

This manuscript is a preprint:

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1 Using fracture-scarp lineations as kinematic indicators on active normal fault scarps

2 Billy J. Andrews¹, Zoë K. Mildon¹, Manuel Diercks¹, Sam Mitchell², Gerald Roberts²,

3 Constanza Rodriguez Piceda¹, Jenni Robertson²

4 1. School of Geography, Earth and Environmental Sciences, Plymouth, United Kingdom

5 2. Birkbeck University of London, London, United Kingdom

6 Highlights

7 1 Fracture-scarp (F-S) lineations are mapped across eight bedrock fault scarps

8 2 F-S lineations may be split into en-echelon and parallel arrays

9 3 Kinematics and orientation of F-S lineations and arrays relate to the slip-vector

10 4 F-S lineations and arrays can act as kinematic markers on bedrock fault scarps

11 5 Kinematics of arrays provides insights into relative velocity across a fault plane

12 Key words

13 Slip-vector, active-tectonics, fault-scarp, earthquakes, fractures

14 Abstract

15 Reliable kinematic (slip vector) data collected from offset piercing points, corrugations or

16 striations, is a key input for fault based seismic hazard assessments. However, it can be

17 difficult to interpret kinematic indicators on degraded fault scarps. In this work, we

18 investigate the orientations and growth history of on-fault fracture networks, which extend

19 into the footwall and have greater preservation potential, to test whether they can be used

20 to infer slip vector. We identify various F-S lineation patterns preserved across eight faults in

21 Italy (Central Apennines) and Greece (Perachora Peninsula), including sinistral, dextral, and

22 parallel arrays. Our analysis reveals F-S lineations exhibit orientations that correlate with the
23 measured slip vector, with kinematics of arrays related to slip-vector rake. Relative age
24 relationships support a model of fracture growth where isolated en-echelon fractures evolve
25 into interconnected networks during successive earthquakes, driven by footwall uplift and
26 the intersection of a 3D strain ellipsoid with the fault plane. Further, we demonstrate F-S
27 lineations and arrays may serve as reliable kinematic indicators, even on degraded fault
28 scarps. Further analysis of on-fault fracture networks will enhance our understanding of
29 earthquake dynamics, long-term fault behaviour, and may contribute to seismic hazard
30 assessments through the identification of fault tips.

31 Supplementary

32 S1 – Summary of all faults and F-S maps used in this study

33 S2 – Data for mapped features

34 S3 – Summary of stereonet analysis and comparison between slip-vector and the rake of F-S
35 lineations and arrays

36 S4– Step-by-step instructions for collection of F-S lineation data

37 S5 – Calculations of slip vector using F-S lineations and F-S arrays

38 S6 – Network Properties for relative ages

39 1. Introduction

40 Active continental normal faults host destructive surface rupturing earthquakes. For
41 instance, the 1915 Avezzano earthquake (M_s 6.9) in the Central Apennines caused extensive
42 damage and ~33,000 deaths in the Fucino Plain (Guidoboni et al., 2019). Consequently,
43 undertaking robust seismic hazard assessments (SHA) within continental extensional regions
44 is important, with many recent approaches adopting fault-based assessments (Pace et al.,
45 2016; Faure Walker et al., 2021). Identifying potential seismogenic faults and measuring key
46 parameters (e.g., fault dip, slip-vector, slip-rate, elapsed time since last earthquake, fault
47 length) are crucial for fault-based seismic hazard assessments (Pace et al., 2016). Many of
48 these parameters can be collected from bedrock fault scarps, and thus field-based
49 observation play a pivotal role in fault-based SHA. These geomorphic features, common in
50 many actively extending regions (e.g., Central Greece and the Italian Apennines), result from
51 repeated surface rupturing earthquakes and are preserved since the last glacial maximum
52 (Roberts and Michetti, 2004; Bubeck et al., 2015; Zou et al., 2021).

53 Bedrock fault scarps are comprised of fault rock and fractured footwall lithologies and 'free
54 face' consisting of fault rocks in the footwall, with the hanging wall consisting of eroded
55 footwall sediments such as alluvium, colluvium, or marine deposits (LEEDER et al., 1991;
56 Tucker et al., 2011; Bubeck et al., 2015). Fault scarps offer prime exposures for collecting
57 structural data along active normal faults (e.g., Roberts and Ganas, 2000; Roberts, 2007;
58 Mildon et al., 2016). This has uncovered systematic slip-vector variations, with right-lateral
59 slip on the left tip, and left-lateral slip on the right, converging towards the fault centre when
60 the fault is viewed towards the footwall from the hangingwall (Roberts and Michetti, 2004;
61 Papanikolaou and Roberts, 2007; Roberts, 2007; Faure Walker et al., 2010, 2021).

62 Convergent slip-vectors aid in determining if multiple surficial bedrock scarp outcrops belong
63 to a single fault at depth (e.g., Ma and Kuszniir, 1995; Roberts, 1996, 2007; Roberts and
64 Ganas, 2000; Faure Walker et al., 2021), essential when assessing fault length for fault-based
65 seismic hazard.

66 To determine slip vectors, one needs to measure kinematic indications along the length of
67 the fault. Types of brittle kinematic indicators used on active faults include striations, steps,
68 pull-apart structures, crescentic or trail markings, asymmetrically deformed clasts,
69 corrugations, and piecing points (e.g., Hancock and Barka, 1987; Petit, 1987; Doblasi et al.,
70 1997). Between surface rupturing earthquakes, degradation of bedrock scarps occurs due to
71 the erosion of the footwall (Allen and Densmore, 2000; Bilal et al., 2020). This leads to
72 increased scarp roughness with height above the present-day scarp-colluvium contact
73 (Tucker et al., 2011; Zou et al., 2021). This can lead to the erosion of subtle kinematic
74 markers (e.g., striations) on degraded fault scarps, making the slip vector difficult to deduce.

75 Fractures are commonly observed but infrequently reported features that cut bedrock fault
76 scarps that extend into the footwall, generally remaining well-preserved during scarp
77 degradation except where vegetation or lichen covers the scarp. Examples include fractures
78 forming around bends on 'wavy faults' (Chester and Chester, 2000); extension fractures
79 perpendicular to fault slip (Friedman and Logan, 1970); comb fractures that have a distinct
80 shape and are typically orientated perpendicular to the slip vector (Hancock and Barka,
81 1987; Stewart and Hancock, 1990; Smeraglia et al., 2018); slip vector parallel fractures
82 (Hancock and Barka, 1987; Smeraglia et al., 2018); and pennant fractures that form en-
83 echelon arrays along brittle shear planes and point in the direction of movement (Coelho et
84 al., 2006; Lacazette, 2009). The identification of individual fractures, or fracture sets, has

85 been used to infer slip vector on active faults in Western Türkiye (Hancock and Barka, 1987).
86 However, fractures do not occur in isolation; rather, they form as arrays or networks (Aydin
87 and Reches, 1982; Sanderson and Nixon, 2015; Peacock et al., 2016). Due to convergent slip
88 vectors, the formation of bedrock scarps over multiple earthquake cycles, and non-
89 characteristic earthquake ruptures (e.g., partial ruptures or multiple rupture patches),
90 fracture patterns are expected to vary along a fault's length and encompass multiple
91 generations of fractures resulting from successive earthquakes. It is therefore important to
92 consider the length, orientation, kinematics, connectivity and growth history of the full
93 network to gain insights into how the network evolved (Peacock and Sanderson, 2018) and
94 thus to understand how they can be used to infer the slip vector.

95 Understanding how bedrock fracture networks form, evolve, and relate to the slip vector
96 could help constrain slip vectors on faults lacking pristine surface outcrops and gain insights
97 into how the footwall deforms across multiple seismic cycles. To investigate this, we
98 document the type, kinematics and networks of fractures visible on fault planes, hereby
99 termed fracture-scarp lineations from eight faults in Italy (Central Apennines) and Greece
100 (Perachora Peninsula, Gulf of Corinth). By comparing observations of fracture orientation
101 with slip vector measurements derived from striations and other kinematic indicators, we
102 also present a methodology to systematically capture fracture data to infer the orientation
103 of the slip vector.

104 2. Geological setting.

105 *2.1 The Italian Apennines*

106 The Central Apennines is a mountainous region of Italy that has been actively extending in a
107 NE-SW orientation for the last 2 to 3 million years (Cavinato and Celles, 1999; Cavinato et al.,
108 2002; Roberts et al., 2002; Roberts and Michetti, 2004; Montone and Mariucci, 2016). The
109 mountain range initially formed as a fold and thrust belt with NE-SW shortening during the
110 Miocene that thrust Mesozoic and Cenozoic limestones onto Miocene Flysch deposits
111 (Anderson and Jackson, 1987; Mazzoli et al., 2005; Vezzani et al., 2010). The switch from
112 compression to extension has been attributed to various mechanisms, including rollback of
113 the Adriatic plate (Patacca et al., 1993; Jolivet et al., 1998), the counter-clockwise rotation of
114 the Adria microplate (e.g., Nocquet and Calais, 2004), or a slab window within the down
115 going slab that enables upwelling mantle to drive extension (D'Agostino et al., 2001;
116 Rosenbaum et al., 2008; Faure Walker et al., 2012). Regardless of the cause, this extension is
117 responsible for the generation of a ~NW-SE trending normal fault system that cross cuts pre-
118 existing thrust sheets (Barchi et al., 2021). Individual faults typically dip towards the WSW,
119 have lengths of ~20 to 40 km and display total throws of less than 2 km (Pizzi and Scisciani,
120 2000; Roberts and Michetti, 2004; Faure Walker et al., 2021). Mapped fault strands are
121 rarely physically connected (Faure Walker et al., 2021), but instead form an array of steeply
122 dipping (~60°) dip-slip faults that show en-echelon or end on fault tip arrangements with
123 adjacent faults (Roberts and Michetti, 2004) (Fig 1a). Faults in the area have a long historical
124 record of shallow (5 to 15 km), moderate-to-large (up to Mw 6.5 to 7.0) earthquakes
125 stretching back to Roman times (Chiarabba et al., 2005; Rovida et al., 2016; Guidoboni et al.,
126 2019). Extension rates across the central Apennines derived from focal mechanisms (1.6

127 mm/yr; Selvaggi, 1998), global positioning systems (2 to 3 mm/yr; D'Agostino et al., 2009)
128 and Holocene fault scarps ($\leq 3.1_{-0.4}^{+0.7}$ mm/yr; Faure Walker et al., 2010) are low, and
129 therefore the recurrence times of surface rupturing earthquakes on any given fault are high
130 (100s to 1000s of years) (Cello et al., 1997; Galadini and Galli, 2000; Boncio et al., 2004; Galli
131 et al., 2008; Galli, 2020).

132 *2.2. The Gulf of Corinth*

133 Greece has been actively extending in a north-south orientation for the past 5 million years
134 (e.g., Ford et al., 2017), and similarly to the Central Apennines, extension overprints a pre-
135 existing Cretaceous-Miocene Alpine fold-and-thrust belt (e.g., Billiris et al., 1991; Doutsos et
136 al., 1993, 2006; Clarke et al., 1998; Roberts and Ganas, 2000). The driving forces behind the
137 extension are believed to be a combination of slab roll back in the Hellenic subduction zone,
138 and the dextral motion of the North Anatolian strike slip fault (Pichon and Angelier, 1979;
139 Jackson, 1994; Jolivet et al., 1994, 2013, 2013; Le Pichon et al., 1995; Jolivet, 2001). This
140 extension has resulted in an array of isolated ~E-W trending normal faults (Fig 1b). The faults
141 have a long history of seismicity associated with them, with moderate-to-large earthquakes
142 recorded as far back as 464 BC (Ambraseys and Jackson, 1990). The Gulf of Corinth is
143 extending between ~5 and 11 mm/yr (Clarke et al., 1998; Briole et al., 2000, 2021;
144 Chousianitis et al., 2015), with historical records suggesting that damaging earthquakes
145 occur on the fault system every decade (Ambraseys and Jackson, 1990).

146 *2.3 Typical bedrock scarp morphology of the studied faults*

147 This study focuses on data collected from five faults within the Central Apennines (Mt
148 Vettore, Martana-Terni, Fucino, Barete, and Campo Imperatore) and three faults situated on

149 the Perachora Peninsula at the eastern end of the Gulf of Corinth (Asprokambos, Pisia, and
150 Skinios). The varying elapsed time since the most recent earthquake, spanning years to
151 millennia, along with the differing elevations of exposed scarps, contributes to varying
152 degrees of scarp degradation between sites. Studied faults exhibit similarities in their fault
153 zone structure, characterised by bedrock fault scarps surrounded by minor fault arrays (e.g.,
154 Roberts, 2007). In a fault perpendicular direction, fault scarps consist of 10s of cm thick
155 limestone fault rock (e.g., breccia and cataclasite), followed by intensely fractured host rock
156 (e.g., Del Rio et al., 2023). In most cases, the hanging wall consists of colluvium and locally
157 alluvium.

158 Surface ruptures occurred along the Pisia and Skinios faults during the 1981 eastern Gulf of
159 Corinth seismic sequence (Jackson et al., 1982; Roberts, 1996a). These earthquakes caused
160 extensive surface rupturing, often manifesting as isolated en-echelon segments with gaps
161 between surface ruptures (Jackson et al., 1982; Mitchell et al., in prep). Ruptures on these
162 faults are frequently situated within dense vegetation, and the preservation of scarps
163 displays considerable variation both up the fault plane and along fault strike due to differing
164 vegetation coverage and lithology cut by the fault. The 1981 seismic sequence increased
165 interest in the eastern Gulf of Corinth, leading to the identification of several active faults in
166 the region, including the Asprokambos fault (Leeder et al., 2005). In addition, the ruptured
167 Pisia and Skinios faults have been investigated for geometry, kinematics, scarp morphology
168 and palaeoseismology to improve our understanding of slip characteristics and fault growth
169 (Jackson et al., 1982; Roberts, 1996b; Collier et al., 1998; Roberts and Ganas, 2000;
170 Mechernich et al., 2018).

