

---

This manuscript has been submitted for publication in GEOLOGY. Please note that subsequent versions of this manuscript may have different content. If accepted, the final version of this manuscript will be available via the 'Peer-reviewed Publication DOI' link on the right-hand side of this webpage. Please feel free to contact any of the authors; we welcome feedback.

---

# 1 How erosive are submarine landslides?

2 **Harya D. Nugraha<sup>1,2,\*</sup>, Christopher A-L. Jackson<sup>1</sup>, Howard D. Johnson<sup>1</sup>, David M.**

3 **Hodgson<sup>3</sup> and Michael A. Clare<sup>4</sup>**

4 *<sup>1</sup>Basins Research Group (BRG), Department of Earth Science and Engineering, Imperial*  
5 *College, London SW7 2BP, UK*

6 *<sup>2</sup>Department of Geological Engineering, Universitas Pertamina, Jakarta 12220, Indonesia*

7 *<sup>3</sup>School of Earth and Environment, University of Leeds, Leeds LS2 9JT, UK*

8 *<sup>4</sup>National Oceanography Centre, Southampton SO14 3ZH, UK*

9 \*E-mail: [harya.nugraha14@imperial.ac.uk](mailto:harya.nugraha14@imperial.ac.uk)

## 10 **ABSTRACT**

11 Submarine landslides are ubiquitous on continental margins worldwide. They can pose a major  
12 hazard through triggering tsunami and can damage essential seabed infrastructure. Although slide  
13 volume, which can change through time due to substrate entrainment, is a key parameter in  
14 offshore hazard assessment, we have a poor understanding however of how erosive submarine  
15 landslides can be. Here, we use a novel method to quantify erosion, by determining the ratio of  
16 deposited ( $V_d$ ) to initially evacuated ( $V_e$ ) slide volumes. Slides that gain volume (i.e. erode) equate  
17 to a ratio of  $V_d/V_e > 1$ . We demonstrate this method by analysing 3D seismic reflection datasets  
18 that include the recent Gorgon Slide ( $500 \text{ km}^3$ ), offshore NW Australia, before determining  $V_d/V_e$   
19 ratios for other large slides worldwide. Nine of the 11 published slides have  $V_d/V_e > 1$  (median  
20 value=2), showing that emplaced slide volumes are typically larger than the initial failed volume,  
21 confirming the erosivity of their parent flows. The Gorgon Slide is the most erosive submarine  
22 landslide currently documented, having ‘bulked up’ by an order of magnitude ( $V_d/V_e=12$ ). We

23 suggest its strongly erosive nature is related to the carbonate ooze substrate, which dramatically  
24 lost strength under loading. This new approach to quantifying erosion is important for geohazard  
25 assessments as substrate—flow interactions control slide speed and run-out distance. Our new  
26 insights into variations in slide volume have important implications for seabed infrastructure  
27 impact assessments and should enable more robust tsunami modelling.

## 28 INTRODUCTION

29 Submarine landslides (hereafter “slides”) are key components of many deep-water  
30 successions, with individual deposits covering areas  $>100 \text{ km}^2$  and comprising volumes  $>10,000$   
31  $\text{km}^3$  (e.g. Moscardelli and Wood, 2016). These slides can be tsunamigenic, such as in Papua New  
32 Guinea where a slide triggered a tsunami that killed  $>2000$  people (Tappin et al., 2001). Slides can  
33 also damage critical seabed infrastructure, such as the global network of telecommunication cables  
34 (Carter et al., 2014), and oil and gas pipelines (e.g. Randolph and White, 2012). To date, most  
35 studies have focused on siliciclastic slides (e.g. see synthesis by Moscardelli and Wood, 2016),  
36 yet, carbonate ooze occupies a significant portion (c.30%) of the world’s ocean floor (see  
37 Appendix DR1, Dutkiewicz et al., 2015). Such carbonate oozes are known to behave differently  
38 to siliciclastic sediments, so how do these differences affect slide dynamics? The post-failure shear  
39 strength of carbonate ooze can be as low as 10% of its original strength, compared to 55% for  
40 siliciclastic clay (Gaudin and White, 2009). Slides involving or being transported over ooze-  
41 dominated seafloor may thus be more erosive (Winterwerp et al., 2012). It is therefore important  
42 to investigate how carbonate slides behave to better understand their potential impact on offshore  
43 infrastructure and their tsunamigenic potential.

