office, (2021). Daily Weather Summary 2021. Retrieved from  
470 [https://digital.nmla.metoffice.gov.uk/IO\\_e9deeb04-8105-4f31-94d6-7d94c00b3c21/](https://digital.nmla.metoffice.gov.uk/IO_e9deeb04-8105-4f31-94d6-7d94c00b3c21/)
- 471 Mwakanyamale, K., Slater, L., Binley, A., & Ntarlagiannis, D. (2012). Lithologic imaging using  
472 complex conductivity: Lessons learned from the Hanford 300 Area. *Geophysics*, **77**(6),  
473 E397–E409.
- 474 Ouellet, S.M., Dettmer, J., Lato, M.J., Cole, S., Hutchinson, D.J., Karrenbach, M., Dashwood,  
475 B., Chambers, J.E. and Crickmore, R., 2024. Previously hidden landslide processes  
476 revealed using distributed acoustic sensing with nanostrain-rate sensitivity. *Nature*  
477 *Communications*, **15**(1), p.6239.
- 478 Perrone, A., Piscitelli, S. & Lapenna, V., 2017. Electrical resistivity tomographies for landslide  
479 monitoring: a review. *Berichte Geol*, **93**, 129–134.

- 480 Slater, L. & Binley, A., (2021). Advancing hydrological process understanding from long-term  
481 resistivity monitoring systems. *Wiley Interdisciplinary Reviews: Water*, **8**, e1513, Wiley  
482 Online Library.
- 483 Supper, R., Ottowitz, D., Jochum, B., Kim, J.H., Römer, A., Baron, I., Pfeiler, S., Lovisolo, M.,  
484 Gruber, S. and Vecchiotti, F., (2014). Geoelectrical monitoring: an innovative method to  
485 supplement landslide surveillance and early warning. *Near Surface Geophysics*, **12**(1),  
486 pp.133-150.
- 487 Tsai, W.-N., Chen, C.-C., Chiang, C.-W., Chen, P.-Y., Kuo, C.-Y., Wang, K.-L., Lin, M.-L., *et*  
488 *al.*, (2021). Electrical resistivity tomography (ERT) monitoring for landslides: Case study  
489 in the lantai area, yilan taiping mountain, northeast taiwan. *Frontiers in Earth Science*, **9**,  
490 737271, Frontiers Media SA.
- 491 Uhlemann, S., Smith, A., Chambers, J., Dixon, N., Dijkstra, T., Haslam, E., Meldrum, P., *et al.*,  
492 (2016). Assessment of ground-based monitoring techniques applied to landslide  
493 investigations. *Geomorphology*, **253**, 438–451. doi:10.1016/j.geomorph.2015.10.027
- 494 Uhlemann, S., Chambers, J., Meldrum, P., McClure, P., & Dafflon, B. (2021). Geophysical  
495 monitoring of landslides—a step closer towards predictive understanding?. *Understanding*  
496 *and Reducing Landslide Disaster Risk: Volume 3 Monitoring and Early Warning 5th*, 85-  
497 91.
- 498 Uhlemann, Sebastian, Chambers, J., Wilkinson, P., Maurer, H., Merritt, A., Meldrum, P., Kuras,  
499 O., *et al.*, (2017). Four-dimensional imaging of moisture dynamics during landslide  
500 reactivation. *Journal of Geophysical Research: Earth Surface*, **122**, 398–418.  
501 doi:10.1002/2016JF003983
- 502 Watlet, A., Thirugnanam, H., Singh, B., Kumar M., N., Brahmanandan, D., Inauen, C., Swift, R.,  
503 *et al.*, (2023). 4D electrical resistivity to monitor unstable slopes in mountainous tropical  
504 regions: an example from Munnar, India. *Landslides*, **20**, 1031–1044.  
505 doi:10.1007/s10346-023-02029-3
- 506 Waxman, M.H. & Smits, L.J.M., (1968). Electrical conductivities in oil-bearing shaly sands.  
507 *Society of Petroleum Engineers Journal*, **8**, 107–122.
- 508 Whiteley, J. S., Chambers, J. E., Uhlemann, S., Wilkinson, P. B. & Kendall, J. M. (2019).  
509 Geophysical Monitoring of Moisture-Induced Landslides: A Review. *Reviews of*  
510 *Geophysics*, **57**, 106-145.10.1029/2018rg000603
- 511 Whiteley, J. S., Watlet, A., Kendall, J. M. & Chambers, J. E. (2021). Brief communication: The  
512 role of geophysical imaging in local landslide early warning systems. *Nat. Hazards Earth*  
513 *Syst. Sci.*, **21**, 3863-3871.10.5194/nhess-21-3863-2021
- 514 Whiteley, Jim, Inauen, C., Wilkinson, P., Meldrum, P., Swift, R., Kuras, O. & Chambers, J.,  
515 (2023). Assessing the risk of slope failure to highway infrastructure using automated  
516 time-lapse electrical resistivity tomography monitoring. *Transportation Geotechnics*, **43**,  
517 101129, Elsevier.
- 518 Wilkinson, P., Chambers, J., Uhlemann, S., Meldrum, P., Smith, A., Dixon, N. & Loke, M.H.,  
519 (2016). Reconstruction of landslide movements by inversion of 4-D electrical resistivity

