



22 instruments (BBOBS), which often employ the same sensors as terrestrial broadband seismic stations  
23 and can operate for as long as two years (Suetsugu and Shiobara, 2014). Whereas short-period instru-  
24 ments are primarily used in active-source experiments, BBOBS are ideal for passive-source experiments  
25 and have been used for tomographic studies, earthquake location, and ocean wave monitoring among  
26 numerous other applications (e.g. Forsyth et al., 1998; Toomey et al., 1998; Webb et al., 2001; Dolenc  
27 et al., 2005; Suetsugu et al., 2005; Shinohara et al., 2011; Ito et al., 2012; Sugioka et al., 2012; Tan  
28 et al., 2016). However, BBOBS are expensive and limited by data telemetry and battery life except  
29 in near-shore environments (Suetsugu and Shiobara, 2014). Recent work has explored several alterna-  
30 tives to conventional BBOBS for offshore seismic monitoring, including free-floating robots equipped  
31 with hydrophones (Hello et al., 2011), moored surface buoys or autonomous surface vehicles for satellite  
32 telemetry acoustically linked to BBOBS (Frye et al., 2005; Berger et al., 2016), and cabled arrays of  
33 broadband sensors (Goertz and Wuestefeld, 2018). Recently, Marra et al. [2018] applied laser interfer-  
34 ometry to convert long ocean-bottom telecommunications optical fiber links into seismic strainmeters.  
35 This work is particularly promising because it would enable the >1 million km of pre-existing trans-  
36 oceanic telecommunications cables to be repurposed as seismic sensors, permitting rapid detection and  
37 location of earthquakes throughout the world’s ocean basins. Unfortunately, the particular technique in  
38 Marra et al. [2018] is limited to measuring propagation delays integrated across an entire cable length,  
39 resulting in a single seismograph with equivalent station location uncertainty on the order of 1 km and  
40 complicated instrument response.

41 Distributed acoustic sensing (DAS) is an emerging technology with strong potential to form the  
42 core of next-generation submarine seismic monitoring infrastructure. A DAS interrogator unit probes a  
43 fiber-optic cable with a coherent laser pulse and measures changes in the phase of the returning optical  
44 backscatter time-series. Optical phase shifts between pulses are proportional to longitudinal strain in  
45 the fiber and can be mapped into the finite, distributed strain across a fiber segment (termed gauge  
46 length) by integration. Applying DAS technology to a fiber-optic cable effectively converts the cable  
47 into a seismic recording array with thousands of single-component channels, real-time data telemetry,  
48 and unlimited deployment duration as long as the DAS unit is powered. For about a decade, DAS  
49 has been successfully utilized in boreholes for active-source seismic profiling (e.g. Mestayer et al., 2011;  
50 Mateeva et al., 2012; Parker et al., 2014). Recent work with onshore trenched or conduit-installed  
51 horizontal fibers has demonstrated the ability of DAS arrays to record earthquakes and other seismic  
52 signals at local to teleseismic distances with high waveform fidelity (Lindsey et al., 2017; Jousset et al.,  
53 2018; Li and Zhan, 2018; Wang et al., 2018; Ajo-Franklin et al., 2019; Yu et al., 2019). In this letter,  
54 we demonstrate that submarine horizontal DAS arrays utilizing pre-existing ocean-bottom fiber-optic  
55 cables are similarly effective for seismological studies and can also record pressure perturbations from

56 ocean wave phenomena. We report our observation of body waves from the 2018-08-19  $M_w$ 8.2 Fiji deep  
57 earthquake on an ocean-bottom DAS array offshore Zeebrugge, Belgium. We then examine ocean surface  
58 gravity waves and associated seismic modes directly observed on the array, which we interpret as evidence  
59 of in-situ microseism generation. Finally, we discuss implications for future DAS deployments in marine  
60 settings.

## 61 2 Results

62 Passively recording during August 2018, the Belgium DAS array (BDASA) occupied a pre-existing  
63 ocean-bottom fiber-optic cable in the Southern Bight of the North Sea offshore Zeebrugge, Belgium.  
64 The fiber was originally installed to monitor a power cable for the Belwind Offshore Wind Farm. A  
65 chirped-pulse DAS system built and installed by the University of Alcalá (Pastor-Graells et al., 2016)  
66 continuously interrogated a 42-km near-shore segment of the fiber with channel spacing of 10 m, creating  
67 4192 simultaneously recording seismic sensors (Fig. 1) (see Section 4). The cable is buried between 0.5  
68 and 3.5 m below the seafloor in water depths shallower than 40 m. The conduit housing the buried cable  
69 is mechanically coupled to the surrounding sediment, making the array sensitive to solid earth strains  
70 like earthquake wavefields and microseism noise. Meanwhile, pore fluid surrounding the cable is close to  
71 hydrodynamic equilibrium with the ocean above, so pressure perturbations and poroelastic strains from  
72 ocean waves are also recorded. The cable geometry is approximately straight over four 10-km segments  
73 and is flat or shallowly dipping, except for a steep channel around 10 km and two  $\sim$ 15 m bathymetric  
74 ridges at  $\sim$ 30 and 40 km from the coast (Fig. 1A).

### 75 2.1 2018-08-19 $M_w$ 8.2 Fiji deep earthquake

76 On August 19, 2018, a  $M_w$ 8.2 deep earthquake occurred in the Fiji-Tonga area, and strong teleseismic  
77 body waves were captured on global seismic networks, including the BDASA (Fig. 1B). Teleseisms  
78 arrived from an epicentral distance of  $146.7^\circ$  ( $>16,300$  km), at a back azimuth of  $358.5^\circ$  ( $27.6^\circ$  oblique to  
79 the mean fiber azimuth of  $330.9^\circ$ ). In this section, we analyze a 1-hr record from the full array containing  
80 the principal body wave phases. Because the 2018-08-19 Fiji event occurred at a depth of 600 km, only  
81 weak surface waves were excited and hence could not be analyzed.