44 During transport, a slide can be detached from its underlying substrate by a thin lubricating  
45 layer at the base of flow, i.e. hydroplaning (e.g. Mohrig et al., 1998). In this case, slide transport

46 and emplacement will result in no erosion, and even volume loss due to partial flow transformation  
47 from debris flow to turbidity current (e.g. Sun et al., 2018). However, three-dimensional seismic  
48 reflection data provide compelling evidence that substrate deformation and entrainment is a  
49 common process, leading slides to gain volume during transport. Indicators of substrate erosion  
50 and deformation include grooves and striations (e.g. Gee et al., 2005), ramps and flats (e.g. Bull et  
51 al., 2009), downslope-diverging peel-back scours (e.g. Sobiesiak et al., 2018), and megaclasts of  
52 substrate within debrites (e.g. Hodgson et al., 2018). Despite widespread evidence for erosion, the  
53 degree of substrate entrainment during slide emplacement is poorly constrained, at least partly  
54 because of the limited exposure of exhumed slides in the field, and poor imaging by and/or limited  
55 coverage of subsurface data (e.g. seismic reflection data). Quantifying erosivity is important  
56 because: 1) entrained material during transport through basal erosion could modify slide speed and  
57 run-out distance, two key parameters for both tsunami modelling and impact assessments on  
58 submarine infrastructures (e.g. Bruschi et al., 2006); and 2) initial failed volume is a key parameter  
59 in tsunami modelling (e.g. Murty, 2003).

60 Here, we use 3D seismic reflection data from the Exmouth Plateau, offshore NW Australia,  
61 to quantify the erosivity of the Gorgon Slide (Fig. 1). This study focuses on the discrepancy  
62 between the volumes of evacuated ( $V_e$ ) and deposited ( $V_d$ ) sediments. A new measure, the  $V_d/V_e$   
63 ratio, is introduced as a first-order estimate to quantify slide erosivity, where  $V_d/V_e > 1$  indicates  
64 substrate entrainment during transport (see Dataset and Methods). In addition, we also analyse  
65 other slides for which  $V_d$  and  $V_e$  are documented (e.g. Moscardelli and Wood, 2016). Our  
66 approach allows us to gain insights into overall physical processes occurring during the transport  
67 processes of slides and help us improve our ability to accurately assess the threat they pose to  
68 seabed infrastructure and to better constrain tsunami triggering models.

69 **GEOLOGICAL SETTING**

70           The Exmouth Plateau formed due to multiple rifting events, which commenced in the Late  
71 Jurassic and continued into the Early Cretaceous (Fig. 1A) (Longley et al., 2002). Post-rift  
72 deposition has been dominated by carbonates since the Late Cretaceous (Apthorpe, 1988).  
73 Miocene collision of the Australian Plate with the Eurasia and Pacific plates triggered structural  
74 inversion, promoting slope steepening across the plateau and present-day shelf (Keep et al., 1998).  
75 High fluid pressures and seismic shaking associated with this structural inversion both primed and  
76 triggered slope failure, and the emplacement of multiple slides across the plateau (e.g. Scarselli et  
77 al., 2013). Here we focus on the most recent slide, known as the Gorgon Slide (Fig. 1B-C).

78 **DATASET AND METHODS**

79           We analyse five 3D seismic reflection datasets (Fig. 1) that image both the evacuation and  
80 deposition zones of the Gorgon Slide and the adjacent, unfailed continental slope (Fig. 1B-C).  
81 Given a near seabed sediment velocity of 1824 m/s, and dominant frequency of 40-60 Hz, the  
82 estimated vertical resolution at the base of the Gorgon Slide (c.500 m below seabed) ranges from  
83 8-11 m, with the 3D volumes having bin spacings of 12.5 x 18.75 m and 20 x 25 m (see Appendix  
84 DR2 for details). The present seabed and base of the Gorgon Slide (see Fig. 1D-E) were converted  
85 from time to depth using average water velocity (1519 m/s) and average near seabed sediments  
86 velocity (1824 m/s), respectively (Appendix DR2). Ten industry wells constrain the water velocity  
87 (Fig. 1B). Well ODP 762, located c.200 km NW of our seismic datasets, penetrated a similar  
88 seismic stratigraphic sequence to that encountered in the study area; we therefore used data from  
89 this well to infer near seabed lithology and its physical properties (e.g. velocity and porosity; Fig.  
90 1A).

91 We calculate the ratio between the volume of the slide source or evacuated area ( $V_e$ ) and  
92 the slide itself ( $V_d$ ) to derive a first-order estimation of slide erosivity (Fig. DR3A). When  
93  $V_d/V_e < 1$ , we infer the slide loses volume during transport; this could reflect partial flow  
94 transformation from debris flow to turbidity current, resulting in turbidite deposition beyond the  
95 slide pinchout (Fig. DR3B). When  $V_d/V_e = 1$ , we infer no net volume change from the initial failed  
96 mass (i.e. no volume addition via erosion along the basal-shear surface and/or volume loss due to  
97 flow transformation; alternatively, both can occur, but are in balance) (Fig. DR3C). Finally,  
98  $V_d/V_e > 1$  indicates net volume gain during transport, suggesting lengthening and/or deepening of  
99 the basal-shear surface was accompanied by substrate entrainment (Fig. DR3D).