520 tomography monitoring data: LANDSLIDE MOVEMENTS FROM ERT INVERSION.  
521 *Geophysical Research Letters*, **43**, 1166–1174. doi:10.1002/2015GL067494  
522 Wilkinson, P.B., Uhlemann, S., Chambers, J.E., Meldrum, P.I. & Loke, M.H., (2015).  
523 Development and testing of displacement inversion to track electrode movements on 3-D  
524 electrical resistivity tomography monitoring grids. *Geophysical Journal International*,  
525 **200**, 1566–1581. doi:10.1093/gji/ggu483  
526

527

## Supplementary Materials

### 528 **Text S1. ERT data processing**

529 Data acquisition comprises dipole-dipole measurements with dipole lengths  $a = 1-4$  electrode  
530 spacings and dipole separations  $na$  with  $n = 1-7$ , including full sets of reciprocal readings. ERT  
531 data quality assessment includes filtering based on low retrieved voltage, repeatability error and  
532 reciprocal error. For each time-steps, apparent resistivities are filtered for outliers above 10%  
533 reciprocal error. An error model that weights each transfer resistance in the inversion is  
534 constructed for each time steps. We rely on a reciprocal error model employing a multi-bin  
535 methodology, which follows the approach outlined by Mwakanyamale et al. (2012). The  
536 reciprocal error is defined as the standard error in the mean of the forward and reverse  
537 measurements.

538 Additionally, following a strategy employed in Boyd et al. (2021) a constant factor of 1% of the  
539 transfer resistance is added to all reciprocal errors, in order to represent for forward modelling  
540 errors. This strategy improves the convergence of the inversion while ensuring the development  
541 of spatially and temporally smooth models.

542 The 3D time-lapse inversion is conducted with the fully parallelised inversion code E4D, as  
543 detailed in Johnson et al. (2010). To generate a 3D mesh for the inversion, input data includes  
544 surface topography derived from a LiDAR scan calibrated with GNSS control points.

545 This time-lapse inversion is undertaken on a set of daily time-steps from 22 November 2020 to  
546 30 March 2022. The time-lapse inversion uses smoothness constraints both spatially and  
547 temporally. The initial model is computed using a 3D smoothness-constrained inversion of the  
548 baseline data. We opt for a L2 norm. Subsequently, each time step is inverted with reference to  
549 the baseline. In the time-lapse inversion, we apply an L2 temporal smoothness constraint. A  
550 target misfit metric ( $\chi^2$ ) value of 1.0 is assigned to the E4D inversion.

551 For the time-lapse inversion, it is essential that the dataset of each time step includes identical  
552 readings as in the baseline. Readings which are in the baseline sequence but become rejected in  
553 subsequent time steps are retained in the inversion but their associated errors are set to the  
554 measurement value itself. This results in minimal weight assigned to the rejected data. Generally,  
555 a reduced number of measurements in the baseline sequence decreases the overall model  
556 sensitivity.

