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# **The vulnerability of tidal flats and multi-channel estuaries to dredging and disposal**

W.M. van Dijk<sup>1,\*</sup>, J.R. Cox<sup>1</sup>, J.R.F.W. Leuven<sup>1</sup>, J. Cleveringa<sup>2</sup>, M. Taal<sup>3</sup>, M.R. Hiatt<sup>1,4</sup>, W. Sonke<sup>5</sup>,  
K. Verbeek<sup>5</sup>, B. Speckmann<sup>5</sup>, & M.G. Kleinhans<sup>1</sup>

<sup>1</sup>*Department of Physical Geography, Faculty of Geosciences, Utrecht University, Utrecht, The Netherlands*

<sup>2</sup>*Water & Environment Division, Arcadis, Zwolle, The Netherlands*

<sup>3</sup>*Department of Marine and Coastal Systems, Deltares, Delft, The Netherlands*

<sup>4</sup>*Department of Oceanography and Coastal Sciences, College of the Coast and Environment, Louisiana State University, Baton Rouge, Louisiana, United States*

<sup>5</sup>*Department of Mathematics and Computer Science, TU Eindhoven, Eindhoven, The Netherlands*

**Shipping fairways in estuaries are continuously dredged to maintain access for large vessels to major ports. However, several estuaries worldwide show adverse side effects to dredging activities, including a shift from multi-channel systems to single-channel systems and the loss of ecologically valuable intertidal flats. We used a physical scale-experiments, field assessment of the Western Scheldt estuary (the Netherlands) and morphodynamic model runs to analyse the effects of dredging and future scenarios. All methods indicate that dredging and disposal strategies are in the long run unfavourable because dredging increases the imbalance between shallow and deeper parts of the estuary, causing a loss of valuable connecting channels and fixation of the tidal flats and main channel positions. Changing the disposal**

21 **strategy towards main channel scour disposal can be economically and ecologically better**  
22 **for the preservation of the multi-channel system. Further channel deepening will accelerate**  
23 **the adverse side effects, whereas future sea-level rise may revive the multi-channel system.**

## 24 **1 Introduction**

25 River mouths, or estuaries, are important centres of global transportation and commerce. Most  
26 estuaries are continuously dredged since the early 20<sup>th</sup> century with an acceleration of activity in  
27 recent decades. Continuous dredging is needed to maintain a minimum depth requirement for the  
28 shipping fairways so that large commercial vessels can access major ports<sup>1</sup>, e.g., Yangtze Estuary  
29 (Shanghai)<sup>2</sup>, Western Scheldt (Antwerp)<sup>3,4</sup> and Elbe Estuary (Hamburg)<sup>5</sup>. The use of estuaries for  
30 shipping also poses considerable issues<sup>6</sup>. Dredging smooths the estuary as obstruction, e.g. shoals,  
31 bars and sills are removed<sup>7</sup>, which affect smaller channels and bars that are important for seabed  
32 animals, fish and birds. The hydrodynamic effects of dredging consists of tidal amplification<sup>8,9</sup>  
33 that increases circulation and increases the flood-dominance of the tidal asymmetry<sup>10</sup>. It is site-  
34 specific which hydrodynamic processes dominate and how these affect sediment transport and  
35 morphodynamics of the system. Moreover, dredging activities are thought to cause a shift from a  
36 multi-channel system to a single-channel<sup>11,12</sup> or loss of ecologically valuable intertidal flats<sup>1,8,13-16</sup>.  
37 Yet, it remains undiscovered what the long-term effects of the current dredging and disposal strate-  
38 gies have on the sustainability of tidal flats and multi-channel estuaries, and what the response will  
39 be from future stresses such as increasing minimum channel depth for shipping and sea-level rise.

40 The ecological quality of multi-channel systems is partly determined by the presence and

41 characteristics of intertidal flats and channels<sup>17</sup>. Multi-channel systems often display a quasi-  
42 regular repetitive pattern that consists of meandering ebb-dominated channels and straight flood-  
43 dominated channels in the inner bends<sup>18,19</sup>. The difference in meander action between ebb and  
44 flood channels, and the opposite direction of residual sand fluxes in these channels lead to the for-  
45 mation of intertidal flats, which are dissected by connecting channels<sup>17,18,20,21</sup>. Estuaries consists  
46 of an ebb-dominated channel and a flood-dominated channel, displaying characteristic morpho-  
47 logic behaviour that is associated with net sediment exchange between channel junctions. Besides  
48 the ecological value of the multi-channel system, there are more reasons that advocate sustaining  
49 the multi-channel system, namely:

- 50 ● side channel shallowing reduces the navigability of smaller inland vessels <sup>4</sup>,
- 51 ● main channel deepening increases tidal range and flood risk <sup>14</sup>,
- 52 ● increased peak velocity in deepened main channel affects navigability <sup>7,22</sup>,
- 53 ● channel deepening threatens bank stability, and tidal flat stability and salt-marsh stability  
54 <sup>14,23,24</sup>,
- 55 ● large morphological changes alter ebb-flood dominance, including duration and asymmetry  
56 <sup>22</sup>, potentially affecting mud and sand budgets.

57 Changes in the connecting channels affect the spatial extent of mudflats, tidal marshes and  
58 intertidal flat ecosystems that provide important services, such as storm protection, shoreline sta-  
59 bilization, and food production, which support the livelihoods of millions of people worldwide<sup>25</sup>.

60 To improve biodiversity and increase tidal flat areas in estuaries it is becoming imperative to use  
61 nature-based solutions. Urgent research questions related to dredging and disposal in large estu-  
62 aries in general are: (1) To what degree can the multi-channel system be sustained/ improved by  
63 current dredging and disposal practices? (2) What are the effects of further main channel deepening  
64 on the morphology of the multi-channel system? (3) What will be the effect of predicted sea-level  
65 rise<sup>26</sup> on the morphological and ecological functioning of the estuary? By a combination of scale  
66 experiments in the laboratory where the effect of dredging was isolated and data assessment from  
67 the Western Scheldt (the Netherlands) for real scale practice, we show how dredging changes the  
68 natural development of estuaries. We applied a numerical model to quantify how disposal strategy  
69 can limit adverse side effects, and how future scenarios, such as increasing shipping draft and sea  
70 level rise, will affect the estuary morphodynamics and the habitat suitability.

## 71 **2 Experimental development of a multi-channel estuary**

72 A new experiment in the Metronome<sup>27</sup> with dredging and disposal was conducted in otherwise the  
73 same conditions as an undredged control experiment that shows three phases of development<sup>21</sup>.  
74 First, alternate bars, i.e. shoals, develop during widening of the estuary. The initial alternate bars  
75 grow and bound a meandering channel, comparable to alternate bars in rivers<sup>28-30</sup>. As soon as  
76 the bars exceed a width-to-length ratio of approximately 1/7, the flood flow cuts barb channels,  
77 described as a one-ended channel that partly crosscuts a bar<sup>31,32</sup>, into the alternate bars. The  
78 seaward barb channels progressively cut through the alternate bars, while the bended channels  
79 expands laterally, forming an estuary planform. This estuary shape follows a Van Veen<sup>33</sup> like

80 structure with mutually evasive ebb- and flood-dominated channels, and is similar to the Western  
81 Scheldt.

82 Second, mid-channel bars formed that are large enough to divert the flow, accelerate outer-  
83 bend erosion, and form major bifurcations and confluences seaward and landward of the mid-  
84 channel bars. A quasi-periodic estuary planform forms, where at the confluence locations the  
85 estuary width remains generally narrow and dynamic channels and bars only occur within a small  
86 stretch of the estuary width. Around this phase dredging was started in the new experiment pre-  
87 sented here (Figure 1 top panel). This required the cutting of an initial shipping fairway after  
88 3000 cycles, or single main channel, which connected ebb and flood channels to follow the natu-  
89 rally deepest course.