171 3 Methods

172 Field measurements were taken using a compass clinometer and the FieldMOVE Clino
173 application on an ISO mobile device. The device's accuracy was verified in the field by
174 comparing measurements to those taken with a compass clinometer before data collection.
175 Bedrock scarp orientations and kinematic markers (striations, corrugations, tool marks, and
176 gouge ribbons) were measured at each field site where present. In cases of limited observed
177 lineations, additional data from the same fault collected on previous field campaigns were
178 included. In most cases, it was not possible to measure the planes of fractures cutting the
179 scarp, so instead we measured and analysed the intersection lineations of fractures with the
180 fault scarp (Fracture-Scarp (F-S) lineations). Three classifications of F-S lineations were
181 observed and corresponding measurements were taken:

- 182 - *Parallel F-S lineations (Fig 2a)*: Isolated or series of parallel lineations, often matching
183 the slip-vector trend in our examples. Measurements: Rake and length of the F-S
184 lineation.
- 185 - *En-echelon arrays (Fig 2b)*: Commonly observed, showing sinistral or dextral shear
186 indicators, and with variable F-S lineation trace and array lengths. Measurements:
187 kinematics of array, rake and length of F-S lineations, and rake and length of the
188 array.
- 189 - *Parallel arrays (Fig 2c)*: Similar to en-echelon arrays but less common, displaying no
190 shear indicators, and with shorter F-S lineation trace lengths compared to en-echelon
191 arrays and parallel F-S lineations. Measurements: Rake and length of F-S lineations,
192 and rake and length of the array.

193 The above F-S lineations and arrays combined to create a lineation network where the
194 presence and relative proportion of each classification differed between localities. Rake may
195 be measured in either a clockwise or anticlockwise manner and in this study we opted for
196 the first approach whereby a rake of 90° represents pure normal faulting. It should be noted
197 that certain authors (e.g., Aki and Richards, 1980) employed the anticlockwise approach,
198 which results in negative values during comparison.

199 To complement field data, high-resolution images capturing key features were taken
200 orthogonal to the fault plane for subsequent digitisation. In QGIS, manual lineament
201 mapping of F-S lineations were undertaken at a constant scale for each photograph, with
202 direct comparisons avoided between data collected at different scales on the same fault.
203 This is because fracture patterns are often scale-dependant (Bertrand et al., 2015; Forstner
204 and Laubach, 2022), so comparing across scales could lead to erroneous conclusions.
205 Additionally, all mapping was undertaken by the lead author to limit discrepancies between
206 datasets caused by the subjective biases of different interpreters (Andrews et al., 2019).
207 Post-digitisation, F-S lineations were visually classified based on the scheme introduced
208 above (Fig 2). Subsequently, the orientations and array trends were quantified and
209 converted to rake. These data were then portrayed as histograms and stereographic
210 projections, with the mean fault plane of the imaged area serving as the fault plane.
211 Employing average fault plane measurements could induce minor errors in F-S lineation and
212 array orientations where the fault plane is non-planar; however, the effect is expected to be
213 minimal and unlikely to impact the overall conclusions drawn from the data.

214 For all localities, we compare the orientation of F-S lineation and arrays with the slip-vector
215 measured from imagery and in the field. We do this by calculating the mean vector and

216 Bingham analysis of each dataset in Stereonet 10 (Allmendinger et al., 2013; Cardozo and
217 Allmendinger, 2013), as well as by assigning clusters through a visual analysis of contoured
218 datasets and assessing rake histograms. For derived clusters we report the trend and plunge
219 of the mode, and the angular spread of the data across the fault plane. Additionally, we
220 compare the rake of F-S lineations and arrays to the slip-vector by taking the mean vector of
221 mapped lineations, or when not present, the equivalent rake of any field derived value.

222 To investigate the evolution of F-S lineation network length and connectivity during the
223 earliest stages of fracture development (up to 15 cm), we analyse three sub-sections from
224 the bedrock fault scarp at Mt Vettore. In each area, we interpret age relationships within the
225 fracture network using topological and cross-cutting relationships. Each sub-section
226 represents a progressively advanced stage of fracture evolution, indicated by the increasing
227 number of age relationships from panels (i) to (iii). For each sub-section, we assess trace-
228 length distributions, fracture intensity, and network connectivity for each interpreted stage
229 of fracture evolution. Fracture intensity was calculated by dividing the total fracture length
230 of fractures at a given age relationship by the area of the subsection (e.g., Dershowitz and
231 Einstein, 1988). To assess connectivity, we analysed network topology, defining the network
232 as a series of nodes (isolated (I), abutting (Y), and crossing (X)) and branches (isolated (I-I),
233 partly isolated (I-C), and fully connected (C-C)) (Manzocchi, 2002; Sanderson and Nixon,
234 2015, 2018). Based on node type proportions, we calculated the percentage of connected
235 nodes (P_c) using the following equation:

$$236 \quad P_c = \frac{(3N_Y + 4N_X)}{(N_I + 3N_Y + 4N_X)} \quad (\text{Equation 1})$$

237 where N_I is the number of isolated nodes, N_A is the number of abutting nodes, and N_C is the
238 number of crossing nodes. We then compare results from each interpreted stage of the
239 fracture evolution to gain insights into F-S lineation development.

240 4 Results

241 4.1: F-S lineation networks

242 The spatial distribution and orientation of F-S lineations and arrays are examined using
243 lineament maps, which include the original photographs showing key features alongside the
244 interpreted F-S lineation network (black lines), including the classified F-S arrays (red, purple,
245 and blue dashed lines). The orientation of mapped lineations, F-S lineation, and F-S arrays
246 are shown using stereographic projections, constructed from the rake of mapped fractures.

247 4.1.1: F-S lineations

248 Abundant on-fault fractures (F-S lineations) were observed across all studied fault scarps
249 (Figs 3, 4), with fracture length ranging from 0.005 m to 20.85 m. Only the largest fractures
250 extend into the scarp beyond the decimeter-thick limestone fault rock. Some larger fractures
251 show small offsets indicating shear, however, most fractures were tight with no observable
252 aperture, complicating the classification of deformation mode. F-S lineations occur as arrays,
253 with dextral, sinistral, and parallel kinematics. Most fractures are unfilled, except for
254 localised vuggy calcite at Terni-Martana and mineralised fractures at the Mt Vettore.

255 The Mt. Vettore locality, with a fault scarp height ranging from ~3 to ~20 meters, provides
256 particularly good exposure of F-S lineations (Fig 3). The outcrop spans a prominent fault
257 bend with a ~30° variation in fault strike from ESE to SSE (Fig. 3c), resulting in mean fault

258 plane orientations with strikes from 116° to 149° and dips from 54° to 82°. Despite changes
259 in fault plane orientation, mapped striation trends remain consistent, ranging from 262° to
260 283° (Fig. 3c, d). This locality exhibits varied footwall degradation, from pristine sections
261 within the coseismically exposed “white ribbon” to degraded zones where fractures remain
262 well preserved, allowing F-S lineations to be mapped at scales of 1:50, 1:10 and 1:1. We
263 describe these data prior to discussing trends observed at other localities.

264 Across Mt Vettore, fracture orientation, connectivity, and length vary by location and the
265 map scale (Fig 3). At the largest scale (1:50), F-S lineations form a well-connected network
266 with a maximum trace length of 20.9 m and mean of 1.6 m. At the 1:10 scale, the network is
267 less connected, with a mean trace length of 0.5 m. At the 1:1, F-S lineations shorter than 5
268 cm are visible that exhibit low sinuosity, while longer fractures show multiple changes in rake
269 (e.g., Fig 3f). Smaller trace length arrays intersect larger F-S lineations, often connecting
270 longer (>5 m) F-S lineations. The spread of rake values increases at the smallest scale (1:1),
271 showing more connections between F-S lineations with different trace lengths.

272 Across other sites, most F-S lineations are isolated, with high network connectivity localised
273 to small areas or where footwall degradation is high (Fig 4, S1-6). While F-S trends show
274 peaks, variability in rakes between and within maps is observed, with some maps showing a
275 bi-modal distribution of F-S rake corresponding to oppositely dipping F-S lineations (e.g.,
276 Barete, Fig S4a). Small trace-length off-trend F-S lineations are locally observed connecting
277 longer F-S lineations (Fig 4a), or at the intersection of F-S lineations (Fig S2, S3b). At Campo
278 Imperatore, F-S lineations exhibit high connectivity and a large spread in F-S lineation trend
279 (Fig S2).

280 Trace length distributions across faults show shallow gradients with abrupt jumps,
281 suggesting characteristic F-S lineation lengths for a given map (Fig 5). Across all datasets, the
282 upper portion of the data displays an increase in gradient away from the characteristic
283 length (Fig 5a). This is particularly clear when data is limited to between 0.01 and 0.15 m,
284 with the gradient change occurring for most faults between 60 and 70% of the data and
285 each map displaying a different characteristic length (Fig 5b). When these lengths are cross-
286 referenced to the fracture maps, it appears that the switch from characteristic F-S lineation
287 length to non-characteristic occurs for features that show a sinuous trace and cut through
288 smaller F-S lineations (e.g., Fig 3f). Initial fracture growth is further discussed in section 4.2.

289 *4.1.2: F-S lineation arrays*

290 F-S lineations could be visually grouped into arrays for all maps, with sinistral and dextral,
291 and, in fewer cases (15 out of 19 maps), parallel arrays observed (Figs 3-5). At Mt. Vettore,
292 mapping scale influenced the proportion of array types and orientations of arrays. For less
293 connected F-S lineation networks (1:10 and 1:1 scales), arrays up to ~0.4 m in length
294 primarily consisted of isolated F-S lineations (Fig 3). Sinistral arrays made up >50% of arrays
295 across all scales, with dextral arrays exceeding parallel arrays (Figs 3-5). Sinistral and parallel
296 arrays showed similar orientations across scales, with array rakes within 40-70° of the slip
297 vector. Conversely, dextral arrays showed greater rake variability, with a bi-modal
298 distribution at the 1:50 scale and a broader range across all scales, often occurring at a high
299 angle to the slip vector (Fig 4, S5).

300 Array orientations varied across other faults and maps (Figs 4, S1-6). While orientations
301 differed between maps, the dominant array type for each map displayed a prominent
302 orientation cluster (Fig 4). Like Mt. Vettore, the less common array type exhibited a wider

303 spread in orientation, often with broad or multiple peaks. For instance, the Skinos fault
304 shows tightly clustered sinistral and parallel arrays around 54°/040°, while dextral arrays
305 displayed greater spread with multiple peaks (Fig 4c). This variation often arises from
306 commonly observed, shallowly dipping, short trace length arrays aligned ~90° to the main
307 trend.

308 Array lengths displayed a negatively skewed distribution, with medians consistently below
309 means (Fig 5c). The shortest arrays (bottom 5-30%) display gradual length increases, with a
310 characteristic length for medium length arrays (40-80%), and a substantial increase in
311 gradient for the largest arrays. Longer arrays, consisting of longer F-S lineations, often bound
312 blocks of fault scarp that contain smaller trace length arrays (Fig 3e, 4a). Array length
313 distributions also varied by shear sense (Fig 5d). For instance, sinistral arrays were longest on
314 the Pisia fault, whereas dextral arrays were longest at two of the three Barete localities.
315 Generally, the most abundant arrays were also the longest, though there were exceptions,
316 and parallel arrays were typically shorter than dextral or sinistral arrays (Fig 5d). Overall,
317 array shear sense, orientation, and length appear to be influenced by slip vector rake, F-S
318 lineation connectivity, dominant array type, and fault plane geometry.

319 ***4.2 Relative age relationships between F-S lineations***

320 Three areas were selected within the 'white ribbon' at Mt Vettore to display a range of key
321 features and were selected to demonstrate how the network differs between where the
322 dominant fractures are more isolated (Fig 6a), show evidence of fracture growth and linkage
323 (Fig 6b), and are dominated by well-connected fractures (Fig 6c). En-echelon arrays are
324 common across all areas, with most fractures displaying abutting or cross-cutting
325 relationships (Fig 6). Isolated large trace-length (> 10 cm) fractures display tip-damage zones,

326 wing cracks, and rake deviations where fractures intersect smaller en-echelon arrays (Fig 6a).
327 In more connected networks (Fig 6b, c), sinuous fracture traces, trailing segments, and
328 abrupt rake changes ($\sim 90^\circ$ in Fig. 6c) indicate interactions between large and pre-existing
329 fractures. Evidence of abandoned tips, linking damage zones, and transfer zones suggest
330 progressive strain localisation onto larger fractures. In Figures 6b and 6c, the largest
331 fractures show shear offsets (< 0.5 cm) and bound smaller trace-length fractures and arrays
332 like observations made at other localities (Figs 3, 4, S1-6).

333 During the initial fracture evolution (relative age 1), all sub-sections display low-to-medium
334 fracture intensity (18.9 to 48.5 fm^{-1}) consisting of en-echelon, and locally parallel, arrays of F-
335 S lineations. The network is largely isolated ($P_c = 0.00$ to 0.02), with 3 to 8% censored
336 fractures and a characteristic length of 2.5 to 3 cm for $\sim 70\%$ of fractures (Fig 7). As fractures
337 evolve (relative age 2), some fractures lengthen and abut against those from relative age 1,
338 increasing the fracture intensity (33.3 to 77.8 fm^{-1}), proportion of censored fractures (15 to
339 15%), and the connectivity of the network ($P_c = 0.15$ to 0.43). The length distribution also
340 shifts, particularly among the longest 15 to 20% of fractures.

341 With further fracture development (relative ages 3 to 6), fracture intensity and connectivity
342 continue to increase (Fig 6, 7). Length distributions and the proportion of censored fractures
343 show only slight deviations, as new fractures often localise at the intersections of larger
344 fractures, while small, early fractures remain isolated. In panels 6b and 6c, the network
345 complexity is higher, with fracture growth becoming increasingly localised on larger fractures
346 that bound blocks of smaller fractures as strain localises onto these structures (Figs 6, 7).

347 In addition to fractures, additional fault rock products are preserved at Mt Vettore such as
348 fault breccias, veins and tool marks that were not observed on any other fault scarps in this

349 study (Fig 3, 6). Fault breccias are elongate, sub-parallel to the slip vector, and contain
350 angular to sub-angular clasts (3mm to 4 cm) that can often be matched to adjacent sections
351 of fault scarp (Fig 6a). The breccia matrix consists of microcrystalline calcite or reworked
352 fine-grained fault rock that occasionally exhibits S-C fabrics indicative of sinistral shear (Fig
353 6a). Locally, hairline calcite veins (<3 cm in length) form parallel or en-echelon arrays (Fig 3f,
354 S1). Calcite veins cross-cut breccias and are, in turn, cross-cut by F-S lineations. Though
355 beyond the scope of this study, these observations imply progressive deformation of the
356 footwall prior to fracture development.