557 Variations in subsurface temperature can have significant impacts on the electrical resistivity  
558 (Brunet et al., 2010). In order to isolate changes in electrical resistivity that can be mainly  
559 attributed to changes in soil moisture, one needs to correct the resistivity models for the effects  
560 of temperature. We rely on temperature data from a vertical profile of six temperature sensors  
561 deployed at depths of 0.1, 0.2, 0.5, 1.0, 2.5, and 4.5 m bgl. in the centre of the ERT array. Given  
562 the relatively large electrode separation at the HHLO, the inverted resistivity time-series are

563 poorly correlated with the shallowest three temperature sensors, indicating that shallow changes  
 564 in temperature don't affect significantly the ERT data. Therefore only data from the deepest  
 565 three temperature sensors are taken into account in the temperature correction. First, daily 1D  
 566 temperature profiles are generated by linear interpolation of the temperature data. The 1D  
 567 temperature profiles are then used to convert the resistivity  $\rho_T$  of each cell of the models into  
 568 standard resistivity  $\rho_{corr}$  (at  $T_{corr} = 20^\circ\text{C}$ ) using the linear model of Keller and Frischknecht  
 569 (1966), valid between 0 and  $25^\circ\text{C}$ , which is defined as:

$$570 \quad \rho_{corr} = \rho_T (1 + m(T - T_{corr})) \quad (\text{Eq.1})$$

571 with a correction factor  $m = 0.02 \text{ }^\circ\text{C}^{-1}$  (Uhlemann et al. 2017).

572 Converting the resistivity models into gravimetric moisture content relies on the methodology  
 573 described for the HHLO in Uhlemann et al. (2017). This uses a petrophysical relationship relying  
 574 on the Waxman-Smits model (Waxman & Smits, 1968) for which the parameters were calibrated  
 575 on soil samples for the two main geological units (SSF and WMF) by Merrit et al. (2016). The  
 576 two zones are delineated from the baseline resistivity model based on a  $28 \text{ } \Omega\text{m}$  threshold in dry  
 577 conditions, which provides a reasonable estimate of the limit (Boyd et al., 2021).

## 578 **Text S2. Low-Frequency DAS data processing**

579 The DAS system consists of an interrogator unit housing a laser source that generates coherent  
 580 laser pulses that are sent along an optical fibre. The fibre acts as a distributed interferometer,  
 581 where the phase of backscattered light from different sites along the fibre varies as the refractive  
 582 index and therefore optical path length at those points changes. The refractive index depends on  
 583 both the strain and temperature of the fibre and therefore a measurement of the phase change of  
 584 the backscattered light between successive pulses can be used to determine changes in strain and  
 585 temperature (Bao & Chen, 2012; Bao & Wang, 2021).

586 The interrogator unit and datalogger are housed in a barn at approximately 700 m from the  
 587 Hollin Hill slope. The fibre optic cable is linked to the interrogator unit via a tight buffered cable.  
 588 On the slope, the fibre optic cable was installed along the ERT lines. Practically speaking, in  
 589 order to keep good coupling of the fibre with surrounding soil materials, the fibre trenches were  
 590 dug  $\sim 5$  cm parallel to the trench hosting the ERT cables.

591 DAS measurements are sampled along the fibre with a 1 m spatial interval over a gauge  
 592 length of 4 m, which defines the spatial resolution. A low-pass filter at 1 Hz is applied on the raw  
 593 data, which were acquired at 500 Hz, and optical phase data are converted to units of strain  
 594 following a methodology described in Ouellet et al. (2024). Since changes in temperature also  
 595 affect the optical phase, temperature effects are separated using two cables having more sensitive  
 596 to temperature and running parallel to one of the lines different sensitivities to strain and  
 597 temperature (Crickmore et al., 2020). The first cable has a "tight-buffered" construction and the  
 598 fibre is well coupled to both strain and temperature. The second has a "loose-tube" construction