82 In the time-domain, raw strain records from the BDASA are uninterpretable due to the superposition  
83 of several coherent signals with incoherent noise from sources such as temperature drift (Fig. S1). A 2D  
84 Fast Fourier Transform to the frequency-wavenumber (f-k) domain allows identification and separation of  
85 coherent seismic and oceanic signals based on their characteristic phase velocities (Fig. 2). F-k domain  
86 analysis of the raw BDASA data is possible here because the chirped-pulse DAS system exhibits negligible

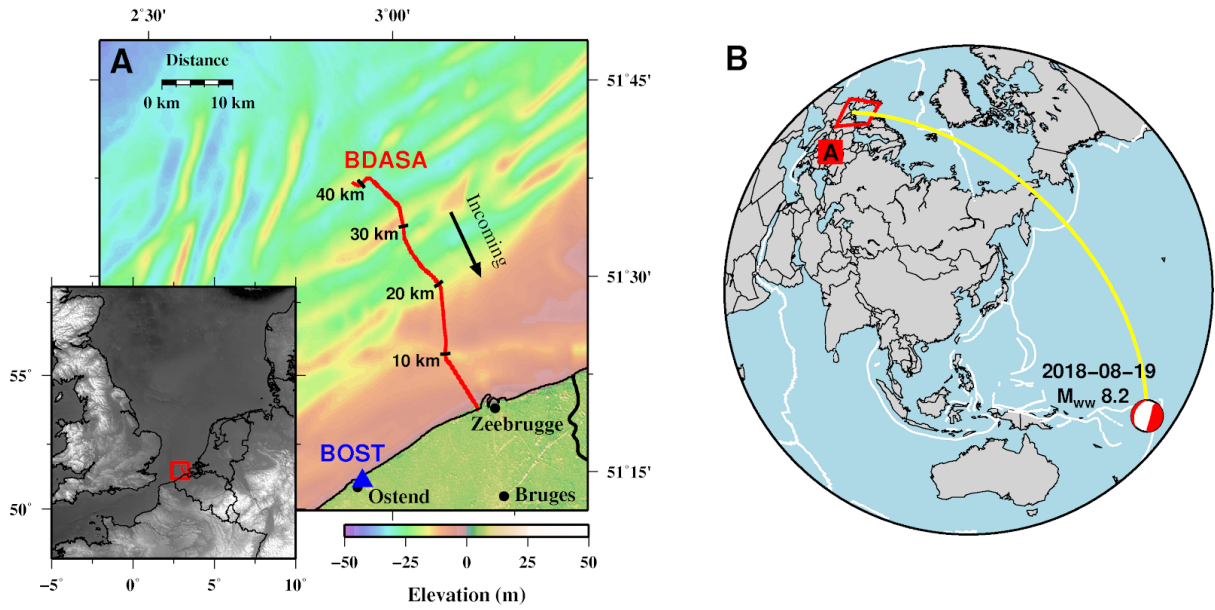


Figure 1: **Array location** (A) Local map showing the location Belgium DAS Array (BDASA, red line) and nearby broadband station BOST (blue triangle), with a regional map inset. (B) World map showing the location of the array (red box), the GCMT solution for the 2018-08-19 M8.2 Fiji deep earthquake, and great circle path between the earthquake epicenter and the array (yellow).

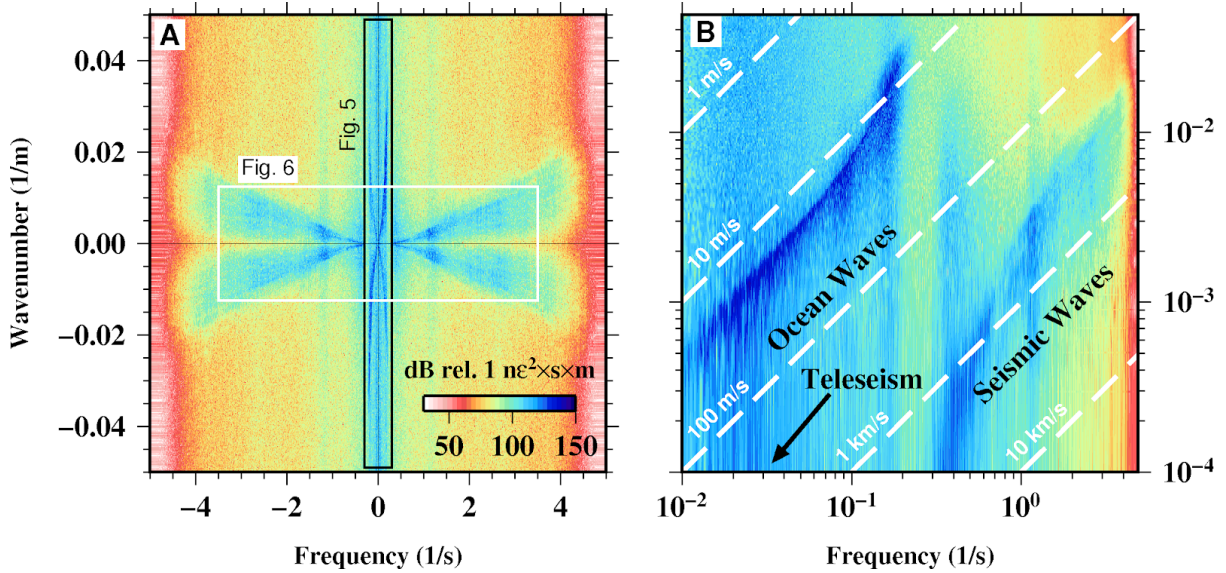


Figure 2: **Separation of ocean and seismic waves** (A) Raw f-k power spectrum of 1 hr of DAS strain data across the full 42-km array. (B) Quadrant 1 (incoming waves) plotted in logarithmic space, showing coherent ocean wave energy at low frequencies and coherent seismic wave energy at high frequencies. Teleseismic waves with near-instantaneous apparent phase velocity appear in the zero-wavenumber bin at low frequencies.

87 fading of sensitivity along the fiber, as is common in conventional DAS and which would require pre-  
88 processing at the expense of bandwidth (see Section 4). Given the quasi-linear geometry of the fiber cable,  
89 no corrective algorithms or fiber sectioning methods were applied to compensate cable turns, resulting  
90 in slight smearing of energy along the wavenumber axis. In the f-k domain, ocean-related signals appear  
91 at low frequencies ( $<0.7$  Hz) with apparent group velocity slower than  $\sim 10$  m/s, and are discussed in  
92 Section 2.2 (Fig. 2). Seismic surface waves appear at high frequencies ( $>0.3$  Hz) with apparent group  
93 velocity faster than  $\sim 300$  m/s, and are discussed in Section 2.3 (Fig. 2). Teleseismic body waves from  
94 the Fiji earthquake are close to vertically incident and expected to arrive almost simultaneously along  
95 the array, hence appearing at wavenumbers lower than can be resolved across a few kilometers aperture.  
96 In order to isolate teleseisms, we apply a 2D band-pass filter in the f-k domain between 0.001-1 Hz and  
97  $0-0.002$   $\text{m}^{-1}$  in the first and third quadrants (corresponding to energy propagating land-ward across the  
98 array from the north/west; Fig. S2), stack waveforms across a 5-km array segment to form a beam trace,  
99 and finally apply a range of bandpass filters to the beam trace to produce the BDASA waveforms shown  
100 in Figure 3 (see Supplementary Material). We compare the BDASA beam trace to nearby broadband  
101 seismometer BOST (30-50 km south of BDASA), after rotating the horizontal channels into the mean  
102 azimuth of the BDASA and bandpass filtering.