100 We calculated the  $V_d/V_e$  ratio for the Gorgon Slide using three established volume  
101 calculation methods (theoretical, bulk, and compacted volume; see Appendix DR4 for details).  
102 The theoretical volume method assumes that  $V_e$  and  $V_d$  have a wedge-shaped (McAdoo et al.,  
103 2000) and half-ellipsoid geometry (e.g. Wilson et al., 2004), respectively. The bulk volume method  
104 estimates  $V_e$  by calculating the volume between present-day and interpreted pre-failure seabed  
105 within the evacuation zone, while  $V_d$  is obtained by calculating the volume of the deposit between  
106 the basal-shear surface and the top surface (e.g. Piper et al., 1997). The compacted volume method  
107 takes a similar approach to the bulk volume method, but counts only the solid-state sediment  
108 fraction, removing water and pore-space (i.e. theoretical zero-porosity) (e.g. Lamarche et al.,  
109 2008). Despite the uncertainties associated with each method (Appendix DR4),  $V_d/V_e$  ratio  
110 provides a first-order estimation of slide erosivity.

## 111 **EROSIVITY OF SUBMARINE LANDSLIDES**

### 112 **The Gorgon Slide**

113           The source area for the Gorgon Slide is defined on its updip margin by a steep headwall  
114 scarp. The slide was transported north-westwards through an evacuation zone and accumulated in  
115 a downdip deposition zone (Fig. 1D). The slide is c.30 km-wide, with a total run-out distance of  
116 c.70 km. The slide deposit covers a total area of 1760 km<sup>2</sup> and thickens downslope to c.500 m.  
117 Transparent and chaotic seismic reflections likely reflect the debritic material forming the slide  
118 matrix (Fig. 1D-E) (e.g. Posamentier and Martinsen, 2011). Packages of subparallel, high-  
119 amplitude reflections encased in the interpreted debrite are interpreted as megaclasts (Fig. 1E) (e.g.  
120 Jackson, 2011; Hodgson et al., 2018), either sourced from the headscarp or entrained from the  
121 substrate. Basal erosion is evidenced by truncation of underlying seismic reflections (Fig. 1E).

122           The Vd of the Gorgon Slide was calculated using the basal-shear surface and seabed (see  
123 Fig. 1D-E). As a small part (c.7%) of the Gorgon Slide is not imaged within the 3D seismic  
124 reflection data (i.e. 166 km<sup>2</sup> of 1760 km<sup>2</sup>, see Fig. 1C), the calculated Vd is a minimum value. Ve  
125 was estimated by using the adjacent unfailed slope as a proxy for the pre-failure physiography  
126 across the evacuation zone (Fig. 2). The estimated Vd/Ve ratios of the Gorgon Slide range from 5-  
127 12, depending on the calculation method (see Appendix DR5). Critically, all methods suggest the  
128 Gorgon Slide was strongly erosive (i.e. Vd/Ve>1), an observation consistent with the abundant  
129 evidence for seismic-scale erosion along the basal-shear surface.

### 130 **Global Trend of Submarine Landslides Erosivity**

131           In order to place our results in a global context, we collated geometrical data from other  
132 slides (see Appendix DR6). Of the 357 slides documented in 97 papers, only 11 had data on both  
133 Ve and Vd. Our analysis shows that 9 of the 11 published slides are erosive, having Vd/Ve>1, with

134 a median value of 2 (Fig. 3). On average, the  $V_d/V_e$  of the documented slides suggests that the  
135 final preserved slide volume can be three times the initial failed volume. The Gorgon Slide has a  
136  $V_d/V_e$  ratio of up to 12 (and a conservative estimate of 5), making it the most erosive slide yet  
137 documented (Fig. 3B).

138 Although most are erosive, two slides display  $V_d/V_e < 1$  (Fig. 3B): 1) in the South China  
139 Sea, where volume loss is attributed to partial flow transformation to a turbidity current resulting  
140 in deposition of (sub-seismic) turbidites beyond the main slide pinchout, and pore volume  
141 reduction due to continuous shearing during transport (i.e. shear compaction) (Sun et al., 2018);  
142 and 2) in New Zealand, the Ruatoria Debris Avalanche, where the evacuation zone was formed by  
143 a combination of slope failure and tectonic erosion due to seamount subduction (i.e. not solely  
144 related to flow processes during transport) (Collot et al., 2001).

## 145 **DISCUSSION**

### 146 **Large submarine landslides are predominantly erosive**

147 Our results show that the volumes of most slides are larger than the initial failed volume,  
148 thereby confirming the erosivity of their parent flows (Fig. 3). Substrate entrainment and volume  
149 gain occurs because the shear stress exerted by the overriding parent flow exceeded the shear  
150 strength of the substrate. The overriding flow may elevate shallow subsurface pore pressures,  
151 causing liquefaction or strain softening (e.g. Ortiz-Karpf et al., 2017), or substrate deformation  
152 (e.g. Butler and McCaffrey, 2010). Both mechanisms will reduce the strength of the substrate,  
153 making it susceptible to entrainment. Substrate entrainment could also occur due to tooling by  
154 rigid blocks (e.g. megaclasts); this process forms tool marks, such as grooves and striations (e.g.  
155 Gee et al., 2005).