90 In the third phase, further extension of the outer bends makes the mid-channel bar favourable  
91 for a short cut during both the ebb and flood flows. New barb channels formed on the mid-channel  
92 bars, which cross cut the bar forming a new main channel in the middle of the estuary (Figure 1  
93 left panel 4401-5887 tidal cycles). In case of dredging, the meander bend and accompanying  
94 disposal of dredged sediment on the shoal in the middle of the flume makes the meander stable  
95 and only migrates in lateral direction. Because of the higher shoal the water level does not exceed  
96 shoal elevation and no new barb channels formed (Figure 1 right panel 4600-5200 tidal cycles).  
97 After the final maintenance dredging event (5200 tidal cycles) the estuary was allowed to evolve  
98 further for 8000 cycles until it reached termination at 13,000 tidal cycles. The lateral migration  
99 of the bend in the middle of the flume continuous even when dredging stopped, whereas seawards

100 mid-channel bars are cross cut. Eventually, a dynamic equilibrium at the bar-confluence scale is  
101 reached, in which sediment from bars and banks is reworked into new bars within the estuary.  
102 In both experiments, with and without dredging, the quasi-periodic planform deviates from the  
103 ideal estuary shape<sup>34</sup>, which describes estuaries as perfectly converging channels, at the end of the  
104 experiments<sup>21</sup> (Figure 1 bottom). In general, the experiments confirm that the shoal elevation and  
105 sizes increases, whereas channel dynamics decreases due to dredging and disposal.

106 The Supporting Movies 1 and 2 presents the development of the two experiments observed  
107 from the overhead cameras.

### 108 **3 Increasing dominance of the main channel and intertidal flats**

109 The development of natural habitats in estuaries is partly determined by the cumulative area of  
110 intertidal flats<sup>35,36</sup>. Particularly, the local physical conditions, i.e. low dynamic areas, are highly  
111 important for ecology in estuaries with a complex spatial configuration of tidal flats, shoals and  
112 channels<sup>16</sup>. Tidal flats with elevation above high-tide level are referred to as supratidal and those  
113 with an elevation below low-tide level are classified as subtidal<sup>36</sup>. Analogue flume experiments  
114 of a multi-channel estuaries show that the tidal flats increase in volume (Fig. 2a), by the increase  
115 of area size as well as elevation, whilst dredging and disposal is ongoing. This increases the total  
116 intertidal area and especially the total supratidal area (Fig. 1). Tidal flats that were frequently used  
117 as disposal locations increased in volume and elevation, causing an increase in elevation difference  
118 with the deeper dredged main channel.

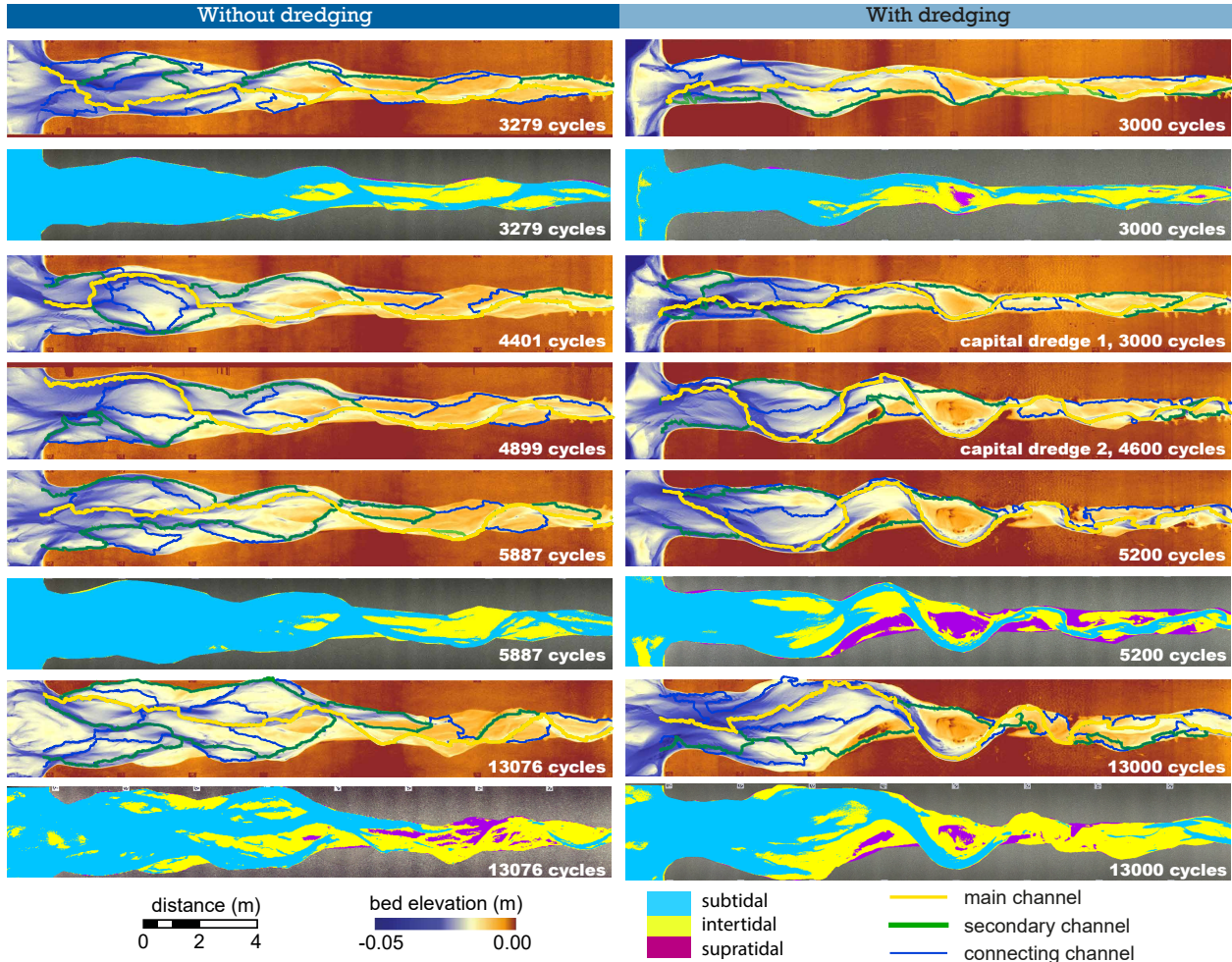


Figure 1: Estuary evolution of the experiment without (left panels) and with dredging (right panels) overlain by the extracted channel network illustrated by bed elevation maps. The sub-, inter- and supratidal area are based on water level measurements.