103 At high frequencies ( $>0.1$  Hz), we recover the PKP phase ( $\sim 550$  s) and its associated pPKP + sPKP  
104 depth phases ( $\sim 690$  s), the travel times of which correspond well to those recorded on BOST (Fig. 3).  
105 The envelopes of the recovered P phases are similar to those from BOST, although the waveforms do not  
106 match wiggle by wiggle, as expected for high frequency waves strongly affected by near-surface structures  
107 and the water layer. At low frequencies ( $<0.15$  Hz), the background noise is substantially stronger, but  
108 we still recover a complex S wavetrain, which exhibits moderate-to-high waveform fidelity when compared  
109 with BOST (mean correlation coefficient of 0.6; Fig. 3, Fig. S3). Recovered P and S waveforms are  
110 both coherent along the length of the array (Fig. S4). Because the BDASA measures strain across a  
111 10-m gauge length whereas BOST measures particle velocity at a single point, theoretical amplitudes  
112 are approximately proportional by a factor of the apparent horizontal slowness for wavelengths longer  
113 than twice the gauge length (Wang et al., 2018). For the Fiji earthquake, the ratio of BDASA strain  
114 amplitude to BOST particle velocity amplitude does not yield reasonable apparent velocities for the  
115 observed phases across any band. Hence, we infer that strain-transfer coupling between the solid earth  
116 and the BDASA fiber, a consequence of the fiber casing and installation, is complex. While a  $M_w 8.2$   
117 deep earthquake is a rare and particularly large event, body wave energy observed in Belgium at  $146.7^\circ$   
118 epicentral distance is lower in spectral amplitude than would be expected for regional earthquakes ( $< 1^\circ$   
119 epicentral distance) greater than  $\sim M3.5$  (see Supplementary Material). Hence, BDASA clearly exhibits  
120 teleseismic and regional seismic monitoring capability, as both P-wave and S-wave travel-times can be

121 recovered across a broad band, and S-wave polarity is robust over the frequencies of interest to global  
122 seismology.

## 123 **2.2 Ocean surface gravity waves**

124 In addition to the broad, low-frequency peak associated with Fiji teleseisms, the power spectral  
125 densities (PSD) of BDASA channels computed over the full 1-hr strain record exhibit four distinct peaks  
126 at 0.09 Hz, 0.18 Hz, 0.36 Hz, and 1.12 Hz (Fig. 4a). Here, we focus primarily on the 0.18 and 0.36  
127 Hz peaks. We attribute the 0.18 Hz peak to poroelastic strains induced by the pressure field of ocean  
128 surface gravity waves propagating across the array. Globally, surface gravity and infragravity waves  
129 between 0.003-3 Hz are excited in oceanic waters by wind-sea interaction. Invoking linear wave theory,  
130 the magnitude of the seafloor pressure perturbations beneath a surface gravity wave scales with angular  
131 wavenumber  $k$  and water depth  $H$  as  $p_d \propto \text{sech}(kH)$  (e.g. Holthuijsen, 2007). We use the dispersion  
132 relation for ocean surface gravity waves,  $\omega^2 = gk \tanh(kH)$ , to calculate a theoretical  $p_d$  along the cable  
133 depth profile and fit the Fourier amplitude at 0.18 Hz as a linear function of  $p_d$  (see Supplementary  
134 Material). We observe a good correspondence between the observed and predicted Fourier amplitude at  
135 0.18 Hz with both water depth and distance along the cable (Fig. 4b,c), suggesting that surface gravity  
136 waves dominate the data at these frequencies.

137 Our interpretation of surface gravity waves at 0.18 Hz is supported by f-k analysis, which shows  
138 strong, coherent energy packets in all four quadrants between 0.01-0.26 Hz with peaks at 0.09 and 0.18  
139 Hz and slow phase velocities on the order of 1-10 m/s (Fig. 2b, 5). These energy packets are bounded by a  
140 sharp upper edge at slow phase velocities, which we fit by the dispersion relation for surface gravity waves  
141 (Fig. 5), representing wave energy propagating axially along the cable. Energy below this edge represents  
142 surface gravity waves with faster apparent phase velocity that obey the same dispersion relation but are  
143 obliquely incident to the fiber. Using the dispersion relation given above, we map energy from these  
144 obliquely incident waves to f-k amplitude as a function of azimuth to quantify the variations in the  
145 directional spectrum of the ocean wavefield with distance along the fiber (Fig. 5c; see Supplementary  
146 Material). The directional spectra appear lobate because DAS measures the axial component of strain,  
147 with a directional sensitivity of approximately  $\cos^2\theta$  for longitudinal waves (Martin, 2018), hence low  
148 broadside sensitivity.

149 For the segment of the BDASA closest to shore, stronger incoming (land-ward propagating) surface  
150 gravity waves occupying f-k quadrants 1 and 3 are observed. The relative strength of outgoing (sea-ward  
151 propagating) surface gravity waves occupying f-k quadrants 2 and 4 increases with distance along the  
152 cable (Fig. 5). For the last 10 km segment of the array between 30 and 40 km the outgoing and incoming

153 waves are of approximately equal energy (Fig. 5b). We infer that outgoing waves must be reflected from  
154 the bathymetric ridge at 30 km and the sloping seabed approaching the coast (Fig. 1b), and note that  
155 such opposing wave groups necessarily interfere to produce a standing wave. In particular, the reflective  
156 effect of the bathymetric ridge at 30 km can be clearly observed in the directional spectra (Fig. 5c), where  
157 incoming wave energy is amplified relative to outgoing energy on the 20-30 km segment and outgoing  
158 energy is amplified relative to incoming energy on the 30-40 km segment.

159 The directional spectrum of surface gravity waves does not change appreciably over time along the  
160 first 30 km of the array. For the last 10 km segment, however, the observed f-k spectrum evolves  
161 over time and is asymmetrical, with faster incoming waves and slower outgoing waves (Fig. 5b). We  
162 fit this asymmetry with a mean-flow correction to the dispersion relation  $(\omega - Uk)^2 = gk \tanh(kH)$ ,  
163 which describes the first-order effect of surface gravity waves propagating in a current, where  $U$  is the  
164 apparent velocity of the current along the cable (Fig. 5b,d,e). Over the 1-hr record, the strength of the  
165 observed current increases gradually from 0.1 to 0.5 m/s apparent velocity in the shore-ward direction.  
166 Contemporary methods of ocean current measurement are largely limited to either high-frequency radio  
167 observation of surface currents (e.g. Chapron et al., 2005; Paduan and Washburn, 2013) or in-situ  
168 observation of current-depth profiles using spatially-sparse moorings, drifters, or ship-board instruments  
169 (e.g. MODE Group, 1978; Lumpkin and Pezos, 2007; Wunsch, 2015). Our observation of spatio-temporal  
170 variations in current speed is significant because it suggests potential application of ocean-bottom DAS  
171 to in-situ measurement and monitoring of ocean currents by exploiting models of wave interaction with  
172 heterogeneous currents (e.g. Huang et al., 1972) to recover high-resolution spatial (and potentially even  
173 depth-dependent) variations in current speed along an array.