156 We suggest that the Gorgon Slide was strongly erosive because of the specific properties  
157 of the carbonate ooze substrate. Carbonate ooze is dominated by fragile foraminifera and  
158 nannofossils, which become weakly cemented at their contacts during early burial; this preserves  
159 higher-than-normal near-surface porosities and results in higher initial strength than (uncemented)  
160 siliciclastic sediments (von Rad et al., 1992). Under loading, these fragile biogenic particles are  
161 crushed, generating excess near-seabed pore pressures, and causing a dramatic loss of strength  
162 (e.g. Sharma and Joer, 2015). When carbonate oozes failed, their residual strength can be only  
163 10% of their initial strength; the residual strength of these materials is significantly lower than that  
164 of siliciclastic sediments (i.e. 55%, see Appendix DR7, Gaudin and White, 2009).

165 In contrast, volume loss during transport could occur due to entrainment of coarse-grained  
166 (e.g. sandy) sediments by the flow (e.g. Dykstra et al., 2011), and/or ingestion of water into the  
167 flow (e.g. Talling et al., 2012). For example, Sun et al. (2018) document a median volume loss of  
168 86 km<sup>3</sup> (c.13.6% of Vd) for a slide in the South China Sea. They relate this volume discrepancy to  
169 flow transformation from the slide (debris flow) into slide-generated turbidity currents. In addition,  
170 continuous shearing during transport may have added to volume loss, as pore volume will be  
171 reduced even when small shear stresses are applied to fine-grained sediments (Piper et al., 1997).

## 172 **Implications of submarine landslides erosivity for geohazards assessments**

173 Vd/Ve ratio provides a first-order, quantitative estimate of whether a slide increases or  
174 decreases its volume during transport. When a slide is erosive and bulks-up, its transport speed  
175 may decrease due to enhanced basal friction, thereby reducing run-out distance (e.g. Puzrin, 2016;  
176 Schulz et al., 2009). Similarly, when a slide experiences minimal erosion and/or hydroplanes, both  
177 its transport speed and run-out distance may increase (e.g. Mohrig et al., 1998). These two factors,  
178 slide speed and run-out distance, are key components for both tsunami modelling (e.g. Murty,

179 2003), and for assessing the potential impact slides may have on seabed infrastructures (e.g.  
180 Bruschi et al., 2006). In addition,  $V_e$  is a key factor for tsunami modelling, as it dictates how much  
181 overlying water is displaced during failure (e.g. Murty, 2003). Accurate volume assessment is  
182 especially challenging if only  $V_d$  is known, and if there is significant erosion or partial flow  
183 transformation. For example, the use of  $V_d$  as an estimate of  $V_e$  for tsunami modelling will  
184 overestimate displacement of the overlying water when  $V_d/V_e > 1$ . Similarly, if  $V_d/V_e < 1$ , tsunami  
185 modelling will underestimate the displacement of the overlying water. Therefore, to understand  
186 uncertainties associated with tsunami modelling, a range of  $V_d/V_e$  scenarios should be considered.  
187 Our study suggests that most slides are erosive, and that under-represented carbonate slides, such  
188 as the Gorgon Slide, could be more erosive than siliciclastic slides.  $V_d/V_e$  ratio is useful as a first-  
189 order estimate to understand slides erosivity and could also be used as a tool for geohazards risk  
190 assessments.

191 **ACKNOWLEDGEMENTS**

192           We thank Geoscience Australia for providing seismic and borehole data. Schlumberger are  
193 thanked for providing software (Petrel) to Imperial College. The first author thanks the Indonesia  
194 Endowment Fund for Education (LPDP) (Grant No.: 20160822019161) for its financial support.  
195 MC was supported by the NERC National Capability CLASS Programme [Climate Linked  
196 Atlantic Sector Science Programme (No. NE/R015953/1)].

197

198 **REFERENCES CITED**

- 199 Apthorpe, M., 1988, Cainozoic depositional history of the North West Shelf: The North West  
200 Shelf, Australia: Petroleum Exploration Society of Australia, p. 55-84.
- 201 Bruschi, R., Bughi, S., Spinazzè, M., Torselletti, E., and Vitali, L., 2006, Impact of debris flows  
202 and turbidity currents on seafloor structures: Norwegian Journal of Geology/Norsk  
203 Geologisk Forening, v. 86, no. 3.
- 204 Bull, S., Cartwright, J., and Huuse, M., 2009, A review of kinematic indicators from mass-  
205 transport complexes using 3D seismic data: Marine and Petroleum Geology, v. 26, no. 7,  
206 p. 1132-1151.
- 207 Butler, R., and McCaffrey, W., 2010, Structural evolution and sediment entrainment in mass-  
208 transport complexes: outcrop studies from Italy: Journal of the Geological Society, v. 167,  
209 no. 3, p. 617-631.
- 210 Carter, L., Gavey, R., TALLING, P. J., and Liu, J. T., 2014, Insights into submarine geohazards  
211 from breaks in subsea telecommunication cables: Oceanography, v. 27, no. 2, p. 58-67.
- 212 Collot, J. Y., Lewis, K., Lamarche, G., and Lallemand, S., 2001, The giant Ruatoria debris  
213 avalanche on the northern Hikurangi margin, New Zealand: Result of oblique seamount  
214 subduction: Journal of Geophysical Research: Solid Earth, v. 106, no. B9, p. 19271-19297.
- 215 Dutkiewicz, A., Müller, R. D., O'Callaghan, S., and Jónasson, H., 2015, Census of seafloor  
216 sediments in the world's ocean: Geology, v. 43, no. 9, p. 795-798.
- 217 Dykstra, M., Garyfalou, K., Kertznus, V., Kneller, B., Milana, J. P., Molinaro, M., Szuman, M.,  
218 and Thompson, P., 2011, Mass-transport deposits: Combining outcrop studies and seismic  
219 forward modeling to understand lithofacies distributions, deformations, and their seismic  
220 stratigraphic expression: SEPM Special Publication, v. 96, p. 293-310.