357 ***4.3 F-S lineation networks across variable fault geometries***

358 Non-planar fault surfaces, such as those with corrugations, influence the distribution and
359 orientation of F-S lineations and arrays (Figs 3, 4, S2-6). Figure 8 highlights a corrugation,
360 where F-S lineation rake changes notably across both the ridge and trough. The
361 Asprokambos locality, which is characterised by abundant variations in dip and dip-direction
362 across the outcrop, further demonstrates how non-planar fault geometries affect F-S
363 lineation networks (Fig 9). Here, the orientation of striations varies widely, with both
364 divergent and convergent slip vectors observed (Fig 9a). Geometrical complexity influences
365 the orientation of F-S lineations (Fig 9c) and the kinematics of F-S arrays (Fig 9d). This is most
366 clearly observed in the parallel arrays (red lines), which diverge and converge around
367 corrugations. Individual corrugations commonly have sinistral and dextral arrays on either
368 ridge, with parallel arrays in trough (Fig 9d). Fracture intensity is greatest along corrugation
369 ridges, and there is an increase in shallowly dipping arrays where dip changes are observed
370 (Fig 9d, e). These observations indicate that non-planar fault geometries, particularly those
371 with corrugations, significantly influence the orientation and distribution of F-S lineations

372 and arrays. Variations in slip-vector rake across ridges and troughs lead to divergence and
373 convergence of F-S lineations, while fracture intensity is highest along corrugation ridges.
374 This suggests that where slip is not orthogonal to the fault plane, the kinematics and
375 intensity of F-S arrays are notably altered, highlighting the importance of fault plane
376 geometry in on-fault fracture formation.

377 ***4.4 Orientation of F-S lineations and arrays relative to the slip vector***

378 Median slip-vector rake ranged from 70° to 135° and for most faults, the spread of lineation
379 rake was small with interquartile ranges of <10°. This enabled us to explore how the trend of
380 F-S lineations and arrays relative to the measured slip vector varied between fracture maps.
381 When comparing the relative orientation of F-S lineations and arrays to the slip vector,
382 patterns emerge that link the rake of the slip vector to the types and orientation of features
383 (Fig 10). F-S lineation histograms for all data exhibit peaks at +45° and -45°, with large
384 standard deviations. When the data is analysed by fault map, faults with slip-vector rakes
385 under 90° show a peak at +45°, while those with rakes over 90° showed a peak at -45°. The
386 proportion of sinistral to dextral arrays also appears to be influenced by the rake of the slip
387 vector with dextral arrays dominating where the slip vector rake is <<90°; sinistral arrays
388 dominating when the slip vector rake is >>90°, and all types, including conjugate fracture
389 sets, present when the slip vector rake is ~90°. When the data is normalised to remove the
390 effect of shear sense, the trend for F-S lineations (Fig 10b) and arrays (Fig 10c) become
391 clearer, with primary peaks for F-S lineations at 40°-45° (with a broad spread up to 55°), 0°-
392 5°, and 80°-90° relative to the slip vector. Arrays display a prominent peak within 5° of the
393 slip vectors (with a broad spread up to 10°), and a minor peak at 80° to 85°. Additionally,
394 where both dextral and sinistral arrays are present, the conjugate bisector of F-S lineation

395 peaks aligns with the slip vector. Despite these general rules, there is scatter in the data,
396 which appears to correlate to corrugations on the fault plane, small arrays that form at the
397 intersection or between large trace length F-S lineations, or variable fault geometry. These
398 findings highlight the complex relationship between slip-vector rake and the orientation of F-
399 S lineations and arrays, with deviations largely influenced by fault corrugations, intersecting
400 arrays, and variations in fault geometry.

401 Discussion

402 *5.1 Model of on-fault fracture growth on bedrock fault scarps*

403 In order to confidently use on-fault fractures to infer slip-vector information, it is first
404 important to present a model of how the fracture network forms. On-fault fractures are
405 common (e.g., Hancock and Barka, 1987); however, how individual fractures evolve into
406 fracture networks is rarely examined. Our data indicates that the geometry of on-fault
407 fractures relate to the slip-vector inferred from striations and that during the initial stages,
408 fracture networks initially form as isolated, small fractures in en-echelon arrays with a
409 consistent spacing between F-S lineations (Figs 3, 4, 6). As deformation of the fault scarp
410 continues, the strain accommodated by the fracture network becomes localised onto a sub-
411 set of on-fault fractures that continue to increase in length and occasionally display minor
412 offsets, whilst other on-fault fractures no longer accrue strain and become isolated (Fig 6).
413 We propose that because we observe on-fault fractures to be predominantly constrained to
414 the fault core, they are not associated with prior deformation (e.g. thrusting), but instead
415 form in response to co-seismic or post-seismic slip during, or following, normal faulting
416 earthquakes.

417 Traditional models of on-fault fractures formed by fault slip assume they form as mode 1
418 fractures that are perpendicular to the slip vector, developing when the intermediate
419 principal stress (σ_2) is parallel to the fault plane (Wilson et al., 2003; Blenkinsop, 2008;
420 Scholz, 2019). However, our observations of en-echelon F-S lineations suggest fractures do
421 not always form perpendicular to the averaged slip-vector. One explanation for this is that
422 fractures form in response to different rupture directions, caused by differences in rupture
423 patches between earthquakes (e.g., Kato, 2020). While this cannot be discounted, you may

424 expect to see similar dispersion in the slip-vector derived from striations and/or
425 corrugations, as well as cross-cutting striations (e.g., Andrews et al., 2020). This is not
426 observed at Mt Vettore, where the dispersion in both field and photo derived striations is
427 very low when compared to the wide array of observed fracture orientations (Fig 3). Another
428 explanation for fractures that do not form perpendicular to the slip vector is that they
429 developed under a stress state whereby the intermediate stress axis (σ_2) is oblique to fault
430 strike (e.g., Cruikshank et al., 1991; Crider and Peacock, 2004; Blenkinsop, 2008). This could
431 occur where the strike and/or dip of the fault plane varies with respect to the orientation of
432 the stress axis. This occurs across a range of scales within fault bends, corrugations, and
433 oblique fault segments (e.g., Withjack et al., 1995; Ferrill et al., 1999; Walsh et al., 1999;
434 Peacock, 2002; Iezzi et al., 2018; Mitchell et al., 2024), where the inferred average slip vector
435 remains consistent around fault bends (Iezzi et al., 2018), suggesting that the orientation of
436 the principal stress axis remain consistent. Therefore, the orientation and shape of the
437 resultant 3D strain ellipsoid would also be expected to remain constant, with the trend of
438 principle strain axis aligned to the regional slip vector. Depending on the relative orientation
439 of the fault plane to the local slip-vector averaged over multiple earthquakes (e.g., derived
440 from corrugations), the rake of the slip vector on the fault plane may exceed or fall below
441 90° (Fig 11b), which combined with any change in fault dip causing the intersection of the
442 fault plane and 3D ellipsoid to resemble a 2D strain ellipse with a sinistral or dextral shear
443 sense (Fig 11d, e).

444 It is well known that the orientation of the stress axis relative to the fault rotates near the
445 surface, due to the free surface effect, as well as in close vicinity to the fault plane (e.g.,
446 Reiter, 2021). Therefore, the shape of the strain ellipsoid at a particular point on the fault is

447 unlikely to remain constant through time. Instead, as throw accumulates, footwall uplift will
448 change in the shape of the strain ellipsoid as the effective normal stress decreases (Fig 11c).
449 At depth (100s m), the strain ellipsoid is prolate causing localised brecciation of the
450 mineralised fault core and the formation of striations, but no on-fault fractures. As the
451 footwall continues to uplift the intermediate strain ellipsoid axis increases and isolated en-
452 echelon fractures begin to form. During initial fracture growth, fracture length and spacing
453 varied between faults, but were similar for individual fracture maps and fractures did not
454 penetrate beyond the mineralised fault core (Fig 5, 6).

455 As the on-fault fracture network continues to develop, fracture intensity and connectivity
456 increase, and strain within the fracture network becomes localised onto a subset of on-fault
457 fractures, which increase in length (Fig 11). As linking fractures grow, it is probable they
458 extend beyond the fault core and into the footwall lithologies. This is observed at Mt
459 Vettore, where erosion along large trace length fractures extends beyond the fault scarp (Fig
460 3b, e). As strain becomes localised onto this subset, the spacing between actively deforming
461 fractures increases, with evidence of slip along the F-S lineation occasionally evidenced (Fig
462 6c). Slip along on-fault fractures, and the interaction between fractures as the network
463 becomes more connected, leads to the development of damage zone features (cf., Caine et
464 al., 1996; Wibberley et al., 2008; Faulkner et al., 2010) that consist of well-connected small
465 trace length fractures. Damage zone fractures increase network connectivity, but due to only
466 being small, have only a small effect on the intensity and trace length distribution of the
467 network (Fig 7). Like observations on normal faults (e.g., (Peacock et al., 2017; Nixon et al.,
468 2020; Hansberry et al., 2021), damage zone fractures preferentially form where there are

469 geometrical complexities along the through-going fracture. For example, at bends that
470 formed when isolated arrays linked during the initial stages of fracture growth (Fig 6).

471 Further strain accommodated within the on-fault fracture network during successive
472 earthquakes will be accommodated by larger trace length connected fractures, leaving
473 blocks of small trace-length, layer-bound, fractures that retain the fracture pattern of the
474 initial stages of fracture growth (Figs 6, 11). As fault-rock products, striations, isolated F-S
475 arrays, and through-going fractures show consistent geometries relative to the inferred slip
476 vector, it is likely that for a given site, the relative orientation of the fault plane to the slip
477 vector remained constant across multiple seismic cycles both prior to, and during fracture
478 development. This model explains the progressive fracture growth as well as why similar
479 fracture patterns, characteristic lengths, and orientations are observed across a range of
480 scales and different faults.

481 *5.2 Inferring slip vectors using on-fault fractures*

482 Previous studies have suggested that individual measurements of comb or pinnate fractures
483 can be utilised to derive slip vectors (Hancock and Barka, 1987; Smeraglia et al., 2018).

484 However, our findings demonstrate fractures form at a range of angles that deviate from
485 typical slip-perpendicular or slip-parallel orientations. It is therefore important to consider
486 the orientation of all fractures and arrays that constitute the fracture network. Where this is
487 done, the generic rules presented in Fig 10 can be used infer the slip-vector from the rake
488 distributions of F-S lineations and arrays (see Supplementary 4 for detailed workflow).

489 The test the effectiveness of the method, we apply the generic rules derived from the entire
490 dataset to each fault individually, infer the slip vector, and then compare the inferred slip

491 vector to the measured slip vector (Table 1, Fig 12). In 12 out of 19 cases, the rake of the slip
492 vector could be inferred to within 5°, and all but the map of the corrugation on the Skinos
493 fault (Fig 8) were within 10° of the measured value. This precision was only possible when
494 the inferred slip vector from F-S lineations and F-S arrays relationships were calculated
495 separately (Fig 12a), and then the mean of both taken (Fig 12b). In every instance, the error
496 in the inferred rake remained within the range of slip vectors measured from the imagery
497 (Fig 12b). Based on these rakes, the average absolute difference in slip vector trend and
498 plunge is 6.2° and 2.2° respectively, which fall within the expected measurement error for
499 field observations (Fig 12c, d).

500 We have demonstrated that on-fault fracture networks can be used to derive the slip vector
501 on active normal faults. However, it is important to note that, due to biases in fracture data
502 collection, a fracture network extracted from imagery or field observations is non-unique
503 and may vary between interpreters. Therefore, it is crucial to account for these potential
504 variations by considering the following guidelines when applying the method. First, the
505 nature of footwall deformation should be assessed in the field to ensure that photo-
506 lineaments extracted from digital data represent actual structures. This approach has been
507 shown to reduce uncertainty during manual lineament analysis (Andrews et al., 2019;
508 Peacock et al., 2019) and has been undertaken for all faults in the Central Apennines with
509 findings from these faults used to guide fracture mapping on faults in the Gulf of Corinth.
510 Additionally, the field classification of fractures enables key information to be gathered (e.g.,
511 fracture type, fill, kinematics) that provide important information about fracture formation
512 (Peacock and Sanderson, 2018). Secondly, the quality of imagery used for interpretation
513 must be sufficiently high to allow confident identification of field structures, and the

514 interpretation should be performed at a constant and appropriate scale of observation
515 (Scheiber et al., 2015; Andrews et al., 2019). Maintaining consistency in the imaged area and
516 ensuring the scale is such the image is not pixelated ensures that the imaged network is
517 consistent between study sites. Finally, fracture mapping is subject to subjective biases
518 influenced by factors such as the interpreter's experience and style, the scientific question
519 being addressed, fatigue during interpretation, and group dynamics (Burns and Brown, 1978;
520 Gillespie et al., 2011; Scheiber et al., 2015; Andrews et al., 2019; Peacock et al., 2019).
521 Andrews et al. (2019) demonstrated that interpreters tend to be internally consistent in their
522 interpretation style and reiterated the importance of establishing a pre-set criteria prior to
523 fracture mapping (Andrews et al., 2019; Gillespie et al., 2011). We recommend that
524 interpretation is conducted by a single experienced interpreter to ensure consistency across
525 different sample areas. If this is not feasible, we suggest a subset of the data is interpreted
526 collectively by all interpreters to ensure standardised mapping techniques (Andrews et al.,
527 2019). Additionally, reanalysing a subset of the data (e.g., 10%) can help quantify the
528 magnitude of uncertainty introduced to the dataset by subjective bias (Gillespie et al., 2011).
529 By addressing these considerations, we believe this method offers a valuable additional
530 constraint on the slip vector of active normal faults.

531 The ability to use on-fault fractures to infer slip vectors is particularly useful for fault scarps
532 with different levels of footwall degradation (Table 1, Fig 12). Indeed, we have shown that
533 slip vectors can be reliably inferred even where abundant kinematic markers are absent. For
534 example, at Campo Imperatore, no striations were visible, however, the data still aligned
535 with the measured corrugation trend (Table 1). The method is less reliable in cases where
536 the F-S network has high trace lengths and is well connected (Fig 3f), where the fault plane is

537 highly irregular and only the mean slip vector can be deduced (Fig 8, 9), or where arrays
538 develop along the T-axis (Fig S5a). Despite this, F-S lineation patterns serve as dependable
539 kinematic indicators, even on degraded bedrock scarps. This is especially valuable in areas of
540 low extension rates and with long recurrence intervals, where fault scarps can undergo
541 significant degradation between earthquakes (e.g., Italy).