### 174 **2.3 Scholte waves and microseism generation**

175 Unlike the 0.18 Hz energy peak, the 0.36 Hz peak observed in the BDASA PSD is almost invariant  
176 with depth and is not adequately described by the pressure-depth scaling of ocean surface gravity waves  
177 (Fig. 4c). Instead, the Fourier amplitude at 0.36 Hz increases gradually with distance along the array  
178 (Fig. 4b). The cable segment in water depths  $< 10$  m is neglected in this analysis, as the PSD of this  
179 region is saturated by incoherent energy across a broad band, likely associated with shoaling of ocean  
180 waves. In the f-k domain, we identify a broad energy packet between 0.3 and 3.5 Hz with peaks at 0.36  
181 and 1.12 Hz characterized by phase velocities faster than  $\sim 300$  m/s (Fig. 6a). When projected from the  
182 frequency-wavenumber domain into frequency-phase velocity space, this high-frequency energy packet  
183 exhibits strong dispersion from phase velocities close to the compressional velocity of water ( $\sim 1500$   
184 m/s) at 0.36 Hz to an asymptotic velocity of  $\sim 250$ -450 m/s above 1 Hz (Fig. 2b, 6b). Again, in the f-k

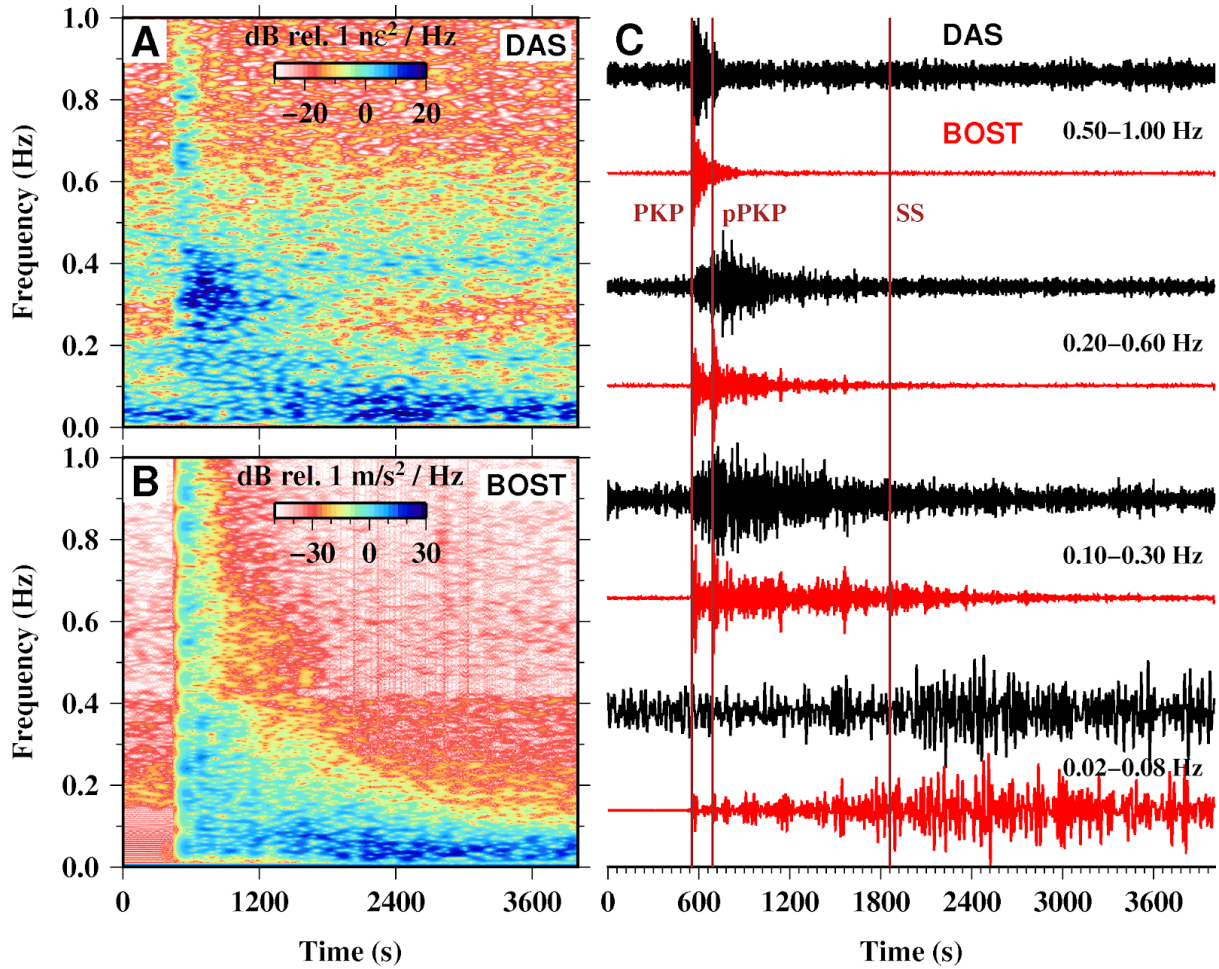


Figure 3: **Teleseismic waveforms** (A) Spectrogram of PSD over time for the f-k filtered and stacked DAS beam trace (black in (C)), showing strong energy between 0-1 Hz around the arrival of the PKP phase around 550 s and below 0.1 Hz following the arrival of the SS phase around 1860 s. (B) Spectrogram for the rotated BOST channel (red in (C)), showing the same major features. (C) Stacked DAS beam trace (black) filtered to various bands between 0.02 and 1 Hz compared with amplitude-normalized particle velocity from broadband station BOST rotated into the mean azimuth of the DAS array (red).



185 domain the sharp, upper edge of the energy packet corresponds to waves propagating along the cable, and  
 186 energy appearing below this edge corresponds to waves propagating oblique to the array (Fig. 6a). We  
 187 consequently attribute the 0.3-3.5 Hz energy to Scholte waves, seismic rock-water interface waves, whose  
 188 dispersion relation follows the compressional velocity of water at low frequencies and the shear-wave  
 189 velocity of the shallow sediment layer at high frequencies (Rauch, 1980).