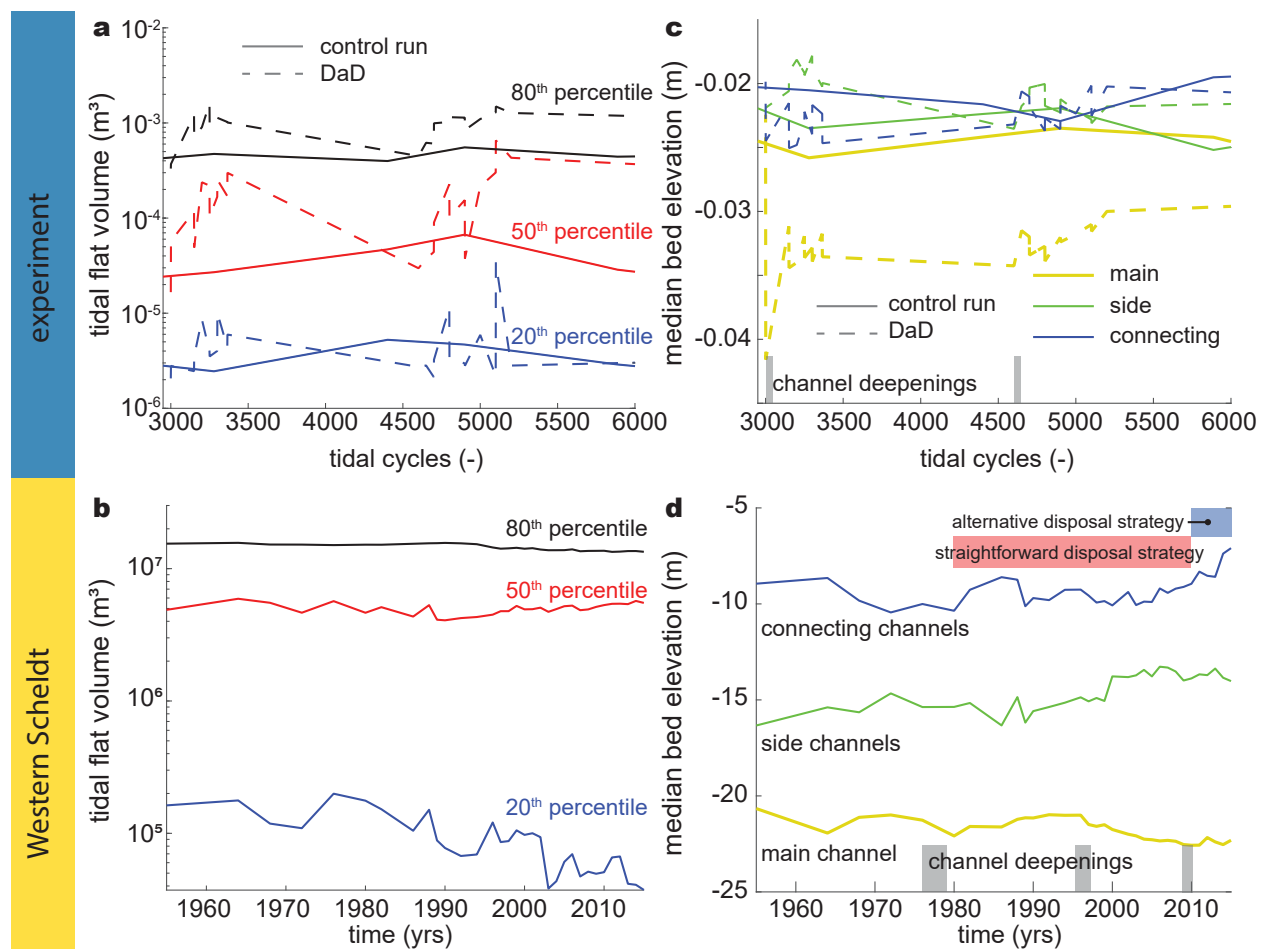


Figure 2: Increasing contrast between the deepening main channel and consolidating tidal flats shown by increasing tidal flat volumes, deepening main channels, and shallowing side and connecting channels. a) Tidal flat volume for two experiments. b) Tidal flat volume in the Western Scheldt since 1955. c) Median bed elevation for all three types of the channel for the two experiments. d) Median bed elevation for the main, side and connecting channels in the Western Scheldt. In a and b the percentiles are taken from the distribution of all tidal flat areas encompassed by the channel network, where the 80<sup>th</sup> percentile represents the larger more significant tidal flats.

119 The bathymetric field data of the heavily dredged Western Scheldt confirms that, as dredging  
120 volume increases, the median tidal flat volumes calculated from area and elevation tends to increase  
121 due to consolidation of shoals since 1990s (Figs. 2b and 3), meaning an increase in intertidal  
122 area. The tidal flat elevation above mean sea level (0 m NAP, Amsterdam Ordnance Datum) has  
123 increased by half a meter since 1955 and slowed down in the last decade<sup>4,37</sup>.

124 Important criteria for the maintenance of a multi-channel system are the channel width-to-  
125 depth ratio and flow velocity of the ebb- and flood-dominated channels<sup>19</sup>. Shallowing of one of the  
126 main (ebb or flood) channels could destabilise the multi-channel system as like in a multichannel  
127 river with unstable bifurcations<sup>38</sup>, which also reduces the number of connecting channels over the  
128 intertidal flats<sup>3</sup>. Flume experiments and field observations show increasing differences in channel  
129 depth among the main, side and connecting channels in case of dredging (see also Supplementary  
130 Figs. 3a, b, d, and e). Dredging deepens one of the channels and causes the secondary channels to  
131 become shallower (Fig. 2c).

132 The flume experiments demonstrate that bed elevation for the main channel becomes signif-  
133 icantly deeper than the side and connecting channels in case of dredging, whereas without inter-  
134 ference, ebb-and flood dominated channels form that are equal in size in the flume experiments  
135 (Fig. 2c). This suggests that, in a natural multi-channel system, all channel scales are equally  
136 important, and the imbalance in bed elevation is a direct effect of dredging. The difference in  
137 channel depth persists long after dredging was terminated in the experiment. These findings show  
138 that dredging leads to an unnatural imbalance among the main, side and connecting channels in

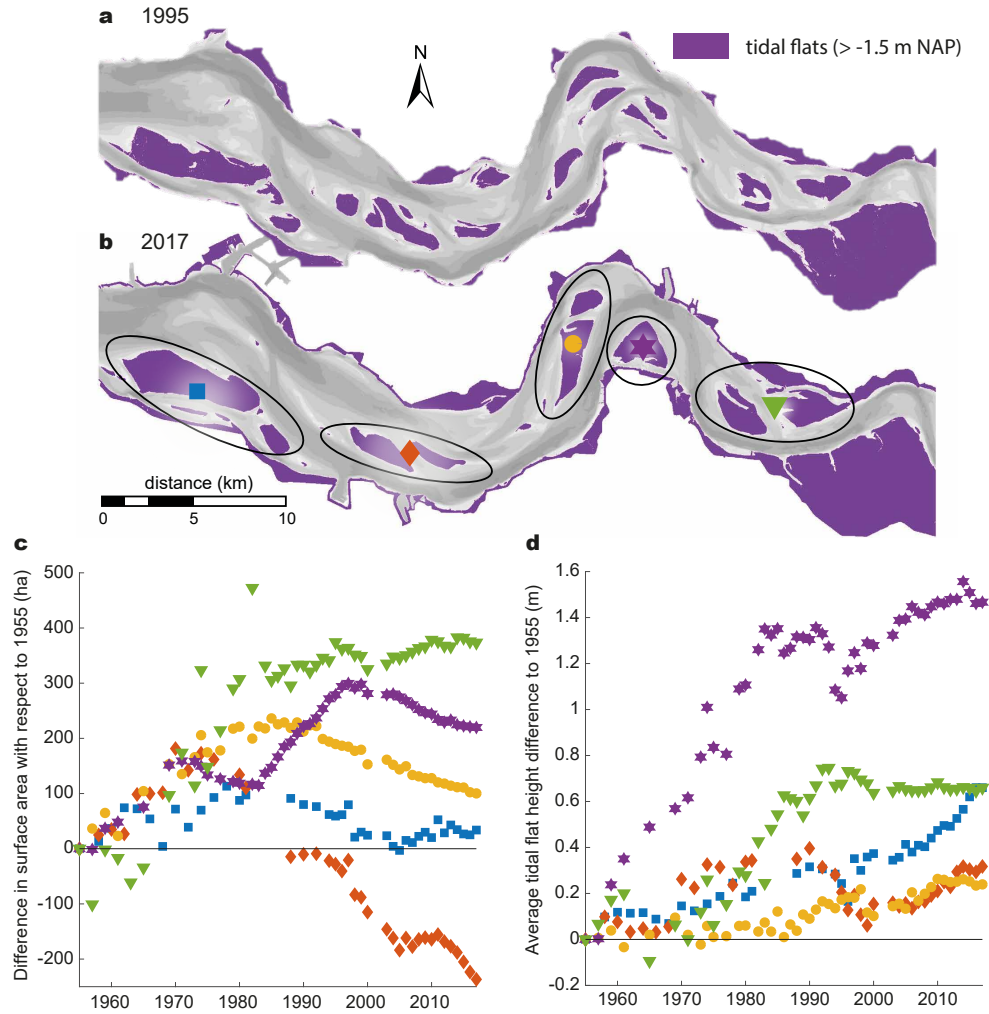


Figure 3: Shoal development in the Western Scheldt from 1955-2017. a-b) Ongoing consolidation of tidal flats, from fragmented shoal complexes (a) to 2-3 large tidal flats per meso-cell (b). c) Shoal surface area difference with respect to 1955 shows a generally increase in tidal flat area. d) Average tidal flat height difference respect to 1955 shows an increase of all tidal flat locations.