542 Conclusions

543 In this study, we focus on the orientations of F-S lineations and arrays and their relationship
544 to the observed slip vector. Our analysis reveals that F-S lineations and arrays consistently
545 exhibit orientations that correlate with the inferred slip vector, with kinematics related to
546 the rake of the slip-vector. We propose a model of on-fault fracture growth in which isolated
547 en-echelon fractures evolve into interconnected networks during successive earthquakes,
548 driven by the intersection of an evolving 3D strain ellipsoid with the fault plane. Initially,
549 footwall deformation is constrained to breccia formation, however, as footwall uplift causes
550 a drop in the effective normal stress acting on the fault, fracture formation within the
551 mineralised fault core occurs. The kinematics recorded in the breccia and fractures are
552 similar, suggesting the slip-vector remains consistent across multiple seismic cycles at the
553 studied sites. Progressive fracture growth leads to the formation of through-going fractures,
554 that localise strain and develop damage zones whilst bounding blocks of isolated small trace
555 length F-S lineations and arrays. These networks reflect the kinematic history of the fault and
556 provide insights into the dynamics of earthquake slip across multiple earthquake cycles. Due
557 to the predictable orientation of on-fault fractures relative to the slip-vector, we
558 demonstrate F-S lineations and arrays may act as a reliable further constraint when inferring
559 slip-vector. We suggest further analysis of on-fault fracture networks could benefit

560 earthquake science by providing information about long-term fault behaviour and fault
561 linkage.

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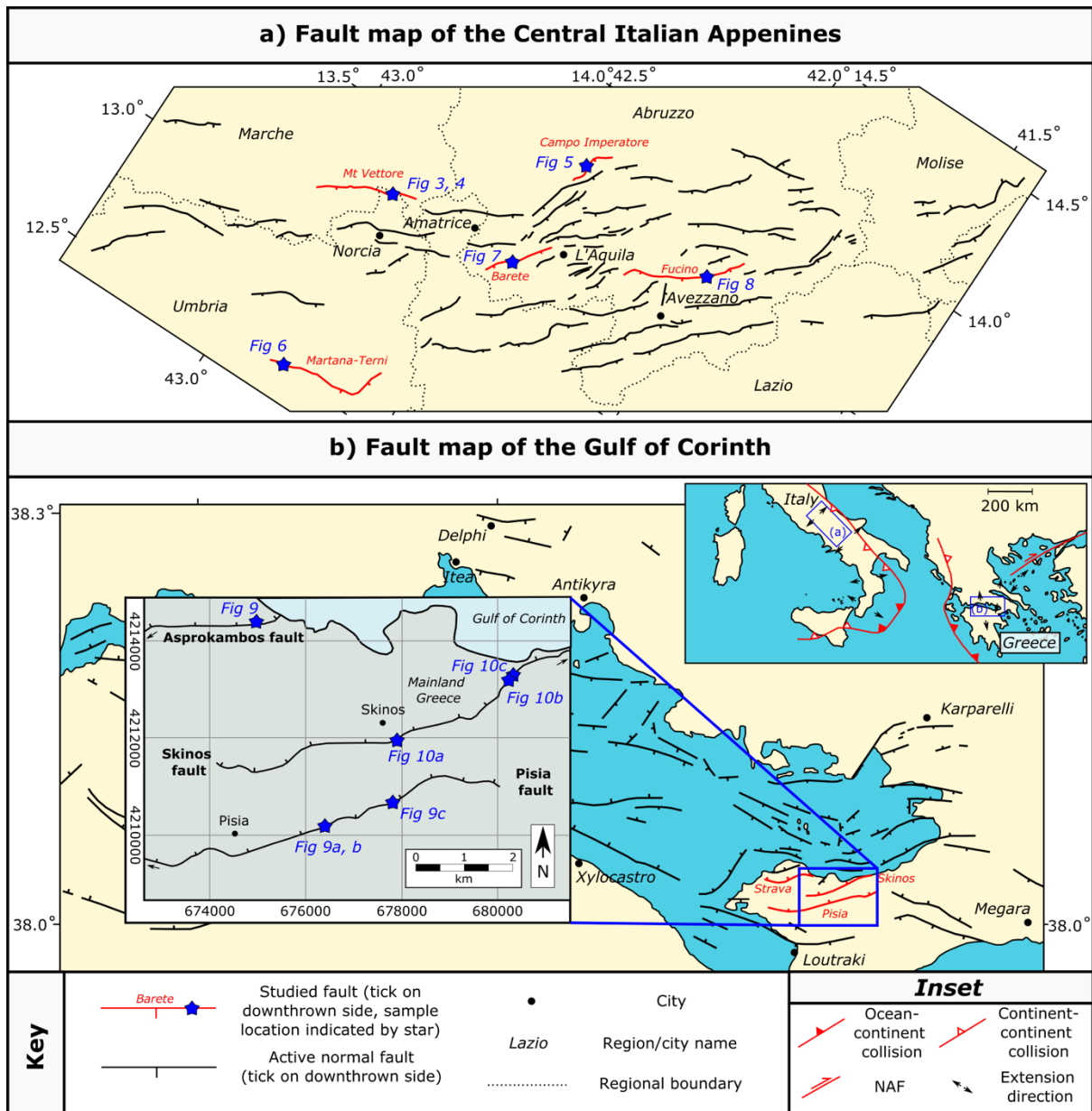
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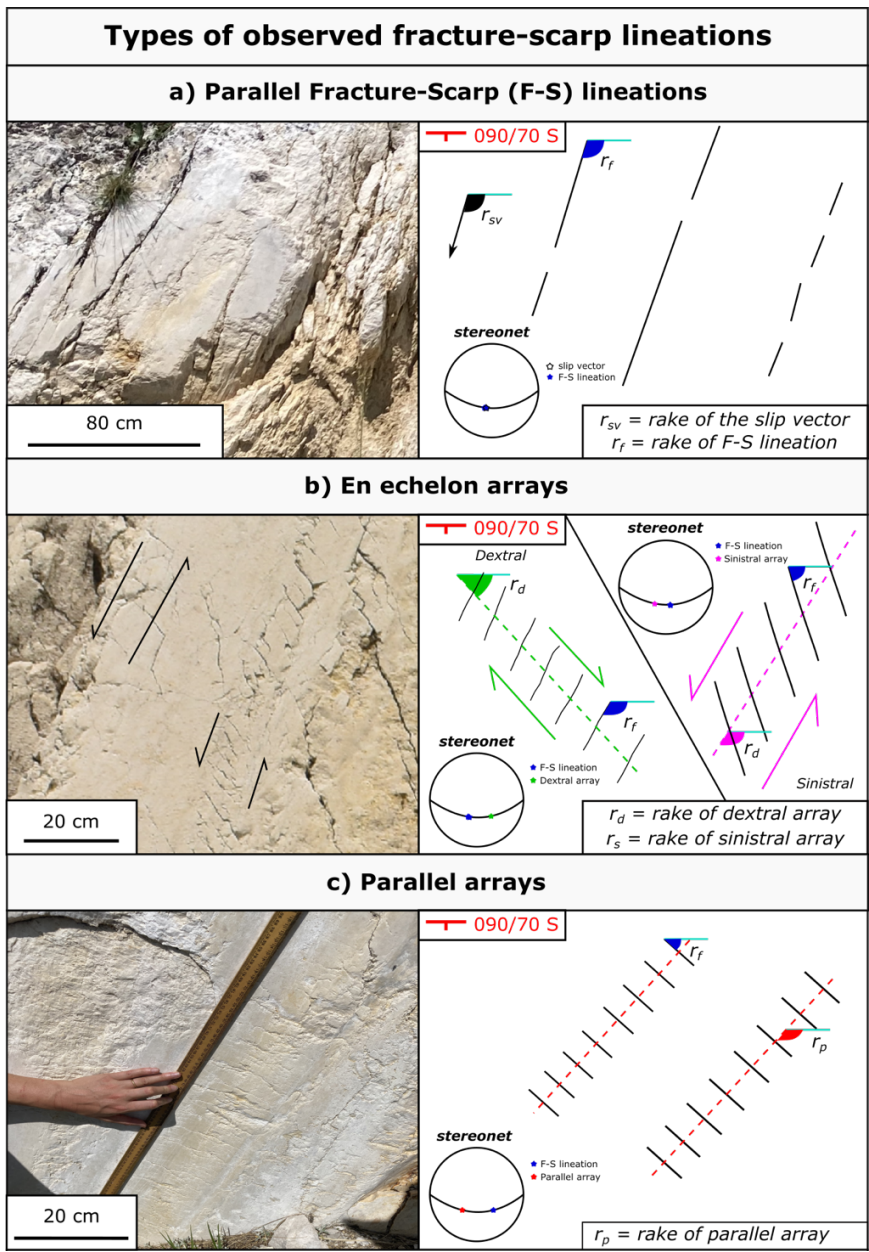
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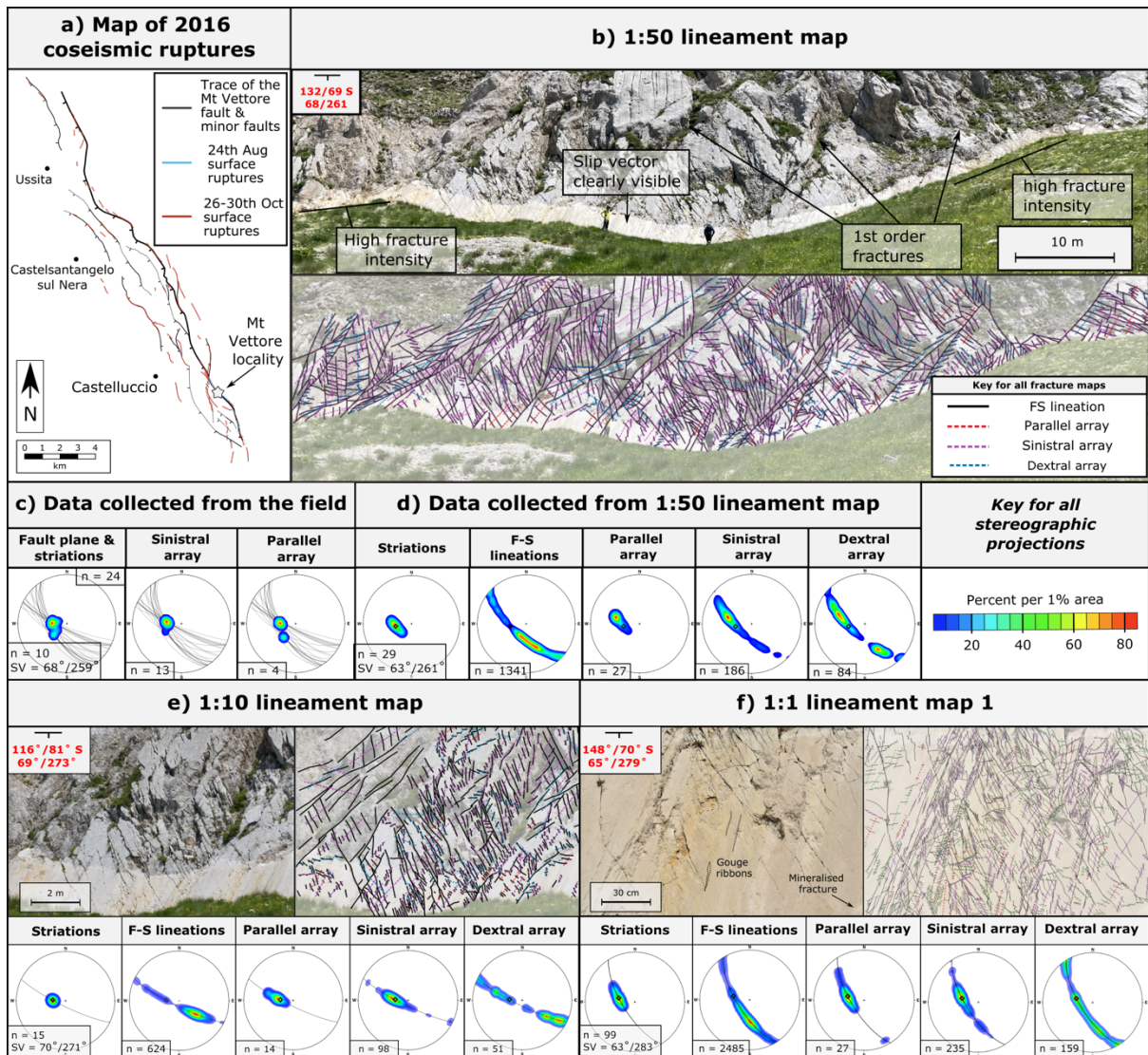
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940 Figure 1: Fault map showing the location of studied faults: a) Fault map of the active faults in
 941 Central Italy (Mildon, 2017); b) fault map of the Gulf of Corinth, showing the location of
 942 studied faults on the Perachora Peninsula (after Moretti et al., 2003). The inset summarises
 943 the regional tectonics of the eastern Mediterranean (after Roberts, 2007).