190 Assuming a true phase velocity of 300 m/s above 1 Hz (the peak velocity in Fig. 6b), we again  
 191 compute the distribution of f-k amplitude as a function of incident azimuth (Fig. 6c; see Supplementary  
 192 Material). The directional spectrum of Scholte waves is relatively symmetric along the outer 30 km of  
 193 the BDASA and shows an azimuthal distribution as would be expected for isotropically propagating  
 194 or diffuse Scholte waves recorded with DAS (Fig. 6a,c). Scholte waves are observed propagating with  
 195 subequal-to-equal energy both land-ward and sea-ward across the array (Fig. 6a), hence we infer that  
 196 these waves must be generated in-situ. We note that the 0.3-3.5 Hz Scholte waves are observed in the  
 197 550 s of data preceding the arrival of the first P-wave phases from the Fiji earthquake and therefore must  
 198 be an independent, local phenomenon.

199 Globally, seismograms record broadband seismic noise with peaks at 14 and 7 s period, termed  
 200 microseisms, which have long been attributed to ocean wave sources (e.g. Kedar et al., 2008). Longuet-  
 201 Higgins [1950] first proposed a mechanism for the double-frequency nature of microseisms, whereby  
 202 nonlinear interaction of opposing groups of surface gravity waves at one frequency generates a depth-  
 203 invariant pressure term of second-order magnitude which oscillates at twice the frequency of the surface  
 204 waves. Hasselmann [1963] expanded this theory to demonstrate that appreciable microseisms are excited  
 205 only by components of the ocean pressure field that match the phase velocities of the seismic modes of the  
 206 coupled water-seabed system. In the simplest case, the phase velocity of Longuet-Higgins's second-order  
 207 pressure term scales as  $c = 2\omega / \|\vec{k}_1 + \vec{k}_2\|$  for two plane surface gravity waves with phase  $\vec{k}_1 \cdot \vec{x} - \omega t$   
 208 and  $\vec{k}_2 \cdot \vec{x} - \omega t$ . Hence, for opposing waves ( $\vec{k}_1 \rightarrow -\vec{k}_2$ ),  $c$  approaches seismic velocities. Based on  
 209 these theories, we assert that the 0.36 Hz Scholte waves discussed above represent secondary microseism  
 210 associated with the 0.18 Hz opposing surface gravity wave groups. This is further supported by our  
 211 observation of gradually increasing Fourier amplitude at 0.36 Hz with distance from the coast (Fig. 4b),  
 212 as we also observed increasing parity of incoming and outgoing surface gravity waves with distance (Fig.  
 213 5) and Longuet-Higgins [1950] predicts that the amplitude of the secondary pressure term is proportional  
 214 to the product of the amplitudes of the incoming and outgoing ocean wavefield components.

215 Due to the aperture limits of the BDASA, we are unable to test whether there might be coherent  
 216 seismic energy at 0.18 Hz, which would represent primary microseism generated in-situ, as demonstrated  
 217 by the null region (black) in Figure 5b. This aperture limitation also prevents us from describing the 0.09  
 218 Hz ocean wave energy and 1.12 Hz Scholte wave energy peaks in detail. Seismic phases associated with

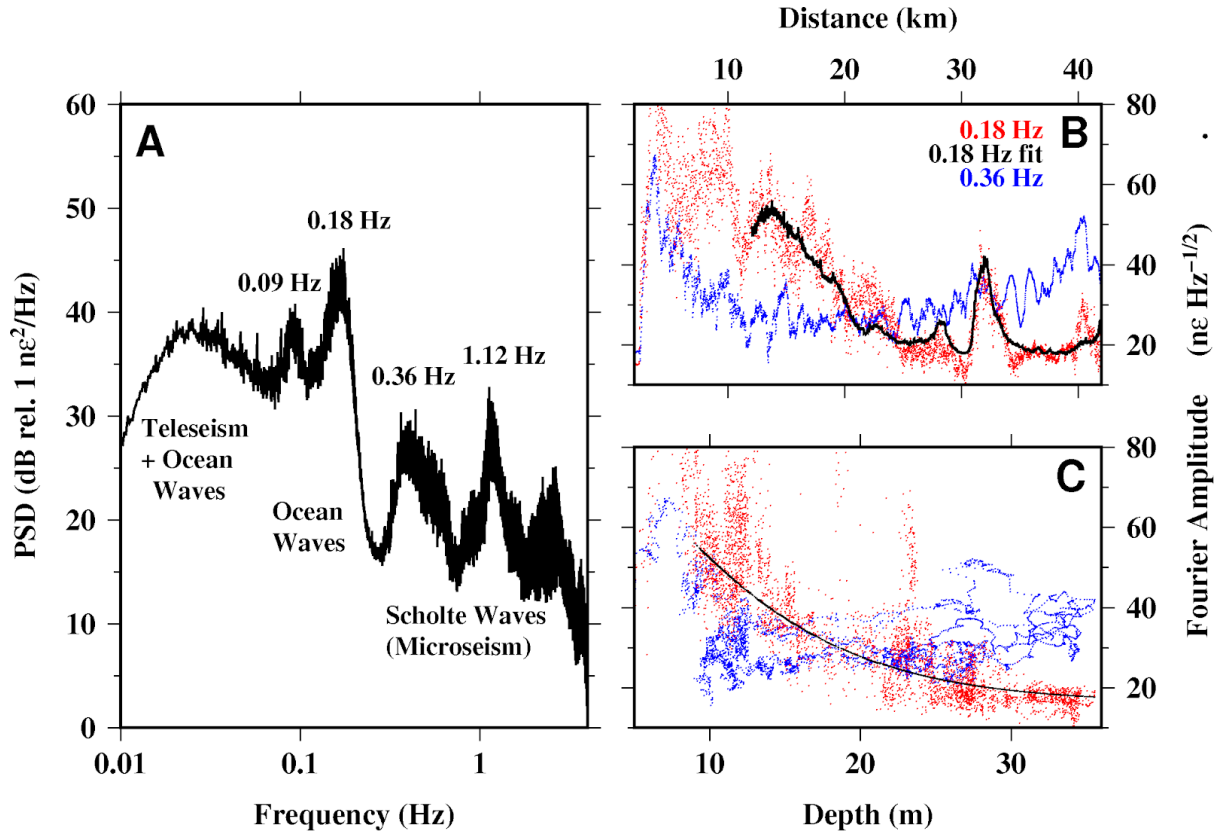


Figure 4: **Comparison of spectra and noise levels** (A) Mean power spectrum of raw DAS strain data over the complete 1 hr record between 35 and 40 km. (B, C) Fourier components of the raw DAS strain spectrum at 0.18 Hz (red) and 0.36 Hz (blue) with noise fit as a function of theoretical pressure at 0.18 Hz (black) plotted as a function of distance along the array (B) and ocean depth (C).