139 a multi-channel system, and we expect that the consequences are irreversible within the human  
 140 lifespan.

141 Field observations confirm that, since dredging started, the main channel became deeper,  
142 as expected, especially following major main channel deepening events (the 1970s, 1997-98 and  
143 2010-11, to the tidal-free water depths of 9.5 m, 11.6 m, and 14.5 m<sup>39</sup>, respectively). The volume  
144 of disposal of dredged sediment in the side channels was reduced when it appeared that this tended  
145 to close them off<sup>3,39</sup>. The conversion to an alternative tidal flat disposal strategy, where 20%  
146 of the dredged sediment was disposed on the downstream end of the intertidal flats, resulted in  
147 stabilisation of the channel depth of the side channels. However, our analysis shows that in the  
148 last 5 years the smaller-scale connecting channels continue to silt up (Fig. 2d). This development  
149 jeopardizes the multi-channel system and fails to improve the desired self-erosive capacity of the  
150 flow in the connecting channels<sup>40</sup>.

#### 151 **4 Decreasing channel dynamics and loss of connecting channels**

152 Channels and intertidal flats form highly dynamic elements in natural estuaries<sup>21,41</sup>. The dynamics  
153 are determined by the displacement and migration of the channels that results in erosion and ac-  
154 cretion of the intertidal flats (see Supplementary Fig. 2). The flume experiments show that because  
155 of the decrease in channel displacement and fixation of the main channel by the dredging activity,  
156 the channel mainly migrates laterally. As result, the meander bend increases in amplitude and sin-  
157 uosity (Fig. 6b). Stabilization of the meander bend reduced the migration rate of the main channel  
158 in the experiments by 10-25% (Fig. 4a). Channels in the Western Scheldt migrate at different rates  
159 depending on channel scale, occupying a large portions of the estuary (Fig. 4b). The variation of  
160 the main channel location is limited laterally by geological constraints and man-made structures

161 and is fixed in place by dredging. In contrast, the side and connecting channels are largely free to  
162 migrate.

163         Actively disposing dredged sediment at the seaward side of intertidal flats was expected to  
164 increase dynamics of the connecting channels<sup>40</sup>, but surprisingly the opposite was observed in the  
165 field and experiments. Smaller-scale connecting channels link the large ebb and flood channels.  
166 These smaller channels often display a quasi-cyclic morphologic behaviour, characterised by pro-  
167 cesses of channel origination, migration, and degeneration at a timescale of years to decades<sup>18,42</sup>.  
168 Water level differences between the ebb and flood channels drives the flow of water through these  
169 connecting channels and the connecting channels form where the difference in water levels is the  
170 largest, typically in shoal areas at the landward end of the flood channel<sup>39</sup>. The large reduction  
171 in dynamics of the connecting channels is demonstrated by the decreasing number of connecting  
172 channels since 1955, whilst the number of side channels remained the same or slightly increased  
173 (Fig. 4d).

174         This observation is confirmed by the flume experiments, which show a general decrease in  
175 the number of channels for the dredged scenarios compared to the control runs (Fig. 4c). This is  
176 again especially true for the number of connecting channels, which reduces by almost 50% during  
177 dredging and remains 10-20% lower for the period after termination of dredging. This is a problem,  
178 because low-dynamic areas were in the past characterised by substantial reworking of their muddy  
179 sediment by migration of the connecting channels. Mud-rich areas are desirable for establishment  
180 of valuable habitats<sup>16</sup>. A decrease in high-dynamic area is beneficial for habitats only if it is

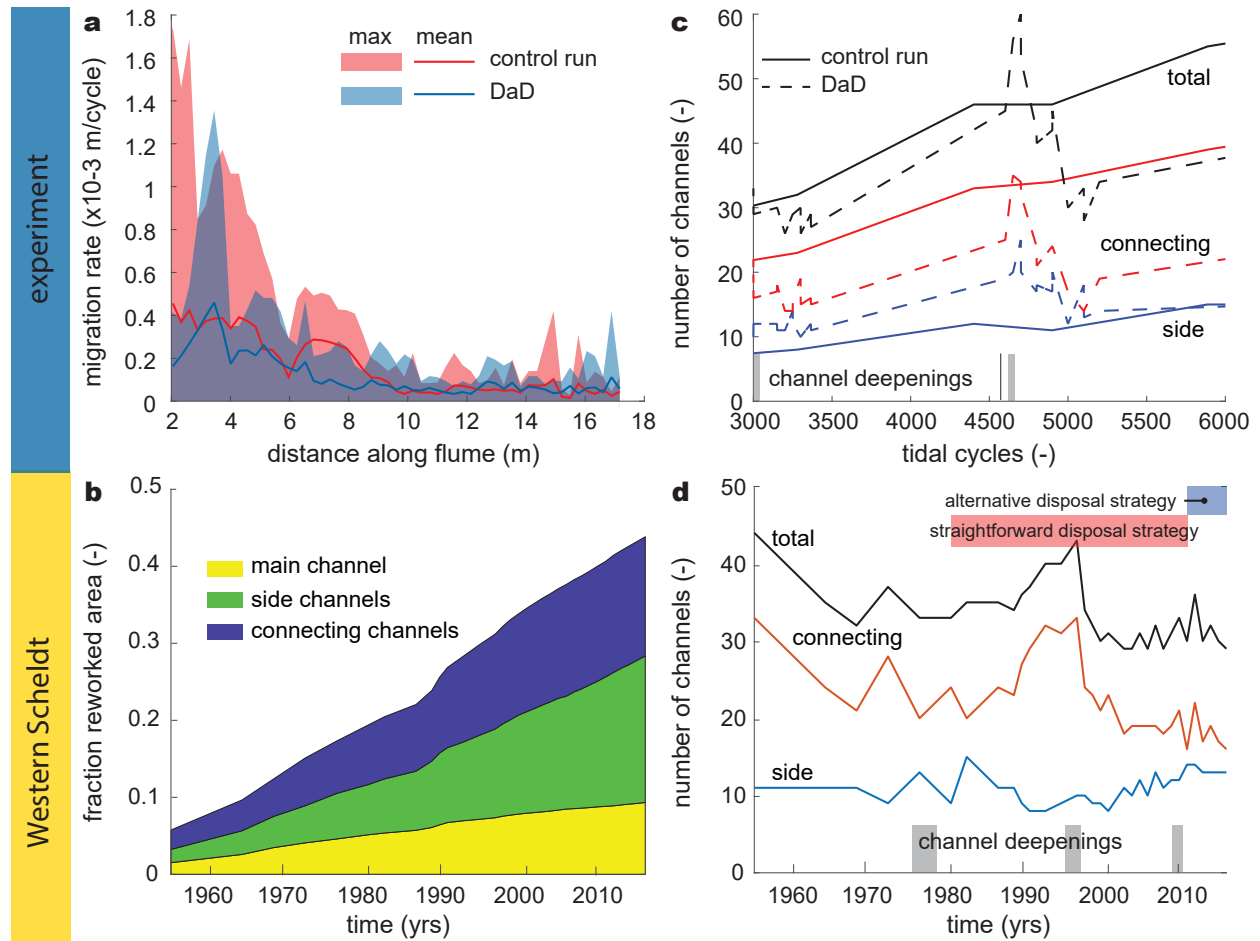


Figure 4: Channel activity and number of channels. a) The migration rate of the main channel for the two experiments. b) Fraction of reworked area in the entire study area over the past 60 years by the main, side and connecting channels in the Western Scheldt. c) The number of channels for the two experiments. d) The number of channels in the Western Scheldt since 1955.

181 replaced by low-dynamic area, but in reality the tidal range increase causes transformation of low-  
182 dynamic areas into high-dynamic areas, which is the opposite of the restoration targets<sup>43</sup>.