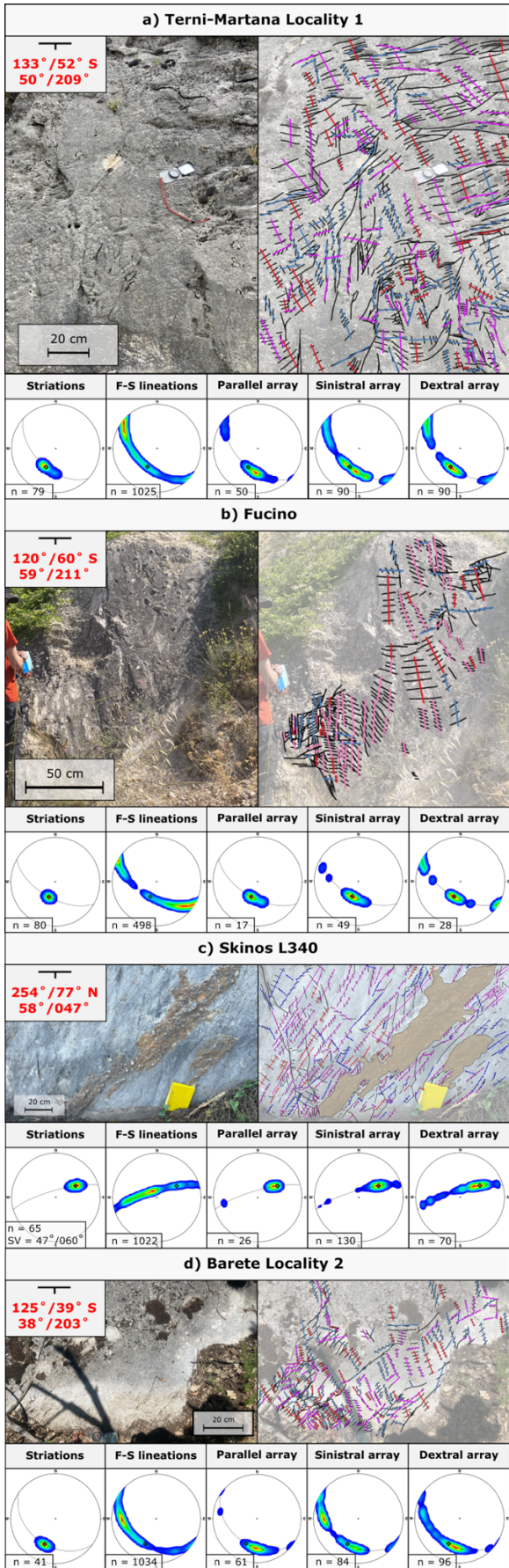
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945 Figure 2: Types of fracture-scarp lineation: a) Parallel Fracture-Scarp (F-S) lineations that
 946 form along a single trend; b) En-echelon arrays consisting of smaller trace length F-S
 947 lineations that display sinistral or dextral shear sense; c) Parallel arrays that are similar to en-
 948 echelon arrays but show no shear sense.

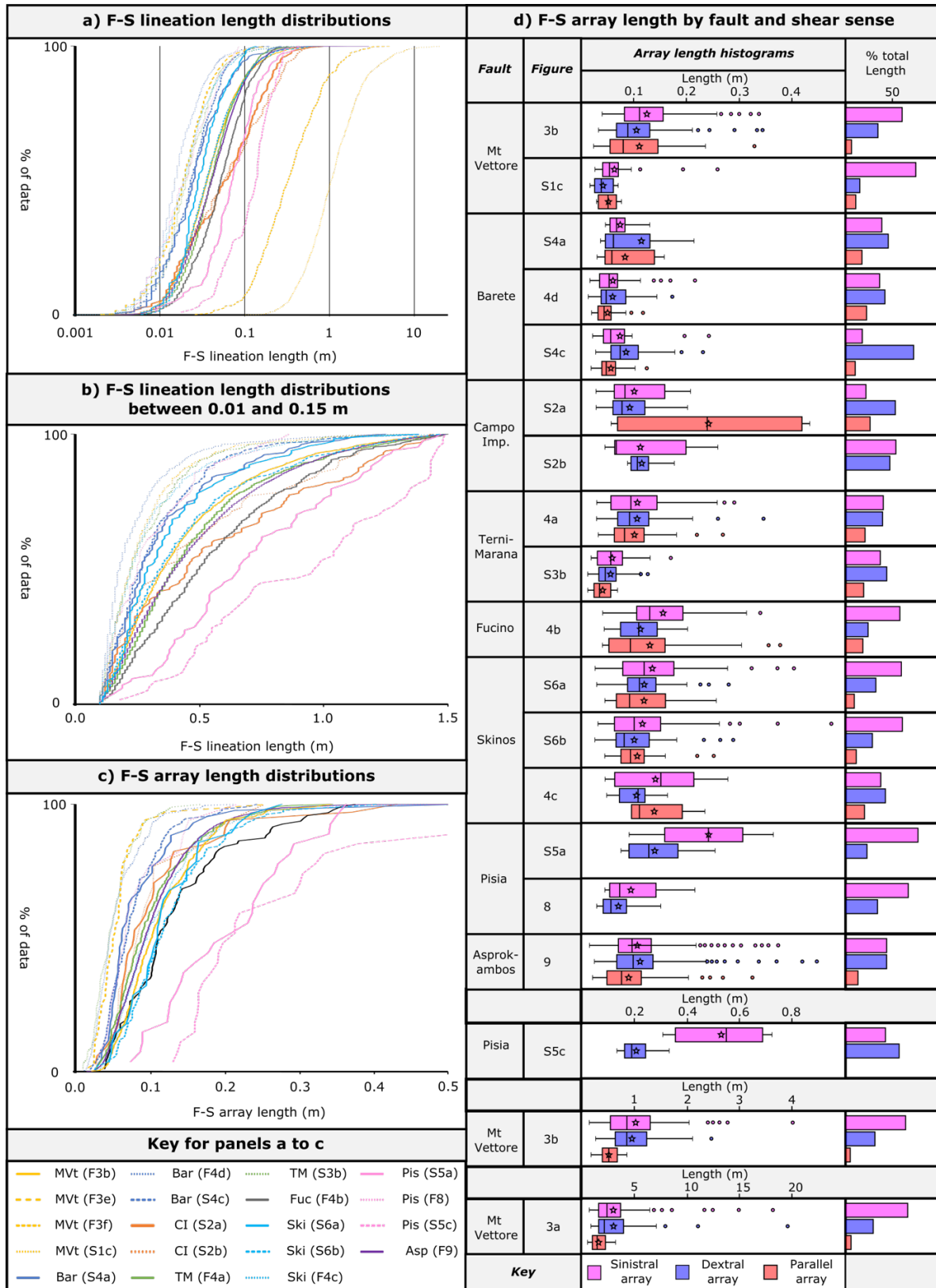


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950 Figure 3: F-S lineation maps for the Mt Vettore location: a) trace of Mt Vettore showing the
 951 location of surface ruptures formed during the 2016 Central Italy earthquake sequence; b)
 952 uninterpreted photograph and 1:50 scale F-S lineation map; stereographic projections of
 953 data collected in the (c) field and (d) extracted from the 1:50 lineament map; uninterpreted
 954 photograph, lineament maps, and stereonets for the (e) 1:10 and (f) 1:1 scale F-S lineament
 955 map. SV = mean dip and plunge of the slip vector, n = number of data points.

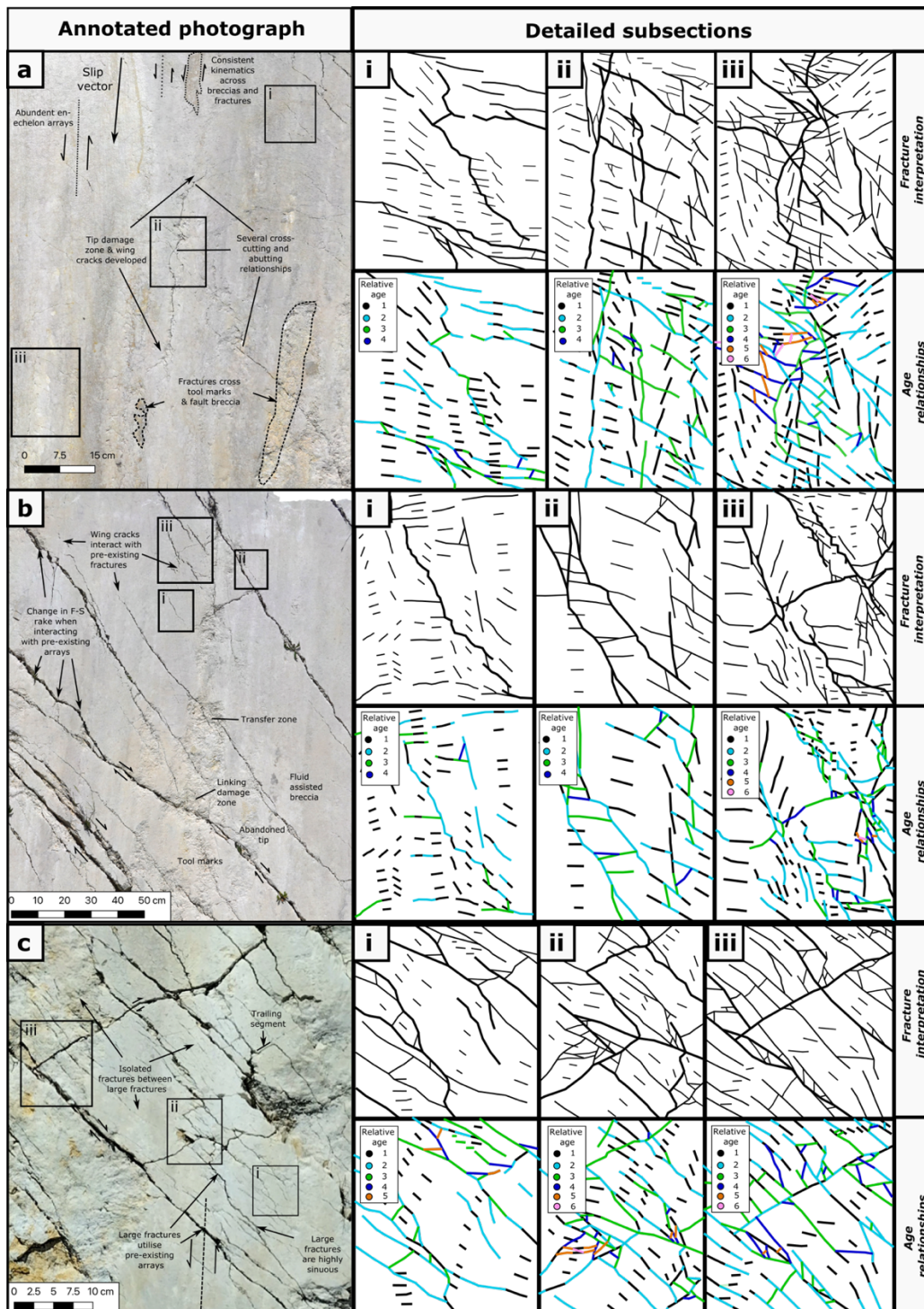


957 Figure 4: Subsection of F-S lineation maps used in this study. Note, all maps are available in
 958 the supplementary information (S1, Figs S1-S6).



959

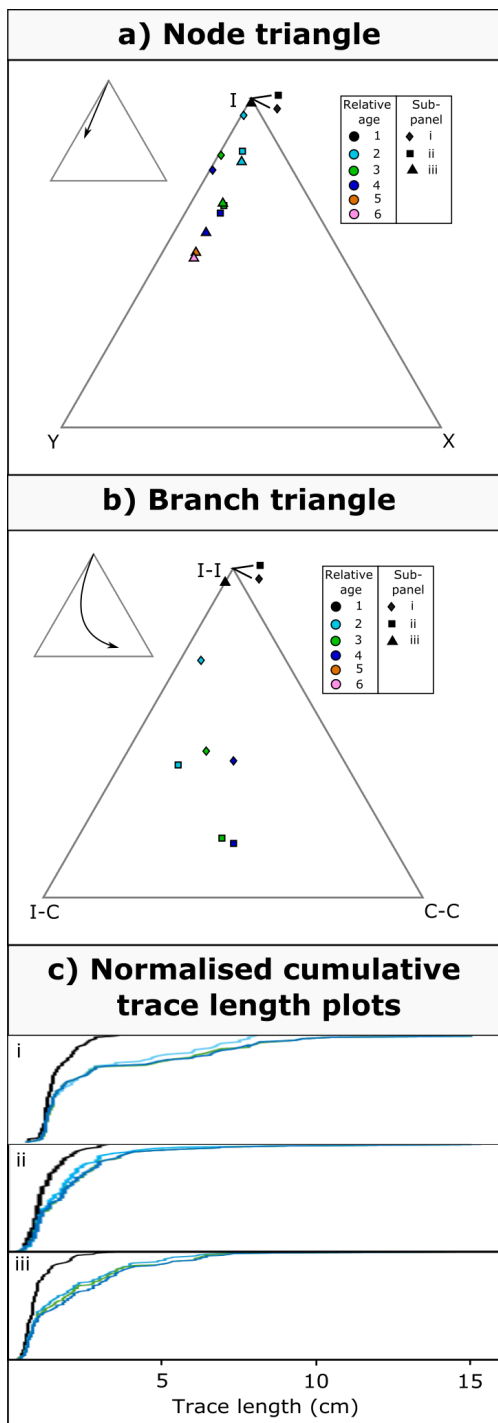
960 Figure 5: Trace length distributions of F-S lineations and arrays: a) F-S lineation length
961 cumulative distributions; b) F-S lineation length cumulative distributions for features, with
962 the x-axis clipped to between 0.01 and 0.15 m to show the distribution of small trace length
963 features; c) F-S array length cumulative distributions; d) box and whisker plots of array
964 length, and proportion of total length, split by the observed shear sense.



965

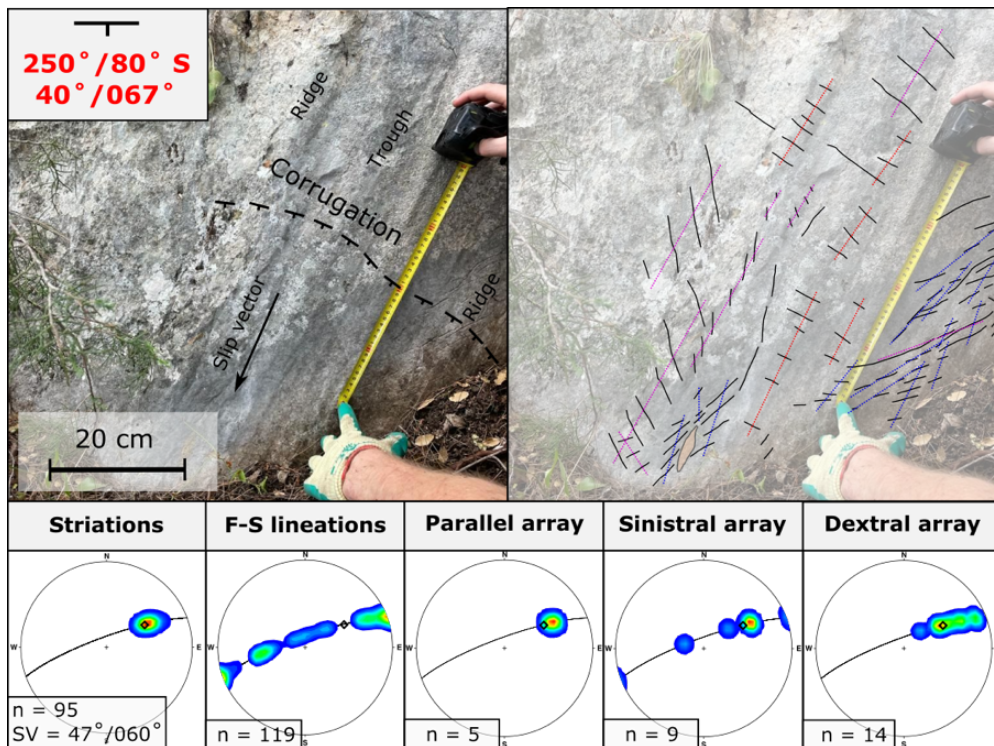
966 Figure 6: Relative age relationships observed across the white ribbon at Mt Vettore. Panels a-
 967 c show progressively trailing more connected fracture networks and for each map, as evidenced by
 968 the increasing fracture intensity, connectivity, and abundance of linkage features (e.g., jogs,
 969 tip damage zones, sinuous fractures). In i-iii, we unpick age relationships for three

970 subsections using abutting and cross-cutting relationships. Note how during age relationship
 971 1 (black lines) all fracture networks start as isolated en-echelon arrays and as the age
 972 relationships increase, fractures progressively increase in length causing fractures to abut
 973 against each other and the connectivity of the network increases.