219 the 0.09 Hz peak would also lie in the null region in Figure 5b. The 1.12 Hz peak and associated high-  
 220 frequency Scholte wave energy observed up to 3.5 Hz (Fig. 5a) could correspond to a pair of opposing  
 221 surface gravity wave groups with dominant frequency of 0.55 Hz, which, following the dispersion relation  
 222 for surface gravity waves, are aliased in our data due to the Nyquist wavenumber of  $0.05 \text{ m}^{-1}$  for the  
 223 BDASA. Alternatively, the 1.12 Hz peak could represent a harmonic seismic mode of the subsurface  
 224 medium, which is excited by resonance, or external environmental noise from an unknown (potentially  
 225 anthropogenic) source.

### 226 3 Discussion and Conclusions

227 We have presented and analyzed our observations of seismic and ocean waves on an ocean-bottom  
 228 DAS array offshore Belgium, demonstrating that DAS arrays utilizing existing ocean-bottom fiber op-  
 229 tic installations can offer high value seismographic and oceanographic data products. In particular, we  
 230 successfully recovered both P- and S-phases from the 2018-08-19 Fiji deep earthquake. Rapid, accurate  
 231 measurement of body wave travel-times is an essential goal of next-generation broadband marine seis-

232 mology (Lay, 2009) and has motivated many recent advances in ocean-bottom seismic instrumentation  
233 (e.g. Hello et al., 2011). Ocean-bottom DAS arrays are an ideal technological solution because they offer  
234 real-time telemetry and are intrinsically synchronized, neither of which are easily achievable features of  
235 OBS networks. While we were unable to recover robust polarity of high-frequency P-phases, we can  
236 expect that ocean-bottom DAS arrays in deep water would have much lower detection thresholds for  
237 seismic signals than observed here, as has been demonstrated for OBS (Webb and Crawford, 2010). For  
238 an ocean-bottom DAS array, the noise floor can be considered as the superposition of instrumental noise  
239 from the DAS interrogator unit and fiber, temperature noise from variations in pore fluid temperature,  
240 pressure noise from ocean waves, and seismic noise. The aggressive filtering procedure we applied to  
241 recover teleseismic waveforms was necessitated to remove environmental signal, not instrument noise, as  
242 coherent signals of physical origin were observed across the full band of interest (0.01-5 Hz). Onshore  
243 studies with DAS arrays have found that instrument noise is approximately inversely proportional to  
244 frequency with a noise floor no higher than  $1 \mu\epsilon/\text{Hz}^{1/2}$  at 1 Hz (Williams et al., 2018). Laboratory  
245 experiments show that in a stable temperature environment, DAS systems can exhibit a noise floor be-  
246 low  $100 \text{ p}\epsilon/\text{Hz}^{1/2}$  at 1 Hz (Costa et al., 2018). On a DAS array, a temperature perturbation of 1 mK  
247 is indistinguishable from a  $10 \text{ n}\epsilon$  strain, so high-frequency temperature fluctuations along the fiber can  
248 contribute spurious signals. Water-bottom temperatures may vary on the order of 1 K at tidal periods  
249 in the near-shore environment; however, such variability attenuates strongly with depth and is inversely  
250 correlated to frequency (e.g. Kaplan et al., 2003; MacDonald et al., 2005). Consequently, instrumental  
251 and temperature noise are not limiting factors for most seismological applications, as seen here. In deep  
252 water settings, the magnitude of pressure oscillations beneath ocean surface gravity waves, the primary  
253 environmental noise which dominates BDASA data between 0.01 and 0.26 Hz, decays exponentially with  
254 depth. Therefore, the shallow-water setting of the BDASA actually represents a ‘worst case’ environment  
255 for recording teleseismic events (Webb, 1998; Webb and Crawford, 2010), and thus our ability to recover  
256 both P- and S-phases is particularly significant.

257 Compared to traditional OBS deployments, another advantage of DAS is the number and density of  
258 stations. Utilizing hundreds of stations from any segment of the array we were able to apply array-based  
259 processing in order to distinguish seismic and ocean signals based on their phase information. So-  
260 called “large N” deployments permit low detection thresholds for small earthquakes, precise location of  
261 earthquakes, low uncertainty in travel-time measurements, and high-resolution imaging studies (e.g. Rost  
262 and Thomas, 2002; Nakata et al., 2015; Li and Zhan, 2018). Further, we have demonstrated that large-N  
263 ocean-bottom networks open up new possibilities in studying ocean wave phenomena and microseism  
264 generation. The vast majority of studies examining the physics of ocean microseism generation have been  
265 limited to remote observation of radiated energy on terrestrial broadband networks (e.g. Friedrich et al.,