## 183 **5 Effects of future pressures on the estuary**

184 The numerical modelling are complementary to the flume experiments and are a valuable tool to  
185 explorer the effect of future pressures on the estuary development. Since dredging began at early  
186 20<sup>th</sup> century, the disposal strategy has evolved with the aim to counteract the adverse effects of  
187 dredging. Model result for an alternative tidal flat disposal shows, however, very little difference  
188 with a previous straightforward strategy (Fig. 5a, b). For the near future, a new strategy was  
189 proposed to dispose dredged sediments in the deep scours of the main channel<sup>44</sup>. Our model  
190 simulations, with a foreseen approach of dredged sediment disposal solely in scours of the main  
191 channel, indicate that this reduces the adverse effect of decreasing channel dynamics (Fig. 5a) and  
192 halts the increase in tidal flat volume (Fig. 5b). In case of the Western Scheldt, the total scour  
193 volume available for disposal is  $1.7 \cdot 10^9 \text{ m}^3$  assuming the current tidal-free navigation depth of  
194 14.5 m. This means that with a disposal rate of  $10 \cdot 10^6 \text{ m}^3$  it will take at least 100 years to fill  
195 the deep scours, assuming that it is not transported out. This promising disposal strategy should  
196 therefore be tested in reality<sup>44</sup>.

197 Increasing vessel draft<sup>45</sup> brings management challenges. Increasing the minimum main chan-  
198 nel depth in the model simulation shows decreasing dynamics of the main channel, whereas there  
199 appears to be a minimum in connecting channel dynamics (Fig. 5c). While channel dynamics

200 decrease with dredging depth, there is no systematic increase in tidal flat volume with dredging  
201 depth. The tidal flat volume is annually 10-25% higher for 16-20 m water depth, respectively  
202 (Fig. 5d). We argue that further deepening of the shipping fairway for short-term economic pur-  
203 poses should be carefully evaluated against long-term ecological value, as a further decrease in  
204 channel dynamics will directly affect intertidal flat dimensions and therefore valuable habitat area  
205 as shown by past developments in the Western Scheldt and by scenarios in the numerical modelling  
206 and experiments.

207 Future threats from sea-level rise (SLR) are expected in estuarine systems<sup>46</sup> and should be  
208 a key issue in future assessments for understanding the dynamic response of channel-shoal inter-  
209 actions in estuaries. Here, we systematically evaluate the response of the estuary to various SLR  
210 scenarios based on the Intergovernmental Panel on Climate Change Fifth Assessment Report<sup>26</sup>. We  
211 expect that SLR has less effect on the channel-shoal interactions compared to the deepening of the  
212 shipping fairway because the rates are small compared to the draft depth rate of 140 mm/yr for the  
213 container-vessels. For this case study of a flood-asymmetric estuary, in which sediment is imported  
214 from the mouth (see Supplementary Fig. 4b), the development depends on sediment availability  
215 at the seaward side. We expect that sea-level rise will transport additional sediment into the estu-  
216 ary. The model simulations showed a doubling of coastal sediment input for the lower bound of  
217 SLR, up to 150% increase for the upper bound of SLR, based on bed elevation differences after  
218 40 yrs morphological development. The actual import will partly depend on ebb delta dynamics,  
219 alongshore drift and sediment availability, which are not considered in the present model runs. The  
220 model scenarios show that limited future sea-level rise will cause a valuable increase in dynamics



221 in terms of the side and connecting channels, whilst the main channel becomes fixed even further  
222 (Fig. 5e). Intertidal flat elevation increases with the sea-level rise in the model run whilst tidal flat  
223 volume decreases (Fig. 5f).

## 224 **6 Discussion and Conclusions**

225 Extensive human intervention is common in many estuaries worldwide. The morphology of es-  
226 tuaries including location and presence of bars and shoals, amount of intertidal flats, number of  
227 channels and side channels are directly impacted by these human interventions. We argue that the  
228 disposal strategy of dredged material is as important as the dredging itself in maintaining suitable  
229 conditions for the persistence of an ecologically valuable multi-channel system<sup>4,47,48</sup>. Model sim-  
230 ulations reveal that current dredging strategies are not sustainable and current disposal strategies  
231 to counter adverse effects are hardly effective. The experiments suggest that channel-shoal inter-  
232 actions in anthropogenically altered estuaries are affected for a much longer time-span than the  
233 period of dredging.

234 A promising strategy could be the scour disposal strategy in which dredged sediment is dis-  
235 posed of in the scours of the main channel<sup>44</sup>, but its effectiveness also depends on future threats  
236 such as increasing vessel draft and SLR. We would argue that further deepening of the should be  
237 carefully considered against adverse effects. In view of future SLR the sediment must be kept in the  
238 system rather than mined or disposed. A further decrease in channel dynamics and displacement  
239 directly destabilise the valuable multi-channel system, including intertidal flats that determines

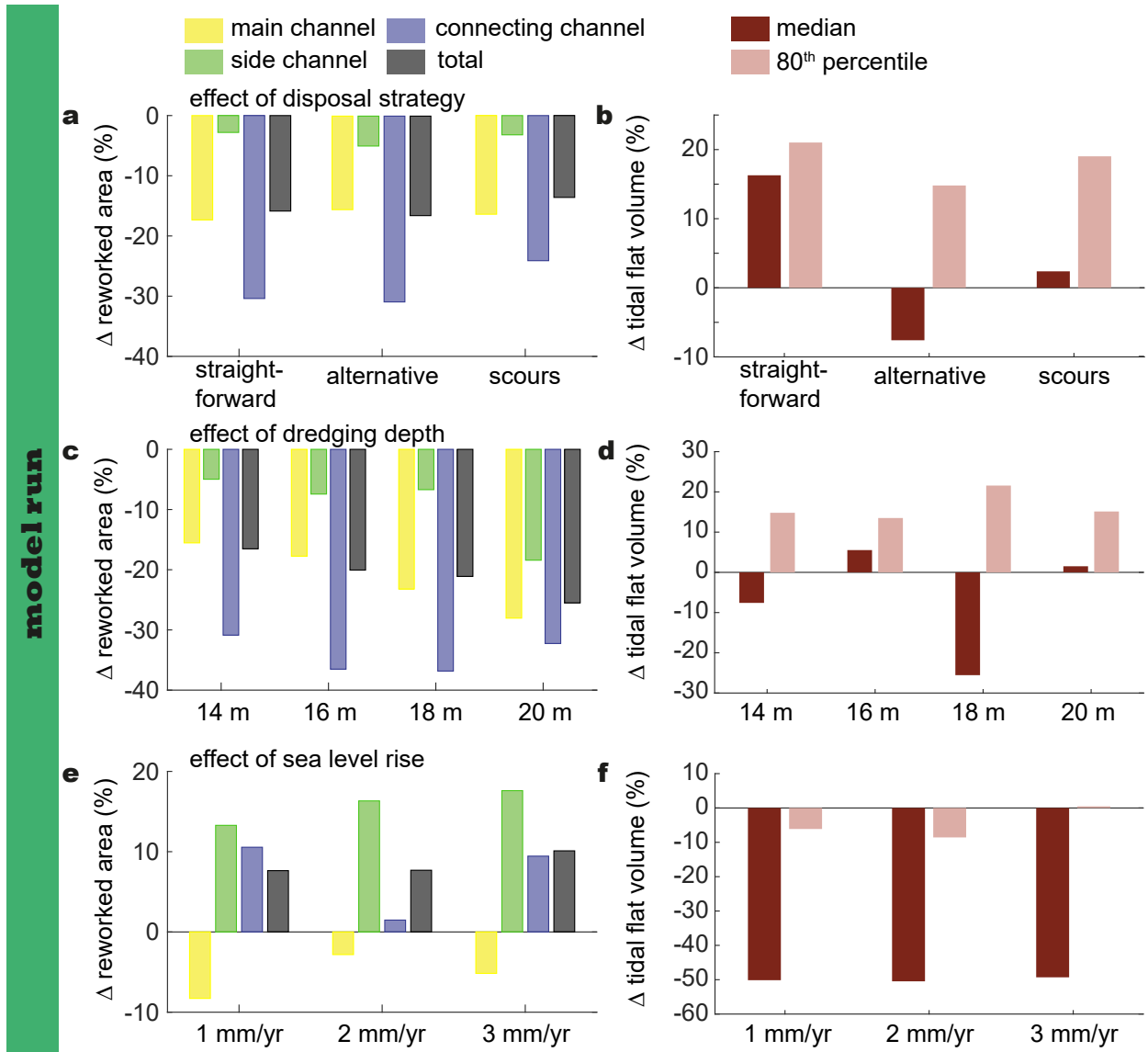


Figure 5: Effect of future scenarios on channel dynamics (reworked area) and ecological valuable waterline length (intertidal flat volume) compared to the control run. a) Effect of disposal strategy on changes in the reworked area. b) Effect of disposal strategy on changes in tidal flat volume. c) Effect of dredging depth on changes in the reworked area. d) Effect of dredging depth on changes in tidal flat volume. e) Effect of sea-level rise on changes in the reworked area. f) Effect of sea-level rise on changes in tidal flat volume.