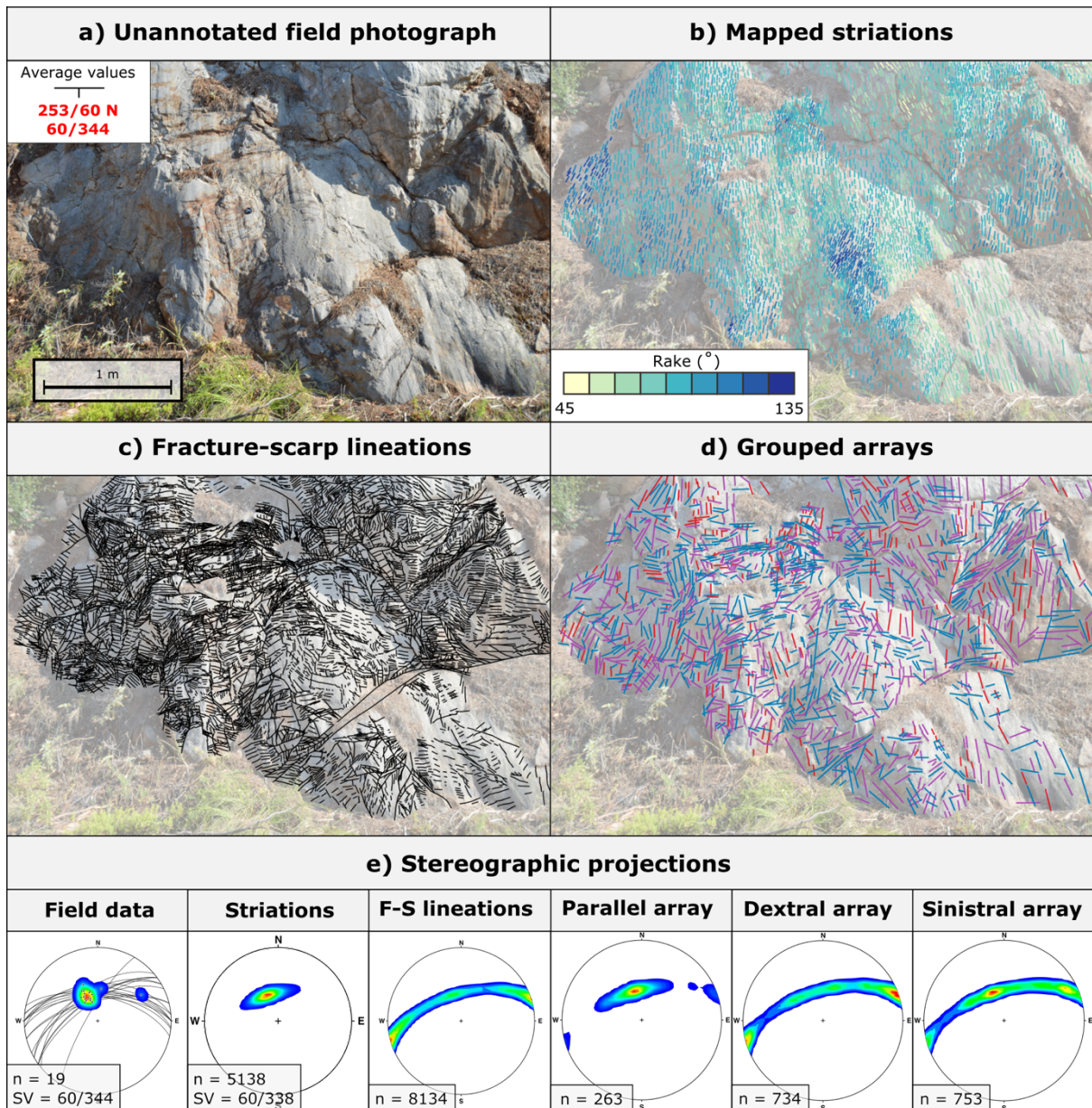
974

975 Figure 7: Topology and length evolution of the F-S lineation network extracted from the
 976 subpanels of the Mt Vettore fault scarp presented in Figure 6a. A) Node triangle showing the
 977 ratio of node types for the subsections of Figure 6a extracted at each relative age
 978 relationship; b) branch triangle showing the ratio of branch classification for the subsections
 979 of Figure 6a extracted at each relative age relationship; c) Normalised cumulative length
 980 plots showing the evolution of F-S length at each relative age relationship. Note how the
 981 connectivity and upper portion of the trace-length distribution increases as the fracture
 982 network develops.



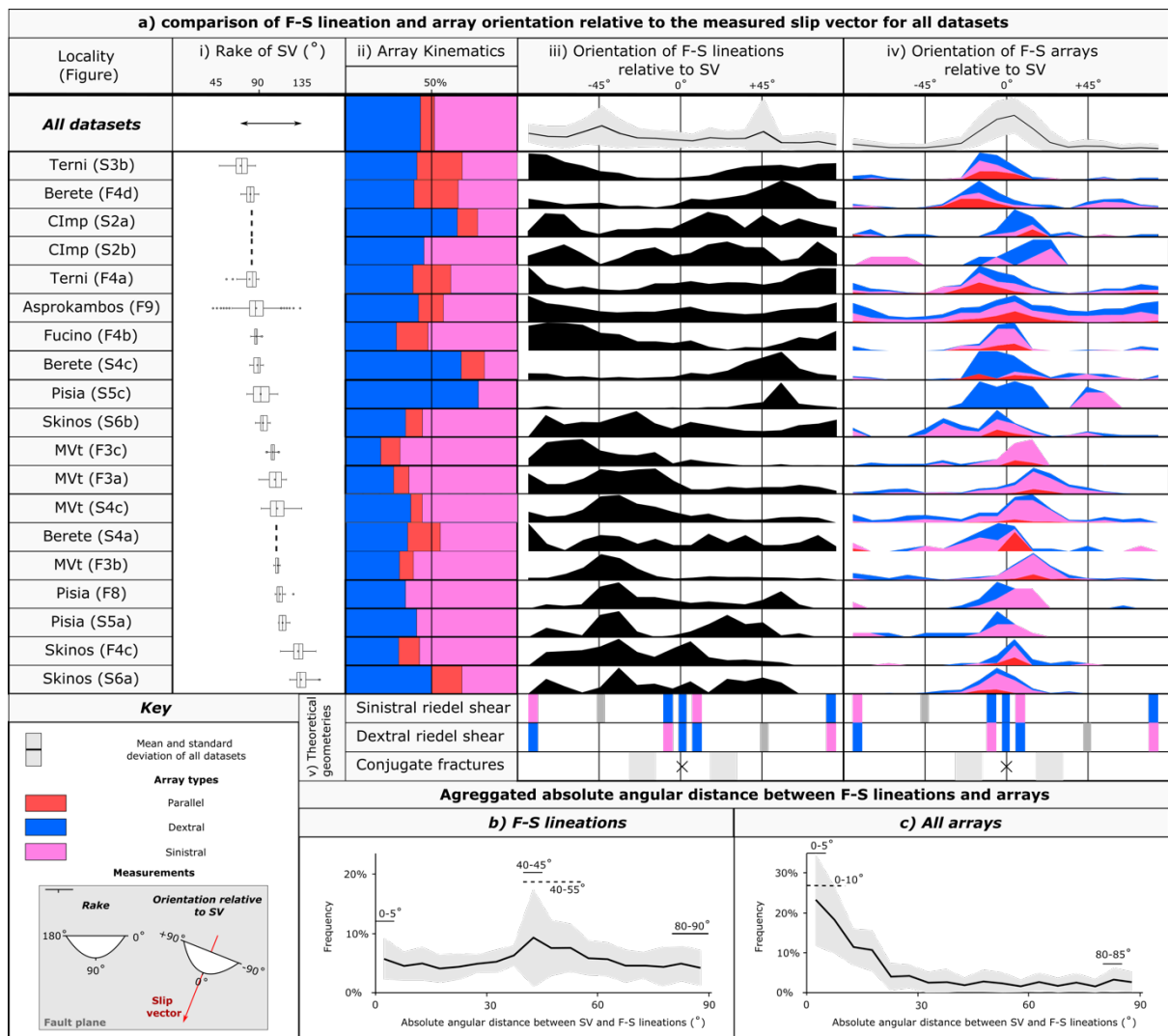
983
 984 Figure 8: F-S lineations and arrays around a corrugation. Note how the orientation and
 985 kinematics of F-S lineation arrays differ either side of the corrugation.

986



987

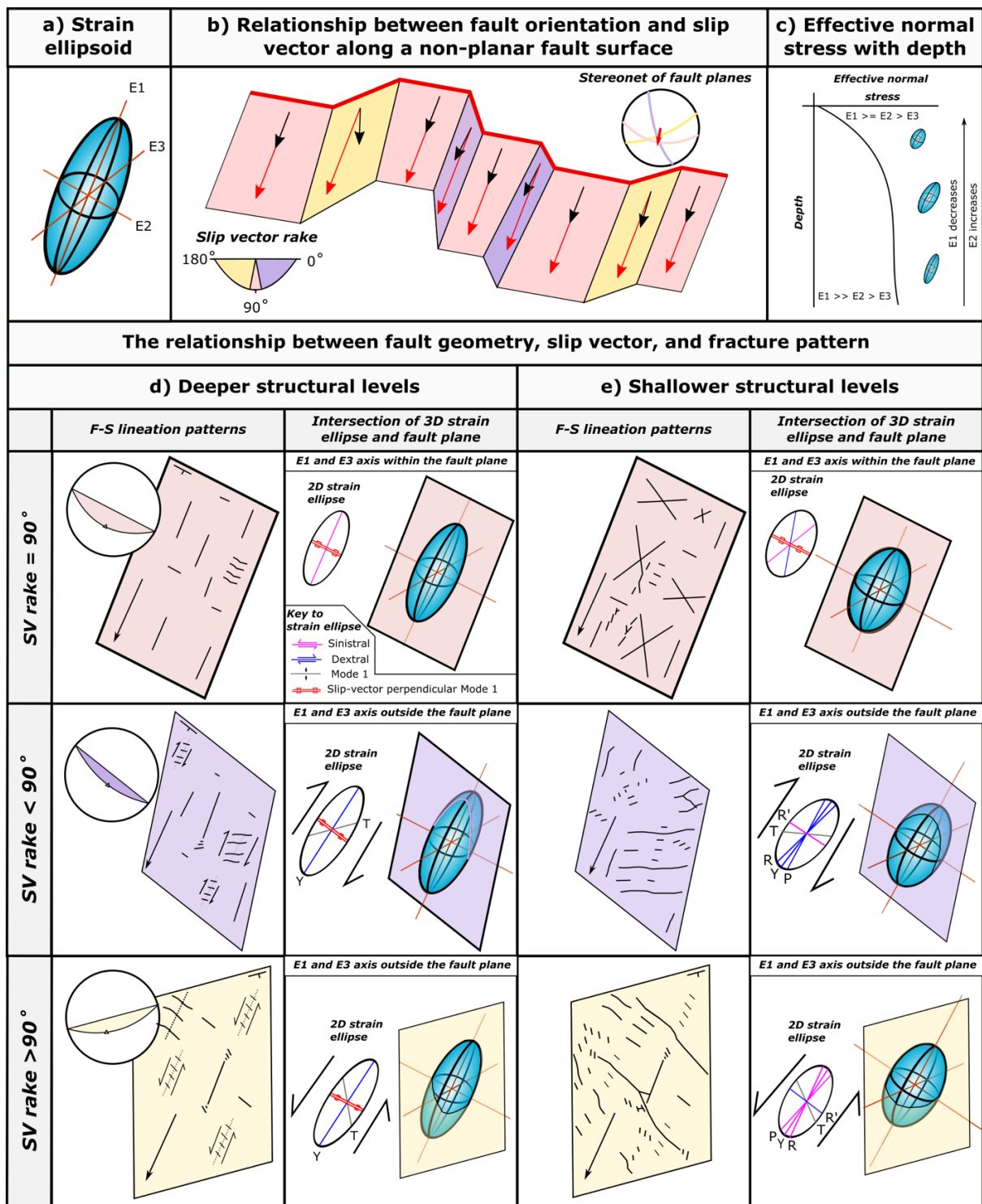
988 Figure 9: Distribution of (b) striations, (c) F-S lineations and (d) arrays across the
 989 Asprokambos fault locality; e) stereographic projections of field and photo derived data.
 990 Note how convergent and divergent slip vectors are recorded, and that in areas where
 991 shallower slip-vectors are observed, that the rake and shear sense of F-S arrays also differ.