599 and has a much lower strain response. The measured phase changes in each cable for temperature  
600 change  $T$  and strain change  $S$ , are given by the following two equations:

$$601 \quad P_1 = \alpha_1 T + \beta_1 S \quad (\text{Eq. 2})$$

$$602 \quad P_2 = \alpha_2 T + \beta_2 S \quad (\text{Eq. 3})$$

603 Where  $P_1$  and  $P_2$  are the measured phase changes in cables 1 and 2, respectively;  $\alpha_1$  and  $\alpha_2$  are  
604 the temperature sensitivity coefficients of cables 1 and 2, respectively;  $\beta_1$  and  $\beta_2$  are the strain  
605 sensitivity coefficients of cables 1 and 2, respectively. The equations can be solved to give  
606 temperature and strain change in terms of the phases  $P_1$  and  $P_2$ .

607 A 1-day moving average is then applied to provide daily strain data corrected for  
608 temperature. The strain dataset comprises two subsets acquired from 22 November 2020 to 30  
609 January 2021 (70 days), and then from 22 November 2021 to 28 February 2022 (100 days).  
610 Daily strain changes are thus calculated from the first day of each of these periods used as  
611 baseline, by subtracting strain measurements from subsequent days to the strain average at the  
612 baseline. Strain data is expressed in microstrain ( $\mu\epsilon$ ) and provide information on the surface  
613 displacements and landslide dynamics (Ouellet *et al.* 2024). Indication of displacement can be  
614 inferred from strain by multiplying the microstrain by the gauge length. Although the larger the  
615 displacement, the higher the risks of losing coupling between the fibre and the soil, resulting in  
616 underestimating actual displacement, as discussed in Ouellet *et al.* (2024). This has certainly  
617 been the case after the major landslide movement of 20-21 January 2021, after which a section of  
618 the fibre on Line 5 near the backscarp got exposed, accommodating strain where the slope  
619 surface makes a convex angle. Remediation took place in the following weeks to re-bury the  
620 exposed section, taking advantage of some slack left at the top of the line.

### 621 **Text S3. Auxiliary datasets**

622 Clusters of point sensors including shallow soil moisture (at 20 cm and 50 cm bgl),  
623 matric potential (at 50 cm bgl) and piezometers monitoring water level in shallow and deep  
624 boreholes are distributed over 6 locations (1-6 in Fig. 1). The way the piezometers have been  
625 installed (i.e. relatively narrow screened interval) allows the measured water level to be related to  
626 the pore pressure. Not all locations feature the same number of sensors, but overall they provide  
627 detailed information on the hydrological subsurface conditions within the different landslide  
628 domains. A weather station, which is part of the COSMOS-UK network, is installed in the  
629 bottom part of the slope and provides, amongst others, rainfall and air temperature data.  
630 Additional 1 km<sup>2</sup> rainfall estimates from the Nimrod MetOffice network of C-band rainfall  
631 radars (Met Office, 2003) are also utilised to investigate the spatial variation of rain intensity in  
632 the area surrounding the HHLO. Geotechnical sensors comprising three tiltmeters (Geosense  
633 Nodes) have been deployed and cover the different landslide domains (at location 2, 4 and 5) and  
634 Shape Accelerometers Arrays (SAA, Abdoun *et al.* 2013), located mid-slope on the translational  
635 zone of the landslide (at location 4 and 5).

636 The 56 GNSS markers are manually surveyed with a Leica GS15 system on a regular  
 637 basis (7 surveys over the 16 months of monitoring featured in this study). The GNSS markers  
 638 mainly provide accurate horizontal displacement data ( $\pm 1$  cm accuracy), given a lower accuracy  
 639 in the Z direction ( $\pm 10$  cm). They are also used to interpolate the electrode positions as the land  
 640 surface changes with the landslide movement.