240 the existence and persistence of the ecologically-important habitat, and the depth of side chan-  
241 nels for navigability of smaller inland vessels<sup>7</sup>. Furthermore, dredging directly increases the tidal  
242 range resulting in higher flood risk, ebb-flood dominance alters, and peak velocity increases that  
243 complicates navigability<sup>14,22</sup>. The increase in channel dynamics associated with SLR provides  
244 an opportunity to restore ecologically valuable areas, by increasing intertidal flats and the num-  
245 ber of connecting channels that flow through and feed these systems, while biophysical feedback  
246 processes may adapt to the SLR<sup>49</sup>.

247 From our laboratory experiments, field data and numerical model study we conclude that  
248 fairway dredging mainly determines the dynamics of channels and ecological valuable tidal flats,  
249 while the disposal strategy aiming to reduce these adverse effects is ineffective. Further deepen-  
250 ing of the navigation channel accelerates the adverse effects of dredging, whereas sea-level rise  
251 scenarios show potential improvement of channel dynamics and intertidal flat volumes.

## 252 **7 Experimental Procedure**

253 We use three independent complementary methods. 1) In physical scale-experiments, the long-  
254 term development and resilience of an estuary with dredging and disposal was compared with a  
255 reference experiment without interventions. 2) Field data from the well-monitored Western Scheldt  
256 was used as a case to measure the morphological changes that occurred over time of an actual  
257 dredged estuary. Literature/reports were used to connect morphological changes to changes in  
258 dredging and disposal strategy. 3) Numerical model scenarios allowed testing of the effects of dis-

259 posal strategy and future changes in dredging regime and SLR scenarios. For all three approaches,  
260 we employ, a novel channel-network algorithm that scale-independently and objectively extracts  
261 channel network topology. The network is then used to determine the channel depth distribution,  
262 channel migration, and the tidal flat volumes.

263 **Physical scale-experiments** Experiments with and without dredging and disposal were conducted  
264 in a periodically tilting flume, the Metronome. The flume is 20 m long and 3 m wide and had a  
265 sandy bed of 7 cm thick. Periodic tilting of the flume enables sediment transport during both ebb  
266 and flood phase<sup>27</sup>, leading to autogenic development of estuarine morphodynamics<sup>21,50</sup>. A single  
267 tidal cycle spans 40 seconds and had a maximum tilting gradient of 0.008 m/m. Further infor-  
268 mation on scaling is reported in earlier papers<sup>21,27,50</sup>. Changes of the experiment were recorded  
269 by time-lapse overhead imagery and DEMs are constructed with the structure-for-motion soft-  
270 ware, AGISOFT Photoscan (version 1.2.6.2038). The DEMs were used to calculate dredging and  
271 disposal volumes and their locations. The development of the experiment with dredging was com-  
272 pared to a control run without dredging (Figs. 6a-b and Supplementary Videos 1 and 2).

273 The experiment started with a narrow initial converging channel in the middle of the sand-  
274 bed. Boundaries are erodible, and continuous erosion and deposition led to the development of a  
275 self-formed estuary before dredging and disposal were started at 3000 tidal cycles (Fig. 1). The  
276 self-formed estuary consisted of a multi-channel system with ebb and flood channels as well as  
277 tidal flats and an irregular shape, similar to the same morphological properties as the control run<sup>21</sup>.  
278 After 3000 cycles, an initial ‘shipping fairway’ was cut along the deepest natural course of the

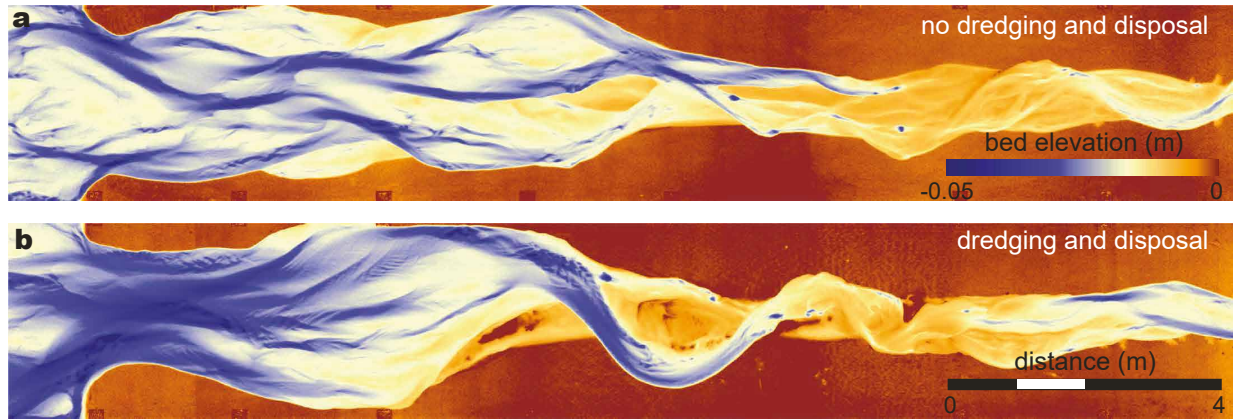


Figure 6: Bed elevation maps for the two flume experiments. a) Final bed elevation for the control run after 13,000 tidal cycles. b) Final bed elevation after 13,000 tidal cycles for the experiment with dredging and disposal (DaD) occurring between 3,000-5,200 tidal cycles.

279 estuary, which linked both ebb and flood channels when necessary (capital dredging). The ship-  
 280 ping fairway was lowered by about 1/5 of the original depth using a palette knife and removal of  
 281 sediment by hand. The minimum depth requirement for the dredging was set to 3.5 cm for the  
 282 first capital dredge, whereas for the second capital dredge, which was necessary because of the  
 283 continuous rapid expansion of the estuary, the minimum depth requirement was set to 3 cm. Main-  
 284 tenance dredging then took place every 50-100 cycles to remove material which made the channel  
 285 ‘unnavigable’, in other words when the water depth was below the minimum depth requirement.  
 286 The width of the dredged main channel was proportional to the width of the estuary in the same  
 287 ratios as for the field example, the Western Scheldt. For the landward end, this was approximately  
 288 10% of the estuary width, 15% moving into the middle reaches of the estuary and at the seaward  
 289 end up to 20% of estuary width. Sediment from the first capital dredge was removed from the  
 290 system entirely, while sediment removed later during maintenance dredging was redistributed on

291 the seaward side of tidal flats, at the entrance of side channels, and in the scours of the main chan-  
292 nel (depth > 4 cm). The disposal location was dependent solely on proximity to the dredge site.  
293 Dredging volumes varied along the estuary, with an increased volume in the middle section (Sup-  
294plementary Fig. 5a). After the final maintenance dredging event (5200 tidal cycles) the estuary was  
295 allowed to evolve further for 8000 cycles until it reached termination at 13,000 tidal cycles.