992

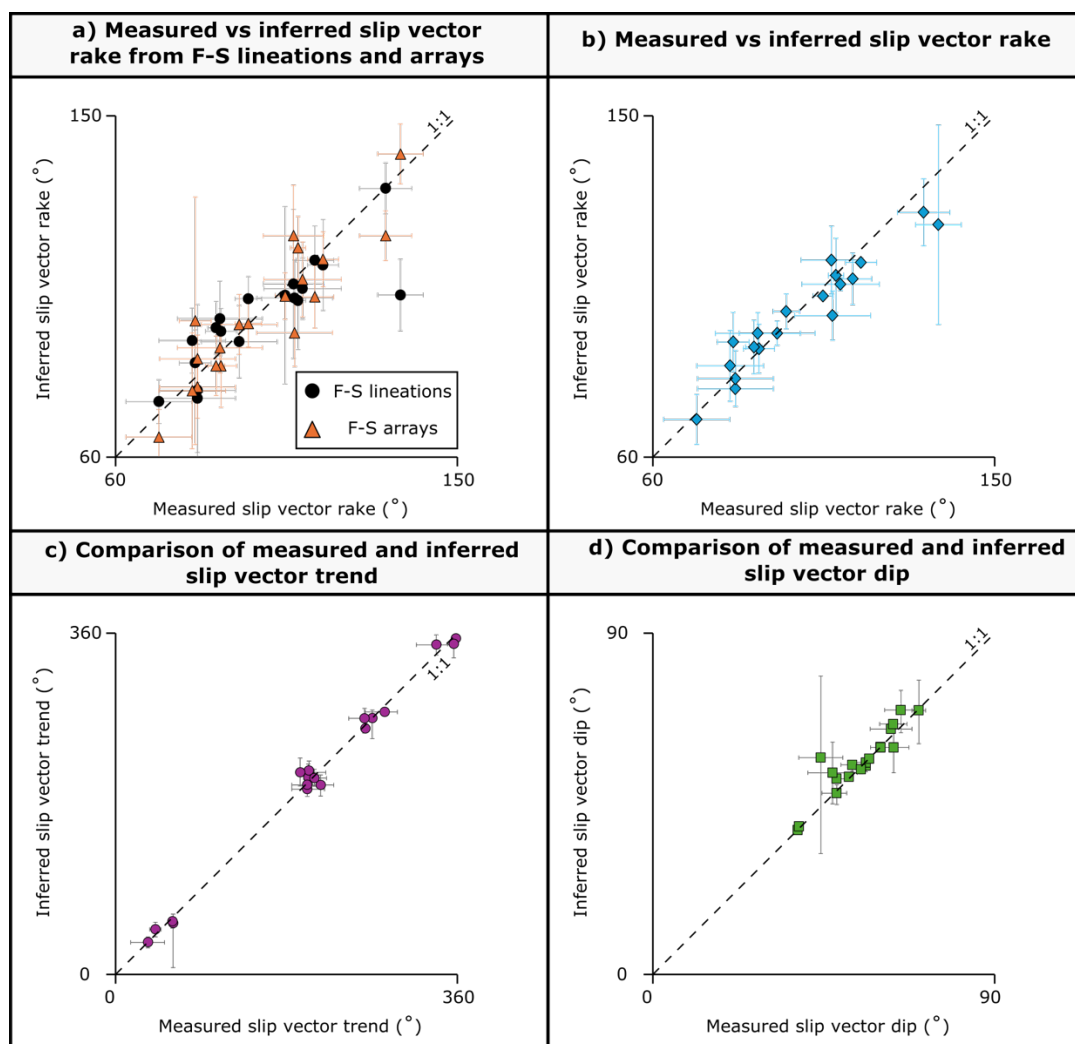
993 Figure 10: The orientation of F-S lineations and arrays relative to the slip vector: a)
 994 comparison of F-S lineation and array orientations with the measured slip vector, showing i)
 995 box and whisker plots of slip vector rake distributions, ii) the relative abundance of different
 996 shear sense arrays, normalised 10bin histograms of iii) F-S lineations and iv) arrays, where
 997 the y-axis is the maximum value for each F-S lineation map, and v) the expected orientations
 998 of features according to a radial shear geometry; normalised aggregated absolute angular
 999 distance between F-S lineations (b) and arrays (c) to the slip vector for all studied faults (see
 1000 measurements in the key for how measurements are taken. Note the relationship between

1001 slip vector rake and proportion of dextral to sinistral arrays, and the peaks observed in (b)
 1002 and (c).



1003
 1004 Figure 11: Conceptual model for the formation of F-S lineations and arrays: a) 3D strain
 1005 ellipsoid, showing the three principle axes E1, E2 and E3; b) a schematic relationship

1006 between fault plane geometry and slip vector around prominent fault bends whereby slip
 1007 vector remains constant; c) the suggested effect of footwall uplift on the effective normal
 1008 stress acting on the fault plane; the relationship between fault plane geometry, slip vector,
 1009 the schematic expected fracture patterns, and the intersection of between the fault plane
 1010 and 3D strain ellipsoid for the schematic fault orientations at (d) deeper and (e) shallower
 1011 depths.



1012

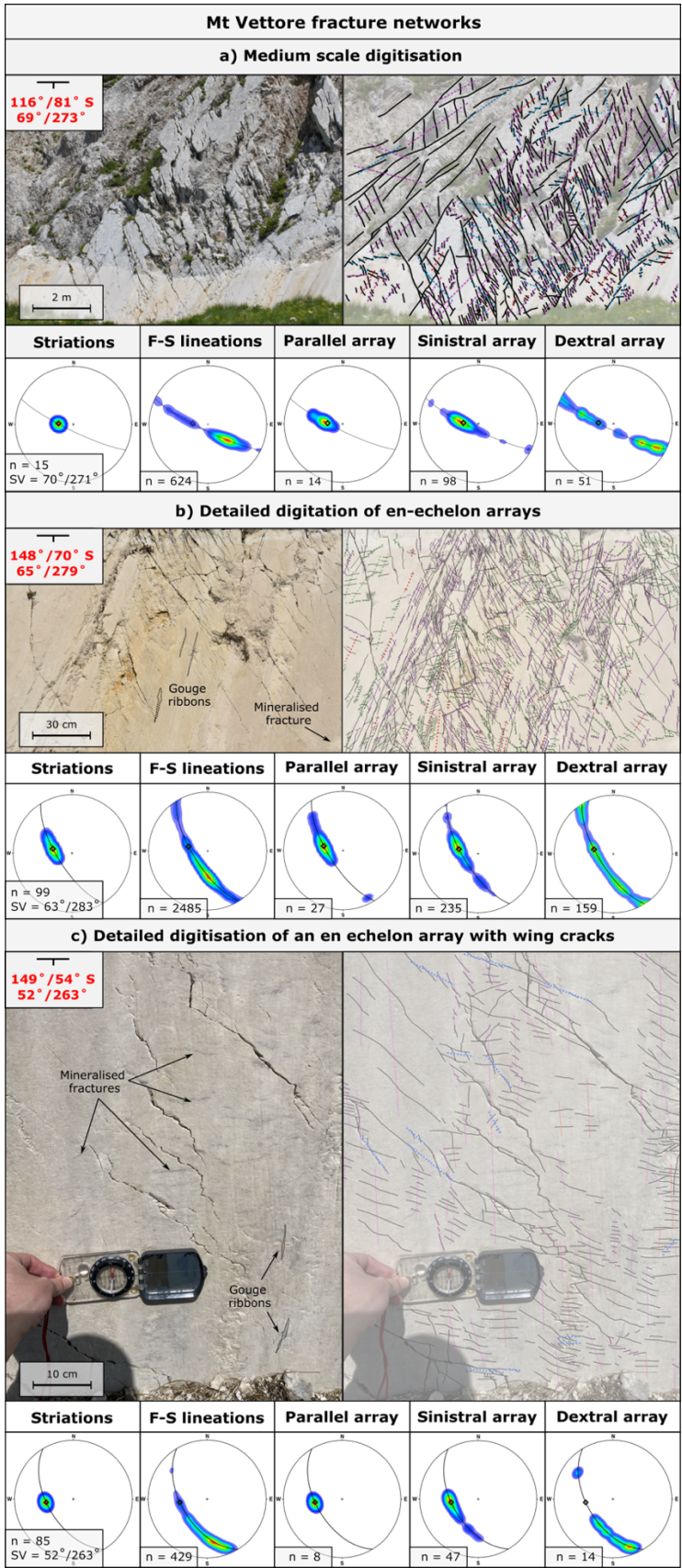
1013 Figure 12: Comparing the measured slip vector from striations to slip vector inferred from F-
 1014 S lineations for all F-S lineation maps: Reliability of assigning generic trends to individual
 1015 faults when inferring slip vector: a) comparison of slip vector inferred using F-S lineations

1016 (circles) and F-S arrays (triangles) with the slip vector measured from striations; b)
 1017 comparison of averaged inferred slip vector using both F-S lineations and arrays with the slip
 1018 vector measured from striations; c) comparison of the inferred slip-vector trend with that
 1019 measured from striations; d) comparison of the inferred slip-vector dip with that measured
 1020 from striations. For all plots, the error bars represent one standard deviation either side of
 1021 the mean. Note how the average of F-S lineation and F-S array inferred rake (b) is closer to
 1022 the measured rake than when they are considered separately.

1023 **Tables**

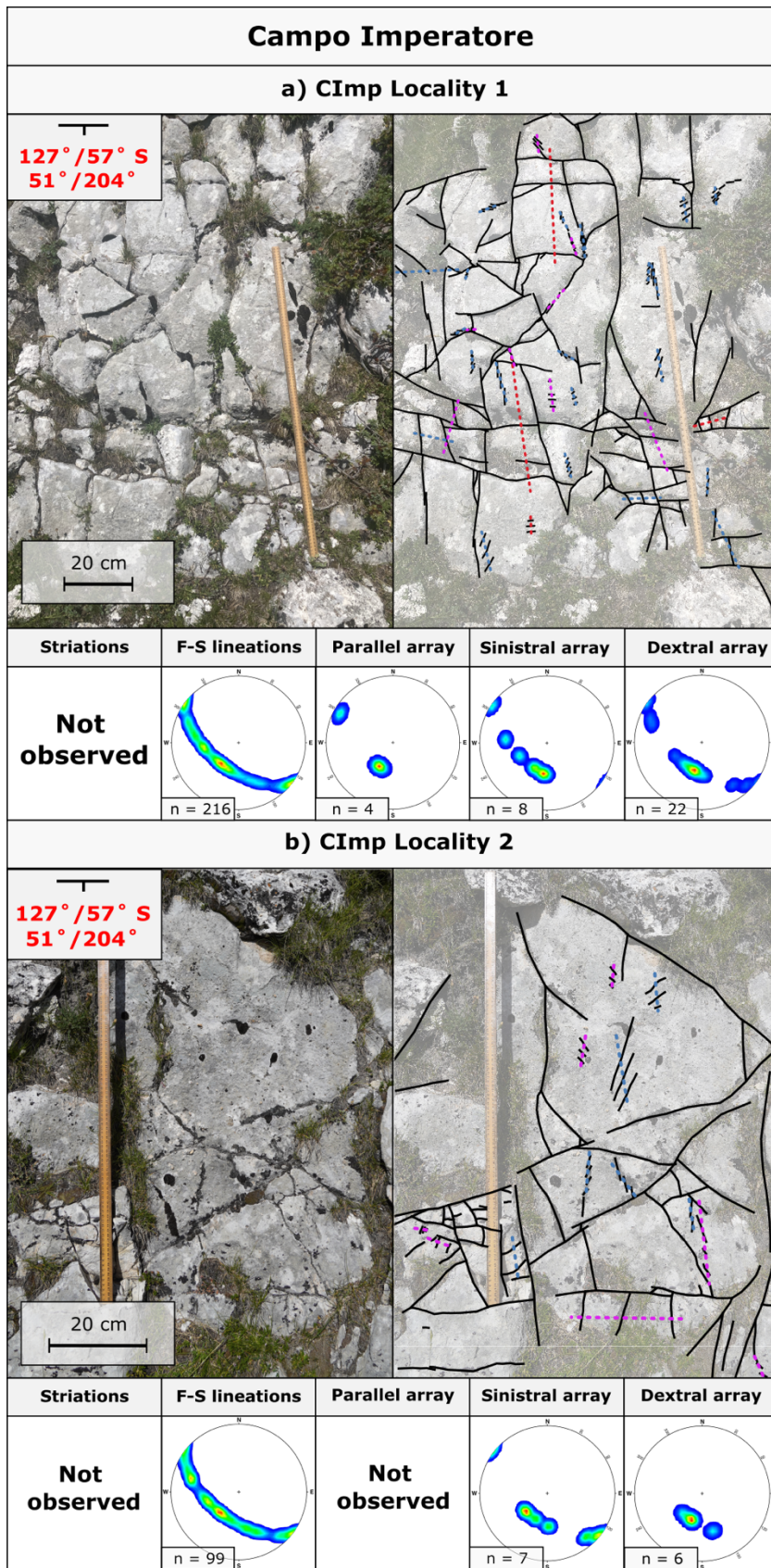
Fault	Fig	Measured SV			Inferred SV			Difference between inferred and measured SV		
		Rake (°)	Dip (°)	Trend(°)	Rake (°)	Dip (°)	Trend(°)	Rake (°)	Dip (°)	Trend(°)
Barete	7a	107	52	216	97	55	200	9.7	3	15.7
	7b	80.9	38	203	90	39	216	9.5	1	12.1
	7c	87.7	38	207	89	38	208	0.9	0	1.1
Campo Imperatore	5a	81.5	56	202	78	55	196	3.4	1	5.9
	5b	81.5	56	202	81	56	200	0.8	0	1.4
Fucino	8	86.4	60	203	89	60	208	2.7	0	5.4
Mt Vettore	4c	104.6	52	263	103	52	260	2.0	1	3.1
	4a	108	70	270	108	70	271	0.3	0	0.4
	4b	109.2	63	284	106	65	277	3.5	2	6.1
	3	106.8	63	262	112	60	271	5.3	3	8.5
Pisia	9a	114.6	63	358	111	66	355	3.2	3	3.4
	9b	112.4	65	356	107	70	349	5.3	5	7.0
	9c	92.5	57	34	93	57	34	0.2	0	0.3
Skinos	10a	135	44	60	121	57	54	13.6	13	6.0
	10c	131.1	47	60	125	53	56	6.4	6	3.5
	10b	94.9	55	42	98	54	48	3.6	1	6.1
Asprokambos	12	87.4	60	338	93	60	348	5.3	0	10.6
Terni-Martana	6a	80.1	48	194	84	52	214	4.0	3	19.3
	6b	71.3	48	209	70	48	207	1.3	1	1.8

1024 Table 1: Calculated slip vector from F-S lineations, see Supplementary 6 for calculation using
 1025 F-S lineations and F-S arrays separately, and for the spreadsheet to calculate slip vector from
 1026 rake clusters.