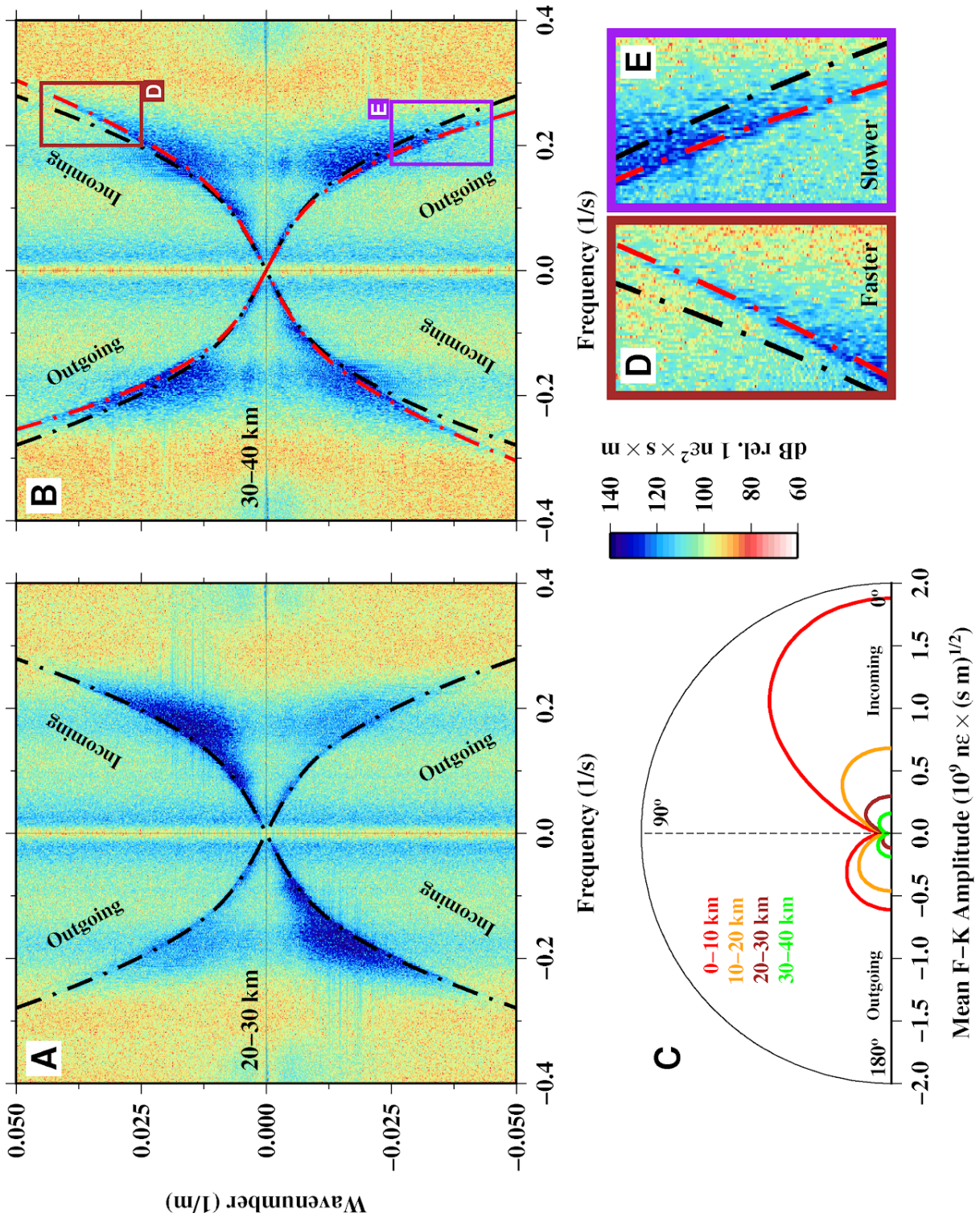


Figure 5: **Ocean surface gravity wave dispersion** (A) Raw DAS f-k spectrum calculated over 10 min between 20 and 30 km with the theoretical ocean surface gravity wave dispersion relation evaluated at  $H = 25$  m (black). (B) Same as (A) but for 30-40 km along the array with the theoretical ocean surface gravity wave dispersion relation modified with a mean-flow term evaluated at  $H = 25$  m and  $U = 0.5$  m/s (red). (C) Mean f-k amplitude as a function of azimuth calculated between 0.05 and 0.25 Hz using the surface gravity wave dispersion relation for four 10-km segments of the BDASA over 10 minutes. Note that DAS measures axial strain and is therefore less sensitive to broadside waves ( $\sim 90^\circ$  incident azimuth). (D), (E) Insets to (B) exhibiting the difference between the mean-flow corrected (red) and uncorrected (black) dispersion relations.

266 1998; Bromirski, 2001; Kedar et al., 2008; Traer et al., 2012). The few studies utilizing ocean-bottom  
267 instrumentation to correlate ocean-wave phenomena with microseism in-situ have been restricted by  
268 small network size, effectively resulting in measurements of microseism direction and intensity at a single  
269 point with or without simultaneous ocean wave information, and have had mixed success in validating  
270 theoretical models (Bradner et al., 1965; Goodman et al., 1989; Dorman et al., 1993; Kibblewhite and  
271 Wu, 1993; Nye and Yamamoto, 1994; Bromirski et al., 2005). Simultaneous observation of ocean pressure  
272 variations and seismic noise across several thousand channels on ocean-bottom DAS arrays of arbitrary  
273 geometry permits reconstruction of the full surface gravity wave and Scholte wave fields, as shown here,  
274 and, with the addition of a time-lapse component to future surveys, offers a leap forward in our ability  
275 to study microseism and its source processes.

276 However, several technological challenges still remain before DAS systems can complement or even  
277 replace BBOBS on a global scale. Foremost is the axial (single-component) directional sensitivity of  
278 DAS. Though work with helically wound optical fibers offering multi-component DAS sensitivity is  
279 underway (Hornman, 2017), modern BBOBS already provide four-component recording capability with  
280 the same state-of-the-art instruments used in terrestrial networks. We noted that teleseismic waveforms  
281 recovered from the BDASA did not exhibit coherent strain amplitude when compared with particle  
282 velocity at BOST, suggesting that the mechanics of strain transfer from the solid earth across the cable  
283 housing and into the optical fiber are complex and deserve further study (Mellors et al., 2018). In the  
284 laboratory, DAS exhibits a linear frequency response, resulting in correct amplitude and distortion free  
285 waves (Jousset et al., 2018; Lindsey et al., 2019), hence amplitude preservation may be currently limited  
286 by installation conditions and not by the DAS technology itself. Finally, ocean-bottom DAS deployments  
287 are not presently possible in remote oceanic locations. Most commercial DAS systems and laboratory  
288 measurements claim operation across up to 50 km of fiber, with sensitivity decreasing along the fiber  
289 due to optical attenuation. With the use of more complex pulse formats or distributed amplification, the  
290 sensing range can be extended to 70-100 km (Fernández-Ruiz et al., 2016; Martins et al., 2015; Pastor-  
291 Graells et al., 2017) with a more even distribution of sensitivity along the fiber, while still using a standard  
292 telecom fiber installation. In principle, longer distances can be achieved with complex dedicated fiber  
293 installations and power supply along the fiber link (via use of optical repeaters (Kim et al., 2001, Gyger  
294 et al., 2014) and/or multiple stage distributed amplification (Wang et al., 2014, Martins et al., 2015)),  
295 but the impact on the cost and DAS sensitivity means that such systems are not currently practical.