296 **Field data** The Western Scheldt Estuary is a well-monitored estuary in the southwestern part of  
297 the Netherlands and refers to the seaward section of the tide-dominated Scheldt estuary. To es-  
298 tablish the development of the Western Scheldt and link this with dredging and disposal strategies  
299 and volumes (Supplementary Fig. 5b), bathymetry data, so called 'Vaklodingen', are used that are  
300 acquired for the period 1955-2015 by Rijkswaterstaat. This dataset consists of single beam mea-  
301 surements at 100-200 m transects. Positioning and height measurements were done with a number  
302 of analogue to digital techniques<sup>51</sup>. Since 2001, the dry parts of the estuaries have been measured  
303 with the LiDar technique that provides full coverage with a resolution of 1-5 m. The estimated  
304 vertical accuracy of the dataset for practical use was determined at 10 cm ( $2\sigma$ ), see Elias and  
305 others<sup>52</sup>. The bathymetry data of the Western Scheldt are used for the network extraction, which  
306 we used to calculate channel dynamics, depth, and tidal flat volumes. Additionally, we determined  
307 the intertidal flat elevation and area by comparing bed elevation distributions of the tidal flats over  
308 time (Supplementary Fig. 3). While field experiments and monitoring provided valuable insights,  
309 the lack of control inhibits the clear conclusions possible with controlled scenario modelling intro-  
310 duced below.

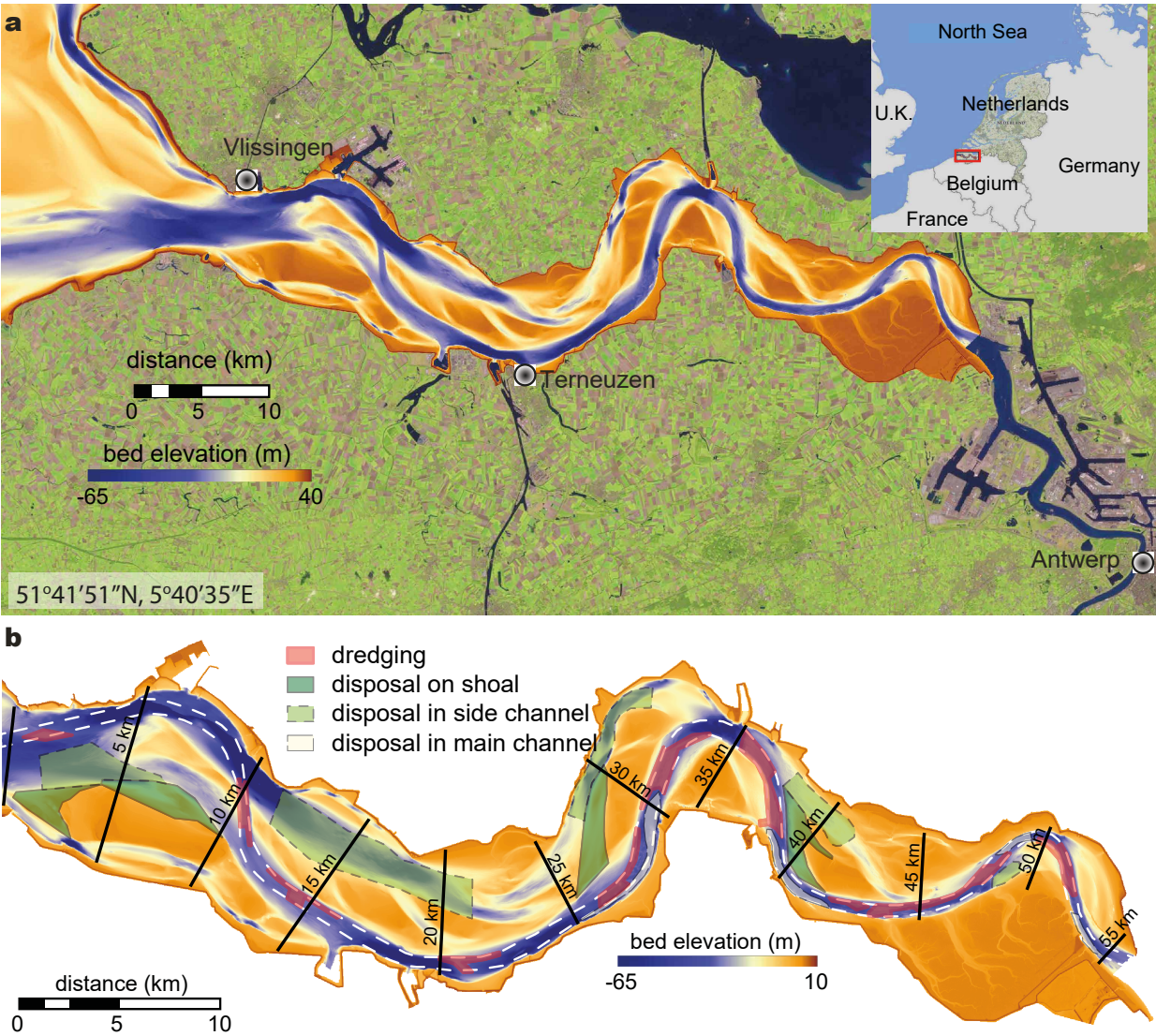


Figure 7: a) 2014 bed elevation of the Western Scheldt. b) Dredging and disposal locations for the model runs plotted as polygons on top of the bed elevation map of 2015. The disposal strategy varies and uses all three types of disposal locations (alternative shoal disposal), only two types (straightforward side and main channel disposal) or only 1 type (foreseen scour disposal). The white dashed line represents the shipping fairway and red polygons are dredging locations.

311 The Western Scheldt is an estuary that has undergone human interference since the 14<sup>th</sup> cen-  
312 tury, which reduced its lateral expansion capacity. At the beginning of the 20<sup>th</sup> century small-scale  
313 sand mining, dredging and disposal became the foci of human activity which has intensified since  
314 the 1970s (Supplementary Fig. 5b). The Western Scheldt has undergone three major deepening  
315 events (in the 1970s, 1990s and 2010s) as well as annual maintenance dredging activities to allow  
316 access to the port of Antwerp<sup>53</sup>. Disposal locations are chosen such that costs, efforts and hindering  
317 the shipping are minimised and thus selected in the vicinity of dredging locations<sup>54</sup>. The “flexible  
318 disposal” approach for the Western Scheldt includes monitoring and adjustment when necessary.  
319 In the last decade, the dredging and disposal strategy has changed in 2010 from straightforward  
320 disposal in the side channels and deeper parts of the main channel to an alternative approach in  
321 which sediment is disposed near eroded intertidal flats. This approach allows slow movement of  
322 material towards the flats with the aim of enhancing subtidal and intertidal habitats<sup>1</sup> and decreas-  
323 ing disposal intensity in the side channels that began to close off<sup>40</sup>. The intention was to maintain  
324 and preserve the equilibrium of the multi-channel system of the Western Scheldt, attain maximum  
325 ecological gain on the edges of inter-tidal flats and preserve the ecologically valuable habitats of  
326 the Western Scheldt<sup>1,55–58</sup>.

327 **Numerical model** In this study, we used a Delft3D model that simulates fluid flow and morpho-  
328 logical changes over time and has been validated and applied previously for rivers, estuaries, and  
329 tidal basins<sup>24,59,60</sup>. Our runs were computed using depth-averaged, nonlinear, shallow-water equa-  
330 tions, wherein the effect of helical flow driven by flow curvature on bed shear-stress direction was  
331 parametrized<sup>60</sup>. The associated transverse bed slope effect is defined as sediment on a slope trans-



332 verse to the main flow direction that is deflected downslope due to gravity. When a secondary  
333 current is present, e.g., in bends, the inward and upslope directed shear stress drags particles up-  
334 slope. We applied the method of Bagnold, and we set the tuning parameter for the transverse  
335 bedload transport,  $\alpha_{bn}$  to 30, so that realistic dimensions of bed slopes for long-term simulations  
336 were maintained<sup>24,61</sup>.