641 The four LiDAR scans were acquired on the 12 November 2020, 23 March 2021, 27  
 642 September 2021 and 15 March 2022 with a Leica Pegasus system. Resulting LiDAR 3D point  
 643 clouds are used to generate Digital Elevation Models (DEM), and vertical distances between  
 644 each instance of the point clouds are computed using the M3C2 algorithm (Lague et al., 2013) of  
 645 the CloudCompare software, thereby providing accurate vertical displacement data ( $\pm 5$  cm  
 646 accuracy) at high spatial resolution. Here we use downsampled data on a 1 m cell size grid  
 647 covering the entire field of the HHLO. These datasets inform on local changes associated with  
 648 slope failure, and seasonal topographical changes associated with clay shrinking and swelling.

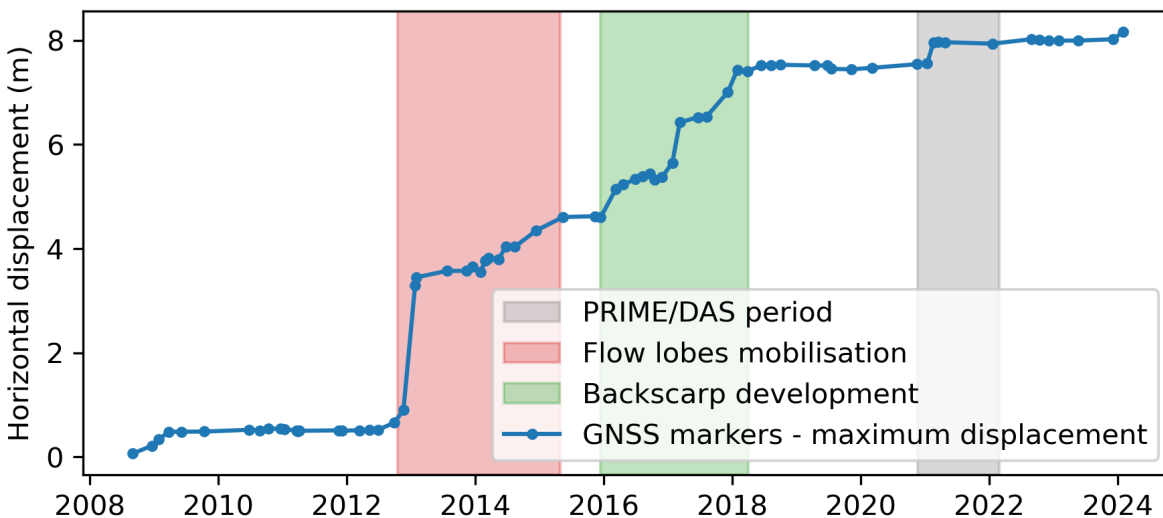
649

650

Location	Sensors				
	Moisture (sensor depth)	Matric potential (sensor depth)	Shape Accelerometer Array	Tiltmeters	Piezometers (borehole depth)
1	0.2, 0.5 m	0.5 m	-	-	3.9 m
2	-	-	-	X	3.0 m
3	0.2, 0.5 m	0.5 m	-	-	-
4	0.2, 0.5 m	0.5 m	X	X	1.85 m
5	0.2, 0.5 m	0.5 m	X	X	2.35 m
6	0.2, 0.5 m	0.5 m	-	-	7.9 m