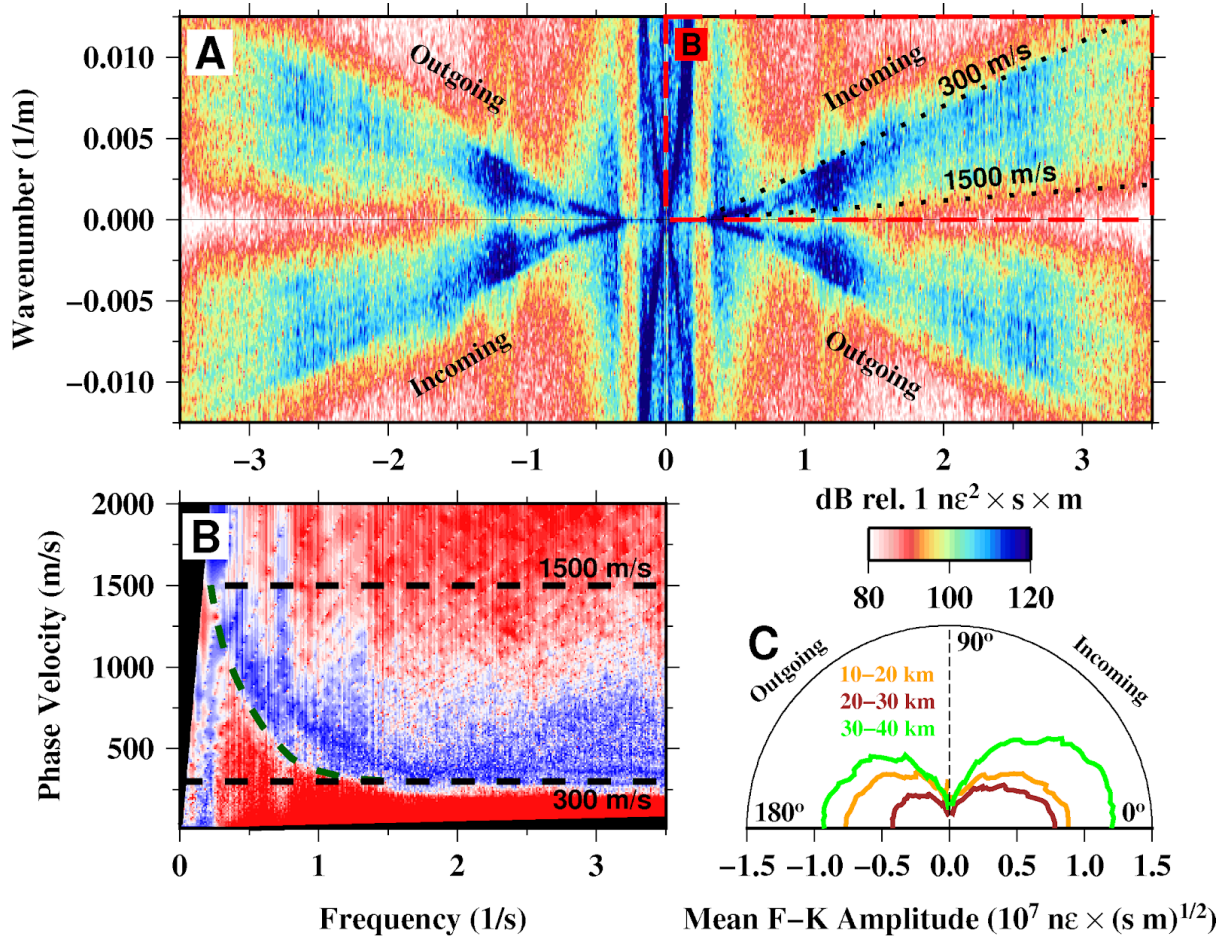


Figure 6: **Scholte wave symmetry and dispersion** (A) One hour of raw DAS strain data from 35–40 km of the array transformed into the f-k domain showing symmetric incoming and outgoing seismic phases between 0.3 and 3.5 Hz. (B) Data from quadrant 1 of (A) projected into phase velocity space showing coherent dispersion from  $\sim 1500$  m/s at 0.36 Hz to 300 m/s above 1 Hz. An approximate dispersion curve is sketched in green. Each frequency bin is normalized, and the black triangles show null regions. (C) Mean f-k amplitude as a function of azimuth calculated between 1.5 and 3.5 Hz by assuming no dispersion (see (B)) and a true Scholte wave velocity of 300 m/s. The theoretical azimuthal sensitivity of DAS to Scholte waves is approximately  $\cos^2\theta$  for our acquisition parameters (Martin, 2018).

## 4 Methods

A chirped-pulse DAS (Pastor-Graells et al., 2016) was used for the interrogator system. In comparison with conventional DAS systems, chirped-pulse DAS offers high signal-to-noise ratio (SNR) and low variations in sensitivity along the fiber (Pastor-Graells et al., 2017, Costa et al., 2018, Fernández-Ruiz et al., 2018a). The key of its performance lies in the use of a linearly chirped probe pulse for the time-domain interrogation. Temperature or strain perturbations around the fiber affect its refractive index, which in turn slightly alters the central wavelength of the propagating light. An appropriately high linear chirp in the probe pulse (i.e., that inducing a spectral content much higher than the spectral content of the transform limited pulse) induces a local wavelength-to-time mapping arisen from the temporal far-field condition (Goodman, 1994). Hence, variations in the central wavelength of the propagating light translate into temporal shifts in the trace at the particular location of the perturbation. The perturbation is then quantified by a time-delay estimation process via local trace-to-trace correlations over temporal windows similar to the probe pulse width.

The principle of operation of chirped-pulse DAS substantially improves the performance of the sensor over conventional DAS schemes. First, strain perturbations can be properly quantified by simply using direct detection. This contrasts with the conventional case, in which it is necessary to detect the trace optical phase for that purpose. Avoiding phase detection brings important advantages. Coherent detection imposes stringent requirement in the coherence length of the laser source, as it limits the DAS operation range due to the need for beating with a local oscillator. In chirped-pulse DAS, the coherent length of the probe laser can be relaxed, in principle simply requiring it to be higher than the pulse width, with almost no detrimental effect on the acoustic SNR (Fernández-Ruiz et al., 2018b). Polarization fading is not observed in chirped-pulse DAS. More importantly, sensitivity of conventional DAS completely fades in certain points along the fiber (acoustic SNR  $<1$  in up to 6% of fiber locations considering a healthy-SNR optical trace) due to the impossibility of maintaining the phase reference in low intensity trace regions caused by its interferometric nature. Those ‘blind spots’ need to be corrected using complex post-processing techniques or multi-wavelength measurements (Chen et al., 2017), typically at the expense of sensing bandwidth and higher measurements times. Chirped-pulse DAS, however, shows no fading sensitivity, enabling the “raw” strain signal as measured by the DAS to be directly processed without using any denoising/smoothing algorithm. This steady sensitivity has particular impact on the subsequent 2D processing applied to isolate seismic events from other sources, since all points are captured with similar noise/sensitivity along the whole fiber length ( $>40$  km) (Fernández-Ruiz et al., 2018a). In this study, we observed DAS sensitivity variation along the 42-km fiber lower than 3 dB. This is in contrast with the typical SNR variations observed in traditional DAS systems, where a variance of  $>18$

329 dB in the SNR distribution is expected over a few thousand channels (Fernández-Ruiz et al., 2018a).

330 The optical resolution (or gauge length) and channel spacing of the employed sensor were both 10 m  
331 (equivalent to one seismometer placed every 10 m, measuring distributed strain over a length of 10 m),  
332 totaling 4192 channels over 42 km. Each channel was sampled at 1 kHz and later downsampled to 10  
333 Hz in order to reduce the dataset size.

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## 344 Author Contributions

345 E.F.W., M.R.F.R., and H.F.M. carried out data analysis and wrote the manuscript; R.M. and R.V.  
346 acquired the data; Z.Z. and M.G.H. advised data analysis and edited the manuscript.

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