337 The Delft3D schematization was based on the optimised NeVla-Delft3D model for hydrodynamics<sup>62</sup>  
338 and morphology<sup>63</sup> of the Scheldt estuary. We used a nested model from the NeVla-Delft3D model  
339 for reducing computational time<sup>24</sup>. The nested model consists of a curvilinear grid with various  
340 grid sizes and we validated the nested model to the original calibrated NeVla-Delft3D model (Sup-  
341plementary Fig. 1). The boundaries of the nested model include a water level fluctuation due to  
342 tides at the seaward boundary and a current at the landward boundary. Sediment fraction was uni-  
343 form with a median grain-size of 200  $\mu\text{m}$ , comparable to field observations<sup>24</sup>. For simplification of  
344 the boundary conditions, these were selected from a single spring-neap tide cycle of January 2013  
345 (about 14 days) and repeated for a 2 year period. We speed up the bed adjustments by multiplying  
346 the morphological change during hydrodynamics timesteps by a factor of 20 ( $M$ ). In some places  
347 the thickness of the bed is limited by underlying non-erodible layers from Holocene and Tertiary  
348 deposits<sup>64,65</sup>. Sediment transport at the boundaries is in an equilibrium state with the flow and is  
349 unlimited, leading to deviations of the sediment balance in the model compared to the observations  
350 (see Supplementary Fig. 4c and Supplementary Table 2). For reduction of the computational time,  
351 several processes are excluded, including wind (direction and magnitude) and salinity, as these  
352 effects are negligible for the large-scale morphological development.

353 Numerically it is not practically possible to apply a flexible approach in which yearly the dis-  
354 posal locations are shifted. Instead, we isolated the effects of three fixed strategies on the long-term  
355 development that represent real-case approaches. These approaches include i) a straightforward  
356 approach where dredged sediment is disposed equally between the main and side channel; ii) an  
357 alternative scenario, as applied from 2010 and onwards, in which dredged sediment is distributed  
358 for 20% on the tidal flats, 38% in the side channels and 42% in the scours of the main channel;  
359 and iii) a foreseen approach where solely sediment is disposed in the scours of the main channel,  
360 as proposed for future strategies. In order to limit the number of variations between the three sce-  
361 narios, we did not adjust the disposal polygons for the third scenario. This was for clarity. For  
362 simplification, the dredged sediment was not distributed in the nearest disposal polygon as done  
363 in reality. Here, the dredged sediment is distributed over all polygons according to the percentage  
364 given above. The maintained dredge depth was set to 14 m and thus controlled at 9 sill locations  
365 (see polygons in Fig. 7).

366 The dredging and disposal locations for the three strategies are given in Figure 7 and are  
367 fixed for the entire duration of the model simulation. Eventually, we expect that disposal locations  
368 in the Western Scheldt will be re-used and the flexible approach merely delays the unwanted shift  
369 from a multi-channel system towards a single-channel system. For further testing of future scenar-  
370 ios, we performed some additional runs for the first scenario with increasing maintenance depth  
371 of 16, 18 and 20 m. Additionally, we ran the model with three scenarios of sea-level rise (1, 2  
372 and 3 mm/yr) to test the effectiveness of dredging against future sea-level rise scenarios<sup>26,66</sup>. By  
373 using a wide range of values we implicitly study the sensitivity of the SLR predictions<sup>66</sup>. Dredging

374 volumes increased with dredging depth, while for SLR scenarios dredging volume slightly de-  
375 creased (Supplementary Fig. 5d). Increasing SLR resulted in an increase in sediment import into  
376 the model domain, whereas the sediment import decreases with increasing dredging depth (see  
377 Supplementary Table 2).

378 **Network tool** We applied a novel, mathematically rigorous framework for extraction of multi-  
379 threaded channel networks from topographic surfaces<sup>67</sup>. In contrast to previous methods, this  
380 framework automatically captures network topology with channel bifurcations, confluences and  
381 channels of various sizes. Specifically, this method is scale-independent and uses only bed eleva-  
382 tion as input, so it works independently from water elevation. For the analysis in this paper, we  
383 used a variation of the original framework, which makes channel recognition more locally than the  
384 original algorithm. This local approach results more stable attribution of channel size, which is  
385 hence better suited for the analysis of channel networks, with a range of channel sizes that evolve  
386 over time (see Supplementary Videos 3-5).

387 The underlying algorithm computes the Morse-Smale complex (MSC) of the terrain<sup>67,68</sup>, a  
388 topological complex that describes the structural elements of the terrain. The MSC contains the  
389 local minima, maxima and saddle points (points that are a local minimum in one direction and a  
390 local maximum in the other), along with steepest-descent paths (called MS-edges) from each sad-  
391 dle point towards a minimum. These MS-edges partition the terrain into pieces (called MS-cells),  
392 each representing a local maximum with the descending area around it. The algorithm proceeds  
393 by merging insignificant MS-cells together to form larger, significant cells, each representing a

394 tidal flat/ shoal in the channel network. The remaining MS-edges around those cells then form the  
395 channels. Whether a cell is significant or not is determined by the volume of sediment contained  
396 in the cell: we keep merging cells until the volume in each cell is larger than some fixed thresh-  
397 old  $\delta$ . This implies that channels are separated by at least volume  $\delta$ , which is morphologically  
398 meaningful, because this volume is related to the morphological work required to cut shoals and  
399 merge channels. By running the method for different threshold values  $\delta$ , we obtain networks with  
400 more and fewer paths, from which main, side, and connecting channels can be extracted. The main  
401 channel is the path with a maximum value for  $\delta$  as there are no tidal flats enclosed. Side channels  
402 are the channels that are connected to the main channel at both ends, and connecting channels are  
403 the channels that connect the side with the main channel. Starting with a low threshold  $\delta$ , and then  
404 gradually increase  $\delta$ , channels disappear from the network one by one. We annotate each channel  
405 in the network by the highest threshold value  $\delta$  for which that channel still appears in the network.  
406 That is, the threshold value for a channel represents the volume of the smaller of the two tidal flats  
407 next to it.

408 To compute statistics on the tidal flat volumes, we used the channel network for a fixed  
409 threshold value  $\delta$  of 100,000 m<sup>3</sup>. The tidal flat volume was calculated by the summation of the  
410 bed elevation above the median bed elevation along the estuary. The median bed elevation was  
411 determined by the same method as Leuven and others<sup>69</sup>. Firstly, a centreline was defined as the  
412 mean location line between the boundaries of the estuary. Secondly, the centreline was smoothed  
413 and resampled at an interval of 200 m. At all resampled points, a cross-section was constructed  
414 with a 20 m transverse grid spacing, perpendicular to the centreline and within the boundaries of

415 the estuary. Then, the median bed elevation was determined for each cross-section, and a linear  
416 regression was fitted to the median bed elevation along the estuary channel. Elevation above the  
417 regression line was included for the tidal flat volume within the channel network. Afterwards, the  
418 20<sup>th</sup>, 50<sup>th</sup> and 80<sup>th</sup> percentile were calculated as representations of channels, intermediate and high  
419 bed elevations.

#### 420 **Data & Software Availability**

421 The Delft3D model software is open source, and the code is available from the Deltares website  
422 (<https://oss.deltares.nl/web/delft3d>). All field data from Rijkswaterstaat are publicly available from  
423 a variety of web portals or via the service desk (<https://www.rijkswaterstaat.nl/zakelijk/open-data>).

#### 424 **Supplemental Information Description**

425 The supplemental information includes model calibration and validation (Text S1), extended de-  
426 scription of the data and network analysis (Text S2), and analysis of dredging volumes and sed-  
427 iment budgets for the experiments, field and numerical modelling (Text S3). Five figures are  
428 included that support the Text S1 to S3. Furthermore, two movies show the experimental develop-  
429 ment of a dredged and non-dredged system and three movies show the changes in extracted channel  
430 network over time for the model simulations (disposal strategy, fairway depth and sea-level rise).

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440 **Author Contributions**

441 W.M.D managed the numerical model simulations. J.R.C. and J.R.F.W.L conducted the physical  
442 scale-experiments. J.C. and M.T. contributed to background information and data of the Western  
443 Scheldt. M.R.H, W.S., K.V. and B.S. developed and tested the network extraction tool. W.M.D.,  
444 J.R.C., J.R.F.W.L and M.G.K. provided critical result interpretation. W.M.D. wrote the initial draft  
445 of the paper, with substantial contributions from all authors. B.S. led network extraction research  
446 and M.G.K. led modelling and experimental research.

447 **Declaration of Interest**

448 The authors declare no competing interests.

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