221 Gaudin, C., and White, D., 2009, New centrifuge modelling techniques for investigating seabed  
222 pipeline behaviour, *in* Proceedings 17th International Conference on Soil Mechanics and  
223 Geotechnical Engineering, Alexandria, 2009, p. 448-451.

224 Gee, M., Gawthorpe, R., and Friedmann, J., 2005, Giant striations at the base of a submarine  
225 landslide: *Marine Geology*, v. 214, no. 1, p. 287-294.

226 Hodgson, D., Brooks, H., Ortiz-Karpf, A., Spychala, Y., Lee, D., and Jackson, C.-L., 2018,  
227 Entrainment and abrasion of megaclasts during submarine landsliding and their impact on  
228 flow behaviour: Geological Society, London, Special Publications, v. 477, p. SP477. 426.

229 Jackson, C. A., 2011, Three-dimensional seismic analysis of megaclast deformation within a mass  
230 transport deposit; implications for debris flow kinematics: *Geology*, v. 39, no. 3, p. 203-  
231 206.

232 Keep, M., Powell, C., and Baillie, P., 1998, Neogene deformation of the North West Shelf,  
233 Australia: *The sedimentary basins of Western Australia*, v. 2, p. 81-91.

234 Lamarche, G., Joanne, C., and Collot, J. Y., 2008, Successive, large mass-transport deposits in the  
235 south Kermadec fore-arc basin, New Zealand: *The Matakaoa Submarine Instability*  
236 *Complex: Geochemistry, Geophysics, Geosystems*, v. 9, no. 4.

237 Longley, I. M., Buessenschuett, C., Clydsdale, L., Cubitt, C. J., Davis, R. C., Johnson, M. K.,  
238 Marshall, N. M., Murray, A. P., Somerville, R., and Spry, T. B., 2002, The North West  
239 Shelf of Australia - a Woodside Perspective, *in* Keep, M., and Moss, S. J., eds., *The*  
240 *Sedimentary Basins of Western Australia 3: Petroleum Exploration Society of Australia*  
241 *Symposium: Perth*, p. 28-88.

242 McAdoo, B., Pratson, L., and Orange, D., 2000, Submarine landslide geomorphology, US  
243 continental slope: *Marine Geology*, v. 169, no. 1, p. 103-136.

244 Mohrig, D., Ellis, C., Parker, G., Whipple, K. X., and Hondzo, M., 1998, Hydroplaning of  
245 subaqueous debris flows: Geological Society of America Bulletin, v. 110, no. 3, p. 387-  
246 394.

247 Moscardelli, L., and Wood, L., 2016, Morphometry of mass-transport deposits as a predictive tool:  
248 GSA Bulletin, v. 128, no. 1/2, p. 47-80.

249 Murty, T., 2003, Tsunami wave height dependence on landslide volume: Pure and applied  
250 geophysics, v. 160, no. 10-11, p. 2147-2153.

251 Ortiz-Karpf, A., Hodgson, D. M., Jackson, C. A.-L., and McCaffrey, W. D., 2017, Influence of  
252 Seabed Morphology and Substrate Composition On Mass-Transport Flow Processes and  
253 Pathways: Insights From the Magdalena Fan, Offshore Colombia: Journal of Sedimentary  
254 Research, v. 87, no. 3, p. 189-209.

255 Piper, D. J. W., Pirmez, C., Manley, P. L., Long, D., Flood, R. D., Normark, W. R., and Showers,  
256 W., Mass Transport Deposits of the Amazon Fan, *in* Proceedings Ocean Drilling Program,  
257 Scientific Results 1997, Volume 155, p. 109-146.

258 Posamentier, H. W., and Martinsen, O. J., 2011, The character and genesis of submarine mass-  
259 transport deposits: insights from outcrop and 3D seismic data: Mass-transport deposits in  
260 deepwater settings: Society for Sedimentary Geology (SEPM) Special Publication 96, p.  
261 7-38.

262 Puzrin, A. M., 2016, Simple criteria for ploughing and runout in post-failure evolution of  
263 submarine landslides: Canadian Geotechnical Journal, v. 53, no. 8, p. 1305-1314.

264 Randolph, M. F., and White, D. J., 2012, Interaction forces between pipelines and submarine  
265 slides—A geotechnical viewpoint: Ocean Engineering, v. 48, p. 32-37.