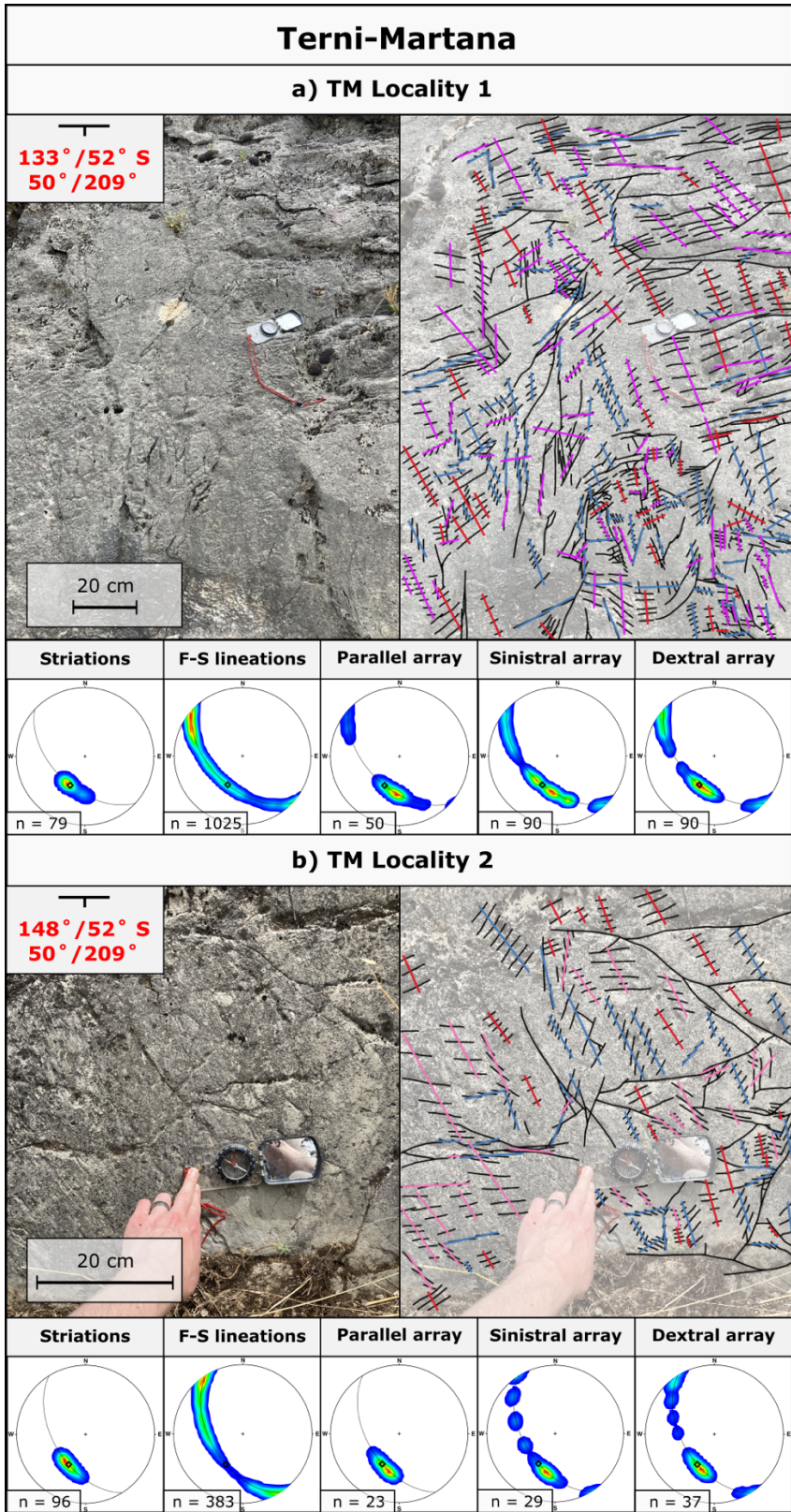
1027

1028 Figure S1: 1:10 and 1:1 F-S lineation and array maps across the Mt Vettore location.



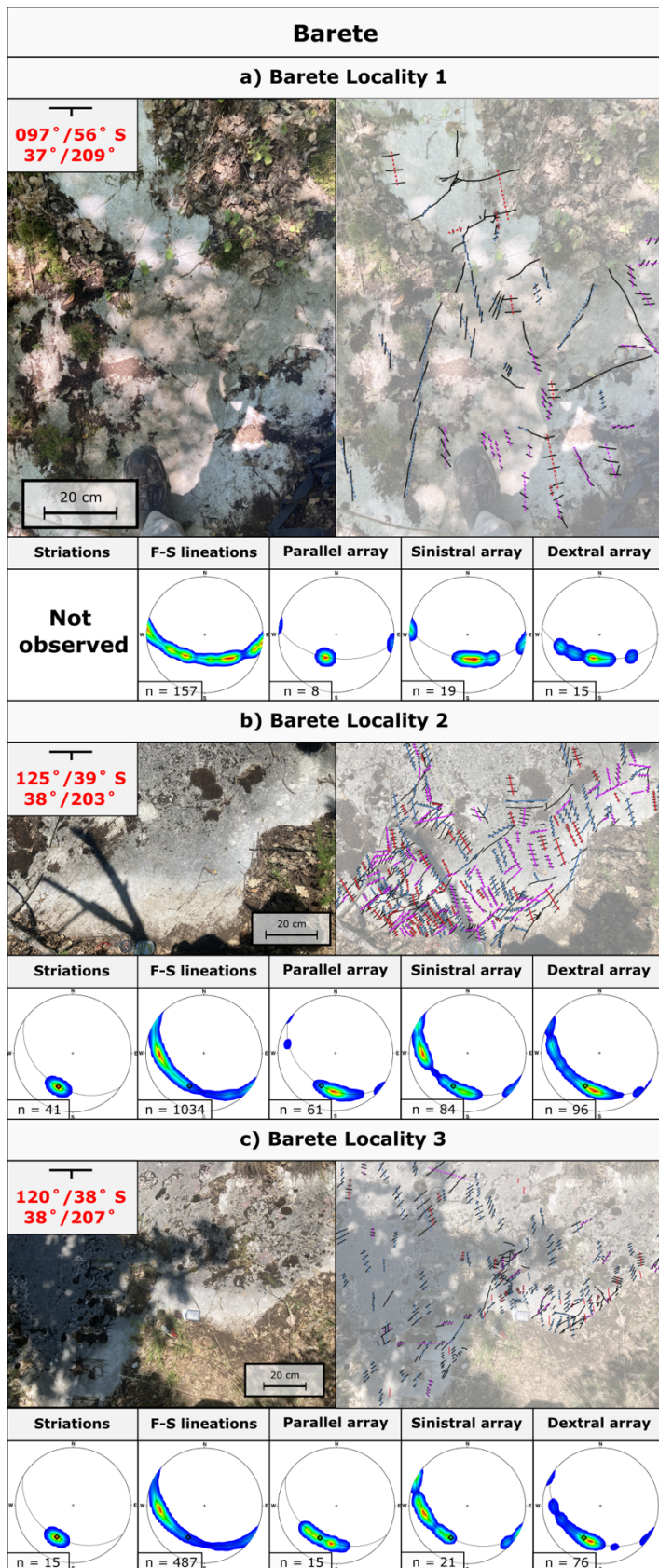
1029

1030 Figure S2: All F-S lineation and array maps across the Campo Imperatore location.



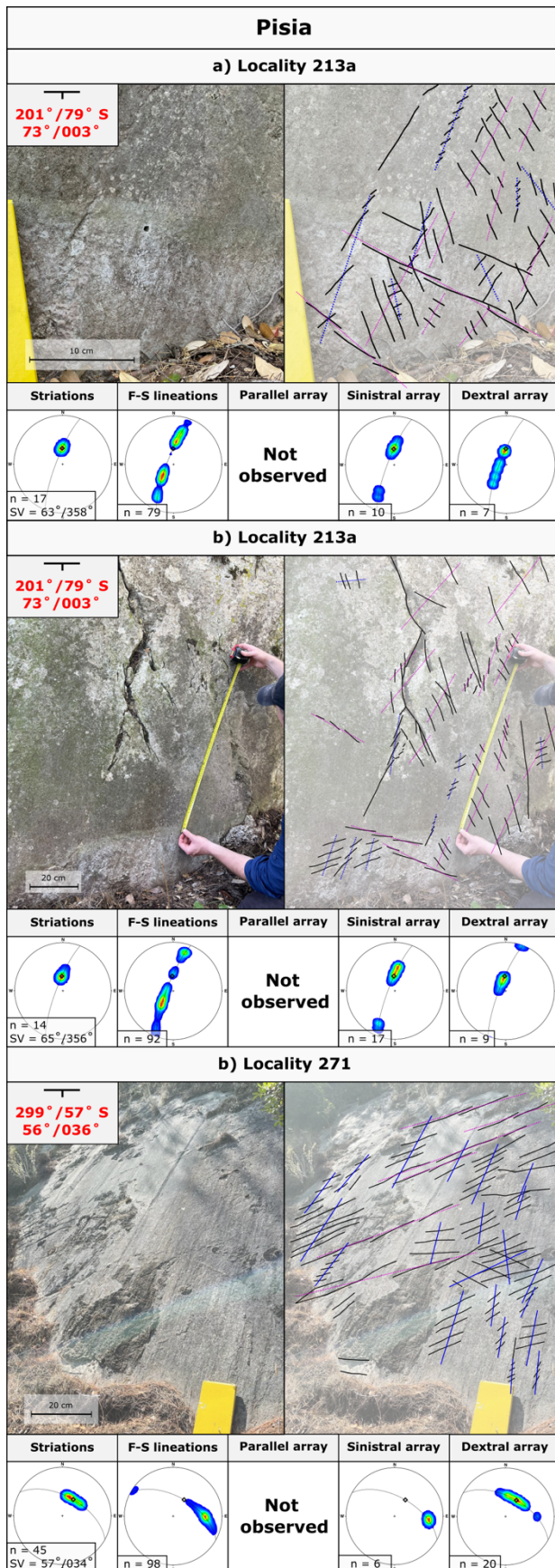
1031

1032 Figure S3: All F-S lineation and array maps across the Terni-Martana location.



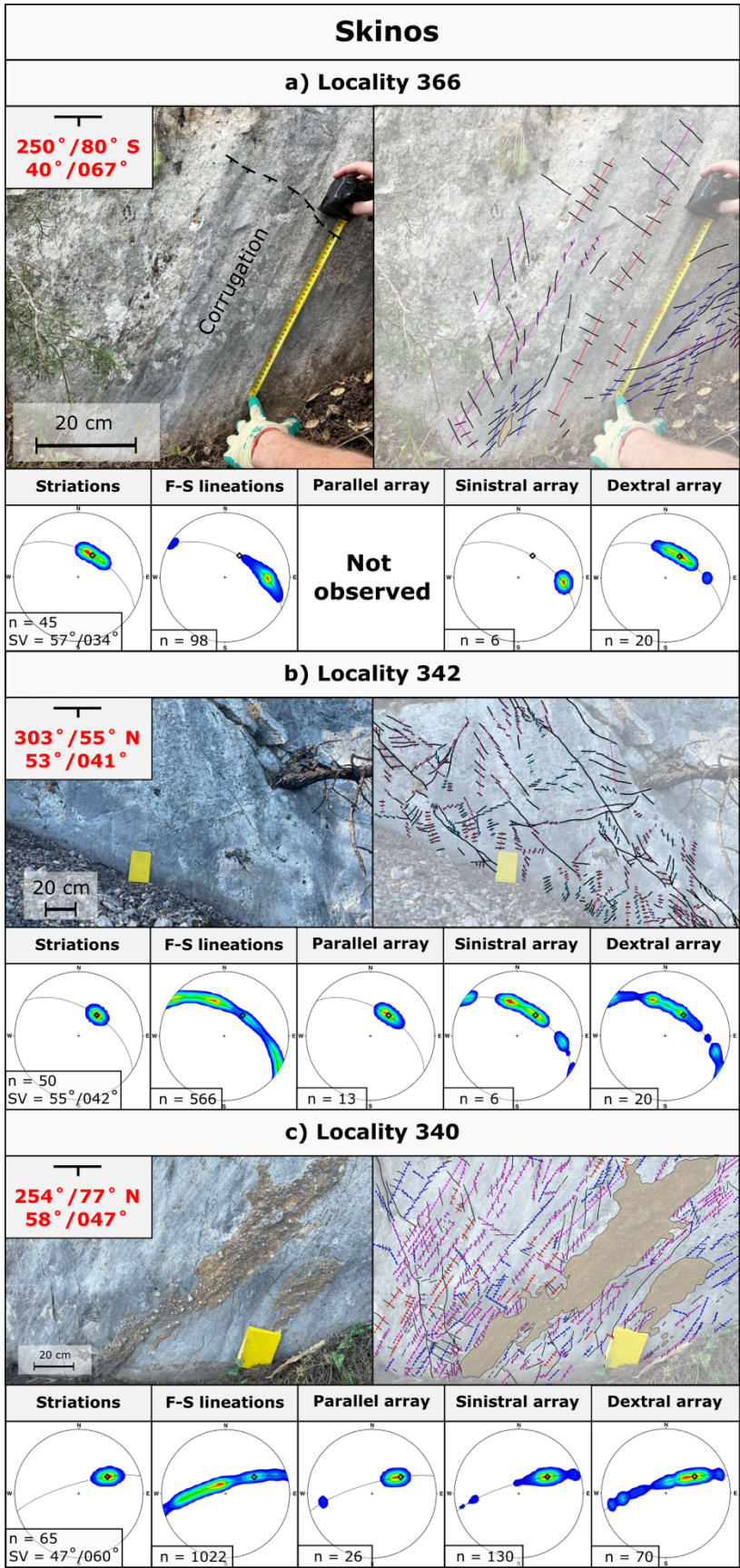
1033

1034 Figure S4: All F-S lineation and array maps across the Barete location.



1035

1036 Figure S5: All F-S lineation and array maps across the Pisia location.



1037

1038 Figure S6: All F-S lineation and array maps across the Skinos location.