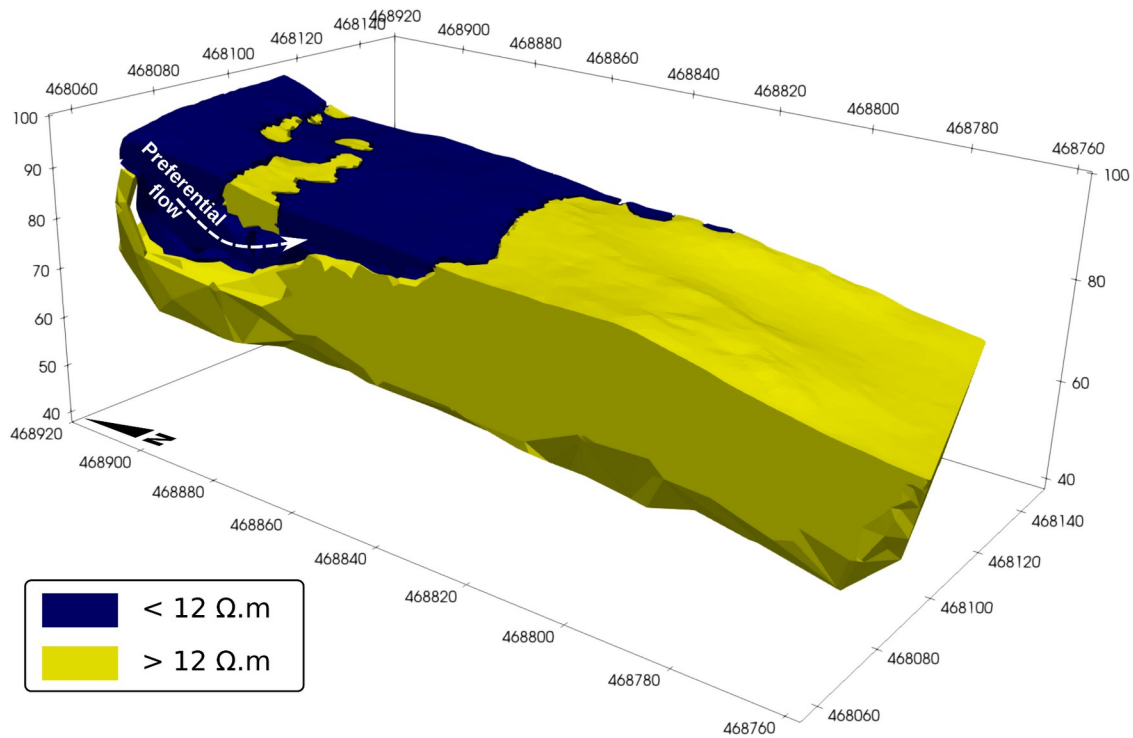
651

652 **Table S1.** Sensors available for this study per location (displayed on Figure 1)  
 653



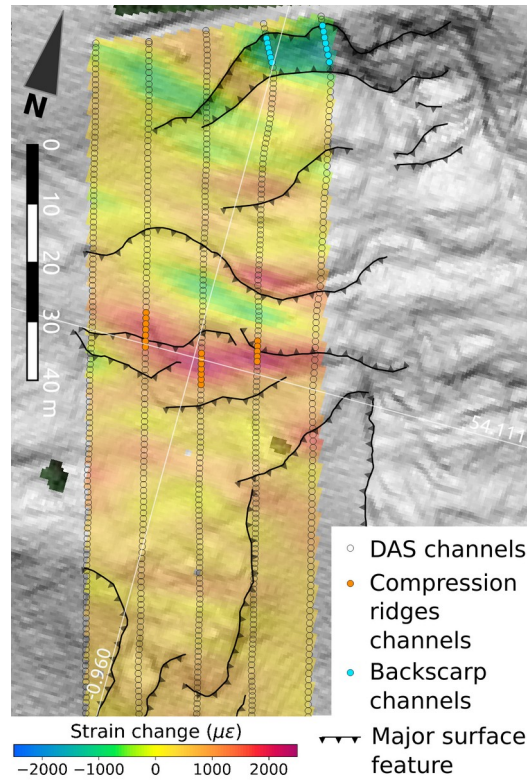
654

655 **Figure S1.** Maximum horizontal displacement recorded by GNSS survey on the set of GNSS  
656 markers. Since 2009, the landslide was most active between 2013 and 2018, with an average of  
657 1.5 m/year maximum horizontal displacement recorded by the GNSS markers. Primary  
658 deformation occurred first on the flow lobes in 2013 and then propagated to the top of the slope  
659 with the development of the backscarp from 2016 onwards. No significant displacement  
660 occurred until reactivation, albeit with lower intensity, in January 2021.