266 Scarselli, N., McClay, K., and Elders, C., Submarine slide and slump complexes, Exmouth Plateau,  
267 NW Shelf of Australia, *in* Proceedings The Sedimentary Basins of Western Australia IV:  
268 Proceedings of the Petroleum Exploration Society of Australia Symposium, Perth, 2013.

269 Schulz, W. H., McKenna, J. P., Kibler, J. D., and Biavati, G., 2009, Relations between hydrology  
270 and velocity of a continuously moving landslide—evidence of pore-pressure feedback  
271 regulating landslide motion?: *Landslides*, v. 6, no. 3, p. 181-190.

272 Sharma, S., and Joer, H., Some characteristics of carbonate sediments from NorthWest Shelf,  
273 Western Australia, *in* Proceedings Frontiers in Offshore Geotechnics III: Proceedings of  
274 the 3rd International Symposium on Frontiers in Offshore Geotechnics (ISFOG  
275 2015)2015, Volume 1, Taylor & Francis Books Ltd, p. 1109-1114.

276 Sobiesiak, M. S., Kneller, B., Alsop, G. I., and Milana, J. P., 2018, Styles of basal interaction  
277 beneath mass transport deposits: *Marine and Petroleum Geology*, v. 98, p. 629-639.

278 Sun, Q., Alves, T., Lu, X., Chen, C., and Xie, X., 2018, True volumes of slope failure estimated  
279 from a Quaternary mass-transport deposit in the northern South China Sea: *Geophysical*  
280 *Research Letters*.

281 Talling, P. J., Masson, D. G., Sumner, E. J., and Malgesini, G., 2012, Subaqueous sediment density  
282 flows: Depositional processes and deposit types: *Sedimentology*, v. 59, no. 7, p. 1937-  
283 2003.

284 Tappin, D., Watts, P., McMurtry, G., Lafoy, Y., and Matsumoto, T., 2001, The Sissano, Papua  
285 New Guinea tsunami of July 1998—offshore evidence on the source mechanism: *Marine*  
286 *Geology*, v. 175, no. 1-4, p. 1-23.

287 Ten Brink, U. S., Geist, E. L., and Andrews, B. D., 2006, Size distribution of submarine landslides  
288 and its implication to tsunami hazard in Puerto Rico: *Geophysical Research Letters*, v. 33,  
289 no. 11.

290 von Rad, U., Haq, B. U., Kidd, R. B., and O'Connell, S. B., 1992, *Proceedings of the Ocean Drilling*  
291 *Program, Scientific Results*, College Station, TX, Ocean Drilling Program.

292 Wilson, C. K., Long, D., and Bulat, J., 2004, The morphology, setting and processes of the Afen  
293 Slide: *Marine Geology*, v. 213, no. 1-4, p. 149-167.

294 Winterwerp, J., Kesteren, W., Prooijen, B., and Jacobs, W., 2012, A conceptual framework for  
295 shear flow–induced erosion of soft cohesive sediment beds: *Journal of Geophysical*  
296 *Research: Oceans*, v. 117, no. C10.