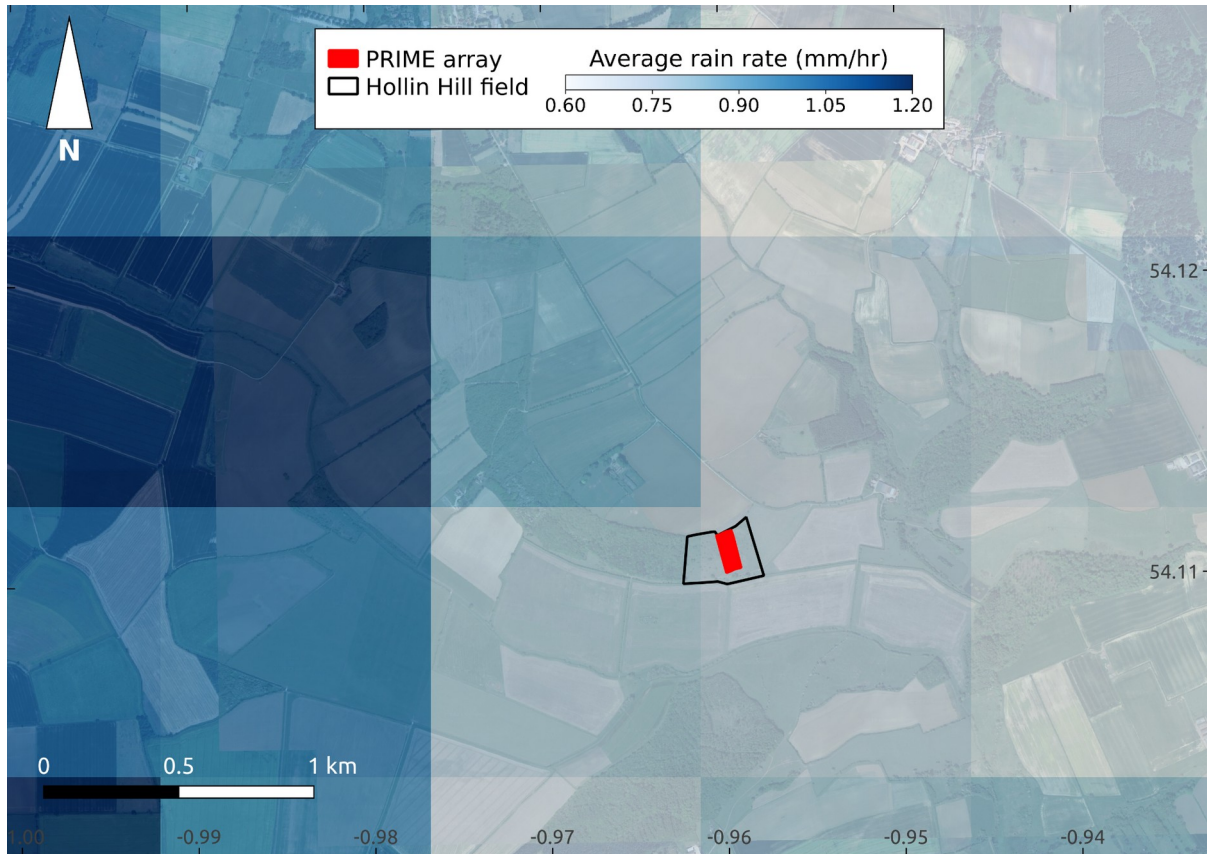


661

662 **Figure S2.** Model highlighting zones below and above 12  $\Omega m$  threshold on the 21 January 2021,  
663 highlighting most conductive zones which indicate potential preferential flow path underneath  
664 the backscarp.



665 **Figure S3.** DAS channels used to determine the compression ridges and backscarp zones shown  
666 in Figure 3 of the main manuscript.



667  
668 **Figure S3:** Average rain rate for the 30 minute window (22:00 to 22:30 UTC on the 20 January  
669 2020) as collected by 1-km rainfall radar (5 minutes intervals) from the Met-Office Nimrod. This  
670 highlights the inhomogeneous rain rate in the area surrounding the HHLO, with higher rain  
671 intensity on the upslope plateau.