297 **FIGURE CAPTIONS**

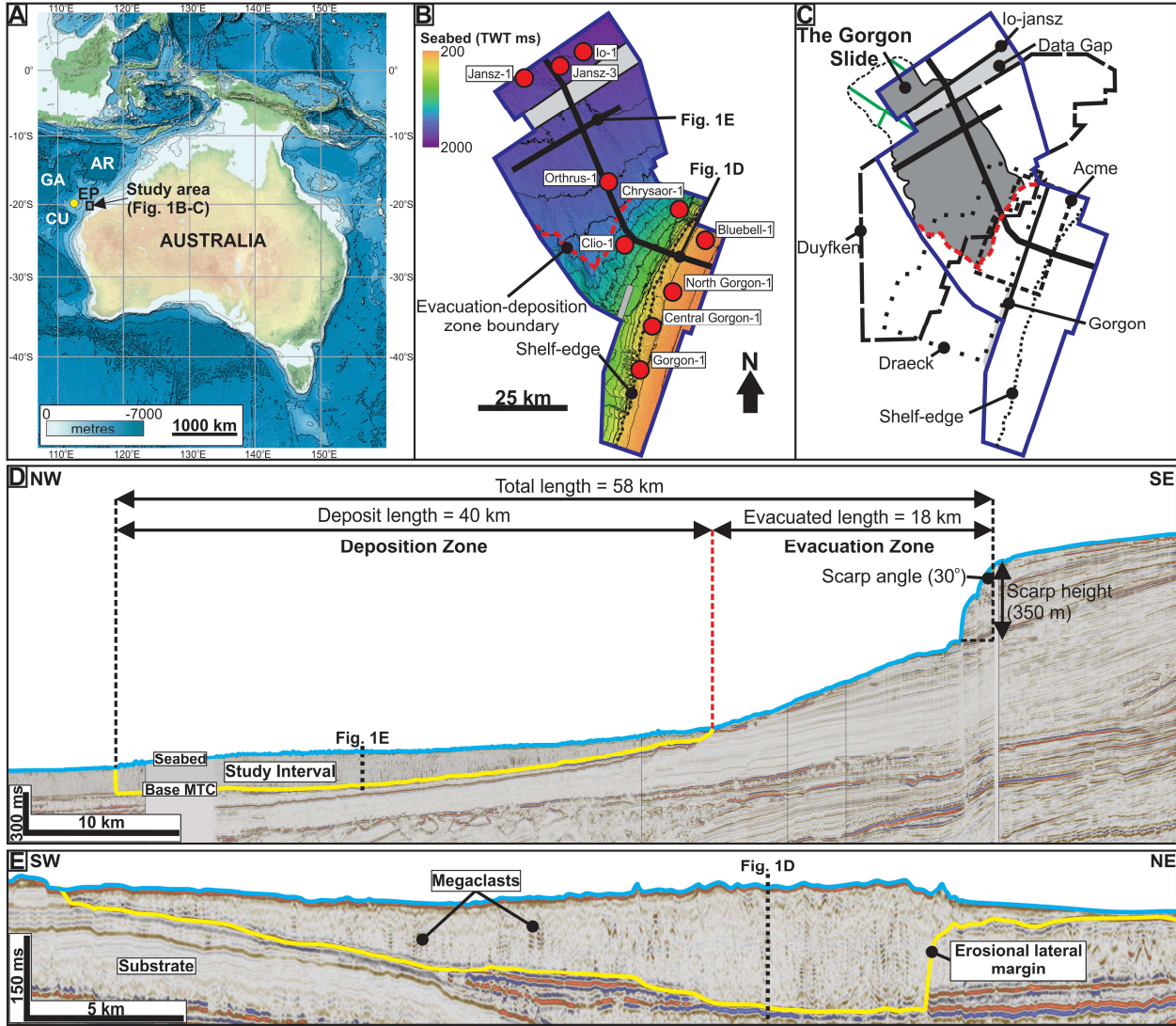
298 **Figure 1.** A: Location of study area (EP: Exmouth Plateau; AR: Argo Abyssal Plain; GA:  
299 Gascoyne Abyssal Plain; CU: Cuvier Abyssal Plain). Yellow dot = location of ODP 762. B: Seabed  
300 time-structure map (top Gorgon Slide) showing slide evacuation and deposition zones. Red dots =  
301 wells used for depth conversion. C: Extent of the Gorgon Slide (grey). Black dashed line defines  
302 the seismic-scale pinchout of the slide; c. 7% of the slide is not imaged by 3D seismic data but is  
303 mapped on 2D seismic profiles (green lines). Gorgon, Acme, Draeck, Duyfken, and Io-Jansz are  
304 the 3D seismic datasets were used in this study. D: NW-trending depositional dip-oriented seismic  
305 profile across the Gorgon Slide, showing cross-sectional view of the evacuation and deposition  
306 zones. E: NE-trending depositional strike seismic profile across the Gorgon Slide. Locations of  
307 seismic profiles are shown in B and C.

308 **Figure 2.** A: NW-trending seismic profile across the unfailed margin, just SW of the headwall of  
309 the Gorgon Slide. B: Seabed time-structure map showing the headwall of the Gorgon Slide and  
310 the adjacent unfailed margin to the SW. C: NW-trending seismic profile across the headwall of the  
311 Gorgon Slide and the reconstructed (i.e. pre-failure) seabed. D: Reconstructed pre-failure seabed  
312 time-structure map.

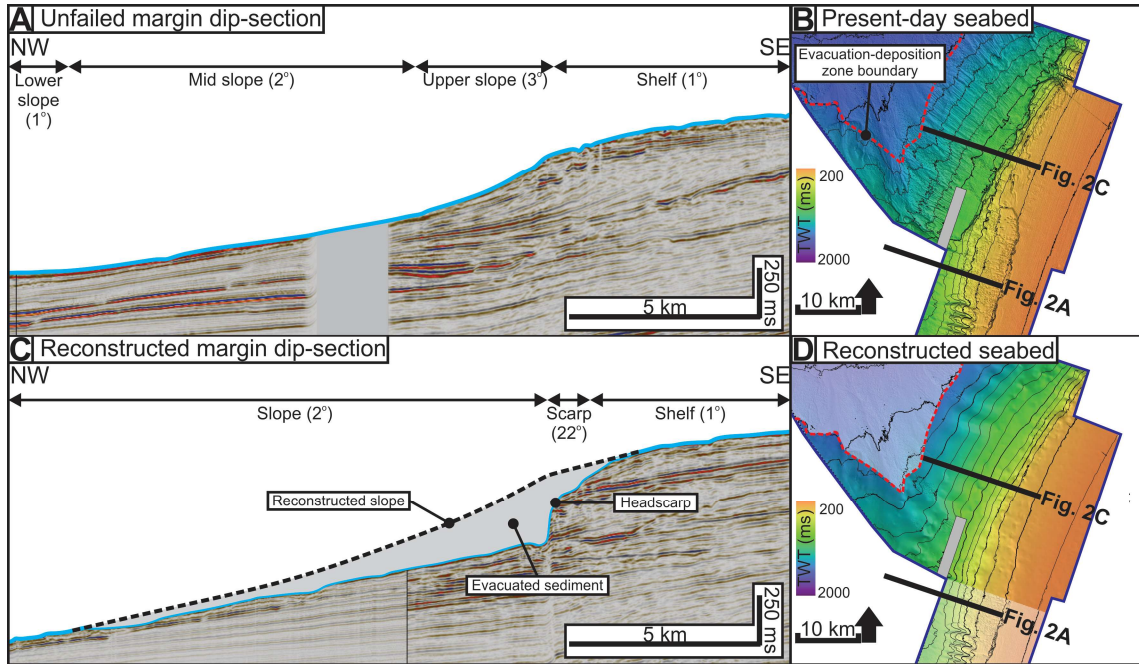
313 **Figure 3.** A: World distribution of documented slides in peer-reviewed literature, containing  
314 information on evacuated ( $V_e$ ) and deposited ( $V_d$ ) volumes. Note that the Gorgon Slide as the  
315 only carbonate-dominated slide. B:  $V_d/V_e$  ratio of the submarine landslide in (A).

316

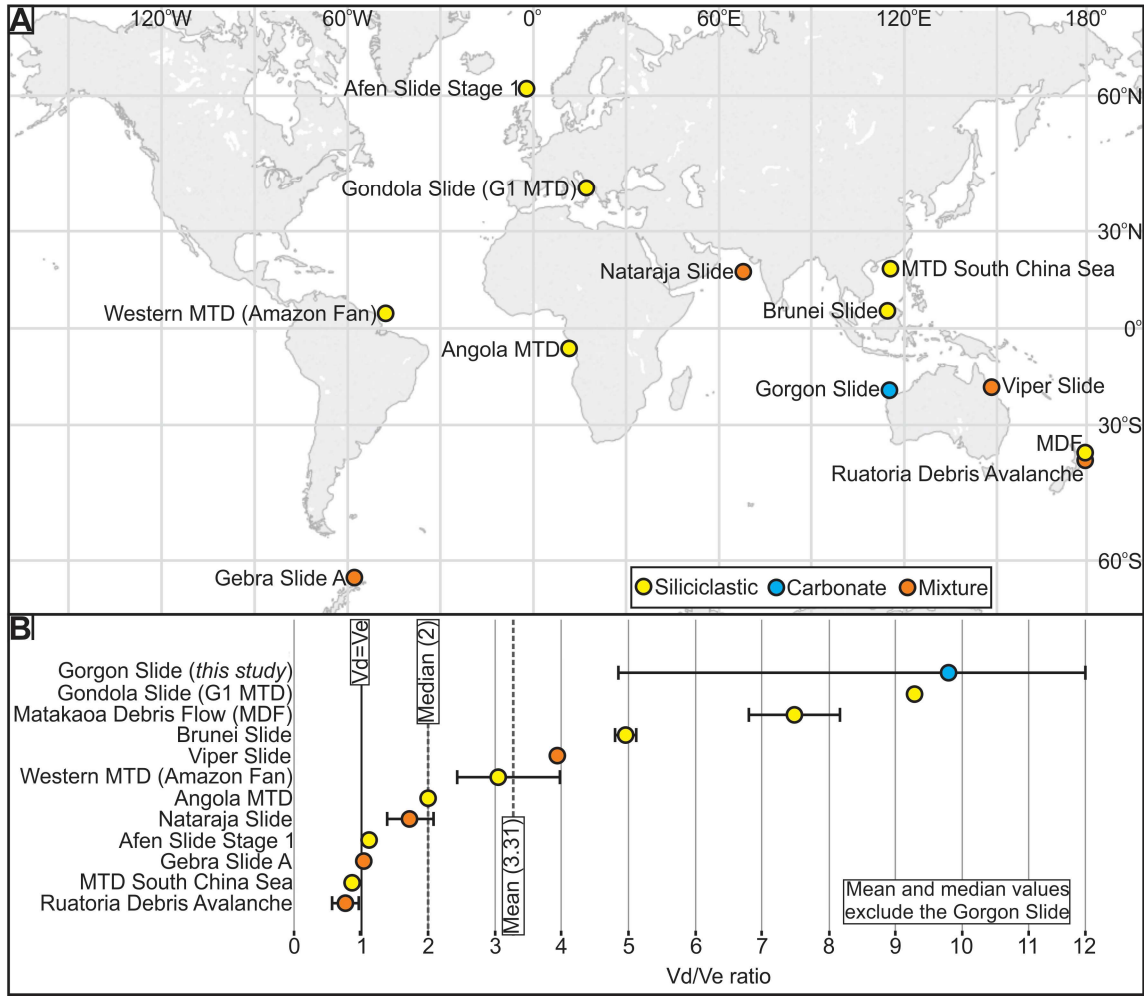
317 Figure 1



318



321 Figure 3



322